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## Reduction of trapped-ion anomalous heating by *in situ* surface plasma cleaning

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Anomalous motional heating is a major obstacle to scalable quantum information processing with trapped ions. Although the source of this heating is not yet understood, several previous studies suggest that noise due to surface contaminants is the limiting heating mechanism in some instances. We demonstrate an improvement by a factor of 4 in the room-temperature heating rate of a niobium surface electrode trap by *in situ* plasma cleaning of the trap surface. This surface treatment was performed with a simple homebuilt coil assembly and commercially available matching network and is considerably gentler than other treatments, such as ion milling or laser cleaning, that have previously been shown to improve ion heating rates. We do not see an improvement in the heating rate when the trap is operated at cryogenic temperatures, pointing to a role of thermally activated surface contaminants in motional heating whose activity may freeze out at low temperatures.

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### I. INTRODUCTION

Trapped ions form the basis of a promising technology for large-scale quantum information processing, combining high-fidelity gate operations and scalable architectures with coherence times that are many orders of magnitude longer than typical gate times. However, anomalous motional heating represents a major obstacle to be overcome before truly large-scale devices can be built [1]. This heating is called anomalous as it has not been explained by known sources of heating, such as Johnson noise; its origins are currently not understood [2]. As all two-qubit gates demonstrated in trapped ions to date have utilized coupling between the motional and internal ion degrees of freedom, anomalous motional heating can limit the achievable coherence and fidelity of two-qubit gates in ion traps, especially in those experiments where care has been taken to eliminate or reduce other sources of ion motional heating (such as external electronic noise). Anomalous motional heating has been found to increase strongly as the trapped ion is held closer to the electrode surface, making it a particularly important problem to be overcome if further miniaturization of ion traps is to continue. Available models suggest that this noise should be thermally activated [3,4], and significant reductions have been found by cooling ion traps to cryogenic temperatures [5,6], but even at low temperatures motional heating can be a significant limitation on gate fidelity.

Several previous studies have pointed to the possible role of surface contaminants in producing anomalous heating. In Ref. [7], the similar motional heating rates of two surface-electrode traps of the same geometry but different electrode materials suggested that surface effects, rather than differences in the bulk, were responsible for the majority of the observed heating. Theoretical models have also been developed [4,8] suggesting that surface adatoms or two-level fluctuators might produce electrical-field noise that could give rise to the observed heating, although these models have so far failed

to predict the detailed scaling behavior of ion-trap heating rates [9].

Furthermore, some previous experiments have shown an improvement in the heating rates of surface-electrode ion traps after surface treatments of the trap electrodes. Treatment with a high-energy pulsed laser source was shown to reduce a trap's heating rate by a factor of roughly 3 [10]. High-energy ion bombardment was observed to reduce trap heating rates by a factor of up to 100 [11–13] where it was verified that surface hydrocarbons were being removed by the process. The effectiveness of these treatments provides additional evidence that surface contaminants, particularly hydrocarbons, can be a major contributor to ion motional heating. At the same time, treatment with high-energy laser pulses or ion beams can heat trap surfaces by hundreds of kelvins and produce additional undesirable effects: The trap in Ref. [10] showed visible damage in some locations due to laser heating, while keV-scale ion beams are known to sputter high-energy material from trap surfaces which can lead to unwanted metal re-deposition.

Radio-frequency- (rf-) produced plasma is also known to be efficient at removing hydrocarbons from surfaces [14] and is widely used to prepare surfaces for microfabrication processes and other applications. Plasma cleaning is a much gentler technique than pulsed laser cleaning or ion bombardment. rf plasma sources can operate at relatively low rf power (in the range of 5–20 W) so that an rf plasma source can be operated near a trap surface without excessive heating of the electrodes. Furthermore, for the input power and background pressure we use, the energies of ions leaving the plasma should be below the sputtering threshold for common electrode materials, such that any sputtering of the trap-electrode material is strongly suppressed.

In this Rapid Communication, we report the use of *in situ* rf plasma cleaning to reduce the room-temperature heating rate of a surface-electrode ion trap by a factor of 4. We produce a mixed Ar-N<sub>2</sub>-O<sub>2</sub> plasma with 15 W of rf power at 13.56 MHz coupled to a simple home-wound coil which can be retracted after plasma cleaning to allow laser access and light collection for ion imaging without exposing the sample to air. Our method is comparatively gentle and heats the trap-electrode surface by no more than about 25 K even after more than an hour of

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plasma cleaning. We also measure the ion-trap heating rates at low temperature (4 K) and, interestingly, do not see an improvement from plasma cleaning. These results suggest that thermally activated surface contaminants play a significant role in anomalous motional heating of trapped ions and that the activity of some (but possibly not all) of these contaminants freezes out at low temperatures and no longer causes heating.

## II. EXPERIMENT

The ion-trapping apparatus used to perform these experiments has been extensively described elsewhere [15]. Briefly, we trap  $^{88}\text{Sr}^+$  ions in a linear surface-electrode trap composed of Nb electrodes sputtered onto a sapphire substrate with typical metal thickness of  $2\ \mu\text{m}$ . A two-stage, vibrationally-isolated cryocooler cools a low-temperature stage and an intermediate-temperature (50-K) shield which, along with a 50-l/s ion pump, provide ultrahigh vacuum (UHV) conditions in the trap chamber without the need for an initial high-temperature bakeout. The trap chip itself is weakly coupled to the low-temperature stage, allowing the trap to be cooled to as low as 4 K; an on-chip heater allows us to heat the trap chip temperature to 295 K while the low-temperature stage remains below 10 K to retain effective cryopumping. A temperature sensor located adjacent to the trap chip indicates the trap chip temperature.

To load ions, we initially cool  $^{88}\text{Sr}$  atoms into a remotely located magneto-optical trap (MOT) then use a resonant push beam to transfer atoms from the MOT to a region near the trap surface where a pair of photoionization laser beams produce  $^{88}\text{Sr}^+$  ions. Those atoms which are ionized within the trapping volume can be confined at a distance of  $50\ \mu\text{m}$  from the surface with lifetimes on the order of minutes due to the excellent cryogenic vacuum. Our trap depth, determined by numerical simulations and the measured trap frequencies, is approximately 15 meV. We load a single ion which we then cool to the ground state of its axial motion (average vibrational occupation  $\langle n \rangle < 0.3$ ) via Doppler cooling and resolved-sideband cooling. To measure heating rates, we apply a variable wait time after cooling the ion to its motional ground state and then measure the average occupation by the sideband-ratio technique [16].

Our rf plasma source (see Fig. 1) consists of a 120-W 13.56-MHz generator and impedance matching network (T&C Power Conversion AG 0113 and AIT-600) coupled to a simple copper coil which is located near the trap chip. The coil has a diameter of 1 cm and a length of 1.5 cm and consists of six turns of 22 American wire gauge solid wire. The coil is mounted via 25-cm-long leads which are soldered to a standard 1.33-in. conflat feedthrough. Electrical shorts are prevented by passing the leads through rigid double-bore alumina tubing, which also provides mechanical stability. The entire coil assembly is mounted on a retractable linear shift stage (UHV Design, LSM38-100-H) which allows 10 cm of single-axis travel. The coil passes through a 1.5-cm diameter hole in the 50-K shield and is located about 1 cm vertically below our trap chip during plasma cleaning. A second hole of similar size on the opposite side of the 50-K shield allows the gas mixture to continually flow past the trap chip during plasma cleaning.

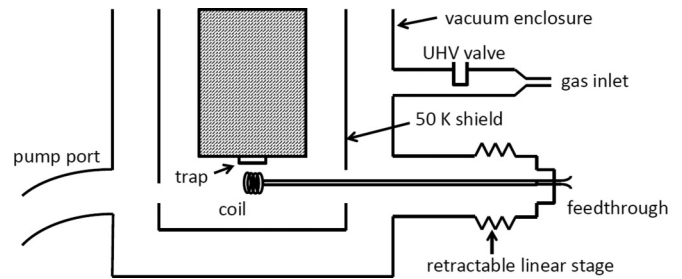


FIG. 1. Simplified schematic of the apparatus used for plasma cleaning studies. A surface-electrode ion trap on a temperature-controllable stage is enclosed within a 50-K radiation shield inside of a larger vacuum enclosure. A mixture of Ar,  $\text{N}_2$ , and  $\text{O}_2$  gases with a total pressure of 700–800 mTorr is introduced into the system via the gas inlet, which can be valved off when the plasma system is not in use. The plasma is generated by rf power applied to a coil located near the ion trap. After plasma cleaning, a retractable linear stage allows the coil to be moved outside of the 50-K shield. Omitted from this simple schematic are many optical access ports as well as the source of neutral  $^{88}\text{Sr}$  atoms. Figure not to scale.

The coil assembly then retracts out of the 50-K shield after plasma cleaning to allow laser and imaging access.

Our plasma cleaning procedure begins by pumping the system down to 50 mTorr with a roughing pump while at room temperature. We then introduce Ar gas at 300–400 mTorr into the system while pumping to create a drift velocity of the background gas. We spark the plasma in a pure Ar environment with 15–20 W of rf power; we then reduce the rf power to 15 W and add gas from a 60%  $\text{N}_2$ -40%  $\text{O}_2$  mixture cylinder until the total system pressure is 700–800 mTorr while maintaining plasma. This plasma is maintained for a variable length of time before the rf power is turned off, the system is pumped back down, and the cryocooler is turned on. Due to the low rf power and high background pressure in our plasma (when compared with typical materials-processing plasma discharges), collisions with the background gas within the plasma sheath [17] should reduce the energies of ions leaving the plasma to below 20 eV, less than the 30-eV sputtering threshold for niobium [18]. After turning off the plasma source and pumping out, our cryogenic vacuum allows us to reach UHV conditions (pressure of  $< 10^{-8}$  Torr) within about 3 h without the need for a system bakeout.

In order to verify that our plasma cleaning technique actually removes surface hydrocarbons, we coated half of the surface of one of our Nb trap chips with a  $1.5\text{-}\mu\text{m}$ -thick layer of a standard photoresist (AZ 1512) which is known to be removable by rf plasma. We then operated our plasma source for  $\sim 60$  min with parameters as described above. A Dektak contact profilometer was used to measure the height of the photoresist layer before and after plasma treatment. We found a reduction in surface height of  $130 \pm 10$  nm, corresponding to a removal rate of about 2 nm/min. The removal appeared fairly uniform over the surface of the resist. In contrast, when we did not continually flow gas through the chamber during plasma cleaning, we also saw material removal, but the removal was extremely uneven across the surface, leading to the possibility that some regions of the chip would not be cleaned effectively.

To characterize the effects of plasma cleaning on ion motional heating, we used our plasma source to clean two identical Nb surface-electrode traps, which we designate as Trap A and Trap B. We ran the plasma source for variable lengths of time but with parameters otherwise as described above. We compared motional heating rates before and after plasma cleaning in both traps. We measured at two trap-electrode temperatures (295 and 4 K) as well as two axial trap frequencies (660 kHz and 1.3 MHz). We conducted additional tests on Trap A to further characterize the heating rate.

### III. RESULTS

Figure 2 shows the ion motional heating rate in quanta/s for Trap A before (red squares) and after (black circles) 20 min of plasma cleaning. We find a reduction by approximately a factor of 2 in the trap heating rate at room temperature after this treatment at both axial trap frequencies investigated. However, the heating rate when the trap chip is held at 4 K is not significantly improved by the plasma cleaning. The frequency dependence of the heating rate is similar to what we have seen in previous measurements of traps with the same geometry [9] and is not changed by the plasma cleaning.

To ensure that the observed reduction in heating rate is due to the plasma treatment, we vented Trap A to air for 72 h then repeated our sequence of measurements. After this air exposure we found that the trap's room-temperature heating rates increased from their postplasma values but did not quite return to their initial values. We then applied a second 20-min plasma cleaning after which the trap heating rates decreased even further to only 25%–30% of their initial values. This motivated

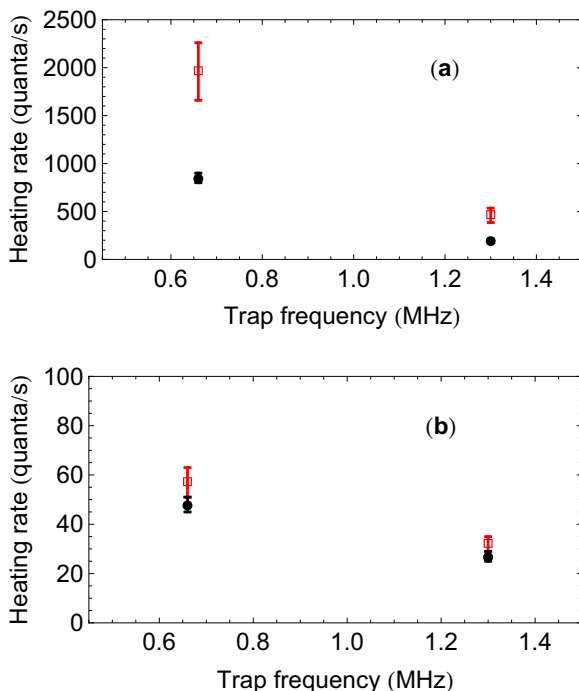


FIG. 2. (Color online) Ion heating rate in Trap A before (open red squares) and after (filled black circles) 20-min plasma cleaning as a function of trap frequency at trap chip temperatures of (a)  $T = 295$  K and (b)  $T = 4$  K.

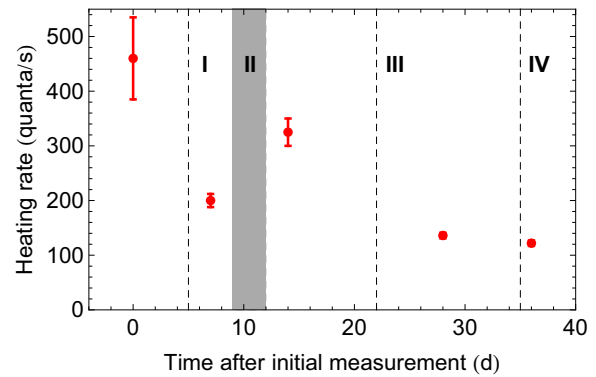


FIG. 3. (Color online) Time course of the Trap-A heating rate (for chip temperature of 295 K and trap frequency of 1.3 MHz). Vertical dashed lines show plasma cleanings (I and III for 20 min and IV for 75 min). The gray area (II) indicates the 72-h exposure to air to allow surface contaminants to re-adsorb to the trap.

us to try a very long 75-min plasma cleaning on Trap A. However, we did not see further improvement as a result of this treatment, suggesting that we had reached the limits of heating-rate reduction achievable with the current procedure. The time schedule of plasma cleanings and air exposures with their associated room-temperature heating rates is shown in Fig. 3. We note that at no point did we see an improvement of the low-temperature trap heating rate due to plasma cleaning. During our 75-min plasma cleaning step (the longest used in these experiments), the temperature as measured by the sensor near the trap chip increased by only 24 K. The total plasma cleaning time we require to achieve the lowest heating rates, about 40 min, is long when compared to the photoresist removal rate of 2 nm/min which we had previously observed. This may indicate that contaminants we do remove via plasma are removed more slowly than the photoresist or perhaps that the last few monolayers of contaminants are not removed as quickly as the bulk photoresist was removed.

For reference, Trap A's heating rate at a 1.3-MHz trap frequency and 295 K before plasma cleaning corresponds to electric-field noise spectral density of  $S_E(f) = 9.0 \times 10^{-12} \text{ V}^2 \text{ m}^{-2} \text{ Hz}^{-1}$ , which ultimately decreased to a final value of  $S_E(f) = 2.4 \times 10^{-12} \text{ V}^2 \text{ m}^{-2} \text{ Hz}^{-1}$  after all plasma cleaning steps. Even before plasma cleaning, this heating rate compares favorably to rates seen in other ion traps with similar geometry [7].

Finally, to further assess the repeatability of our treatment, we applied plasma cleaning to a second trap, Trap B, identical in design to Trap A. After conducting an initial series of heating-rate measurements on Trap B, we applied a 75-min plasma cleaning sequence. We chose to use this long cleaning time as we had observed in Trap A that a cleaning time of only 20 min was not sufficient to reach the lowest possible heating rates. After applying the plasma cleaning process and pumping our chamber down to UHV conditions, we then waited for 120 h before initiating measurements, allowing us to verify that reduction in heating rates can last at least several days. Figure 4 shows the room-temperature and cryogenic heating rates of Trap B before and after plasma cleaning for 75 min. This single plasma cleaning step resulted in a heating-rate

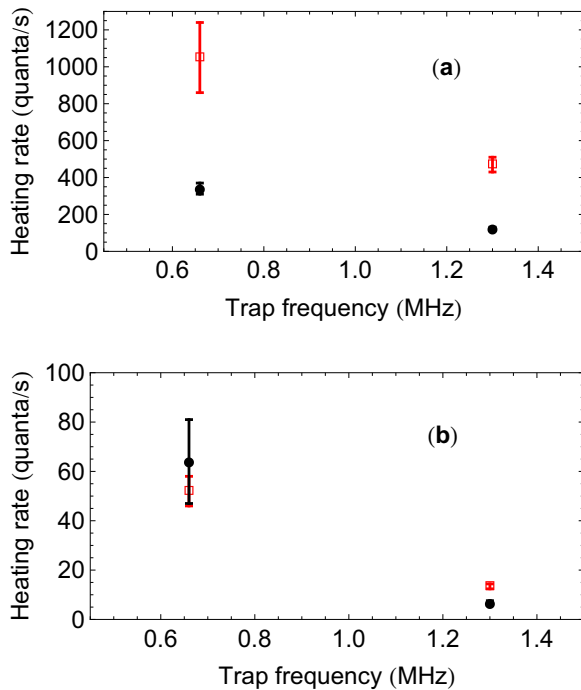


FIG. 4. (Color online) Ion heating rate in Trap B before (open red squares) and after (filled black circles) 75-min plasma cleaning as a function of trap frequency at trap chip temperatures of (a)  $T = 295$  K and (b)  $T = 4$  K.

improvement at room temperature of a factor of  $3.1 \pm 0.6$  at a 660-kHz trap frequency and a factor of  $3.8 \pm 0.3$  at a 1.3-MHz trap frequency.

For Trap B, cryogenic measurements did not indicate any improvement in heating rate at 660 kHz but did indicate a small but significant improvement in heating rate at 1.3 MHz. Any improvement at low temperatures is clearly much less dramatic than the improvement at 295 K, consistent with the results observed in Trap A. The Trap-B data at a temperature of 4 K and a trap frequency of 1.3 MHz are close to the lowest heating rates we have observed in this apparatus, so we cannot rule out the possibility that this particular set of measurements is limited by technical noise. The observation of such low heating rates under these conditions, however, offers strong evidence that the other sets of heating-rate measurements are not limited by technical noise.

#### IV. CONCLUSIONS

We have demonstrated a technique to reduce the anomalous motional heating of trapped ions: *in situ* plasma cleaning. This

approach is simple and robust and causes minimal perturbation to the trap-electrode material, unlike other surface treatments which have previously demonstrated reduction of ion motional heating. We have demonstrated a reduction by a factor of 3 to 4 in the room-temperature heating rate via a 75-min low-power rf plasma cleaning. Interestingly, we did not observe a similar reduction in the heating rate when the trap electrodes were at cryogenic temperatures, possibly indicating that the plasma's role is to remove thermally activated surface contaminants which are frozen out at low temperatures. We note that our observed cryogenic heating rates are still lower than the room-temperature heating rates we measure after plasma cleaning, possibly indicating that some contaminant species remain on the trap chip even after plasma cleaning.

The factor-of-4 heating-rate reduction we observe is more modest than the two orders of magnitude reduction achieved via ion milling in Refs. [11,12] (in traps of roughly comparable dimensions and parameters). The electric-field spectral noise density  $S_E(f)$  we ultimately achieve at room temperature of  $2.4 \times 10^{-12} \text{ V}^2 \text{ m}^{-2} \text{ Hz}^{-1}$  is roughly one order of magnitude higher than what was achieved in those efforts. Numerous differences between the experiments preclude making a definitive statement comparing the two methods. However, there is some evidence that high-energy ion-bombardment techniques cause some structural reorganization of the trap-electrode material at the surface [19], which may be, in part, responsible for the reduction in heating rates associated with this technique. It is possible that the lowest achievable heating rates will combine the two techniques. A one-time *ex situ* ion bombardment may initially lower the heating rate, whereas periodic *in situ* plasma cleaning may be able to remove contaminants that slowly adsorb onto the trap surface. Plasma cleaning may also be able to yield immediate improvements in the motional heating rate of noncryogenic ion traps, although further experiments will be necessary to confirm that the benefits of plasma cleaning remain after a system bakeout or whether UHV conditions after plasma cleaning can be achieved without the need for a second bakeout.

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