Wattsworth:
A Vision for Cyber Physical System Design

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Abstract

The combination of powerful and inexpensive embedded computers, advanced sensor technology, and high speed wireless networks could revolutionize how we interact with our physical environment. Sensor networks that provide real time feedback offer significant value in terms of energy reduction, fault detection, equipment diagnostics, monitoring, security and more. This revolution will not happen in a positive way without a clear vision of how sensor, network, and control technologies can be applied to enhance human abilities and improve our lives.

Such systems have been frustratingly difficult to implement. An old dilemma is becoming increasingly apparent. Networking provides remote access to information and control inputs. Gathering useful information, however, may require the installation of an expensive and intrusive array of sensors. Without this array, networked control provides colorful but minimally useful real information. Technological marvels like solid-state or micro-electromechanical sensors may ultimately reduce the cost of individual sensors through mass-production. They may not, however, reduce installation expense. They also do nothing to recover waste of resources. Even with the array, it may be difficult for a facilities operator to make informed control and maintenance decisions that intelligently affect mission critical components. Large datasets remain difficult to use.

This thesis presents a design approach for creating cyber physical infrastructure that addresses these challenges to delivering actionable real time feedback. At the core of the system is a suite of non-intrusive sensors that dramatically reduce the cost of data acquisition. These sensors process and store data locally, without any dependency on external servers. This removes the security and privacy concerns that plague conventional sensor networks. A decentralized cloud infrastructure securely connects users to sensor platforms and provides powerful visualization and programming interfaces to customize data presentation.

This work covers the complete system design from embedded analog sensors to enterprise grade backend server architecture, to the frontend human computer interface. Such a wholistic design approach is critical to ensure a cyber physical system delivers quantifiable value to the end user. Several case studies illustrate the success of this design approach, including an automatic watch stander system for the
US Coast Guard, an energy monitoring platform for a US Army Base, and realtime equipment diagnostic platforms installed in a wide variety of environments including an Army hospital and a local elementary school.

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Chapter 1

Introduction

Much of the current thinking for making systems “smart” takes advantage of inexpensive hardware and fast wireless networks in a loose design approach that gives little thought to the actual problems facing the end user. In energy monitoring, for example, utilities have installed millions of smart meters that provide little or no actionable information to the facilities owner to help manage or reduce consumption. Engine rooms of modern naval vessels bristle with sensors, each generating data that is faithfully recorded, and typically ignored. Data meant to help becomes a hindrance when operators have to debug hundreds of sensors to find the source of a false alarm. From the smart home to the smart grid, sensors generate clouds of data that overwhelm instead of inform. Databases storing this information have grown so large that analyzing them has become an academic discipline in itself. Even sophisticated players in the data analysis market find themselves unable to capitalize on the promise of cyber-physical systems with both Microsoft and Google canceling their respective energy monitoring projects soon after inception [1]. Designing truly functional cyber-physical systems requires both an analytic mastery and practical expertise. Industry fails to appreciate the complexities of sensor design, looking for quick profit with off-the-shelf components, while academics focus on isolated algorithms and circuits at the expense of the system. This research combines analytical rigor with attention to the practical details required to deploy a complete system from the front-end sensor and signal processing to the back-end network encryption and server architecture.
necessary to bring actionable information to the end user. This work is running in homes, ships, military bases, and schools.

1.1 Non-Intrusive Sensors

System design begins with the sensor. Real time electricity meters enable energy conservation but require current and voltage sensors that are expensive and inconvenient. These sensors require Ohmic contact to measure voltage and geometric isolation of each phase to measure current. Installing such a system involves a trained electrician and a service interruption that often costs more than the savings promised. To make these systems practical I designed non-contact sensors that can measure both current and voltage from outside the insulation of a power line making it safe and easy to install. The sensor measures voltage by sampling the electric field with the differential capacitive design shown in Figure 1-la. The currents are extracted from the magnetic field, which is a superposition of the phase and neutral lines. These currents produce zero net flux outside the cable, but sensitive devices like tunneling magnetoresistive (TMR) elements can detect the magnetic dipoles that escape due to the wire geometry. TMR elements offer high sensitivity but poor linearity, a drawback that I resolved with magnetic feedback to set a zero bias operating point at the sensor interface (see Figure 1-1b) [2].

Multiple magnetic sensors along two flexible arms collect linearly independent measurements, and recover the current in each conductor through an inversion matrix. The complete sensor, shown in Figure 1-4a, costs thirty dollars and takes less than five minutes to install and calibrate.

Water flow meters are similarly intrusive, requiring a plumber to insert monitoring equipment inline with the pipe. Working with a mechanical engineer I designed a retrofit sleeve that converts a standard meter used for utility billing into a high bandwidth flow rate monitor (see Figure 1-2). The system attaches with a zip tie and matches the accuracy of industry standard inline devices [3]. Two compensated TMR elements on the sleeve track the rotation of the magnetic displacement wheel within
Figure 1-1: Non-Intrusive sensors provide access to rich datasets with minimum installation cost and no service interruption.

the meter’s brass enclosure. Using a version of the Hilbert transform this rotational frequency provides a precise flow rate measurement [4].

Both the energy meter and flow rate sensors are designed to be accurate as well as non-intrusive. As hardware costs continue to decrease sensor installation and maintenance begin to dominate the total cost of ownership, making non-intrusive designs particularly advantageous. Non-intrusive systems also provide exciting possibilities for in-situ diagnostics where physical and operational constraints make traditional sensor platforms impractical. For example, the US Navy and Coast Guard want to develop better ways to perform diagnostics on ship motors and generators. Current practice requires intrusive instrumentation. Sensors developed in this thesis can provide similar diagnostics without electrical or mechanical connection to the equipment which means they can run underway [5,6]. Figure 1-3 shows these sensors installed aboard the USS SAN DIEGO. This gives operators real time assessment of machin-
ery health in forward deployed environments where such information is critical for survivability.

1.2 Embedded Signal Processing

Non-intrusive implies reducing total sensor count. By applying the appropriate signal processing a single sensor placed in the right location can provide data equivalent to dozens of distributed sensors that would require complex communication protocols, power, and of course installation. When only one sensor is required, more resources can be devoted to its design. Recent advancements in mobile computing have lowered the cost and power consumption of microcontrollers to the point where powerful 32 bit systems with floating point DSP can be directly embedded in the sensor platform. The next generation of sensors should not just measure and transmit; they should process their own data locally. This design enables richer signal acquisition because data does not have to move across a network. It also eliminates the ethical complexities of using external storage providers like Microsoft and Google, who may have ulterior motives with user data. Current smart meters report power consumption at most once per second, but electrical diagnostics and load identification require sampling
Figure 1-3: Vibration diagnostic sensor for rotating machinery

at a kilohertz or more. I have devoted a large portion of my research to the design of a power meter that is not constrained to these low sample rates by using highly optimized signal processing to store and process meter data locally. The Wattsworth power meter shown in Figure 1-4 uses non-contact sensors to measure current and voltage at 3kHz, which on a three-phase system generates over 2GB of data per day [7]. An embedded Linux device the size of a card deck (Figure 1-4b) processes all of this data locally. Manipulating high bandwidth data on an embedded system instead of a desktop or server requires very efficient data structures and algorithms. The processor reads thousands of samples per second off the sensor, transforms the magnetic field measurements to currents, phase aligns these to the sensed voltage, uses the combination to compute real (P) and reactive (Q) power, and extracts the envelope of the first, third, fifth and seventh harmonic for both P and Q each line cycle. This data is then time stamped by microsecond and stored in a custom database optimized for high bandwidth time series [8, 9]. As implemented, this entire signal processing chain consumes less than 10% of the embedded system’s resources.
(a) non-contact flex sensor

(b) single board computer

Figure 1-4: Hardware renderings of the Wattsworth power meter system.
1.3 Distributed Cloud Architecture

Retrieving actionable data from these embedded sensors presents a different challenge. Without a means to communicate, non-intrusive sensors, however sophisticated, would not provide a practical solution to any problem. This thesis introduces a cloud architecture that connects end users with remote sensors. In typical usage “cloud” describes a central server hosting content that is consumed by remote clients. When the content is located on the sensors themselves, the “cloud” acts as an intermediary instead of a repository. Figure 1-5 illustrates this distributed architecture. Sensors and users authenticate to a trusted server that authorizes transactions between the two. Encrypted tunnels between the sensor and user ensure that data remains confidential. This is in stark contrast to current cloud models where users have little to no control over where or how their data is used. In addition to enforcing authorization policies, the servers also provide powerful tools for users to visualize and manipulate sensor data. A powerful plotting interface supports data visualization. Embedded processors at each sensor cache iteratively decimated copies of the raw data.

These decimated versions are used to construct plots matching the resolution of the client’s screen. Devices return higher resolution data as the requested time range decreases. Dynamic pan and zoom controls populate the interface with new data seamlessly, giving the impression that all of the data is available on the user’s local machine. The cloud servers coordinate this visualization between multiple sensors allowing users to simultaneously plot data that resides across multiple different physical locations. With this tool, the user can plot data from any of sensor over any timescale using minimal network resources. To deliver truly actionable information, sensor platforms must be customizable. Not only are the requirements of residential, commercial and industrial consumers quite diverse, they also change quickly. In centralized frameworks users are at the mercy of the service provider for data processing and analytics. By moving the data and processing tools out of the cloud and onto the sensor, this new distributed framework supports an unprecedented level of customiza-
tion. To realize the benefits of this new design approach I have developed a complete suite of development tools to support user-designed signal processing and data visualization on embedded sensors. This work has two primary components. First, an application programming interface (API) allows users to inject custom code or “apps” into the sensor’s data processing pipeline. User apps can create new data streams, generate graphic reports, alert based on particular conditions, and more. The second component is a web-based integrated development environment (IDE) where users can write, debug and share sensor apps enabling a new type of decentralized interaction where data is private but the code is collaborative [10].
Chapter 2

Non-Intrusive Sensors

2.1 Introduction

Advances in MEMs and integrated fabrication and nanotechnology have both increased sensor resolution and decreased sensor cost. This has led to a proliferation of commercial products that promise to make it easy to fully instrument a facility for any metric of interest. However the cost of the sensor itself is only a fraction of the total "cost of ownership". The cost of installation and maintenance is often significantly greater than the hardware itself. This is because installation can involve equipment downtime and require skilled professional labor for installation. In many environments bringing equipment offline is prohibitively expensive or simply not possible, as in the case of Navy ships or Army bases.

In order to realize the benefits of this new technology, the sensor platform must be non-intrusive. That is, the sensor should retrofit or "design-in" to existing and new equipment, and installation should involve no skilled labor or equipment downtime. The sensors presented in this Chapter meet these requirements. They have been deployed in real world environments where traditional sensor platforms are at best inconvenient, and at worst infeasible.

Section 2.2 presents a non-contact current sensor that monitors current flow in an multi-conductor wire bundle by measuring the magnetic field. Section 2.3 discusses the design of an electric field sensor that can measure the voltage of an AC conductor
with no Ohmic contact. This work was done in collaboration with David Lawrence and also appears in [11]. Together these non-contact sensors provide a complete power monitoring solution. Section 2.4 presents two other non-intrusive sensor designs that have been developed to augment the non-contact power monitor in particular applications.

2.2 Non-Contact Current Sensor

One of the primary difficulties in non-contact power monitoring is designing a sensor capable of measuring current flow at a distance. Ampere’s Law establishes the linear relationship between magnetic fields and current, but without a closed path around the conductor, accurately measuring this magnetic field is a challenging task. On the surface of a circuit breaker and the exterior of a power cable, the magnetic fields are not uniform or symmetric, and depending on the particular geometry, can be very small—less than 1 Gauss for bench top load currents in typical wires. Sections 2.2.1 and 2.2.2 introduce two circuit topologies that can accurately sense these small fields and can do so even in the presence of DC offsets introduced by nearby magnetic elements such as steel breaker panels, and the Earth itself.

The first circuit, based on a Hall Effect sensor, is a cost effective solution suitable for measuring larger loads or in situations where the wire topology exposes a relatively strong magnetic field. The second non-contact circuit uses a Tunneling Magnetoresistive (TMR) element (a recently introduced sensor technology [12]) with an inductive feedback technique to accurately measure extremely small fields.

2.2.1 Hall Effect Sensor

The schematic for this circuit is shown in Figure 2-1 and the fabricated prototype is shown in Figure 2-2. The Hall Effect is widely known and used in many current sensor designs. One of the most sensitive devices available in quantity is Allegro MicroSystem’s A1362 Hall Effect sensor [13]. The A1362 has a programmable gain which can be set up to 16 mV/G, sufficient to resolve the magnetic fields around a
Figure 2-1: Schematic of Hall Effect non-contact sensor

Figure 2-2: Hall Effect non-contact sensor prototype. Ferrite legs focus the field onto the sensor surface.

standard power line. The quiescent output level is also programmable but not tightly controlled. Therefore, in order to measure small fields without saturating the output, we add a high pass filter with a cutoff at 1.5 Hz to AC-couple the sensor to the inverting amplifier gain stage. The large capacitive input of the filter stage requires a follower to buffer the sensor output. Overall gain can be adjusted by tuning the feedback leg of the gain stage.

The circuit is evaluated in the experimental setup shown in Figure 2-3a. A signal generator coupled with a power amplifier drives a solenoid at 200Hz to generate a magnetic field around the sensor. The circuit’s output is compared to the field strength as measured with a fluxgate-magnetometer (an Aim Instrument I-prober 520). Results are shown in Figure 2-4. Two levels of field strength illustrate the degree of hysteresis in the sensor response. Steeper slope reflects higher sensitivity.

In situations where the geometry of the fields is approximately known, the response of the Hall Effect circuit can be improved by attaching magnetic material parallel to
the field lines around the A1362 chip. The prototype in Figure 2-2 uses two ferrite segments to form a partial torus around the sensor package. This geometry captures radial fields near the surface of a multiconductor cable such residential and commercial power lines.

As Hall Effect technology continues to improve, new commercial sensors offer higher sensitivity at a similar cost and footprint. The non-contact sensor described in this section has been significantly improved by the substitution of the Allegro IC with the Melexis MLX91206 Triaxis IMC-Hall Current Sensor [14]. This sensor offers improved sensitivity- up to 40mV/G in a SOIC 8 package. At this sensitivity the sensor can be directly connected to an ADC without intermediate analog gain stages. See Appendix B.1 for a reference design.
2.2.2 Tunneling Magnetoresistive Sensor

The TMR effect describes the change in resistance of a particular material due to applied magnetic fields. An explanation of the effect was first published in the 1970’s but garnered little interest because practical implementations generated relatively small changes in material resistance [15]. Recent advancements using new materials and advanced fabrication techniques have improved the sensitivity of TMR devices. Modern state of the art sensors have a tunnel magnetoresistance ratio of over 600% at room temperature [16, 17]. Interest in these devices has increased as they have become integrated into high density magnetic disk drives and MRAM [18].

The STJ-340 is a TMR Wheatstone bridge sensor produced by MicroMagnetics. The sensor has four active TMR elements, arranged in a Wheatstone bridge architecture. Changes in the field induce an imbalance in the bridge which can be measured by a differential amplifier [12]. While the STJ-340 can detect very small fields (25mV/G as constructed), there are two significant challenges in using it as a current sensor. First, as with the Hall Effect-based sensor, DC offset errors quickly saturate the sensor output. The offset errors from the environment and from imbalance in the bridge itself (which can be up to 10%) must be removed before applying any significant gain.
to the output. More troubling is that the TMR sensor's response to large changes in magnetic field is inconsistent and non-proportional; that is, there is no constant ratio between the change in the magnetic field and the resulting change in the sensor output. Figure 2-5 compares the true current as measured by a commercial current sensor (an LEM LA-55-P) to the output of an uncompensated TMR-based sensor. Even with proper amplification and DC offset removal, step changes in the load current produce non-linear responses in the sensor output.

The circuit shown in Figure 2-6 addresses both the DC offset and the non-linearity problems of the TMR sensor. The DC offset error is corrected by an integrator connected to the REF pin of the instrumentation amplifier. Any DC component is subtracted from the amplifier output resulting in a purely AC signal. This output is then fed through a high gain stage which drives an air core solenoid wrapped around the STJ-340. The current through this solenoid builds a magnetic field that opposes the applied field, creating a feedback loop that zeros the operating point of the STJ-340. Keeping the sensor element exposed to very small fields improves the sensor linearity and increases its range of operation. The current driven in the compensation solenoid is sensed as a voltage across a 150Ω resistor. The final stage
is a high pass filter and gain stage that removes any offset not compensated for in the integrator.

The conceptual operation of the feedback topology is shown in Figure 2-7. In steady-state operation the sensed \( H_{src} \) and driven \( H_{comp} \) fields are approximately equal and the TMR element is exposed to only a very small residual field. The air-core solenoid has proven remarkably effective because closed-loop feedback is used to control the compensation coil.

The circuit is evaluated using the same procedure as the Hall Effect circuit. The

---

Figure 2-6: Schematic of the compensated TMR-based current sensor

Figure 2-7: Illustration of TMR feedback technique
Figure 2-8: Response of compensated TMR sensor to applied fields

The experimental setup is presented in Figure 2-3b. The results in Figure 2-8 show the high sensitivity (relative to the Hall Effect sensor in Figure 2-4) and linear response of the compensated TMR-based sensor. The saturation effects are due to the power rails and not the operation of the circuit itself. The hysteresis in the high field data series is also a result of the power rail limits. The feedback loop cannot drive sufficient current to eliminate the magnetic field at the sensor surface thus, exposing the TMR's inherent non-linearities.

The high sensitivity of the compensated TMR circuit makes it useful for applications outside of power monitoring. In particular the sensor can be used to measure water flow rate by retrofitting it onto a commercial utility water meter. The majority of utility water meters share a common core design. A solid brass enclosures with a positive displacement paddle wheel spins as water flows through the meter. As shown in Figure 2-9, the paddle wheel has a magnet on its axle that couples to a similar magnet on the billing hardware outside the brass enclosure. Usually the billing hardware is a simple mechanical accumulator. Using magnets instead of a mechanical coupling ensures the structural integrity of the pipe and reduces the chance for leaks.

The TMR sensor measures the small magnetic fields that escape the meter enclosure. The frequency of oscillation is proportional to the flow rate of the water.
Figure 2-9: Utility water meter. Internal paddle wheel couples magnetically to billing hardware outside the watertight enclosure.

Unlike current signals which are fixed at the line frequency (50 or 60 Hz), the frequency of the field generated by the meter varies from zero up to the maximum pipe flow rate. The feedback design in the compensation circuit eliminates low frequency components of the magnetic field. By adding an additional output from the ref pin of the instrumentation amplifier, these low frequency components can be recombined with the sensor output in software. The adjusted circuit is shown in Figure 2-10.

The signal processing for this application was developed by Chris Schantz and is presented in [4]. The complete prototype is shown in Figure 2-11. This design uses

![Compensated TMR schematic for water flow monitoring](image)

Figure 2-10: Compensated TMR schematic for water flow monitoring
two TMR sensor elements to generate an analytic signal which allows for more robust frequency estimation and provides information about direction of flow as well as rate.

2.3 Non-Contact Voltage Sensor

Non-contact measurement of electric potential has proven useful for circumstances in which it is difficult to establish Ohmic contact with the conductors in question. Non-contact sensors offer ease of installation and robust high-voltage isolation in exchange for lower accuracy and increased susceptibility to external disturbances.

Non-contact measurement of static electric potentials was first proposed by [19] in 1928. A vibrating plate is placed near an unknown potential, forming a time-varying capacitance. The voltage of the vibrating plate is adjusted until the vibrations induce no current through the plate, indicating that the plate’s potential is equal to the unknown potential. The bandwidth of the sensor is limited by the vibration frequency of the plate. Reference [20] proposes a method by which the residual current through the sensor plate is integrated to determine the higher frequency components of the unknown potential.

Recent work has focused on capacitive sensors that do not vibrate. The induced current is integrated to obtain the unknown potential at all frequencies of interest. Reference [21] uses a capacitor to perform the integration. References [22] and [23] are optimized for the geometry of high voltage transmission lines. However, the gain
of non-vibrating capacitive sensors is dependent upon the distance to the unknown conductor. Two sensor plates can be separately measured to compensate for this dependence [24]. Alternatively, large sensor plates can be placed close to a wire in order to enter a regime of operation in which the transfer function is not dependent on the separation distance [25].

The unique challenge of non-contact voltage sensing is reconstructing the input signal while rejecting pickup from other sources. Specifically, the currents induced by the input signal must be integrated in order to recover the input voltage. However, the currents induced by other sources have significant low-frequency components, which are amplified by an ideal integrator. There is a fundamental trade-off between the accuracy of voltage measurements and a sensor’s signal-to-noise ratio.

This design is a non-contact sensor that takes a differential measurement of two vertically stacked non-vibrating sensor plates in order to maximize the dependence of gain on plate-to-wire distance, so that the signal from a nearby wire is selected and the signals from more distant wires are rejected. The sensor is especially well suited measurements that do not require the absolute scaling factor to be determined (e.g. total harmonic distortion and line regulation).

A three layer capacitor with a uni-polar analog circuit improves the design presented in [2] in both resolution and cost. The sensor uses a digital FIR filter optimized for measuring 60 Hz line harmonics with improved behavior across the range of worldwide utility frequencies relative to the previous analog design. The FIR filter has an exceptionally short impulse response for a digital integrator which improves the rejection of electric field impulses generated by voltage discontinuity in large inductive loads (eg when a motor is turned off). Cost reduction is achieved with careful component selection, uni-polar operation, and a board design that incorporates the capacitive pickups directly into the PCB layers rather than requiring copper foil applied as a post processing step.
2.3.1 Principle of operation

A parasitic capacitance $C_p$ develops between a sensor plate and a nearby wire ($C_{p1}$ and $C_{p2}$ in Figure 2-12). The sensor plate is attached to AC ground by a resistance $R$ and a capacitance $C$. The transfer function from the wire voltage to the sensor plate voltage is given by

$$
\frac{V_o(s)}{V_i(s)} = \frac{sRC_p}{sR(C + C_p) + 1}.
$$

Conventional capacitive-divider sensors choose $R$ to be very large. The transfer function is then approximated by

$$
\frac{V_o(s)}{V_i(s)} \approx \frac{C_p}{C + C_p}.
$$

If $C$ is kept much smaller than $C_p$ (which requires careful construction), the equation simplifies further to $V_o(s) \approx V_i(s)$. Unfortunately, this approach is not practical for the new sensor because $C_p$ is tiny and the resistance required would impractically large. Instead, the new sensor operates in the regime where

$$
|sR(C + C_p)| \ll 1
$$
and so

\[ \frac{V_o(s)}{V_i(s)} \approx sRC_p. \]  

(2.2)

The sensitivity of the sensor is proportional to frequency. It is inversely proportional to the distance \( d \) between the wire and the sensor plate, because

\[ C_p \propto \frac{1}{d}. \]

Note that the sensor measures the input signal \( v_i \) relative to its own ground, which must be connected (or at least AC coupled) to the input signal’s ground.

As proposed in [2], improved localization is obtained by taking a differential measurement from two stacked sensor plates. This arrangement is shown in Fig. 2-12. Parasitic capacitance between the two plates is neglected from this model because in the differential mode it is equivalent to additional capacitance between each plate and ground.

The full transfer function of the differential sensor is given by

\[ \frac{V_o(s)}{V_i(s)} = \frac{sR(C_{p2} - C_{p1})(sRC + 1)}{(sR(C + C_{p1}) + 1)(sR(C + C_{p2}) + 1)}. \]  

(2.3)

For frequencies satisfying \( |sRC| \ll 1 \), the transfer function is approximated by

\[ \frac{V_o(s)}{V_i(s)} \approx sR(C_{p2} - C_{p1}) \]  

(2.4)

which is analogous to (2.2) for the single-plate sensor.

If the sensor plates are at a distance \( d \) from the wire and separated from each other by a distance \( d_0 \ll d \), the differential capacitance is

\[ C_{p2} - C_{p1} \propto \frac{1}{d} - \frac{1}{d + d_0} \approx \frac{d_0}{d^2}. \]

Therefore the sensitivity of the differential sensor is inversely proportional to the square of the distance between the wire and the sensor plates.

An alternative approximation aids in understanding the frequency-dependent be-
behavior of the differential sensor. When \( C_{p1} \ll C \) and \( C_{p2} \ll C \), the transfer function is roughly

\[
\frac{V_o(s)}{V_i(s)} \approx \frac{sR(C_{p2} - C_{p1})}{sRC + 1}.
\] (2.5)

The input voltage is recovered by integrating the output voltage—in other words, the zero at the origin is canceled by a new pole at the origin. At low frequencies, the remaining pole at \( s = -1/RC \) has minimal effect. As the signal frequency increases, first order low-pass behavior will be observed.

Once the output is integrated, the differential capacitance \( C_{p2} - C_{p1} \) must be determined in order to identify the sensor gain and recover the original input signal. If this capacitance is not known, the output will include an unknown constant scaling factor.

### 2.3.2 Analog implementation

There are two factors which determine the sensitivity and performance of the sensor: the geometry of the sensor plates, and the quality of the differential amplifier that is attached to them. Since the sensor should measure the voltage on one nearby wire without mixing in voltages from more distant wires, the sensor plates should not be made too large.

Based on the size of service entry cable and typical clearance constraints around existing wiring, the sensor plates are designed to have an area of 1 cm\(^2\). To minimize the cost of fabrication, the plates are built into the bottom two layers of a standard 1.6 mm four-layer printed circuit board (PCB). In a standard FR4 PCB, the bottom two layers are separated by 0.25 mm of laminate with a dielectric constant of approximately 4.5. Therefore the inter-plate capacitance is

\[
C_{ip} = 4.5 \cdot \varepsilon_0 \cdot \frac{1\,\text{cm}^2}{0.25\,\text{mm}} = 15.9\,\text{pF}.
\]

The prepreg thickness can be adjusted to fine tune the inter-plate capacitance but in practice the default fabrication thickness senses line voltage well and is optimal in terms of production cost.
Figure 2-13: Non-contact voltage sensor schematic and 3D view of PCB stackup. The board dimensions are 1 cm by 2 cm. From top to bottom, layers contain: (1) connector, instrumentation amplifier, and supporting components, (2) ground plane, (3) negative differential sensor plate, (4) positive differential sensor plate and Hall effect IC.
Figure 2-14: The sensor plate geometry selectively targets conductors directly below the sensor surface, shown on the left. The ground shield blocks fields originating above the sensor and the differential pickup rejects common mode fields originating on the sides of the sensor as illustrated on the right.

With this information, the differential capacitance between the sensor plates and a nearby wire can be estimated. Suppose that the effective area of overlap between a wire and the sensor plates is 0.5 cm², and the wire and the closer plate are separated by 1 mm of insulation with a dielectric constant of 2.1 (such as Teflon). The capacitance between the wire and the closer plate is

\[ C_{p2} = 2.1 \cdot \varepsilon_0 \cdot 0.5 \text{ cm}^2 \cdot 1 \text{ mm} = 0.930 \text{ pF}. \]

Then \( C_{p1} \) is given by the series combination of \( C_{p2} \) and \( C_{ip} \), i.e.

\[ \frac{1}{C_{p1}} = \frac{1}{C_{p2}} + \frac{1}{C_{ip}} \]

and the differential capacitance is

\[ C_{p2} - C_{p1} = \frac{C_{p2}}{C_{ip} + C_{p2}} = 0.051 \text{ pF}. \]

The amplifier’s input bias currents must be much smaller than the currents injected into the bias resistors by \( C_{p1} \) and \( C_{p2} \). (This requirement is independent of the resistor values.) The limiting case is the lowest voltage of interest at the lowest frequency of interest—for design purposes, a 1 V signal at 60 Hz. The differential
current produced by this signal is

\[ 2\pi f(C_{p2} - C_{p1})V = 2\pi \cdot 60 \text{ Hz} \cdot 0.051 \text{ pF} \cdot 1 \text{ V} = 19 \text{ pA}. \]

To avoid distorting the signal, the amplifier’s input bias currents should not exceed about 1 pA. The Texas Instruments INA332, meets this specification and is significantly less expensive than the AD8421 used in [2].

In the differential mode, the inter-plate capacitance of \( C_{ip} \) is equivalent to a capacitance between each plate and ground of

\[ 2C_{ip} = 31.8 \text{ pF}. \]

This capacitance reduces the bandwidth of the sensor and should be kept as small as possible. However, the amplifier is susceptible to common-mode disturbances which cause its inputs to exceed their allowable voltage range. In order to have some capacitive filtering of common mode inputs, an additional capacitance of 10 pF is provided between each sensor plate and ground. This gives a total differential mode plate-to-ground capacitance of

\[ C = 41.8 \text{ pF}. \]

The last design task is to select the bias resistors attached to the sensor plates. The sensor gain is given by \( sRC_d \), so to maximize sensitivity \( R \) should be as large as possible. However, larger values of \( R \) increase the time constant \( RC \) and decrease the sensor bandwidth. A good balance between these requirements is achieved by \( R = 1 \text{ M} \Omega \). The breakpoint of the input network is placed at

\[ \frac{1}{2\pi RC} = 3.81 \text{ kHz} \]

which is significantly faster than the signals of interest, but the sensor gain remains large enough to obtain usable voltage signals out of the amplifier.
Using (2.5), the transfer function of the specified analog sensor is

\[ \frac{V_o(s)}{V_i(s)} \approx \frac{s \cdot 51 \text{ ns}}{s \cdot 42 \mu s + 1}. \]  

(2.6)

For sufficiently low frequencies, (2.4) applies and

\[ \frac{V_o(s)}{V_i(s)} \approx s \cdot 51 \text{ ns}. \]

The final analog sensor schematic is given in Fig. 2-13 and the PCB is depicted in Fig. 2-14. Because of the high impedances present on the PCB, special care must be taken to include guard traces around sensitive nodes and to clean conductive residue from the board after assembly. (Because the new voltage sensor is intended for non-contact power metering applications, this PCB also includes footprints for a Hall effect-based magnetic field sensor, an EEPROM, and a connector for cabled attachment to a microcontroller.)

2.3.3 Digital signal processing

The sensor output must be integrated to recover the original voltage being measured. Past implementations have used an analog integrating filter [2], but better performance is possible by performing the integration digitally. The design of the integrating filter presents a fundamental tradeoff between accuracy and disturbance rejection. Specifically, there are three design requirements:

1. The filter must faithfully reconstruct the voltage being measured.
2. The filter must reject low frequency disturbances, such as those caused by thermal drift.
3. The filter must recover quickly from impulsive disturbances.

These requirements correspond to the following three properties of a linear filter:

1. The filter should act as an integrator at line voltage and its harmonics. That is, the frequency response should be inversely proportional to the frequency, and
introduce 90 degrees of phase lag, for every frequency present in the voltage being measured.

2. The filter's frequency response should roll off quickly below the frequencies of interest.

3. The filter's impulse response should be short.

These goals have previously been realized by a cascade of two analog filters: a high-pass filter which admits the signals of interest but blocks low frequency disturbances, followed by an integrator to recover the original voltage signal. The challenge is that a causal analog filter cannot have a sharp transition between its stop band and pass band without introducing significant phase distortion—but if the transition to the stop band is gradual, low frequency disturbances will be admitted and amplified by the integrator.

Throughout this section, $\omega$ refers to a normalized angular frequency with units of radians per sample. Suppose that there are $2N$ samples per line cycle, so that the frequency of the $n$th harmonic is $\pi n/N$ radians per sample. The frequency response of an ideal integrating filter is given by

$$H_i(\omega) = \frac{\pi}{j\omega N}.$$  \hspace{1cm} (2.7)

(This filter is "ideal" only in that it integrates signals perfectly and has a unit magnitude response at line frequency. It does not satisfy the second and third filter requirements.)

If the sampled line frequency of $\pi/N$ radians per sample corresponds to 60 Hz in continuous time, the frequency response of the analog filter in [2] is given by

$$H_a(\omega) = \frac{j\omega \pi/N}{(j\omega + 1/\tau_0)(j\omega + 1/\tau_1)}.$$  \hspace{1cm} (2.8)
Figure 2-15: Impulse response $h_1[t]$ for $N = 25$. The impulse response is zero when $|t| \geq 25$.

with

$$
\tau_0 = (2.2 \, \mu F) \cdot (12.1 \, k\Omega) \cdot (60 \, Hz) \cdot 2N \\
\tau_1 = (2.2 \, \mu F) \cdot (47 \, k\Omega) \cdot (60 \, Hz) \cdot 2N.
$$

This analog filter is compared with two digital finite impulse response (FIR) filters. The FIR filters have antisymmetric impulse responses (such filters are known as “Type 3” FIR filters). As a consequence, they have zero group delay, introduce 90 degrees of phase lag at all frequencies, and do not pass signals at zero frequency or at the Nyquist rate.

The first FIR filter is the Type 3 filter with $2N - 1$ taps whose frequency response $H_1$ satisfies

$$
H_1 \left( \frac{\pi n}{N} \right) = \frac{1}{jn} \quad n \in \mathbb{Z}, 1 \leq |n| < N.
$$

The second FIR filter is the Type 3 filter with $4N - 1$ taps whose frequency response $H_2$ satisfies

$$
H_2 \left( \frac{\pi n}{2N} \right) = \frac{2c_n}{jn} \quad n \in \mathbb{Z}, 1 \leq |n| < 2N
$$
Figure 2-16: Impulse response $h_2[t]$ for $N = 25$. The impulse response is zero when $|t| \geq 50$.

Figure 2-17: Magnitude behavior of the filters for $N = 25$. Note the logarithmic horizontal scale. The analog filter introduces phase distortion which is not depicted on this plot. Amplification of low frequency disturbances is roughly proportional to the area under the left half of the response curve.
Deviations from ideal frequency response

![Deviation graph](image)

Figure 2-18: Magnitudes of the relative deviations from the ideal frequency response for $N = 25$. Both of the FIR filters have zero error at line frequency and its harmonics. Deviation from the ideal response is necessary and desirable at frequencies below line frequency.

![Simulated response graph](image)

Figure 2-19: Simulated response of the filters to an impulsive disturbance with magnitude 30 at $t = 0$. The disturbance affects FIR 1 for $-25 < t < 25$ and FIR 2 for $-50 < t < 50$, but the analog filter has not yet recovered from the disturbance at $t = 400$. The filters are designed for a line frequency of 50 Hz with $N = 25$, but the input signal is provided at 60 Hz to demonstrate that the filters perform well even when line frequency is not known in advance.
The pink noise was generated as the cumulative sum of a sequence of numbers chosen uniformly at random between \(-0.5\) and \(0.5\).

with

\[
    c_n = \begin{cases} 
        1/2 & |n| = 1 \\ 
        1 & 2 \leq |n| < 2N - 1 \\ 
        3/4 & |n| = 2N - 1. 
    \end{cases}
\]

The filter impulse responses are computed using the inverse discrete Fourier transform:

\[
    h_1[t] = \frac{1}{N} \sum_{n=1}^{N-1} \left( \frac{1}{n} \cdot \sin \left( \frac{\pi nt}{N} \right) \right) \quad |t| < N \quad (2.9)
\]

\[
    h_2[t] = \frac{1}{N} \sum_{n=1}^{2N-1} \left( \frac{c_n}{n} \cdot \sin \left( \frac{\pi nt}{N} \right) \right) \quad |t| < 2N \quad (2.10)
\]

where \(t\) is an integer representing the discrete time. The impulse responses are plotted in Fig. 2-15 and Fig. 2-16.

By definition, \(H_1(\omega) = H_2(\omega) = H_3(\omega)\) at line frequency and all of its harmonics below the Nyquist rate. Therefore these filters are optimal for the target application of sensing line voltage harmonics. \(h_1\) is the shortest impulse response whose Fourier

Figure 2-20: Simulated response of each filter to the same sequence of pink noise. The pink noise was generated as the cumulative sum of a sequence of numbers chosen uniformly at random between \(-0.5\) and \(0.5\).
transform has this property, and \( h_2 \) is designed to have a smoother frequency response at the expense of being twice as long as \( h_1 \).

From the impulse responses, the discrete time Fourier transform gives the continuous frequency responses. The analytical expressions are omitted here because they provide no additional insight. Fig. 2-17 shows the magnitude response of each filter and Fig. 2-18 shows the relative magnitude of the difference between each filter’s response and the ideal response. We consider the response of each filter to the signal

\[
x[t] = \sin(\pi t / N \cdot 60/50) + 30\delta[t].
\]

This represents the case where the digital filters were designed for a line frequency of 50 Hz but the actual frequency is 60 Hz, and an impulsive disturbance of magnitude 30 occurs at time \( t = 0 \). These responses are plotted in Fig. 2-19 and exemplify the benefits and drawbacks of each type of filter.

Lastly, to illustrate the superior disturbance rejection of the digital filters, the output of each filter is computed for the same input sequence of pink (i.e. \( 1/f \)) noise. The results are plotted in Fig. 2-20. Clearly, the analog filter exhibits a greater amount of error amplification.

Although the FIR filters are non-causal, both become causal when composed with a finite time delay. It is therefore possible to implement them, with the caveat that the output will not be known in real time. In particular, the first FIR filter delays its outputs by half of a line cycle and the second FIR filter delays its outputs by one full line cycle.

2.3.4 Experimental results

Three experiments are reviewed in this section to demonstrate the improved performance of the new voltage sensor. As the design is optimized for sensing line voltage,

\(^1\)Such disturbances often occur when a large inductive load is disconnected, resulting in a high instantaneous rate of voltage change on the inductor. This produces a powerful electric field which causes the sensor plate voltages to briefly exceed the common-mode input range of the amplifier. The INA332 drives its output to the positive rail when this condition occurs.
the experiments use an additional set of non-contact current sensors to illustrate the performance of the sensor in a power monitoring application. In the first experiment, the sensor is used to extract harmonic envelopes of real power in a three phase cable bundle. The second experiment illustrates the improved performance of the FIR filter versus the previous analog filter across a wide range line frequency harmonics. Finally the third experiment shows the improved disturbance rejection of the FIR filter to variations in the electric field generated by inductive appliances.

The first experiment illustrates the utility of the voltage sensor in a power monitoring application. The voltage sensor was installed along with non-contact current sensors on a three phase bundle shown in Figure 2-21. A traditional power meter using commercial voltage sensors and current transformers was installed in parallel so that the results could be compared. Various electrical loads were switched on and off in order to obtain the time series data depicted in Figure 2-22. Mismatch between the traditional power meter and the non-contact power meter did not exceed 10 W over a dynamic range of 1000 W, showing that the new voltage sensor was able to accurately distinguish real and reactive power.

In order to obtain more detailed results showing the performance of the new
Figure 2-22: Data collected by non-contact and traditional power meters. The turn-on transients depicted are from (i) a 250 W incandescent light bulb, (ii) a 1500 W space heater, (iii) an 0.25 hp induction motor, and (iv) a 600 W bank of dimmable incandescent light bulbs.
digital filters, the voltage sensor was attached to an 18-AWG computer power cable with line voltage supplied by an HP 6834B AC source. (This cable was chosen because thinner conductors produce the smallest coupling capacitance and therefore pose the most difficult sensing challenge.) This experimental setup is shown in Figure 2-23. The sensor was attached to an Atmel SAM4S microcontroller, which sampled the sensor with its built-in ADC at a sample rate of 3 kHz and a desktop Linux installation processed the signal using both of the FIR filters. The analog filter of [2] was constructed using a Texas Instruments OPA4376 operational amplifier and its output was connected to a second ADC channel. The output from all three filters was streamed from the microcontroller to a computer. With a line frequency of 60 Hz, there were 50 samples per line cycle and \( N = 25 \).

The output voltage from each filter was measured for sinusoidal inputs at various voltages and frequencies. Equation (2.4) was solved to find that the differential capacitance was 1.22 pF at 120 V and 60 Hz. At other voltages and frequencies, the percent magnitude error was computed for the output of each filter. The phase error of the analog filter relative to the (zero-phase) digital filters was also computed. This data is given in tables 2-1 and 2-2.

The collected data shows that the digital filters significantly outperform the analog
Figure 2-24: Response of the voltage sensor to a 100 mA fan motor being turned off 30 cm away from the sensor at $t \approx 0.5$. The digital filter recovers from the electromagnetic disturbance quickly, so non-contact power metering is not affected by the disturbance.
<table>
<thead>
<tr>
<th>Input V RMS</th>
<th>Analog % error</th>
<th>FIR 1 % error</th>
<th>FIR 2 % error</th>
<th>Analog phase error, degrees</th>
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</thead>
<tbody>
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<td>2.3</td>
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<td>1.6</td>
<td>1.6</td>
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Table 2-1: Output error from each filter for various input voltages at 60 Hz.

<table>
<thead>
<tr>
<th>Input Hz</th>
<th>Analog % error</th>
<th>FIR 1 % error</th>
<th>FIR 2 % error</th>
<th>Analog phase error, degrees</th>
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<tr>
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<td>1.6</td>
<td>-4.2</td>
<td>-4.2</td>
<td>2.69</td>
</tr>
<tr>
<td>360</td>
<td>0.8</td>
<td>-5.2</td>
<td>-5.2</td>
<td>2.48</td>
</tr>
<tr>
<td>420</td>
<td>0.1</td>
<td>-6.2</td>
<td>-6.2</td>
<td>2.33</td>
</tr>
<tr>
<td>480</td>
<td>-1.3</td>
<td>-7.6</td>
<td>-7.6</td>
<td>2.22</td>
</tr>
<tr>
<td>540</td>
<td>-2.8</td>
<td>-9.1</td>
<td>-9.1</td>
<td>2.16</td>
</tr>
<tr>
<td>600</td>
<td>-4.8</td>
<td>-11.2</td>
<td>-11.2</td>
<td>2.14</td>
</tr>
</tbody>
</table>

Table 2-2: Output error from each filter for various input frequencies at 30 V RMS.
filter with respect to phase lag and voltage linearity. As predicted by (2.5), all filters suffer from frequency-dependent gain, with a slightly more pronounced effect for the digital filters. Finally, the disturbance rejection of each filter was tested by turning off a 100 mA fan motor at a distance of 30 cm away from the sensor. (The motor does not have a clamp circuit, so an inductive voltage spike generates a strong electric field every time it is turned off.) The response of the three filters to this situation is shown in Fig. 2-24. There is good agreement with the simulated behavior in Fig. 2-19. The digital filters are only affected by the disturbance for one or two line cycles, but the analog filter has not recovered after many line cycles. Fig. 2-24 also shows that the digital filters prevent the disturbance from affecting power metering.

2.4 Ancillary Sensor Platforms

The previous sections have presented sensors designed for electric power monitoring. While a great deal of information can be extracted from power signals, some systems are better characterized by other physical metrics. Rotating machines (pumps, motors, generators) produce vibrations related to their mechanical health and mount condition. In many systems temperature indicates pending failures. A hot spot in a breaker panel indicates a loose or corroded connection. A hot gear or rotor in a transmission may indicate a bearing failure. In these situations augmenting electric power data with ancillary metrics can greatly improve the diagnostic capability of a sensor system.

Augmenting a non-intrusive platform must be done carefully. The total number of sensors must be minimal and the additional sensors must be easy to install without skilled labor or equipment downtime. The Captcha, developed in collaboration with Jim Paris is a vibration sensor designed to capture motor dynamics, and “Hottee” explores how multi-domain images can provide high resolution thermal information.
2.4.1 Captcha: A Vibration Diagnostic Platform

One of the most interesting parameters to measure with large machinery is vibration. This is appealing because vibration naturally radiates through a structure allowing a sensor to be placed in an easily accessible location, and a large body of work supports the use of vibration monitoring as a diagnostic tool. This work was performed in close collaboration with the US Navy and Coast Guard to develop pump vibration monitoring tools that enable underway diagnostics. Shipboard applications have a unique set of requirements. The sensors are installed on pumps before an underway cruise, left running for the duration of the cruise and then recovered. Therefore, the sensors must be rugged enough to withstand the harsh operating environment of a ship engine room, they must supply their own power, and they must be able to record large amounts of data. The "Captcha", developed with Jim Paris, is a battery powered platform that uses an ADXL345 MEM's accelerometer which records vibration measurements to a micro SD cards at 3.2 kHz. Such high bandwidth data transfer to an SD card is non-trivial when constrained to a low power micro controller.
and significant effort has gone into the firmware and hardware design of the board to
enable this high data rate. The sensor and its batteries are sealed in a rugged plastic
enclosure and adhesively mounted to the pump’s exterior housing. Figure 2-25 shows
the first revision of the circuitry mounted in its plastic enclosure. Figure 2-26 shows
the fully assembled sensor mounted to pumps onboard the Navy ships.

2.4.1.1 Hardware

The sensor board has several components that work together to provide the embedded
data logging functionality. Figures 2-28a and 2-28b show the current revision of the
hardware. Figure 2-27 lists the functionality of each area of the board. Power is
provided by a 3.7 volt rechargeable Lithium-Ion battery which provides 3-Amp hours
of charge. This is enough to run the data capture continuously for approximately
5 days. The charge management circuitry (B) recharges the battery over USB. A
buck/boost converter (C) maintains the 3.3 volt power rail required by the digital
circuitry. This allows the device to operate while recharging (when the charging
circuitry raises the battery to over 4 volts) and also guarantees a stable voltage
across the lifespan of the battery. The SD card has variable response times to write
requests and periodically stalls for hundreds of milliseconds. In order to prevent data loss while the SD card is not accepting writes, extra data is stored on an 8MB FRAM chip (F). This memory can buffer several seconds of accelerometer data and flush out the data to the card when it is ready again. A real time clock with internal oscillator (I) provides accurate time stamps for all of the data. A coin cell backup (E) maintains the clock time even if the main battery is fully discharged or disconnected. The accelerometer (K) is placed between two mounting points to ensure a stable and accurate vibration measurement. An AT90USB1286 AVR microcontroller (J) coordinates all of these parts and is programmed using a standard ISP header (D), although it can also run a boot loader which accepts programming commands over USB.

### 2.4.1.2 Firmware

In addition to recording vibration data to the SD card, the micro controller provides a terminal interface when connected over USB. This allows the user to view the status of the device, the number of files currently stored, and issue commands to start and stop data capture. The firmware also has a self test diagnostic feature that reports the status of all of the different components of the board. In addition to acting as a terminal emulation device, the sensor can be mounted as a high speed USB storage device if it is plugged into a computer while depressing the panel button (G).
Figure 2-28: Captcha circuit board
mode the USB management chip (A) connects the SD card (H) directly to the host computer which can then transfer data off the device just like a portable thumb drive.

2.4.1.3 Software

To improve the write speed and storage capacity of the device, all of the samples and timestamps are stored in a binary stream. A simple python script converts the binary data to standard ASCII text. The resulting file has one line per sample with 4 columns: time stamp, x-axis force, y-axis force, and z-axis force. This data file can be directly loaded into Matlab for further analysis.

2.4.1.4 Operational Verification

Vibration measurements are traditionally taken from accelerometers which are hard fixed to the machine under inspection. Some pumps have threaded mount points for specialized sensors but most do not and technicians affix the sensor to the machine with "super glue" or epoxy adhesives. The Captcha is designed to be easily installed and removed from a wide variety of pump equipment as non-intrusively as possible. In order to minimize the impact to the machine under test the Captcha enclosure is secured with adhesive tape pads instead of glue. In order to verify that using adhesives rather than epoxy or bolts does not distort the vibration signal, several different mounting techniques were tested in the lab. For a baseline an accelerometer was mounted directly to the body of a standard ventilation fan which was power cycled three times. A spectrogram of the collected data is shown in Figure 2-29. This was compared to the signal recorded by an adhesively mounted Captcha also on the fan body. The Captcha spectrogram is shown in Figure 2-30. Both spectrograms show the same general information with some attenuation present in the adhesively mounted device- which is to be expected. Given that the dominant vibration modes occur at frequencies on the order of motor rotation the adhesive mounts are suitable for this application. Indeed since the adhesive mounts act as a low pass filter, they can help in preventing aliasing of high frequency content into the sampled data.
Figure 2-29: Accelerometer chip mounted with a pipe clamp

Figure 2-30: Custom sensor package adhesively mounted
2.4.2 Hottee: A multi-domain thermal imager

Thermal video records infrared energy and produces heat maps of the imaged objects. Thermal images of motors and electric power distribution equipment can help identify mechanical faults before they become dangerous failures. Traditional thermal cameras are prohibitively expensive but a new compact device manufactured by Melexis, the MLX90620, provides a resolution of 16x4 in a compact package that can be connected to an FPGA or traditional microcontroller with I2C. This device is a combination EEPROM and IR Array in a single TO-39 package. The low resolution limits the utility of the device as a standalone sensor but when the thermal data is superimposed against a visual spectrum video of much higher resolution the effective thermal resolution can be greatly increased. This is because the high resolution image can be used to infer the dominant source of temperature in a low resolution thermal pixel.

2.4.2.1 System Architecture

"Hottee" uses low resolution thermal video and high resolution visual spectrum video to provide realtime thermal diagnostics. The prototype in Figure 2-31 uses a USB webcam for visual video and an AVR microcontroller to interface with the MLX90620. The AVR enumerates as a USB device similar to the webcam. Processing high resolu-
tion video can be difficult in a microcontroller so the prototype design is implemented on an FPGA which is expected to perform the signal processing algorithms faster and with higher efficiency. To facilitate the production of the prototype the Bluespec hardware design language was used to program the FPGA. This imposed some limitations on the prototype architecture. The Bluespec interface does not support USB directly so a host computer is used to process the camera images and send them to the FPGA for processing over the Scemi buffer (a Bluespec bus architecture). This toolchain is illustrated in Figure 2-32.

2.4.2.2 Signal Processing

The thermal sensor output is a nonlinear function of IR intensity and each pixel has separate scaling coefficients that are calibrated by the factory and stored in the sensor EEPROM. The pixels also have a dynamic offset relative to the die temperature so the sensor temperature itself must be calculated. These operations require significant computational resources but can be optimized to run in hardware using the Bluespec floating point modules.

The signal processing consists of three main steps:

1. Computation of die temperature

2. Per pixel compensation
3. Pixel temperature calculation

Once the die temperature is computed the pixel calculations are independent and can be run in parallel as hardware resources allow. In most situations the die temperature should change at a much lower rate than the object being imaged. In this case the computation is fully parallel for the duration the die temperature is unchanged (which is easy to detect by simply reading the PTAT register value).

**Die Temperature**  The die temperature is calculated by (2.11) using a PTAT sensor on the camera module \( V_{TH} \). Coefficients \( K_{T1} \) and \( K_{T2} \) are stored factory calibrations stored in EEPROM.

\[
T_a = \frac{-K_{T1} + \sqrt{K_{T1}^2 - 4K_{T2}[V_{TH} - PTAT\_data]}}{2K_{T2}} \tag{2.11}
\]

**Pixel Compensation**  The pixel voltages are relative to the die temperature so to recover absolute temperature the voltages must be offset by \( T_a \). The size of this offset varies by pixel. The pixel offset to temperature is calculated at the factory and stored in EEPROM as a pair of constants \( A_i \) and \( B_i \) per pixel \( (i, j) \).

\[
V_{IR(i,j)\_OFF\_COMP} = V_{IR(i,j)} - \left( A_{i(i,j)} + \frac{B_{i(i,j)}}{2B_{i\_scale}}(T_a - T_o) \right) \tag{2.12}
\]

Each pixel voltage is then compensated for thermal gradient correction again using coefficients stored in EEPROM.

\[
V_{IR(i,j)\_TGC\_COMP} = V_{IR(i,j)\_OFF\_COMP} - \frac{TGC}{32} \times V_{IR\_CP\_OFF\_COMP} \tag{2.13}
\]

Additionally, if the emissivity \( \epsilon \) of the material being imaged is known this can be included in the compensation calculation to improve the temperature accuracy.

\[
V_{IR(i,j)\_COMPENSATED} = \frac{V_{IR(i,j)\_TGC\_COMP}}{\epsilon} \tag{2.14}
\]

**Pixel Temperature**  The 64 compensated pixel voltages are then used to compute the per-pixel temperature. The voltage temperature relationship is nonlinear and
unique to each pixel. Each pixel is scaled by a factory calibrated coefficient $a$ computed by (2.15).

$$a_{(i,j)} = \frac{\alpha_0}{2^{\alpha_{SCALE}}} + \frac{\Delta a_{(i,j)}}{2^{\Delta a_{SCALE}}}$$

(2.15)

Combining the compensated pixel voltage, scaling coefficient, and die temperature, (2.16) provides temperature imaged by the pixel.

$$T_{O(i,j)} = \sqrt[4]{\frac{V_{IR(i,j)\_COMPENSATED}}{\alpha_{(i,j)}}} + (T_a + 273.15)^4 - 273.15$$

(2.16)

### 2.4.2.3 FPGA Implementation

As suggested above the operations to calculate temperature are best done with floating point. The presence of powers of 4 and square roots make fixed point implementations very difficult and error prone. The FPGA is programmed using the Bluespec software suite which does not support floating point natively so a set of Verilog libraries provided by Xilinx are used instead. The AWB/Leap computing group in CSAIL has published a set of wrappers to expose the floating point modules to Bluespec [26]. One drawback of using raw Verilog is that designs can no longer be run in Bluesim (the Bluespec simulation environment). This makes working with floating point much more difficult because everything must be synthesized and run directly on the FPGA to check if it works. In order to preserve the ability to use Bluesim for other parts of the FPGA design there are two versions of the "Hottee" temperature calculation module. The first uses floating point modules to calculate the temperature, and the second fills the temperature vector with a set of dummy values and does no other math. The dummy module can be used for quick simulations and the real module is substituted in for synthesis. The Xilinx libraries are exposed as modules with a server/client interface. Modules receive requests with either one or two operands, and produce responses containing the result as well as the floating point status flags.

This design use the following floating point modules: addition, multiplication,
Figure 2-33: Thermal imager colormap used for video overlay

division, square root, integer to double precision conversion, and double precision to integer conversion. Constants are stored as reals and converted to floats statically using the helper function $realtobits(). One additional complication with the Xilinx libraries is that the Verilog files are only headers and cannot be synthesized. The actual functional code is in a set of *.ngc files which is done to protect the Xilinx IP. Unfortunately the standard build utility for Bluespec does not allow the inclusion of additional *.ngc files, so a custom build script had to be designed. The build script adds the necessary flags to the Xilinx tool chain to incorporate the libraries. This is wrapped in custom_build.sh and can be called just like the normal build command.

2.4.2.4 Image Reconstruction

The result from both the thermal and visual video pipelines must be combined to create a single image. The visual video pipeline has 3 channels for R, G, and B but the thermal pipeline only has the temperature values. To convert the temperatures to colors a color map lookup table is used. The color map based off the common Jet profile using Matlab's color map editor. This provides an intuitive interface to assign colors to values. The reds are placed around human body temperature and the blues around the freezing temperature of water since this covers the majority of the images we expect to encounter, although the sensor provides readings from -50 to 300 C. The color map is show in Figure 2-33.

The map has 70 entries and the temperatures in Fahrenheit are indexed into this table. Any temperature outside [30, 100) is fixed to the respective max or min. The next step is to map each thermal pixel to the region of pixels it matches on the visual image. This is a set of static offsets and scale factors that are specified at compile time since the cameras are physically attached so the aspect does not change with time.
Finally the thermal image (now three-channel RGB) must be masked with the visual image. This is done with alpha compositing which is simplified from its general form with the assumption that the background image is opaque [27]:

\[ \text{out}_{RGB} = \text{src}_{RGB} \times \text{src}_\alpha + \text{dst}_{RGB} \times (1 - \text{src}_\alpha) \]  

(2.17)

The final combined image is sent back to the user via a SCEMI port. This is fully implemented in Bluespec and works on the FPGA.
Chapter 3

Signal Processing

3.1 Introduction

Nonintrusive sensing can impose an extra signal processing burden to extract and process useful information from an aggregate data stream. Recent advances in microprocessors driven primarily by the smart phone market has resulted in powerful, energy efficient processors that can perform sophisticated signal processing in an embedded environment. By combining the non-intrusive sensor with an embedded processor programmed to run the signal processing algorithm, non-intrusive systems can serve as drop in replacement for conventional sensors.

Section 3.2 presents the signal processing algorithms required to convert data from the non-contact sensors in Sections 2.2 and 2.3 into current and voltage. This requires a calibration process but it can be performed on a completely live system by an end user without any specialized training.

Section 3.3 presents the signal processing algorithms that provide underway diagnostics for ships using the vibration diagnostic platform in Section 2.4.1 and a modified non-contact voltage sensor. This work was done in collaboration with Ryan Zachar and Pete Lindahl. The experimental setup is presented in detail in [28] and the algorithm and results are published in [29].
3.2 Non-Contact Power Measurements

Non-contact sensors provide measurements of magnetic and electric fields, not current and voltage. In a single conductor system the fields are linearly proportional to current and voltage making this conversion trivial, but in many systems of interest there are multiple conductors and multiple phases so that both the electric and magnetic fields are a superposition of several currents and voltages. In this case signal processing can be used to disaggregate these fields to provide the current and voltage data.

3.2.1 Multi-Conductor Power Systems

In many systems of interest there are multiple current-carrying conductors. If the magnetic fields of the conductors overlap, the output of any single non-contact sensor will be a combination of these fields, misrepresenting the current flowing in the nominal conductor of interest. Figure 3-1 compares the output of Hall Effect non-contact sensors to traditional LEM current sensors on two conductors in close proximity. Each non-contact sensor picks up significant interference from current in the neighboring conductor. This section introduces techniques to accurately measure individual currents with non-contact sensors in environments with complex, superposed magnetic fields.

3.2.1.1 Monitoring a Circuit Breaker Panel

Due to the close proximity of circuits on a breaker panel and the steel construction of the panel itself, the magnetic fields are often fully mixed so that any single sensor detects some portion of every current flowing through the panel or cable. Even if a precise location for minimal interference could be determined, the narrow dimensions of many breaker panels limit placement options as seen in Figure 3-2. Assuming the breaker currents are linearly independent, the number of sensors (X) must be equal to the number of breakers (Y) in order to calculate the currents in the panel. The \( x^{\text{th}} \) sensor output for such a system can be expressed as:
Figure 3-1: Comparing actual current to Hall Effect non-contact sensors on a multi-conductor cable. Interfering magnetic fields corrupt non-contact sensor measurements.

Figure 3-2: Monitoring a circuit breaker panel with TMR sensors
\[ S_x = M_{x1}I_1 + M_{x2}I_2 + \ldots + M_{xY}I_Y \]  \hspace{1cm} (3.1)

Or, equivalently using the inverse relationship, the \( y^{th} \) breaker current can be expressed as:

\[ I_y = K_{1y}S_1 + K_{2y}S_2 + \ldots + K_{Xy}S_X \]  \hspace{1cm} (3.2)

The full system can be expressed in matrix form where the current flowing in the breaker directly under each sensor is represented by the diagonal \( K \) values and the interference terms are the off-diagonal \( K \)'s.

\[
\begin{bmatrix}
I_1 \\
I_2 \\
I_3 \\
\vdots
\end{bmatrix}
= \begin{bmatrix}
K_{11} & K_{12} & K_{13} \\
K_{21} & K_{22} & K_{23} \\
K_{31} & K_{32} & K_{33} \\
\vdots & \vdots & \vdots
\end{bmatrix}
\begin{bmatrix}
S_1 \\
S_2 \\
S_3 \\
\vdots
\end{bmatrix}
\]  \hspace{1cm} (3.3)

### 3.2.1.2 Cables with Neutral Return Path

The equations are slightly different for a multiple conductor power cables. These systems do not have fully independent conductors and are subject to the additional constraint of Kirchoff’s Current Law (KCL):

\[ I_1 + I_2 + I_3 + \ldots + I_{\text{neutral}} = 0 \]  \hspace{1cm} (3.4)

This equation reduces the dimension of the solution space. Standard power cables have only two current-carrying wires- hot and neutral. In this simple case only a single sensor is needed. The equations to find current are:

\[
\begin{align*}
I_{\text{hot}} &= KS \\
I_{\text{neutral}} &= -I_{\text{hot}}
\end{align*}
\]  \hspace{1cm} (3.5)

The same technique can be extended for multiple phases and a common neutral.
Figure 3-3: By applying the appropriate fit matrix interfering magnetic fields can be corrected to correctly measure line currents.

For a three phase power cable, such as the one shown in Figure 3-5, there are four current carrying wires so the full matrix has 16 elements but KCL reduces the number of unknown currents by one. A nine element matrix using only three sensors is enough to determine all the currents. The equations for a three phase power cable are:

\[
\begin{bmatrix}
I_1 \\
I_2 \\
I_3
\end{bmatrix} =
\begin{bmatrix}
K_{11} & K_{12} & K_{13} \\
K_{21} & K_{22} & K_{23} \\
K_{31} & K_{32} & K_{33}
\end{bmatrix}
\times
\begin{bmatrix}
S_1 \\
S_2 \\
S_3
\end{bmatrix}
\]

\[I_{\text{neutral}} = -(I_1 + I_2 + I_3)\] (3.6)

3.2.1.3 Example Reconstruction

By applying the fit matrix \([K]\) for the waveforms in Figure 3-3 the non-contact sensors accurately measure the true current waveforms in each line.
3.2.2 System Calibration

Equations (3.3), (3.5) and (3.6) can calculate all currents of interest in complex systems, but they cannot be used until the $K_{xy}$ terms in the fit matrix are determined. If only one current is present, the calibration matrix $[M]$ reduces to a set of equations relating the current to the output of a specific sensor $(S_x)$:

$$
\begin{align*}
S_1 &= M_{11}I_1 \\
S_2 &= M_{21}I_1 \\
S_3 &= M_{31}I_1 \\
&\vdots
\end{align*}
$$

Iterating with a known current on each conductor produces the full matrix $[M]$. The fit matrix can be found as

$$
[K] = [M]^{-1}
$$

While technically correct, this method places an undue burden on the user to first shut down all connected loads and then connect a single known load to each conductor in sequence. If the system of interest is a circuit breaker panel this type of calibration is unrealistic – a homeowner or facilities manager is unlikely to shut off the power and walk around in the dark connecting test loads. In environments with mission critical equipment, such as a microgrid on an Army Forward Operating Base (FOB), this type of calibration is impossible.

In order to calculate the elements of the $[M]$ matrix without interrupting service, a known current must be separated from the background environment. This can be done by applying pulse width modulation (PWM) to a calibration load to create an identifiable pattern in the current waveform. There are a variety of methods to design
a PWM load. Our calibration load tracks the input voltage and draws power for 15 out of every 20 line cycles generating a 75% duty cycle. The full design of the calibration load is presented in [30]. On a 60 Hz service this corresponds to a PWM frequency of 3 Hz as shown in Figure 3-4. Assuming there are no other significant loads cycling at 3 Hz, the calibration load can be differentiated from the background environment using spectral analysis. A complete calibration procedure using this PWM load is developed first for a single phase system and then extended for multiphase systems.

### 3.2.2.1 Single Phase Systems

To determine the coefficients of matrix [M] for a given system of conductors, the calibration load is introduced in turn to each of the conductors. In each case, the outputs of the non-contact voltage and currents sensors are fed to a preprocessing algorithm which calculates real and reactive current flow. The preprocessor, fully described in [9,31] uses the positive zero crossings of the voltage waveform to compute estimates of real (P) and reactive (Q) current each for line cycle. If all conductors are on the same phase (as in the case of a single phase breaker panel), then the zero crossings of the line voltage correspond exactly to the zero crossings of the non-contact voltage sensors. The calibration load is resistive, drawing purely real power, so only the P output of the preprocessor is used for the calibration procedure.
The preprocessor computes P and Q each line cycle and the calibrator PWM waveform is also defined by line cycles (rather than absolute frequency) which allows the same calibration procedure to be performed on both 50 and 60Hz services and is also robust against line frequency variation during calibration.

If the calibration load is operated in isolation, the real component of the preprocessor output is a line cycle time series that can be defined as follows:

\[
P_{\text{cal}}[n] = \begin{cases} 
I_{\text{cal}}, & |n| \leq 7 \\
0, & 7 < |n| \leq 10 
\end{cases}
\]

and

\[
P_{\text{cal}}[n + 20] = P_{\text{cal}}[n]
\]

where \( I_{\text{cal}} \) is the known current draw of the calibration load and \( n \) is the line cycle. There is a subtle caveat in the case where the non-contact sensor is 180 degrees out of phase with the true current. Since the preprocessor computes P and Q on positive zero crossings the edges of the \( P_{\text{cal}} \) pulse will be \( 0.5I_{\text{cal}} \) instead of \( I_{\text{cal}} \). In practice this distortion contributes negligible error to the calibration process and can safely be ignored (see Figures 3-3 and 3-7).

In a live environment other loads draw arbitrary power throughout the calibration process. Therefore the real component of the preprocessor output for a sensor \( x \) is the combination of the calibration load on a conductor \( y \) plus an unknown amount of background load:

\[
P_x[n] = M_{xy}(P_{\text{cal}_y}[n] + P_{\text{bgd}}[n])
\]

where \( M_{xy} \) is the unknown scale factor representing non-contact sensor \( x \)'s response to the calibration load on conductor \( y \) and \( P_{\text{bgd}} \) is the current drawn by other loads in the system. The goal of this analysis is to find the value of \( M_{xy} \). These coefficients are used to form the matrix \([M]\).

First \( P_{\text{bgd}} \) must be removed from the signal. At the harmonics of the calibration waveform, \( P_{\text{bgd}} \) is 0 based on the assumption that the calibrator is the dominant load.
at its PWM frequency. Using the Discrete Fourier Transform (DFT) defined as:

\[ \hat{x}[k] = \frac{1}{N} \sum_{n=0}^{N-1} x[n] e^{-2\pi j \frac{k n}{N}} \quad (3.11) \]

and only considering \( k \)'s corresponding to harmonics of \( P_{cal} \), the signal measured by the non-contact sensor can be represented in the frequency domain as:

\[ \hat{P}_x[k] = M_{xy} \mathcal{F}\{P_{cal}[n]\} \quad (3.12) \]

Using a 200 point DFT and considering only the fundamental of the calibration waveform, Eq 3.12 becomes:

\[ \hat{P}_x[10] = M_{xy} \times \hat{P}_{cal}[10] \quad (3.13) \]

\( \hat{P}_{cal}[10] \) is a constant defined by the structure of the calibration waveform. The Fourier Series coefficients of a unit amplitude rectangular pulse with period \( T \) and width \( T_1 \) are [32]:

\[
a_k = \begin{cases} 
\frac{\sin[(2\pi k/T)(T_1+\frac{T}{2})]}{T \sin[2\pi k/2T]} & k \neq 0, \pm T, \pm 2T, \ldots \\
\frac{2T_1+1}{T} & k = 0, \pm T, \pm 2T, \ldots 
\end{cases} \quad (3.14)
\]

\( P_{cal}[10] \) corresponds to term \( a_1 \). With the parameters of the load defined in Eq 3.9:

\[ P_{cal}[10] = I_{col} \frac{\sin(3\pi/4)}{20 \sin(\pi/20)} = C_1 \quad (3.15) \]

where \( C_1 \) is introduced for notational convenience. Substituting Eq 3.15 into Eq 3.13 yields an equation for \( M_{xy} \):  

\[ M_{xy} = \frac{\hat{P}_x[10]}{C_1} \quad (3.16) \]

The magnitude of \( \hat{P}_x[10] \) is required in Eq 3.13 because the calibration waveform detected by the pickup is actually \( P_{cal}[n + n_0] \) where \( n_0 \) is an uncontrolled time shift due to the fact that the calibration load is not time aligned with the sampling.
interval. This time shift becomes a phase shift in the frequency domain [33] making 
\( \hat{P}_x[10] \) complex:

\[
\hat{P}_x[10] = M_{xy}C_1e^{-jk(2\pi/20)n_0} 
= M_{xy}C_1e^{-j\Phi}
\]

where \( k = 1 \) and \( \Phi \) is an unknown phase shift. By using only the magnitude in Eq 3.16 this phase term is eliminated, but the sign of \( \hat{P}_x[10] \) is eliminated as well.

Fortunately, the sign can be recovered by using higher harmonics of the calibration waveform. In a 200 point DFT the second calibration harmonic is present at \( \hat{P}_x[20] \). Expressing the second harmonic in the same form as Eq 3.18 yields:

\[
\hat{P}_x[20] = M_{xy}C_2e^{-j2\Phi}
\]

where \( C_2 \) corresponds to \( \hat{P}_{cal_y}[20] \) which, like \( C_1 \), is a constant that can be determined using Eq 3.9 and Eq 3.14.

The compensated phase difference between \( \hat{P}_x[10] \) and \( \hat{P}_x[20] \) can be used to recover the sign of \( M_{xy} \). We define the compensated phase difference between the fundamental and the \( k^{th} \) harmonic in a Fourier Series as:

\[
\Delta_{ph}(k) \equiv k\angle a_1 - \angle a_k
\]

In the case where \( M_{xy} \) is positive, the phases of these two terms are:

\[
\angle \hat{P}_x[10] = -\Phi
\]

\[
\angle \hat{P}_x[20] = -2\Phi
\]

The compensated phase difference between these terms is:

\[
\Delta_{ph}(2) = 2(-\Phi) - (-2\Phi)
\]

\[
= 0
\]

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However if \( M_{xy} \) is negative, the phases of the same two terms are:

\[
\angle \hat{P}_x[10] = \pi - \Phi \\
\angle \hat{P}_x[20] = \pi - 2\Phi
\]  

(3.24) \hspace{1cm} (3.25)

which results in a compensated phase difference of:

\[
\Delta_{ph}(2) = 2(\pi - \Phi) - (\pi - 2\Phi) = \pi
\]  

(3.26)

Thus the final expression for \( M_{xy} \) incorporating both magnitude and sign is:

\[
M_{xy} = \begin{cases} 
\frac{|\hat{P}_{nc}[10]|}{C_1}, & \Delta_{ph}(2) = 0 \\
-\frac{|\hat{P}_{nc}[10]|}{C_1}, & \Delta_{ph}(2) = \pi
\end{cases}
\]  

(3.27)

where

\[
\Delta_{ph}(2) = 2\angle \hat{P}_x[10] - \angle \hat{P}_x[20]
\]

This analysis relies on the presence of even harmonics in \( P_{cal} \). In the case of a symmetric waveform with no even harmonics, the compensated phase difference cannot be used to determine the sign of \( M_{xy} \). To see why this is the case consider the first two non-zero terms of the Fourier Series for a symmetric waveform:

\[
\text{positive: } a_1 e^{-j\Phi} + a_3 e^{-j3\Phi} \\
\text{negative: } -a_1 e^{-j\Phi} - a_3 e^{-j3\Phi}
\]  

(3.28) \hspace{1cm} (3.29)

The compensated phase difference between the fundamental and the third harmonic is:

\[
\Delta_{ph}(3) = 3\angle a_1 - \angle a_3
\]  

(3.30)
Substituting in the phases for each coefficient yields:

positive: \[ 3(-\Phi) - (-3\Phi) = 0 \]  
(3.31)

negative: \[ 3(\pi - \Phi) - (\pi - 3\Phi) = 2\pi = 0 \]  
(3.32)

The compensated phase difference is the same for both positive and negative waveforms. Intuitively this makes sense because the polarity of a symmetric waveform is ambiguous without a DC component \((a_0)\). This is why the calibration load has a PWM duty cycle of 75% rather than 50%.

### 3.2.2.2 - Multiphase Systems

The preprocessor requires accurate voltage phase information to calculate real \((P)\) and reactive \((Q)\) current. In single phase systems the electric field is always in phase \((\pm \pi)\) with the line voltage regardless of the number of conductors. In multiphase systems this is not necessarily the case. In typical three phase systems the voltages of the conductors are mutually offset by 60 degrees resulting in a basis for the electric field that spans \(\mathbb{R}2\). To accurately measure phase in these complex environments, a correction factor must be applied to the non-contact voltage sensor output.

Once the voltage waveforms for each phase are known, the calibration procedure to find the \(M_{xy}\) coefficients for the non-contact current sensors is identical to the single phase procedure described previously.

To understand the difficulty in voltage reconstruction, consider the output of a non-contact voltage sensor in a three phase system:

\[ v_{nc}[n] = S_1v_1 + S_2v_2 + S_3v_3 \]  
(3.33)

where \(S_x\) is sensitivity to the field produced by voltage \(v_x\). The \(v_x\) terms can be expressed as complex sinusoids with the following form:

\[ v_x = V_xe^{j\omega t + \phi_n} \]  
(3.34)
Because all of the $v_x$ terms have the same frequency ($\omega$), Eq 3.33 can be rewritten as:

$$v_{nc}[n] = \mathcal{R}\{e^{j\omega t}(S_1 V_1 e^{\Phi_1} + S_2 V_2 e^{\Phi_2} + S_3 V_3 e^{\Phi_3})\} \quad (3.35)$$

The sum of $S_x V_x e^{j\phi_n}$ terms can be represented as a single complex exponential:

$$v_{nc}[n] = \mathcal{R}\{Ae^{j\omega t}e^{j\phi}\} \quad (3.36)$$

where $A$ is the amplitude of the sensor output and $\phi$ is the phase. Depending on the particular geometry of the system there may be degenerate nodes where the electric fields contributed by each phase sum to zero. In this case $A = 0$ and the sensor should be repositioned.

If the voltage amplitude $V$ is a known constant for all phases, the output of a single non-contact sensor can be used to reconstruct the line voltages:

$$v_1[n] = v_{nc}[n](\frac{V}{A}e^{j\psi_1}) \quad (3.37)$$
$$v_2[n] = v_{nc}[n](\frac{V}{A}e^{j\psi_2}) \quad (3.38)$$
$$v_3[n] = v_{nc}[n](\frac{V}{A}e^{j\psi_3}) \quad (3.39)$$

The only unknowns are the correction terms ($\psi_x$) which align the measured phase ($\phi$) to a particular line phase.

The correction terms can be calculated to within $\pm \pi$ using the calibration load. The calibration load draws only real power so the output of the preprocessor at the PWM frequency should be all P and no Q. However, a misalignment between the line phase and the phase of the non-contact sensor will cause the preprocessor to compute a different ratio of P and Q. The correction factor $\psi_n$ is the rotation required to produce all P and zero Q. This is simply the negative of the power factor angle calculated by the preprocessor:

$$\psi_x = -\tan^{-1}\left(\frac{Q_x}{P_x}\right) \quad (3.40)$$
Due to the interference of background loads, Equation 3.40 is only valid at the PWM frequency and its harmonics. Using a 200 point DFT to measure the fundamental frequency of $P$ and $Q$ gives the following equation for $\psi_x$:

$$\psi_x = \tan^{-1}\left(\frac{\dot{Q}_x[10]}{\dot{P}_x[10]}\right)$$  \hspace{1cm} (3.41)

It is important to note that this procedure calculates $\psi_x$ to within a factor of $\pm \pi$ which means the sign of the voltage waveform cannot be uniquely determined. However, this does not affect the accuracy of the preprocessor's calculation of real ($P$) and reactive ($Q$) power. Conceptually an offset of $\pm \pi$ in $\psi_x$ is equivalent to a current sensor being flipped 180 degrees spatially. Both introduce the same apparent phase difference between sensed voltage and sensed current. Eq 3.28 associates a sign to each term of the fit matrix $[M]$ to correct for this difference. Therefore the computed real ($P$) and reactive ($Q$) power is always correct despite the ambiguity in $\psi_x$.

### 3.2.2.3 Rapid Calibration

To more efficiently compute the fit matrix in a multi-conductor system, calibration loads can be connected to each phase and run simultaneously. This is advantageous when multiple phases are available at a single point such as the 240V dryer outlets in residential environments and three phase outlets in industrial environments. Simultaneous calibration requires that each load toggle at a distinct frequency such as 0.5Hz, 3Hz, and 7Hz so that the Fourier coefficients of the fundamentals do not interfere and their harmonics do not overlap.

### 3.2.3 Power Measurement Example

In Figure 3-5, three non-contact sensor prototypes are mounted with custom enclosures to a three phase power cable. The close proximity of the conductors causes significant overlap in the magnetic fields outside the cable. A visualization of the non-contact current sensor vectors is shown in Figure 3-6. The "traditional" current sensors form an orthonormal basis shown in dashed lines. Despite the mixed fields,
Figure 3-5: Monitoring a three phase power line with non-contact sensors

the non-contact sensors are still linearly independent and span $\mathbb{R}^3$. After applying the calibration load to each phase, the fit matrix $[K]$ was calculated using the process described. Figure 3-7 shows a comparison between standard current sensors and the non-contact sensors for loads on all three phases.
Figure 3-6: Visualization of normalized sensor vectors versus the orthonormal phase basis
Figure 3-7: Hall Effect non-contact sensors and traditional current sensors on a 3 phase system
3.3 Vibration Transfer Function

The non-contact voltage sensor of Section 2.3 enables a fresh approach to another critical electromechanic diagnostic technique, vibration monitoring. Applying the voltage sensor for back-EMF sensing allows an electromagnetic machine to be used as its own mechanical network analyzer for structural diagnostics. This section introduces a signal processing technique to estimate this vibration transfer function from non-intrusive sensors.

3.3.1 Motivation

Profiles for the maintenance of electromechanical systems arise from essentially three different engineering management strategies. Maintenance can occur when a system breaks or becomes excessively revealing, essentially deferring costs to a “day of reckoning” when the system is guaranteed to be unavailable. Alternatively, critical maintenance can occur on a scheduled or routine basis to attempt to ensure system availability though with recurring expenses. Or lastly, one can attempt to optimize maintenance costs and system availability by working to predict needed repairs before systems become extreme failures [34–36]. This third option, often referred to as condition-based maintenance, is appealing in the sense that, if the requisite condition-monitoring is efficient and effective, a desired degree of mission capability can be achieved with well-reasoned expenses [34, 35].

For electromechanical systems, vibration measurements are often utilized as an input to condition-based maintenance decision-making [34–37], and many organizations have issued standards for mechanical vibration and condition-based maintenance [38, 39]. Further, researchers continue to develop condition monitoring and diagnostic procedures which utilize vibration sensors. For examples, using various signal processing techniques, vibrational monitor outputs can be used to detect frequency modulations characteristic of ball bearing defects [40–43], and to supplement traditional motor current signature analysis in detecting rotor faults [44, 45].

The majority of these vibration-based algorithms rely on measurements taken at
rated speeds. As such, the information gained for diagnostic purposes is limited to discrete excitation frequencies, i.e. the electrical and mechanical fundamental, harmonic, and modulated frequencies. This information, while clearly useful for specific diagnostic purposes, may lack the richness to distinguish actuator pathologies from degraded mechanical structure, e.g. the vibration mounts. A machine’s vibrational transfer function (VTF), which relates excitation, e.g. rotor speed, to vibration over a range of operating speeds, offers a more complete view of the system and is commonly used to determine diagnostic information such as the natural resonance characteristics as well as noise transfer paths [46].

Empirical characterization of vibrational frequency responses in mechanical systems typically requires special experimentation, e.g. a strike-hammer or a shaker for wide-band excitation [46,47]. This paper presents an alternative, less intrusive approach for VTF characterization that takes advantage of a machine’s spin-down. During turn-off, a machine’s operation covers a continuous wide-frequency band, i.e. from rated operating speed to stand-still. This operating interval of swept operation allows the estimation of the machine’s VTF in-situ and with minimal sensor installation. This paper describes this minimal set-up and the signal processing methods utilized for VTF extraction, and demonstrates spin-down estimation of the VTF in laboratory experiments and field applications aboard serving U.S. Navy warships.

3.3.2 Background

From a simplified perspective, an electric motor or generator mounted on resilient mounts can be modeled as a spring-mass-damper system with an eccentric mass vibration [47], as depicted in Figure 3-8.

The equation which governs the motion of the actuator mass is,

$$m \ddot{x}_m(t) + c \dot{x}_m(t) + k x_m(t) = F_m(t),$$  \hspace{1cm} (3.42)

where $m$ is mass, $x_m$ is the position of the system, $k$ is the spring constant, $c$ is the damping ratio associated with the mount, $t$ is time, and $F_m(t)$ is a forcing function.
This equation can be rewritten in terms of system acceleration as,

\[ ma_m(t) + c \int_{-\infty}^{t} a_m(\tau) d\tau + k \int_{-\infty}^{t} a_m(\tau) d\tau = F_m(t), \]  

(3.43)

where \( a_m(t) \) is the acceleration of the motor. Taking the Laplace transform of this equation and rearranging into transfer function form, reveals the Laplace-domain relationship between the acceleration, \( A_m(s) \), and the system forcing, \( F_m(s) \), as,

\[ \frac{A_m(s)}{F_m(s)} = \frac{s^2}{s^2 + \frac{c}{m} s + \frac{k}{m}}, \]

(3.44)

where \( s \) is the Laplace transform operator.

For a rotating machine with an eccentric mass under steady-state conditions, this system forcing, \( F_m(t) \), takes the form,

\[ F_m(t) = C\omega_m^2 \cos(\omega_m t), \]

(3.45)

where \( C \) is a constant related to load mass and imbalances, and \( \omega_m \) is the speed of
the rotating shaft. A proportionally related virtual input function can be defined as,

\[ \Phi_m(t) = \omega_m^2 \cos(\omega_m t), \]  

(3.46)

and its corresponding Laplace representation substituted into (3.44) to get,

\[ \frac{A_m(s)}{\Phi_m(s)} = \frac{C \omega_m^2}{s^2 + \frac{c}{m} s + \frac{k}{m}}. \]  

(3.47)

This is the equation we refer to as the vibration transfer function (VTF) with units of kg\(^{-1}\) assuming (3.46) maintains the units of (3.45).

(3.46) is a function that can be derived from the motor speed, \(\omega_m\). When combined with accelerometer measurements, this information can generate (3.47). This VTF is a transfer function that contains the same dynamic properties, e.g. natural frequency, as (3.44), and also scales as the forcing coefficient, \(C\), changes, e.g. due to an increased load imbalance. During a motor spin-down when the speed is reducing from the motor’s steady-state operating speed to stand-still, speed and vibration sensors can be used to generate an empirical representation or “eVTF” of (3.47) in that frequency range. The properties of this eVTF can then be used for machinery diagnostics.

**Example Application: Machine Radiated Noise**

One area of concern to many machinery operators is the force transmitted from the machine to the surface underneath, \(F_T\) (Figure 3-8). For example, a Navy ship may need to maintain its radiated acoustic noise at a minimum to avoid detection, and an increase in force transmitted from the machine can lead to increased noise levels. With knowledge of \(\omega_n\), an estimation of the force transmitted by the machine through its mounts to the supporting structure, relative to a value when the force is known to be acceptable, can be made from single accelerometer measurements on the machine system itself.

In steady-state, an electromechanical machine has a transmissibility in the isolation range that is similar to that for zero damping. Therefore, \(c\) can be ignored as long
as the operating speed is away from resonance [48, 49]. This means the force transmitted through the mounts to the baseplate occurs primarily through the stiffness of the mounting (the spring in Figure 3-8), and follows Hooke’s law,

\[ F_T \approx k \cdot x(t). \quad (3.48) \]

From (3.47), the natural frequency of this 2nd order system is given by \( \omega_n = \sqrt{\frac{k}{m}} \).

Since the machine is following simple harmonic motion with acceleration described as \( a(t) = A_{m,ss} \cos(\omega_{ss} t) \), where the \( ss \) denotes steady state conditions, (3.48) can be written in terms of \( m, \omega_n, \omega_{ss} \), and \( a(t) \), as,

\[ F_T = -\frac{m \omega_n^2 a(t)}{\omega_{ss}^2}. \quad (3.49) \]

For diagnostic purposes, only the magnitude of \( F_T \) is of concern; taking the magnitude of (3.49) yields,

\[ |F_T| = \frac{m \omega_n^2 A_{m,ss}}{\omega_{ss}^2}, \quad (3.50) \]

where \( A_m \) is the magnitude of the acceleration. In many situations, the system mass, \( m \), and the machine’s steady-state operating speed, \( \omega_{ss} \), are consistent whenever the machine is in normal operation. As such, an estimate of the ratio of force transmissions from a time when the machine is in a known “good” condition, \( |F_T| \), to the present condition, \( |F_T'| \), can be achieved from only acceleration and speed measurements of the motor, i.e.

\[ \frac{|F_T'|}{|F_T|} = \frac{\omega_n^2 A'_{m,ss}}{\omega_n^2 A_{m,ss}} \quad (3.51) \]

Here, \( \omega_n^2 \) and \( A_{m,ss} \) are values from when the machine is in the “good” condition and \( \omega_n^2 \), and \( A'_{m,ss} \) are derived from the most recent measurements. Practically, (3.51) indicates the value of estimating the eVTF for (3.47) during machine spin-down. From the eVTF, it is possible to estimate the transfer function peak or, essentially
the natural frequency of the system from the observed resonant peak. Estimation of the natural frequency of the mount from the eVTF makes it possible to distinguish machine imbalance from degradation of the mount, both of which can cause increased transmitted vibration that might be indistinguishable from steady-state measurements alone. Changes in the forcing function, e.g. the vibration energy created by operating the machine, will generally increase the magnitude of the entire eVTF. Aging or degradation of the mount alone will shift the resonant frequency of the eVTF. Comparison of successively observed eVTF's can be used to distinguish progressive imbalance from aging of the mount.

3.3.3 Sensor Measurements and eVTF Generation

In practice, estimation of the eVTF requires knowledge of the actuator vibration and speed during spin-down or during a similar operating sweep. We have developed an electronic sensor that can generate an eVTF without installation of a tachometer, strictly from relatively non-intrusive electrical measurements.

3.3.3.1 Data Collection

A single-axis accelerometer mounted vertically is used to measure vibration. This stream is considered the “output” of the system and requires little preprocessing other than scaling the output from mV to m/s² to provide the estimate, \( \dot{A}_m(t) \).

The “input” to the system, (3.46), is estimated from the motor speed. This speed is inferred using a back-EMF sensor measuring winding voltages on the machine. A back-EMF sensor is the preferred method for gathering spin-down speed as it is accurate, portable, and easy to install in the field. When a motor is disconnected from its power supply, or the prime mover is turned off in the case of a generator, the rotor will continue spinning due to its inertia. Residual magnetism generates voltage on the stator. The characteristics of this voltage, e.g. amplitude and zero-crossings, can then be used to estimate rotor speed.

The back-EMF sensor Figure 3-9 employed in this study uses non-contact differential capacitive sensing to detect the electric field generated by the phase lines of
the machine. Three copper plates, shown in Figure 3-9a, are secured against the insulating jackets of the phase lines inside the machine's terminal box. These plates are also electrically connected to a circuit with the simplified schematic shown in Figure 3-9b. Here, plate A \((PA)\) connects to the (+) side of the first AD8421 differential amplifier, plate B \((PB)\) connects to the (-) side of the first AD8421 as well as the (+) side of the second AD8421, and plate C \((PC)\) connects to the (-) side of this second amplifier. These plates capacitively couple to the phase line voltages, \(VA\), \(VB\), and \(VC\), respectively. A more detailed explanation of the non contact voltage sensor can be found in [2].

Under this configuration, the voltages generated at the outputs of the back-EMF sensor are given by,

\[
V_{o1} = g_{a1}VA - g_{b1}VB + g_{n1}V_n, \tag{3.52}
\]

and,

\[
V_{o2} = g_{b2}VB - g_{c2}VC + g_{n2}V_n. \tag{3.53}
\]

In these equations, \(V_n\) represents a common-mode background noise present at the output of the circuit, and the \(g\) terms represent combined gains of the capacitive coupling and amplifier stages of the circuitry. The ratio, \(r_g = \frac{g_{n1}}{g_{n2}}\) can be estimated by performing a scalar fit of \(V_{o1} = r_gV_{o2}\) with measurements achieved when the machine is at stand-still and the phase voltages are zero. Then, the differential calculation, \(V_o = V_{o1} - r_gV_{o2}\), gives the voltage measurement,

\[
V_o = (g_{a1}VA - g_{b1}VB) - r_g(g_{b2}VB - g_{c2}VC), \tag{3.54}
\]

which has the common-mode noise term eliminated. While this voltage signal does not have a physical meaning related to the system, it is linearly proportional to the rotor's back-EMF voltage.

This mechanical speed can be estimated from (3.54) in a number of ways based on the signal's amplitude and/or frequency. For this research project, if the following conditions are met,
Figure 3-9: The non-contact back-EMF sensor system used for estimating motor speed.
• There is no clipping in the back-EMF sensor waveforms during steady-state operation, and

• There is no active electromagnetic control (e.g. braking) applied to the system during spin-down,

then the machinery spin-down speed profile is extracted from the signal envelope using a Hilbert transform based method. Here, the Hilbert transform produces a waveform linearly related to the signal amplitude. This waveform is then scaled to match the mechanical excitation speed, \( \omega_m \), based on knowledge of the machine’s steady-state speed rating. Further information on this method is given in [5, 50].

If these conditions are not met however, then the signal amplitude is not linearly related to speed throughout the entire spin-down. In this case, the electrical-speed, \( \omega_e \), profile is achieved based on signal frequency estimates gained from a zero-crossing detection procedure. In this procedure, the \( k_{th} \) zero-crossing is identified by a change of sign between two adjacent waveform samples at \( t_n \) and \( t_{n+1} \), and its time-location, \( t[k] \) estimated based on the zero-value of the linear interpolation of the signal values \( V_n(t_n) \) and \( V_n(t_{n+1}) \). Then, the signal frequency at time instance, \( t[k] \), is estimated as,

\[
\hat{\omega}_e(t[k]) = \frac{2\pi}{t[k+1] - t[k-1]}.
\]  

(3.55)

In the discussion above \( n \) represents the sample time-index, and \( k \) represents the time indexing of zero-crossings.

In general, this method may be less noise-immune than the Hilbert transform method as it is prone to uncertainty around zero-crossings, particularly at low frequencies as the signal amplitude also decreases with speed. While many methods exist for accurate zero-crossing detection in noisy environments, e.g. [51–53], for the purpose of gaining eVTF estimates here, all zero-crossings including those generated by additive noise were detected as described above and outliers removed prior to the frequency estimation of (3.55). From the \( \hat{\omega}_e \) estimates, the mechanical speed estimate, \( \hat{\omega}_m \), is calculated based on the number of pole-pairs in the machinery. Then, this stream is linearly interpolated to match the sampling rate of the original mea-
measurements for calculating the virtual input function, $\Phi_m(t)$, from (3.46). Finally, the virtual input is calculated. In the case where the vibrational excitation is provided directly from eccentricities in the machine’s rotor, $\Phi_m(t)$ is estimated from $\dot{\omega}_m(t)$ as,

$$
\Phi_m(t) = \dot{\omega}_m^2(t) \cos \left( \int_0^t \dot{\omega}_m(\tau) d\tau \right). \tag{3.56}
$$

An example of the two time-domain signals required for the eVTF are shown in Figure 3-10. The top plot shows the measured acceleration of the machinery during the spin down, which starts around the 1 second mark as noted by the beginning of the attenuation of the speed curves in the bottom plot. Here, the curves are normalized by their peak values for simultaneous plotting. The blue curve shows the estimated speed, in this particular case, based on the Hilbert transform procedure. The orange curve is the square of the blue curve, and the yellow curve is the calculated virtual input, $\Phi_m(t)$.

### 3.3.3.2 Short-Time Fourier Transform Analysis

In accordance with (3.47), the time-domain spin-down signals of Figure 3-10 need to be transformed into frequency domain signals. Empirically estimating a transfer function through spin-down analysis can be susceptible to noise from other nearby machinery [49]. Further complicating the process, the excitation frequency changes continuously with rotor speed. As such, the Short-time Fourier Transform (STFT) is used to process the signals to reduce the uncorrelated noise and minimize frequency of excitation spreading in the analysis. Under this method, the time domain waveforms are windowed at a series of time locations during the spin down process, and the Fast Fourier Transform (FFT) is used to process each modified time signal resulting in a time-binned frequency representation of the original signals.

For this STFT application, a Hanning window is used as the mask for the input and output waveforms. This window is tunable through two parameters, the time-width of the window, $T_w$, and the overlap between adjacent windows, $o_c$. The Hanning windows are multiplied with the input and output waveforms to create “masked” versions.
As an example, the windowing of the virtual input at the 1.5 second mark during a motor spin-down is shown in Figure 3-11. The same processes is also performed on the output.

A full series of Hanning windowed inputs and outputs for a motor during spin-down is shown in Figure 3-12. Here, the tunable parameters are set to $T_w = 1$ second and for clarity, $o_v = 0\%$. The top plot shows the individual windows and their time locations, the middle plot shows the series of resulting masked virtual input waveforms, and the bottom plot the series of masked vibrational output waveforms.

Via the Fast Fourier Transform (FFT), each Hanning-windowed input and output allows for the generation of a frequency spectrum specific to a short period of time during the spin down process. These spectrums can be indexed as $\Phi_{m,i}(j\omega)$ and $A_{m,i}(j\omega)$, respectively, where $i$ denotes the Hanning window index. A corresponding
Figure 3-11: A Hanning window masking of the normalized virtual input centered at 1.5 seconds.

Figure 3-12: Hanning Windows and Masked Inputs and Outputs
"center" frequency for each index can be defined as,

$$\omega_i = \arg \max_{\omega} \left| \frac{A_{m,i}(j\omega)}{\Phi_{m,i}(j\omega)} \right|.$$  \hfill (3.57)

To generate the eVTF, first all the output spectrums are "masked" around the corresponding center frequencies such that,

$$A'_{m,i}(j\omega) = \begin{cases} 0 & \omega \leq \omega_i - w/2 \\ A_{m,i}(j\omega) & \omega_i - w/2 \leq \omega \leq \omega_i + w/2, \\ 0 & \omega \geq \omega_i + w/2 \end{cases} \quad (3.58)$$

where the variable $w$ limits the "valid" vibrational response frequencies to those around the frequency of virtual input excitation. This is done to preserve linearity in the eVTF and to ignore sources of noise at extraneous frequencies. Maximum envelope excitation and response spectrums are then defined as,

$$\Phi_{env}(j\omega) = \max_i \left[ \arg \max_{\Phi_{m,i}(j\omega)} \left| \Phi_{m,i}(j\omega) \right| \right], \quad (3.59)$$

and

$$A_{env}(j\omega) = \max_i \left[ \arg \max_{A'_{m,i}(j\omega)} \left| A'_{m,i}(j\omega) \right| \right], \quad (3.60)$$

respectively. That is, at a given frequency, these envelopes are defined as equal to the corresponding indexed spectrum with the maximum magnitude at that particular frequency. The eVTF is then determined as,

$$\frac{A_m(j\omega)}{\Phi_m(j\omega)} = \frac{A_{env}(j\omega)}{\Phi_{env}(j\omega)}. \quad (3.61)$$

Generating the eVTF in this manor allows the maximum amount of information gained during the STFT based analysis to be passed on to the eVTF while also ensuring linearity.

Figure 3-13 shows a graphical representation of this process. In this figure, the
Figure 3-13: Fast Fourier Transform of Masked Inputs and Masked Outputs with Envelopes

The magnitudes shown on the y-axis are normalized to the maximum values of each input and output spectrum series, \( \Phi_{m,i}(j\omega) \) and \( A_{m,i}(j\omega) \), respectively. The dashed curves represent the STFT envelopes of (3.59) and (3.60), while the solid lines represent individual spectrums from a windowed time segment roughly half-way through the spin-down. This period also corresponds to the peak resonance in the system. The figure shows that the FFT for the virtual input signal has a maximum at around 31.5 Hz while the resulting FFT for the output vibration signal has a maximum at around 33 Hz. This offset is due to the fact that there is a time delay in the vibrational response to the forcing input. For this analysis, the width parameter, \( w \), for the output response is set to 6 Hz. As such, the indexed response spectrum is cut off at the frequencies of 28.5 Hz and 34.5 Hz to ensure the maximum envelope is created from the linear vibrational response while still allowing the capturing of the delayed peak response. This particular analysis results in the eVTF plot for the 50A durometer mounts in Figure 3-16.
3.3.4 Tests on Purpose Built Machine Set

To test the method for generating the eVTFs as described in the previous section, and to showcase application of this hardware and signal processing for machinery diagnostics, a test stand consisting of a prime-mover, inertia, and generator was constructed. This test stand, shown in Figure 3-14, centers around a DC permanent magnet motor with dual couplings. One end is coupled to a three-phase induction machine, and the other is connected to a single phase synchronous AC motor, which is disabled and acts only as a flywheel. The three machines are mounted onto a single metal sub-base as is typical for many industrial actuator installations. The sub-base is mounted to a steel box girder with vibration reducing mounts at eight points. A second shaft coupler is attached to the induction motor as an attachment point for an imbalance. This is done to simulate a rotor imbalance, a type of machinery fault, which should appear in the eVTF as an increase in vibration magnitude at resonance. Five commercial vibration dampening mounts of different durometer (30A, 40A, 50A, 60A and 70A) were used to emulate a scenario where the mounts' stiffness increases or decreases over time, the effect of which should appear in the eVTF as a shift in resonance.

3.3.4.1 Comparison of Spin-down eVTF and Steady-state eVTF

Initial tests were performed on a subset of mounts to validate the eVTFs generated during the machinery spin-down by comparing them against eVTFs generated from steady-state measurements. A Python script is used to automate the steady-state measurement collection by commanding a series of DC-voltages from a power supply connected to the DC motor. At each discrete voltage level, the script reads motor speed from a shaft encoder and measures the sub-base vibration with a standard industrial accelerometer. The script removes data collected prior to when the machines reach steady-state at each voltage level, and the remaining vibration data is analyzed using Welch's power spectral density estimate [54]. At each voltage level, the peak of the power spectral density at a frequency closest to but greater than the measured
speed of the motor is taken as the vibration magnitude at the measured speed. Finally, each corresponding measured operating speed is squared to generate a virtual input for generation of the steady-state eVTF.

Figure 3-15 gives a comparison of a spin-down eVTF with a steady-state eVTF for the 60A durometer mounts and machine setup described above. For this particular test, the DC motor was run in steady-state at 105 discrete voltage levels with 4 seconds of steady-state operation at each resulting motor speed. The spin-down eVTF was calculated from the data collected following the motor’s power supply turning off after the maximum voltage level was reached. This spin-down process took approximately 10 seconds, and the analysis parameters were set to $T_w = 1s$, $\omega_o = 90\%$, and $\omega = 3$ Hz.

As seen in the figure, the two curves are very similar and show the same resonant peak, indicating that the spin-down procedure accurately captures the important features of the system’s VTF. The spin-down eVTF appears much smoother with less variance in measurements because the virtual input is derived from the Hilbert Transform and lowpass filtered rather than calculated directly from speed measurements.
as is the case for the steady-state eVTF. This particular result is well representative of the results gained from other durometer mounts.

It should be noted that the number of features present in the eVTFs exceeds those allowed by the second order model described in Section 3.3.2. This is due to the fact that the model assumes a single-degree of freedom and linearity in the system, while real-world machinery systems have three-degrees of freedom and many sources of non-linearity. Nevertheless, for the purposes of diagnostics, e.g. sensing changes in transferrable noise, the measured eVTF around the resonant peak approximates a second order system and provides useful parametric estimations as illustrated below.

3.3.4.2 eVTFs with Condition Changes

With confidence in the eVTF method described, the process was applied to a total of 10 conditions across the 5 mount types and with and without a 17 g imbalance attached to the rotor system. These tests were done to show the utility of the eVTF method towards machinery diagnostics in accordance with the example application described in Section 3.3.2. The premise of this method is that eVTFs gained opportunistically during a machinery spin-down can provide useful information, e.g. changes in vibration amplitude and resonant frequency, indicative of system failures,
Figure 3-16: eVTFs from tests of the 30A and 50A mounts showing a shift in natural frequency with a change in durometer, and an increase in amplitude due to an increase in system imbalance.

i.e. machinery imbalance and mount degradation, respectively.

Figure 3-16 illustrates this premise with eVTFs gained during testing. In this figure, the solid black curve shows the eVTF gained during machinery spin-down when the 30A mounts were installed and no additional imbalance applied to the system. This curve shows a resonant peak just above 22 Hz at a magnitude of approximately $3.2 \times 10^{-5}$ kg$^{-1}$. When the 17g imbalance was added to the shaft, the magnitude of the vibration increased significantly, but without a significant shift in resonance as shown by the dashed red plot, which has a peak around $1.4 \times 10^{-4}$ kg$^{-1}$ at just under 22 Hz. However, when 50A durometer mounts were used without an imbalance, while the magnitude of the eVTF remained similar (approximately $3.6 \times 10^{-5}$ kg$^{-1}$), the resonant frequency shifted significantly to 33 Hz (dot-dashed blue curve). Thus, the spin-down generated eVTF increases the amount of distinguishing information available to an operator in diagnosing issues in the machinery system.

Table 3-1 compiles the results from all tests involving the 5 mount types described.
Table 3-1: Comparison of eVTF characteristics for various durometer mounts and rotor imbalances.

<table>
<thead>
<tr>
<th>Durometer</th>
<th>Imbalance (g)</th>
<th>Number of Tests</th>
<th>Natural Frequency (Hz) [mean (std)]</th>
<th>Peak Amplitude (kg$^{-1}$) [mean (std)]</th>
</tr>
</thead>
<tbody>
<tr>
<td>30A</td>
<td>0</td>
<td>4</td>
<td>22.3 (0.170)</td>
<td>32.5 (1.98) $\times 10^{-6}$</td>
</tr>
<tr>
<td></td>
<td>17</td>
<td>4</td>
<td>21.8 (0.153)</td>
<td>136 (1.45) $\times 10^{-6}$</td>
</tr>
<tr>
<td>40A</td>
<td>0</td>
<td>4</td>
<td>26.1 (0.117)</td>
<td>39.9 (0.463) $\times 10^{-6}$</td>
</tr>
<tr>
<td></td>
<td>17</td>
<td>4</td>
<td>25.6 (0.125)</td>
<td>158 (1.38) $\times 10^{-6}$</td>
</tr>
<tr>
<td>50A</td>
<td>0</td>
<td>4</td>
<td>32.7 (0.193)</td>
<td>36.1 (0.386) $\times 10^{-6}$</td>
</tr>
<tr>
<td></td>
<td>17</td>
<td>2</td>
<td>31.2 (0.155)</td>
<td>143 (2.20) $\times 10^{-6}$</td>
</tr>
<tr>
<td>60A</td>
<td>0</td>
<td>4</td>
<td>38.5 (0.108)</td>
<td>33.2 (0.387) $\times 10^{-6}$</td>
</tr>
<tr>
<td></td>
<td>17</td>
<td>3</td>
<td>36.4 (0.122)</td>
<td>134 (10.55) $\times 10^{-6}$</td>
</tr>
<tr>
<td>70A</td>
<td>0</td>
<td>5</td>
<td>44.3 (0.195)</td>
<td>41.2 (0.887) $\times 10^{-6}$</td>
</tr>
<tr>
<td></td>
<td>17</td>
<td>4</td>
<td>41.4 (0.083)</td>
<td>161 (1.92) $\times 10^{-6}$</td>
</tr>
</tbody>
</table>

above. The 3rd column of this table indicates the total number of tests performed on each mount and imbalance. Mean values from each set of tests for the system’s natural frequency and peak eVTF amplitude are given in columns four and five, respectively. Also, in each of these columns the accompanying standard deviations are included to give an indication of repeatability. As observed there, the tests are very consistent for each configuration with the standard deviation in measured natural frequency less than 1% of the mean value and that of the peak amplitude less than 8% for all tests.

3.3.5 Field Tests on U.S. Navy Equipment

A series of field tests were conducted on an active U.S. Navy mine countermeasures ship (MCM). The ship has 3 ship service diesel generators (SSDGs) each rated at 375 kW. Each generator set is mounted on a metal sub-base, which is attached to the hull of the ship via 8 resilient mounts in a configuration similar to the laboratory setup described in the previous section. The U.S. Navy is interested in non-intrusive, in-situ characterization of these mounts for tracking changes in the vibration energy.
Table 3-2: Statistical characteristics for the eVTFs gained during MCM generator spin-down.

<table>
<thead>
<tr>
<th>Generator Number</th>
<th>Number of Tests</th>
<th>Natural Frequency (Hz) [mean (std)]</th>
<th>Peak Amplitude (kg(^{-1})) [mean (std)]</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>5</td>
<td>18.4 (0.146)</td>
<td>136 (9.12) \times 10^{-6}</td>
</tr>
<tr>
<td>2</td>
<td>5</td>
<td>19.0 (0.109)</td>
<td>103 (7.77) \times 10^{-6}</td>
</tr>
<tr>
<td>3</td>
<td>4</td>
<td>19.2 (0.0618)</td>
<td>96.8 (4.35) \times 10^{-6}</td>
</tr>
</tbody>
</table>

passed to the hull of the ship. The work described here is part of a larger project to integrate a self-sustaining sensor [5,6,55] inside the SSDG terminal box, which would alert the operator when the mounts are beginning to degrade. For this experiment however, the standard industrial accelerometers and the back-EMF sensors described earlier were used.

Each generator set contains a 6-cylinder, 4-stroke diesel engine for driving the prime mover at 30 Hz (1800 RPM). The cylinders are fired in pairs at 15 Hz with a 120 degree phase shift between pair firings. This generates significant vibrational energy at 45 Hz. For the subsequent analysis presented here, this vibrational component from the piston firing rather than the rotational speed of the shaft was used to generate the eVTF plots, with the virtual input appropriately scaled so that,

\[
\Phi_m(t) = (1.5\tilde{\omega}_m(t))^2 \cos \left(1.5 \int_0^t \tilde{\omega}_m(\tau)d\tau\right),
\]

Additionally, during these tests the back-emf sensor outputs were observed to be clipping in the steady-state so the zero-crossing method was used for estimating \(\omega_m\). The spin-down of these generators took approximately 25 seconds, and the analysis parameters were set to \(T_w = 1s\), \(o_v = 90\%\), and \(w = 4\) Hz.

A total of 14 spin-downs were measured on the generators under various ship conditions including while the ship was in-port with no other machinery operating, and under-way when several other pieces of machinery were simultaneously operating. Fig. 3-17 shows example eVTFs gained during spin-down of each of the three ship
Figure 3-17: Mine countermeasure ship generator eVTFs as measured during generator spin-downs.

generators, and Table 3-2 compiles the statistical characteristics for all the eVTFs tests performed. Fig. 3-17 shows clear resonant peaks in all three generators around 19 Hz and all with a similar amplitude of approximately $10^{-4}$ kg$^{-1}$. These curves are well representative of all the eVTFs gained for each corresponding generator, regardless of the ship’s condition, and simultaneous electromechanical load use. This is confirmed by comparing the standard deviations in resonant peak amplitude and frequency locations with their corresponding mean values in Table 3-2. Here, for all tests, the standard deviation in peak amplitude estimates was less than 8% of the mean, while those in the peak amplitude frequency locations were less than 1% for each test. Thus, while there is little exposed by these tests to differentiate any physical characteristics of each generator, the consistency in each test gives confidence in the repeatability of the method. Additional research is required to track the evolution of the eVTF characteristics over a longer period of time, and plans are in place to do so as a part of future self-sustained sensor developments discussed in [5, 6, 55].

In addition to the generator experiments, vibrational analysis tests were performed
on two of the ship’s auxiliary seawater (ASW) pumps. Each pump operates at 59 Hz (3545 RPM) and is driven by a 3-phase induction motor rated at 15 kW (20 HP). The crew had noted that one of the ASW pumps (Pump 2) had recently been overhauled, while the overhaul date of the other pump (Pump 1) was unknown. The spin-down times for these pumps were approximately 4 seconds. As such, the window-width parameter, $T_w$, was shortened to 0.25s, the overlap parameter, $o_o$, was increased to 95%, and the masking width, $w$, set to 8 Hz. Example eVTFTs resulting from this analysis are shown in Figure 3-18, while Table 3-3 give the statistical characteristics
of all tests performed.

As can be seen in Figure 3-18, there are characteristic differences between the two pump eVTFs with the recently overhauled ASW Pump 2 showing a peak magnitude about 14% lower than ASW Pump 1 and at a frequency about 6 Hz higher. The results shown here are well representative of all the tests performed on the two pumps as observed in Table 3-3, which shows the standard deviation in the resonant peak amplitude was less than 4% of the mean and that of its frequency location less than 1.5% of the mean for both pumps.

While Figure 3-18 shows more compelling differences between machines than the eVTFs generated from the generator spin-downs (Figure 3-17), concrete conclusions on the causes of these differences cannot be made. The most recently overhauled pump (ASW 2) does show a decreased magnitude in its eVTFs compared with those of ASW 1, though their resonant peak frequency locations are increased, which as shown in Section 3.3.4 would suggest a stiffening of the rubber typical of aging mounts. Still, these characteristic differences were clear and repeatable for all tests.

### 3.3.6 Conclusions

This section has demonstrated the value of a non-intrusive vibration measurement and analysis technique for use during an electromechanical machine’s spin-down procedure. As the speed of the machine decreases from its normal operating speed to stand-still, the process inherently provides vibrational-excitation swept across a range of frequencies, permitting estimation of the vibrational transfer function (eVTF). As shown in laboratory tests, this transfer function reveals characteristics useful for machinery diagnostics which are unavailable for estimation during steady-state operation. The consistency of the field test results combined with the interpretability of laboratory test results demonstrates that this analysis method can provide useful information for electromechanical machinery diagnostics. Specifically, the eVTF approach with back-EMF sensing can be deployed as part of a self-contained sensor that provides effective and useful information about both electromechanical machinery and the health of an associated mount.
Chapter 4

Distributed Cloud

The final challenge is providing secure, reliable access to the information acquired by non-intrusive sensors to the end user in a format that is both informative and actionable. The Wattsworth system provides this mechanism through NILM Manager, a web application that allows users to visualize their data and design "Energy Apps" that customize the operation of their non-intrusive sensors. NILM Manager is a distributed application that operates very differently than traditional sensor network platforms. Traditional sensor networks centralize data storage and processing in large server centers. This presents significant security and privacy concerns and also requires a persistent Internet connection for both users and sensors. Many locations such as military or industrial facilities are unwilling or unable to install such a sensor network. The Wattsworth system requires no central storage and control and as such can be deployed and scaled with much greater flexibility. Non-intrusive monitors can join a NILM Manager instance running on the public Internet, hosted on a private network, or even running locally on the monitor itself. This section presents the Wattsworth distributed cloud architecture and describes how NILM Manager can be used for both visualization and control. See Appendix B.4 for a discussion of the servers and configurations used for a Wattsworth cloud deployed at MIT.
4.1 Introduction

Recording current and voltage with enough resolution to identify load characteristics requires sampling at relatively high rates. NILMs capable of interesting diagnostics and load recognition typically generate very large data sets. (4.1) can be used to estimate the storage requirements for a typical installation:

\[ R = 2N_\phi \times f_s \times B_{adc} \]  \hspace{1cm} (4.1)

where \( R \) is the data rate in bytes per second, \( N_\phi \) is the number of phases (usually two for residential and three for industrial environments), \( f_s \) is the sampling frequency, and \( B_{adc} \) is the ADC resolution, or the number of bytes used to represent a sample measurement (usually about two). The product of these factors is multiplied by two because both current and voltage waveforms are recorded for each phase.

Using (4.1), a NILM running at \( f_s = 8 \text{kHz} \) will produce over 5GB of data per day for a standard home. Data sets of this size are difficult to transmit over a residential network. In NILMs deployed in [56], for example, equipment operators mailed hard drives and DVD's back to the lab for analysis. The cost in resources and man-hours make this type of installation impractical for all but the most limited deployment scenarios. Even if data can be reliably collected, plotting the current and voltage over a single day involves billions of individual samples which is beyond the capability of many standard software packages (such as Excel). Previous work has focused on using signature detection to reduce the dataset size, storing only equipment “on” and “off” events instead of current and voltage [57–59]. However, such an aggressive data reduction step without a clearly defined outcome or monitoring objective artificially limits the utility of the NILM.

NILM Manager, a cloud platform that enables quick and easy access to NILM data, solves the access and analysis challenges created by high bandwidth or “big data” power monitoring. A “remote” NILM is installed at a facility to be monitored. Desktop-power computing is readily available in “deck of cards” sized hardware that
Figure 4-1: NILM Manager system architecture. The management node relays requests from authenticated clients to remote NILMs over a secure VPN. Clients can issue commands and retrieve data over a web interface.

can be installed quickly at a site with terabytes of local storage, at prices comparable to those of a modern solid state electricity meter. Data collected by this remote NILM is never fully transmitted from the site, minimizing network traffic. Rather, data is managed locally on the site computer by custom high-speed database software, NilmDB, described in [8]. NILM Manager provides a central management node that connects multiple remote NILMs with a virtual private network (VPN) and hosts a website that allows authorized users to view and analyze data collected by NILM systems.

4.2 NILM Virtual Private Network

NILM Manager controls the computing “center” of a virtual private network that securely connects remote NILMs, each running NilmDB, to the management node. The network is virtual in the sense that all communication occurs over the public Internet but is encrypted so only NILMs and the management node can decipher the content. Extensive computation on acquired data is relegated to local computing managed by
Figure 4-2: NILM network topology as visualized by Nagios [60]. Servers in the management node are outlined in the labeled box. NILM’s connect to the management node through the backbone server. Nagios provides realtime visibility of the network enabling rapid fault detection and diagnosis. The two NILM’s marked with red crosses indicate they are down for maintenance.

NILmDB at on the non-intrusive monitor itself. New programs or “energy apps” can be downloaded from NILM Manager to a NILmDB installation. New analysis results can be uploaded from a remote site to NILM Manager for web presentation, which can of course be through secure connections. Small energy apps and small reports or analysis results, typically a few kilobytes, can provide full, powerful access to remote high bandwidth data with minimal network data requirements. A (low technology) cell phone can and has provided more than enough bandwidth for managing a full industrial monitor in our experiments.

Figure 4-1 shows a conceptual view of the NILM VPN. Users can request data from a NILM and send it commands all without any physical access to the machine. The management node coordinates VPN traffic and ensures that only authorized users have access to NILM systems.
4.3 Web Platform

Users interact with NILMs though a website hosted by the management node. The website is available over the public Internet which means it is accessible from any connected device including tablets and cell phones. Users authenticate with a username and password although certificate based authentication or other forms of protection could be implemented if additional security is required.

By presenting users with a web interface rather than a direct connection (for example via SSH) to the remote meter, the user interaction tools (NILM Manager) are decoupled from NILM system tools. This means NilmDB and other backend software on the NILM can be updated without affecting how the user interacts with the NILM data.

4.4 Data Visualization

One of the primary difficulties in Nonintrusive Load Monitoring is visualizing the high bandwidth data collected by the current and voltage sensors. A NILM produces thousands of data points each second. Tools such as Excel and MATLAB consume significant system resources to produce plots for datasets of this size. Complicating matters further, NILMs often have limited network bandwidth making transmission of the raw data to a workstation difficult or impossible. NILM Manager solves this problem by using a decimation algorithm to visualize large datasets.

4.4.1 Stream Configuration

NILMs connected to the management node are configured through the web interface shown in Figure 4-3. This interface presents the data collected by the NILM as a series of files organized into directories. Users can navigate through the data on the NILM just as they would navigate folders on their desktop. While they appear as flat datatypes on the web interface, each file corresponds to a hierarchy of streams on the NILM itself.
Figure 4-3: The NILM configuration interface. The plot resolution slider controls how many data points are displayed in data visualization tool (shown in Figure 4-4).

Figure 4-4: Data visualization using the web plotting tool. Data visualization using the web plotting tool. The upper plot shows 24 hours of power data and the lower plot shows a higher resolution view of the highlighted segment. This view represents 5.1M samples but is drawn using just 2K decimated samples (less than 0.05% of the raw samples).
As the NILM adds data to a stream, it simultaneously computes a decimated child stream. For every four elements in the parent stream, the child contains a single \([\text{min, max, mean}]\) tuple. This process is performed recursively with each successive child containing a factor of four fewer elements than its parent. When this process is carried out to completion (the final child containing only one sample), the total storage requirement only increases by a factor of two [8].

The plot resolution slider in the top right of the interface sets the number of data points returned by the NILM when a user requests an interval of data. NILM Manager checks how many data points are contained in the requested interval and returns the lowest decimated child stream that fits within the configured plot resolution. The raw data is only returned if the interval requested is small enough that there are fewer raw samples than the plot resolution setting.

### 4.4.2 Presentation

The NILM Manager website provides an intuitive plotting interface shown in Fig. 4-4. Note that this figure shows real data from a monitoring site in our research program. The system has been running for nearly two years, and the remote monitor contains tremendously detailed data, down to the envelopes of individual electrical transients as shown in the figure. Nevertheless, access to this data is almost instantaneous from any web connection anywhere. The interface uses decimated streams to allow users to view any dataset from any remote NILM at any time scale. Panning and zooming through the data operates like Google Maps with progressively higher resolution data returned as a user "zooms in" to a particular area of a waveform. Progressive views are delivered essentially instantaneously.

The plotting interface is implemented in Javascript which runs in the client browser. The code is derived from the open source "Flot jQuery" plugin although it has been highly customized for this application [61]. The plotting code has three display modes. If the time interval is short enough that the raw data fits within the plot resolution setting, a simple line graph is displayed. If, as is usually the case, the raw data contains too many samples, data from the selected decimation level is displayed as a
Figure 4-5: NILM Manager automatically adjusts the plot type based on how many points are in the selected dataset. (a) When a stream has too much data and no available decimations a solid line indicates the plot cannot be displayed. (b) If decimations are available an envelope of the dataset is shown, and (c) if the time interval is short enough, the raw data is plotted directly.

[min, max] envelope around the mean which is plotted as a line graph. The envelope is the same color as the mean with added transparency. This provides feedback about the structure of the data without obscuring other time series on the same plot (as in the case of Matlab or Excel). Finally if a time interval contains too much data in all available decimation levels (which occurs when a NILM has not yet decimated a new stream), a thick horizontal line is drawn in place of the data and an asterisk is added to the legend indicating the inability to plot the particular stream at the selected time scale. Figure 4-5 shows the three plot display styles. The client code automatically switches between styles as the user navigates between datasets and timescales.

4.5 Data Processing

Current smart meters typically transmit their measurements wirelessly to a central monitoring node which limits their resolution, as these links generally cannot carry sufficiently large amounts of data [62–64]. Exposing raw data also exacerbates privacy concerns. The on-board CPU cores in even a low-cost NILM process data locally.
Data need never be moved in bulk from the monitoring site. Short, actionable reports and analyses can be transmitted to a facilities manager or service provider as privacy restrictions permit. The information can also be used locally for control. Moving computation from a centralized server to a distributed embedded environment requires an efficient data processing framework. The following sections describe this framework, and illustrate how “apps” on distributed NILM energy boxes can analyze, report on, and control power systems.

4.5.1 Management and Preprocessor

NILMs support remote management through a specialized application programming interface (API), which allows clients to upload and execute custom scripts. This API is exposed to the management node over HTTP with security provided by the VPN tunnel. The management node uses this API for system administration tasks such as database cleanup, software updates and system diagnostics. The management node establishes a sandbox on top of this API in which end users can execute their own scripts called “Energy Apps.” These scripts use input hooks to link to data streams stored on the NILM. An app can use data from multiple streams, each of which may have different intervals of data and sampling rates. The NILM runs a two-stage preprocessor that consolidates input data from diverse source streams into a single time stamped array which makes it easier to write energy processing algorithms.

4.5.1.1 Multistream Wrapper

Data streams may be electrical measurements, data from secondary sensors, or outputs from other NILM processes. For processes that require inputs from multiple streams care must be taken to schedule the process appropriately and only run it over time intervals where all of its input streams are available. Sensor data may arrive in bursts with significant lag, and streams produced by other processes create scheduling dependencies. The multistream wrapper manages these dependencies and ensures that a process is only run over intervals where its inputs are available.
4.5.1.2 Resampler

Once the input streams have been assembled, the resampler produces a single composite data set with timestamped rows where each column is a process input. If all inputs come from a common source stream then this array is straightforward to assemble, however apps using inputs from different streams generally require resampling. For example, an app that uses outside temperature and real power consumption as inputs (to compute energy usage as a function of weather for example) must use either down-sampled energy measurements or up-sampled temperature measurements. When multiple streams are used as inputs the user specifies a “master” stream and resampler runs a linear interpolator or a decimator on the other inputs to create a uniformly sampled dataset.

The stream iterator framework makes it easy to write custom applications that use this dataset to run analysis and control algorithms.

4.5.2 Stream Iterators

Each “energy app” is based around a stream iterator which enables computation on large NILM datasets. Traditional iterators such as for and while loops operate on static datasets, but NILM data arrives continuously. Stream iterators provide the ability to operate on continuous datasets by combining a traditional looping iterator with a persistent state. When the stream iterator has finished processing the available data it saves its state variables so that when it runs on the next chunk of data, it can pick up exactly where it left off. This allows the programmer to treat the datasets as continuous streams while giving the NILM flexibility to choose chunk size and processing rate based on the available system resources.

Listing 4-1: The setup function for a NILM stream iterator

```python
a = [...]; b = [...] # filter coeffs
def setup(state):
    zi = [...] # initial state for filter
    state.initializeSlot("filter_zi", zi)
```

Building a stream iterator is a two step process. First, the user defines a setup
function (see Listing 4-1). This function initializes a state object which provides persistent storage between process runs. Data is stored in slots which are accessed by string identifiers, similar to a dictionary. This function only runs the first time the app is executed. The setup function in Listing 4-1 initializes state for an example app which runs a linear filter on a NILM data stream. The filter coefficients do not need to be stored in state because they are constants which do not change between runs of the process.

Listing 4-2: The run function for a NILM stream iterator

```python
# data is 2 column array: [timestamp, sample]
def run(data, state, insert):
    # initialize filter
    with saved zi values
    zi = state.retrieveSlot("filter zi")
    # run filter against this chunk of data
    (y,zf)=scipy.signal.lfilter(b,a,data[:,1],zi=zi)
    data[:,1]=y # update data in place
    insert(data) # save output
    state.saveSlot(zi,"filter_zi") # update zi
```

After initializing the app state in setup, the user then defines a run function. This function receives the resampled input streams from the preprocessor and performs the actual data processing (see Listing 4-2). In this function traditional iterators and third party libraries can be used to build complex signal processing algorithms. Listing 4-2 shows a simple example which runs a linear filter using SciPy, an open source Python library. More advanced code could perform load identification, equipment diagnostics or a variety of other data analysis. The insert argument is a function handle for saving results to an output data stream. After processing the input, any variables that should persist between runs are stored in the state object. The NILM repeatedly runs this function as more input data becomes available.

### 4.5.3 Reports

In addition to generating output data streams (such as the filter example in Listings 4-1 and 4-2), “energy apps” can also produce reports. Reports run over a specific interval of data and produce an HTML document that can contain custom text, plots, and tables. After the stream iterator has processed the specified duration of
Figure 4-6: The stages of a NILM report. 1: The end user designs a report in the Web IDE. 2: The management node adds support code to build an executable script which it then sends to the remote NILM. 3a-b: The script links to streams in the NilmDB, and runs to completion. 3c: The HTML report and associated figures are sent back to management node. 4: The management node stores the report in its MySQL database. 5: Authorized users can view the report in their web browser.

data (e.g., hour, day, week, etc.), an HTML generator produces the report document. A report is defined by an analysis function and an HTML template. The analysis function uses the process state to compute summary statistics and figures. These are injected into the report template to create a full HTML document.

Figure 4-6 shows the process of creating an energy app report. In step 1, the user defines the stream iterator, analysis function, and HTML template. Next, the management node adds the support code making an executable script which is sent to the target NILM. In steps 3a-3c the NILM runs the energy app which generates an HTML document and associated figures. The NILM returns these files to the management which stores them in a MySQL database and makes them accessible through the web interface to authorized users. Hosting the report document on the management node rather than the NILM insulates the NILM from external network traffic providing an additional layer of security and reducing the demand for its limited bandwidth. If privacy is a greater concern than network bandwidth, the NILM can
Figure 4-7: NILM Manager IDE for designing Energy Apps

retain the report in local storage instead.

4.5.4 NILM Manager IDE

The NILM Manager website provides a complete integrated development environment (IDE) to write, test, and deploy “energy apps”. Figure 4-7 shows the app designer interface. The left hand panel is a syntax highlighting code editor with multiple tabs for app initialization, stream iterator definitions, and report templates. To run the app in development mode the user selects input streams and a time range using the plotting window on the bottom right. Text output generated by the app is continuously retrieved from the NILM and displayed in the upper right hand panel. This panel also displays debugging information in the event of an error. In development
mode the output stream is temporarily allocated on the remote NILM, and each time
the app runs, it overwrites the previous output.

Once the user is satisfied with the app’s performance, the code can be deployed to
one or more target NILMs and scheduled as a continuous process. The management
node tracks deployed processes and archives system logs and metrics so that users
can manage the computational resources on their NILMs appropriately. When an
app is deployed in production mode its output stream is permanently allocated on
the target NILM and made available to other users either to plot or use as an input
to other apps.

4.6 Designing Energy Apps

Users with appropriate security permissions can now design useful applications on
the NILM to monitor and control their power systems. “Energy apps” run entirely
on the NILM itself and do not rely on external services or high bandwidth network
connections. The following example shows examples of how these apps are designed
at real monitoring sites.

4.6.1 Cycling System App

Reports present actionable information to end users turning NILMs into powerful
monitoring and diagnostic tools. Consider a standard cycling system such as a shop
air compressor. This system requires periodic maintenance based on hours of op-
eration and excessive runtimes may indicate leaks or abnormal usage, but adding
sensors to track air compressor runs is generally too expensive for the benefit it pro-
vides. NILM is the cost effective solution. A single NILM can monitor multiple
air compressors, and indeed any electric machine in a shop, eliminating costly (and
maintenance-prone) sensor networks [65].

Figure 4-8 shows an example of a report for tracking trends in air compressor
runtime. The report is built in two stages. First a stream iterator, defined by setup
and run functions, processes data over a specified time interval. The stream iterator
Report for Air Compressor

120 runs for a total operating time of 197 minutes

Distribution of Runtimes

Machine status: maintenance required

Figure 4-8: Example of a NILM report for monitoring an air compressor (generated by Listing 4-4)

identifies machine turn on and turn off events by tracking transients in the power waveform. When a machinery run is detected it is added to an array stored in the process state.

After the stream iterator processes the data, the analysis function in Listing 4-3 generates summary statistics and builds a histogram of machine runtimes. The statistics are added to the process state, and the saveFigure function saves the plot using a similar string-tag syntax.

Finally the HTML generator builds the report using the template shown in Listing 4-4. Markdown is used for simplicity although raw HTML and CSS can be mixed in for finer grained control of the document format. Content from the process state is injected into the template using double braces {{ }}, and the insertFigure command embeds plots as HTML images.

The HTML document and plot image are sent back to the management node and hosted through the web interface. Reports like this example, can be scheduled to
Listing 4-3: The analyze function for a report process

```python
def analyze(state, savefig):
    # retrieve data calculated by [run] function
    runtimes = state.retrieveSlot("runtimes")
    # calculate statistics
    mins = int(np.sum(runtimes)/60) # minutes
    state.initializeSlot("time", mins)
    state.initializeSlot("runs", len(runtimes))
    # if any runtime > 3 hours raise alarm
    if(np.max(runtimes)>180):
        state.initializeSlot("status", "maintenance required")
    else:
        state.initializeSlot("status", "OK")
    # make a histogram of the runtimes
    fig = plt.plot(runtimes)
    savefig("runtime_histogram", fig)
    #... additional plot formatting not shown
```

Listing 4-4: Template for report HTML

```html
Report for Air Compressor

{{runs}} runs for a total operating time of **{{time}}** minutes

{{insertFigure("hist")}}

#### Machine status: {{status}}

run once or run continuously. When set for continuous operation the user specifies a repeat interval and duration. For example a report can be set to run every hour using the past 24 hours of data. The web interface provides a navigation tool to browse series of reports which can be help identify trends and spot abnormalities in equipment operation.

4.6.2 Power Quality App

In modern machine shops sensitive devices like CNC tools and 3D printers are colocated with other large equipment that can interfere with the line voltage causing droops and harmonics. In this experiment, a 3D printer shares shop space with a laser cutter and an air compressor, both of which introduce power quality problems including voltage sags. Shop preference is to avoid sharp voltage sags of more than two volts during operation of the 3D printer. A NILM monitors the aggregate current and voltage for the entire shop. Figure 4-9 shows the power consumption of the shop
Figure 4-9: Training the load identifier on shop equipment. The cross correlator presented in [8] uses exemplars to identify turn-on/off events of machines. The exemplar for “Compressor Off” is shown in the popup window.

during normal operation. A cross correlator (discussed in [8]) is trained to identify these loads. The turn-on and turn-off events are indicated in the figure by colored bars. Here, four transients are identified corresponding to a run of the laser cutter and air compressor respectively. The lower power cycling waveform is the PWM bed heater of the 3D printer. Energy apps on the NILM can both quantify the shop’s power quality and and improve the power quality to the 3D printer during operation by ensuring proper scheduling of the loads.

Over this time interval the NILM detected voltage disturbances large enough to interfere with the 3D printer’s operation. Figure 4-11 shows the power waveform as well as the line voltage as measured by the NILM. The app outlined in Listing 4-5 identifies voltage transients larger than 2V. When such a transient occurs the app checks the machine events identified by the cross correlator to determine which piece of equipment caused the transient. If no events occurred at the time of the transient, the voltage disturbance is due to an external load not monitored by the NILM. Such information can be used to quantify power quality complaints when negotiating with the utility. The bars on Figure 4-11 indicate voltage transients and the colors assign responsibility either a piece of equipment in the machine shop or to the utility in the case of external loads.

While the laser cutter does create a large voltage droop it does so gradually and so does not disturb the printer. The air compressor has much more rapid transients
Figure 4-10: Identifying large shop loads. The cross correlator identifies transients of machines in the shop that might interfere with the 3D printer.

Listing 4-5: Energy App pseudo code for identifying and assigning responsibility for voltage transients. `find_equipment_transient` is implemented by the cross correlator trained in Fig 4-9

```python
def run(data, state, insert):  #pseudo-code
    for dv in diff(volts):
        if(abs(dv)>2):  #Voltage transient > 2V
            eqp = find_equipment_transient(dv)
            if(eqp==None):  #no equipment turn-on/off
                insert("utility")
            else
                insert(eqp.name)
```
and is identified as an interfering load by the app. There is also a voltage transient that cannot be associated with machines in the shop and the app assigns the transient to the “utility”. In fact this transient was due to a nearby shop vac that, while not physically located in the machine shop, did cause voltage disturbances on the line. This type of disturbance is typical of power quality problems induced by operations “outside” of the facility. The NILM, configured as an energy box, is not only capable of controlling load sequencing within a facility, it is also able to recognize internal versus external power quality offenders.

4.6.3 Adding Control to an Energy App

As desired, energy apps can also control loads directly using smart plugs. Smart plugs connect to a WiFi network and allow remote clients to control an embedded relay to switch a load on or off. These plugs are available from a variety of vendors [66,67] but use proprietary protocols that make them difficult to use outside of their private commercial ecosystem. The plug in Figure 4-12 is a modified Belkin WeMo Insight. The stock Insight only communicates with a smart phone app and provides limited metering capability. We designed a drop-in replacement control PCB that provides the stock functionality as well as persistent storage to an SD Card, a battery backed real time clock, and high bandwidth metering. This plug interfaces directly with the NILM so energy apps can monitor and control individual loads.

The app outlined in Listing 4-6 uses one of these smart plugs attached to the air compressor to improve the power quality to the 3D printer. When the 3D printer turns on (as detected by the cross correlator), the app turns the air compressor off. When the printer has been inactive for at least \texttt{WAIT\_TIME} seconds, the compressor is turned back on. The actual compressor runs are determined by a pressure gauge on the machine itself.
Figure 4-11: Identifying the causes of voltage transients. An Energy App correlates machine turn-on/off events with voltage transients. If a transient occurred without a matching machine event, the disturbance is assigned to the utility.
Listing 4-6: Energy app pseudo code that only allows the air compressor to run when the 3D printer is off. The app identifies the 3D printer by the bed heater waveform and only enables the smart plug relay for the air compressor with the bed has been off WAIT_TIME or longer.

```python
def run(data, state, insert):
    #pseudo-code
    if detect_printer(data):
        #printer is running: disable the compressor
        set_compressor_relay(OFF)
        last_run = cur_time
    elif (cur_time - last_run > WAIT_TIME):
        #printer has been off at least WAIT_TIME:
        # enable the compressor
        set_compressor_relay(ON)
```

Figure 4-12: Custom smart plugs allow the NILM to monitor and control individual loads. This plug is a commercial Belkin WeMo [66] retrofitted with a custom control PCB. Energy Apps can control the plug relay and read the embedded solid state meter.
Figure 4-13: The Power Quality App in action: running the code in Listing 4-6 protects the 3D printer by disabling the air compressor during print jobs.
Chapter 5

Case Studies

This chapter explores the real world applications of non-intrusive power monitoring using NILM and the Wattsworth infrastructure. These deployments were done in close collaboration with numerous graduate students and the facilities staff at each of the respective locations. Section 5.1 shows how a NILM can track energy consumption by load and quantify energy savings measures. This work was done with Mark Gillman and James Paris and is covered in greater detail in [68]. Section 5.2 uses a NILM to diagnose configuration problems and equipment failures that are difficult to detect in an operational building. This work was done with William Cotta and Mark Gillman and is covered in detail in [69]. Section 5.3 uses a complete Wattsworth system to provide automatic ship logs to the crew of a Coast Guard cutter. This work was done with Greg Bredariol and is presented in [70].

5.1 Cottage Elementary: Energy Scorekeeping

The Cottage Elementary School in the Sharon School District in Massachusetts has served as a fascinating and representative test bed to demonstrate the NilmDB/NILM Manager approach for monitoring. The school is actively used by hundreds of students and teachers. The load sizes, types, and levels of automation seen here are uncommon to residences. Many of the devices are systems of loads, an extension of multistage loads. The boiler, for instance, has a draft fan, blend pump, actuators,
burner controls, and a transformer igniter. Each component has a unique signature and a prescribed sequence of operation in non-pathological operation.

An electrician installed the NILM system using traditional contact voltage and current sensors on a 3-phase subpanel known as the emergency panel (EBPP). Figure 5-1 shows the connection scheme. The EBPP is the critical electrical node servicing the school’s communications, heating system, kitchen appliances, septic system, and other important loads. In the event of a power outage, the backup generator supplies power to this panel enabling the school to provide shelter, heat, food, and communication capabilities to the surrounding community. There are more than 30 subpanels at Cottage, but the EBPP accounts for about 1/4th of the school’s total electrical power consumption during winter months.

5.1.1 Electrical System Background

In cold weather, the largest power draw on this panel is from the machinery involved in creating and distributing heat. Cottage’s heat system is a closed-loop reverse-return hot water system regulated by an integrated building control system (see Figure 5-2). Operation of the heat system depends on several user-established inputs. If the
outside air temperature is below 55°F, the boilers will operate according to water temperature settings in the loop. If the return-loop temperature is below 170°F, the boilers will operate until it reaches 185°F. To prevent cracking inside the boiler, a blend pump mixes return water with supply water. Cottage’s boilers heat water using natural gas, but the electrical signatures of the draft fan and blend pump are detectable during operation. The Variable Frequency Drive (VFD) circulation pumps pressurize the supply loop and move the water through the piping system to the school. The VFD operational speed depends on system pressure. Head pressure, like voltage, maintains the desired flow inside the system. Upper and lower limits are set and measured by the pressure differential. When the pressure is too low or too high, the pumps will speed up or slow down by increasing or reducing voltage frequency.

Cottage’s emergency panel has many other loads unrelated to the heat system, including the IT Room, hot water pumps, large kitchen appliances, etc. These are listed by circuit-breaker number in Figure 5-3. The minimum and maximum kW values correspond to the range of their unloaded and loaded power draw. Some devices, including lights, are frequently on or off, while others continuously operate.
<table>
<thead>
<tr>
<th>Breaker</th>
<th>Load</th>
<th>Min (kW)</th>
<th>Max (kW)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>IT Room:</td>
<td>0.14</td>
<td></td>
</tr>
<tr>
<td></td>
<td>Extreme UPS</td>
<td>0.06</td>
<td></td>
</tr>
<tr>
<td>3</td>
<td>IT Room:</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>Phones UPS</td>
<td>0.09</td>
<td></td>
</tr>
<tr>
<td></td>
<td>SMC</td>
<td>0.07</td>
<td></td>
</tr>
<tr>
<td></td>
<td>Sonic Wall Video AC Pump UPS</td>
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<td>0.06</td>
</tr>
<tr>
<td>5</td>
<td>cable amplifier</td>
<td>0.025</td>
<td></td>
</tr>
<tr>
<td></td>
<td>PA/clocks desktop CPU server</td>
<td>0.16</td>
<td>0.07</td>
</tr>
<tr>
<td></td>
<td>apple CPU server</td>
<td>0.025</td>
<td>0.07</td>
</tr>
<tr>
<td></td>
<td>UPS</td>
<td>0.21</td>
<td>0.13</td>
</tr>
<tr>
<td>7</td>
<td>IT Room:</td>
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<td></td>
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<tr>
<td>9</td>
<td>unknown off/on a lot</td>
<td>0</td>
<td>1.37</td>
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<td>unknown 208V</td>
<td>0.9</td>
<td>0.9</td>
</tr>
<tr>
<td>15</td>
<td>unknown 208V</td>
<td>0.25</td>
<td>0.25</td>
</tr>
<tr>
<td>21</td>
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<td>0</td>
<td></td>
</tr>
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<td>23</td>
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<td>0</td>
<td></td>
</tr>
<tr>
<td>25</td>
<td>freezer</td>
<td>1.2</td>
<td>1.2</td>
</tr>
<tr>
<td>27</td>
<td>unknown ~17 min run time</td>
<td>0.05</td>
<td>0.6</td>
</tr>
<tr>
<td>29</td>
<td>Boiler System:</td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>Boiler 1 Draft Fan</td>
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<td>0.86</td>
</tr>
<tr>
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<td>Boiler 2 Draft Fan</td>
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<td>0.74</td>
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<td>Transformer 2</td>
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<td></td>
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<td>High-flame solenoid 1</td>
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</tr>
<tr>
<td></td>
<td>High-flame solenoid 2 control</td>
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<td></td>
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<td></td>
<td>Boiler 2 Blend Pump</td>
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<td>0.54</td>
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<td></td>
<td>boiler control</td>
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<td>0.13</td>
</tr>
<tr>
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<td>Y-pump Kitchen</td>
<td>0.11</td>
<td>0.11</td>
</tr>
<tr>
<td>35</td>
<td>R-pump</td>
<td>0</td>
<td>0.07</td>
</tr>
<tr>
<td>37</td>
<td>Y-pump School</td>
<td>0.11</td>
<td>0.11</td>
</tr>
</tbody>
</table>

**Breaker Load:**

<table>
<thead>
<tr>
<th>Breaker</th>
<th>Load</th>
<th>Min (kW)</th>
<th>Max (kW)</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>septic pumps</td>
<td>0</td>
<td>1.3</td>
</tr>
<tr>
<td>4</td>
<td>septic pumps</td>
<td>0</td>
<td>1.3</td>
</tr>
<tr>
<td>6</td>
<td>septic pumps</td>
<td>0.02</td>
<td>1.32</td>
</tr>
<tr>
<td>8</td>
<td>VFD circ pumps</td>
<td>0</td>
<td>1.5</td>
</tr>
<tr>
<td>10</td>
<td>VFD circ pumps</td>
<td>0</td>
<td>1.5</td>
</tr>
<tr>
<td>12</td>
<td>VFD circ pumps</td>
<td>0</td>
<td>1.5</td>
</tr>
<tr>
<td>14</td>
<td>freezer</td>
<td>0</td>
<td></td>
</tr>
<tr>
<td>16</td>
<td>chair lift</td>
<td>0</td>
<td></td>
</tr>
<tr>
<td>18</td>
<td>Make Up Air Fan</td>
<td>0</td>
<td>0.28</td>
</tr>
<tr>
<td>20</td>
<td>Make Up Air Fan</td>
<td>0</td>
<td>0.28</td>
</tr>
<tr>
<td>22</td>
<td>Make Up Air Fan</td>
<td>0</td>
<td>0.28</td>
</tr>
<tr>
<td>24</td>
<td>fire protection</td>
<td>0</td>
<td></td>
</tr>
<tr>
<td>26</td>
<td>heat control</td>
<td>0.28</td>
<td></td>
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<tr>
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<td>elev rm lights</td>
<td>0</td>
<td></td>
</tr>
<tr>
<td>32</td>
<td>elev rm outlets</td>
<td>0.07</td>
<td></td>
</tr>
<tr>
<td>34</td>
<td>boiler rm lights</td>
<td>0</td>
<td></td>
</tr>
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<td>36</td>
<td>boiler rm outlets</td>
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<td>38</td>
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<tr>
<td>42</td>
<td>unknown</td>
<td>0.09</td>
<td>0.56</td>
</tr>
</tbody>
</table>

**Legend:**

- **Always On**
- **Baseline Load**

Figure 5-3: Loads monitored by NILM at Cottage Elementary School
Others quietly consume power keeping their internal systems running on standby, even when not in full use. Also of note is the number of 3-phase loads, indicated by multiple breakers with the same label, such as the Make-Up Air fan in the kitchen. The total draw from such loads is the sum of the power drawn on each phase. For instance, the circulation pumps are 3-phase VFD motors drawing a maximum of 1.5 kW per phase, or 4.5 kW total. Other loads in the building create a base load present on the panel electrical phases. Loads not of interest for tracking the heat system, to include smaller pumps and much of the electronic equipment in the IT room, were purposely set aside to draw attention to the larger, more energy-consuming equipment.

### 5.1.2 Load Disaggregation

Power signals at a central point are simply the sum of each individual load's power draw. As an example, Figure 5-4 depicts one hour of the collective power signal on phase A on Monday, March 26, 2013, from 12:00-1:00 PM. Two Python programming scripts developed for Cottage filtered the preprocessed data. The following figures demonstrate how the filters decompose this signal into its individual loads. With the
Figure 5-5: Load transients modeled with step functions

DC offset removed, each transient is then modeled with a step function, the superposition of which effectively reconstructs the original signal. The filtering software detected 23 transients during this hour. Two key features are apparent from the graph: the transients and the baseline. One refrigerator transient is circled. The baseline, about 3.2 kW, is the power draw of all machines that remained on for the entire hour. Graphically, it is the low point on the plot. From Figure 5-5, the other phase-A loads that make up the baseline are the Freezer, Make-Up Air Unit, circulation pumps, and several smaller loads (control equipment, communications equipment, etc.).

Step functions with a magnitude equal to the average delta kW values for each device were used to model the changes in steady state power level as loads activated. Actual turn-on transients for most machines are not clean step functions but in fact vary according to the physical task it performs [71]. In Cottage, most loads were distinguishable using relatively simple characterizations of the “load transient,” i.e., just the change in steady power consumption.
For example, see Figure 5-5. The Boiler Pump must physically move water that is initially static and thus requires more force at first to overcome inertia. As more laminar flow is reached, however, the power requirements on the pump quickly approach steady state operation. Inrush current peaks at about 2 kW for fractions of a second. Power fluctuates for another few milliseconds before leveling off at a level that is somewhere in the range of 0.46 - 0.58 kW at steady state. The other transients follow similar patterns for moving air and sewage. Given that these transients each reach a quasi-steady state within a few seconds and given that the operating durations are on the order of minutes, the step function is a good approximation (less than 5% error) to use to determine kWh consumed. Recalling that real power consumption is the area under the power curve, the turn-on and turn-off transients disclose the duration of each machine's operation. Using this logic, the boiler 1 pump can be modeled using a step function of ±0.51 kW, the refrigerator ±0.89 kW, and the septic pump ±1.38 kW. The baseline, or the DC offset, is about 3.2 kW. Each machine's operation over this one-hour period, graphed separately, is shown in the bottom right corner of Figure 5-5.

The superposition of these three individual transient models closely approximates
the original power signal (Figure 5-6), validating the efficacy of this modeling method. Once the edges can be detected, named, and kWh can be approximated, we can then keep score of each machine's activity and cost.

5.1.3 Case Study Results

The NILM system detected some 5100 events over a period of 6 winter days in 2013 (11-13 March and 24-26 March). Peak hours featured more than 50 events, while the minimum number in a one-hour period was 18. Software corroborated the results. When events were classified, flags were raised if the same machine turned on twice without turning off in between. All such errors were checked graphically. In total, more that 98% of the events were classified without error. Most often, the issue was simultaneous events. A few events were also missed because they occurred too close to the hour (within a few samples). This issue has been remedied for future experiments by eliminating the one-hour file sizes, opting instead to concatenate stored file segments into one large file. With the errors visually corrected, daily run times, cycle durations, and power consumption costs were tallied based off of the NILM output. The results are shown in Figure 5-7. From the monthly power bill, Cottage paid just over 9 cents per kWh to the utility company.

The heat system represents the highest cost on the EBPP, more than $10 per day. It is made up of the 3-phase circulation pumps and the boilers. Broken down into its subsystems the largest single loads are the circulation pumps. One VFD pump is always on while the heating system is on, though the speed and thus power draw fluctuates. From recorded data, these pumps consume, as a rough average, 1.3 kW per phase costing over $8 per day. Combined, the creation and transmission of heat represented almost 11% of the monthly bill in March. Note that this does not include the contribution of the uni-vents in all of the classrooms that distribute the heat to the tenants.

In this experiment, NILM showed promise as a plausible sensor for natural gas sub-metering. Since the burner specifications and boiler hours-of-operation are known, then the amount of natural gas consumed by the boilers is estimable. Therefore
even though natural gas is not sub-metered at Cottage the gas consumption can be estimated. Using this method as an estimate, the Gas utility billed the school for 6554 ccf during the month monitored. Using data from the six-day period highlighted above, the combined (both boilers) average run-time is 8 minutes and 25 seconds per cycle. This is the duration that the draft fan is operating. From the burner manual (Gordon-Piatt R-8 Model), the first 90 seconds (on a timer) of fan time purges the system. No gas flows into the boiler. For the next 10 seconds afterwards, low-flow gas is injected into the burner to facilitate ignition. Considering only the high gas consumption time, there are 6.75 minutes per cycle. From the results, the boilers run an average of 90 cycles per day, which equates to 10.1 hours of high-gas operation time per day. The firing rate of the burner is 2136 MBH according to the data plate, which represents the maximum numbers of BTUs per hour through the burner. Thus, the total number of MBTUs per month is

\[
2136 \text{MBTU/hr} \times 10.1 \text{hr/day} \times 30 \text{day/month} = 647.208 \times 10^6 \text{MBTU/month} \quad (5.1)
\]

From the utility statement, the gas conversion rate is 1 cf = 1.02 MBTU. Converting the MBTUs to cf, we estimate the monthly gas consumption of the boilers during this month to be 6345 cf, which closely resembles the 6554 ccf utility bill. There are other gas appliances whose combined capacity is about 25% of a boiler burner, but
it is interesting to note that this estimate produces a close approximation and merits further study.

Another result made possible by the NILM is a comparison between the boilers. Each has two main electrical components, a draft fan motor and a blend pump. The make and model of the two draft fans are dissimilar between boilers. The blend pumps also differ in model. It is common practice to set unoccupied times on building such as this school. It allows the school to maintain a colder temperature during off hours. As the the temperature dips lower more energy is required to warm the building back up the next morning. This ramp-up period was monitored closely so that a comparison between the boilers could be made. Boiler use is frequently alternated between Boiler 1 and 2 for maintenance purposes. On March 11th, Boiler 1 operated alone from midnight to 8AM. On March 12th and 13th, Boiler 2 ran alone during the same time frame. The temperature profiles for those days being similar (lows of 36, 38, and 32 degrees, respectively), we determined that while Boiler 1’s blend pump uses 20% less power, the draft fan uses 50% more power when running. The duration times of operation varied drastically, with Boiler 1 staying on nearly 2 hours longer to create (presumably) the same amount of heat. Their operation profile differed as well. Boiler 1 ran 15 times with an average duration of about 22 minutes compared to Boiler 2, which ran 26 and 29 times on consecutive days, respectively. Figure 5-8 contains a summary of their head-to-head statistics, revealing that Boiler 1 is about 22% more expensive to operate than Boiler 2 and also puts more about 28% more hours on the machinery for comparable work.

The NILM also measured the effect of a major change to the system. On 25 March, the weather turned warmer. This led to complaints from the teachers about the heat in the rooms. In response, the maintenance technicians throttled all heat valves remotely from their central control station. A corresponding three-phase power reduction of 2.7 kW was observed instantly (Figure 5-9). Because the VFD pumps are pressure controlled, a sudden decrease in demand caused an increase in pressure, and the active pump responded by slowing down significantly. This decrease was observed for the remainder of the school day (about 6 hours), only to increase again.
during the evening hours when the weather cooled off and demand again increased. In total, this saved about $1.50. Knowing the actual savings, rather than relying on assumptions or rumors, empowers the customer with actionable feedback for future decision-making.

The power study uncovered useful information during the training phase as well. First, there are at least 24 loads that are always drawing power, 14 of which are in the Head-End room housing all of the network switches and other communications equipment. Including the Uninterrupted Power Supply (UPS), they draw a collective 1.2 kW at rest (while school is not in session). The UPS was in permanent bypass mode because it was not operating correctly, which the network administrator knew. It was already scheduled for replacement. What was not known was that, even in bypass, the UPS continued to draw about 0.4 kW at a monthly cost of about $26 just to cool itself and maintain standby posture. Measurements of the total load connected to the UPS also led to the recommendation to reduce the size of the replacement UPS from 10kVA to between 5-8 kVA as their maximum load was less than 2 kW.

The reconstructed model in Figure 5-6 accurately models the original signal, validating NILM’s disaggregation method. While the model is visually similar in its basic shape, there are elements of the original that are clearly not in the reconstructed model. First, the power peaks, including their peak amplitudes, are not shown as...
Figure 5-9: Significant three-phase power drop when the VFD demand drops suddenly
explained in Section II. Second, the slow, smooth fluctuations, such as the subtle changes in the variable speed drive, are not accounted for. In general, these represent room for improvement but do not invalidate the approach. While important, the precision of the kWh measurements is secondary to the accuracy of cataloging the individual device patterns from an aggregate feed.

Understanding the details of electrical systems empowers decision makers to make changes without service interruptions or sacrificing environmental comfort levels. Systems like Cottage that employ integrated control systems are commissioned when first emplaced. Over time, as equipment or conditions change, these settings require updates to keep the system optimal. U.S. Department of Energy calls this "continuous commissioning," or updating system controls over time as conditions change [72]. NILM is able to provide early warning that conditions have changed.

Some limitations became obvious from this experiment. The higher the load count, the higher the likelihood of ambiguous results. Two (or more) loads may turn on, off, or one-on/one-off at the exact same time. Higher sampling frequency could improve resolution, but this would bring the added requirement of more memory. Previous research has advocated collecting all questionable identifications after filtering in order to run "anomaly" algorithms. These make successive comparisons of the anomaly delta kW against both combinations of known transient delta kWs and known machine states (on or off) [71]. Also, only changes are visible with the NILM. If loads rarely (or never) cycle, i.e. they are always on, then they are not uniquely distinguishable. The sum of continuous loads comprises the baseline load, which can be discretely determined only by shutting everything off and then back on one at a time.

5.1.4 Implications

The study at Cottage demonstrated a new software architecture for nonintrusive power system monitoring that takes advantage of low-cost in-situ or on-site computing. Detailed appliance-level consumption feedback is possible through NILM. The hardware footprint is minimal, a low cost embedded computer and and associated sensors. Network bandwidth requirements are very small. A commercial or
industrial setting with or without automation could benefit greatly from the energy scorekeeping provided by the NILM software suite. This field test also demonstrated the ability of the NILM to "derive" details of other utility consumption like natural gas. This directly points out the value of increased local "intelligence" or signal processing in unraveling the "big data" problem associated with consumption feedback and diagnostic monitoring.

The NILM system is uniquely suited for austere electrical networks where loads are standardized. It may be a spectacular tool for assisting with micro grid control and economization. For small or islanded networks, the library of loads can theoretically be pre-set, reducing the extent or possibly eliminating the need for a training phase. In terms of network requirements, the bandwidth required for communication is very tractable. We have already begun to examine this approach in oil refineries, and other possible examples include oil rigs, solar plants, wind farms, industrial parks, and other micro grid installations such as military forward operating bases. In the military's case, where there is already a mandate to reduce consumption [73, 74], accountability is made available quickly and inexpensively.

5.2 US Army: Continuous Commissioning

Current building and facility commissioning methods and maintenance/FDD programs focus on providing top down or bottom up analysis of building systems, respectively. The NILM combines functionality of both methods, and does so without requiring a network of machine sensors typical of conventional monitoring systems. Additionally, the NILM provides a platform which can be further developed. Using only new software, an entirely new suite of monitoring tools can be uploaded to provide additional monitoring functionality. Moreover, the back end database allows comparison of different NILM installations allowing best practices to be analyzed against similar facilities.

Two main site locations were utilized for NILM installations and real-world demonstration of NILM methods for identifying energy inefficiencies. These locations are
5.2.1 Fort Devens, MA

Fort Devens, MA houses the Army's Base Camp Integration Lab, a test bed for new technology and a training site for Army reserve units. This facility includes climate-controlled insulated tents, latrines, showers, laundry, and electric kitchen and dining facility. This rapidly deployable package, capable of supporting 150 troops, is powered from two three-phase 120 V, 600 A electrical panels, both monitored by NILM systems. The primary power-consuming loads at the base are the HVAC systems, water pumps, kitchen refrigeration units, and lighting systems.
5.2.2 Fort Polk, LA

Fort Polk, LA is an active duty Army post and home to one of the Army’s three Combat Training Centers. This training center has several FOB base camps used to emulate conditions in current theaters of operation. Figure 5-10 shows an aerial view of one FOB camp. At Fort Polk, the FOB electrical service is distributed with each panel receiving feeders directly from pole-mount transformers and typically serving three structures. As such, a single NILM cannot monitor all loads in the camp from the same location. In the interest of relating energy monitoring to occupant usage trends, two panels were monitored: one powering three buildings all used as sleeping quarters (outlined in blue in Figure 5-10), and one powering two headquarter buildings and one sleeping quarter (outlined in white). These two building types are equivalent in size and major loads, i.e. environmental control units (ECUs) and lighting systems, but their usage schedules differ.

5.2.3 Top-Down Monitoring for Energy Savings

Energy saving objectives at U.S. Army FOBs are driven by the high financial and casualty costs of resupply missions [75,76]. However, any implemented energy savings
measures are constrained by the necessity to perform critical mission tasks. As such, the data collected at the Fort Devens and Fort Polk FOB test sites were used to test top-down approaches towards ongoing commissioning. Specifically, these approaches were designed to provide a local commander whole-system and disaggregated energy usage data for easy comparison with unit schedules and building occupancies. This sort of information allows the commander to make informed decisions aimed at reducing energy expenditures through changes in human activity without sacrificing the unit’s ability to perform critical tasks or use critical equipment.

5.2.3.1 HVAC Operation Schedule

A first example comes from Fort Devens, MA, when a 90 person Army unit occupied the base from 08-10 November, 2013, for a weekend of training. The average temperature for the weekend was 40°F, with a high of 55°F and low of 26°F. The unit occupied the FOB continuously for 48 hrs with the exception of a training session conducted on the weapons range from 0900 to 1700. The NILM itemized the power consumption of the largest loads over the weekend as seen in Figure 5-11. 73% of the energy went towards ECU heating coils; an additional 15% went to the supply fans, which circulate air across the heating coils. Overall 88% of the energy cost was attributed to the 11 ECUs. Adding in the smaller space heaters, which include the
window unit air conditioners used in the showers, latrines, and kitchen, 98% of the
total cost was attributed to HVAC.

When viewing the base’s power usage (Figure 5-12) while considering the unit’s
schedule, it’s clear energy savings measures were not employed when the unit attended
training at the weapons range. In fact, the NILM detected heater runs during this
time period. Considering the minimally insulated buildings that compose a FOB,
this represents a large inefficiency. As depicted in Figure 5-12 by the shaded region,
the actual energy use during the unoccupied period was 913 kWh; overlaid during
the unoccupied time is the “ideal” power draw, i.e. the estimated power draw of
only baseline loads. Based on a similar-temperature day when only these loads were
operating, the minimal energy use for the unoccupied 8 hours was estimated as 208
kWh. The difference of 705 kWh over 8 hrs represents 14% of the total energy
consumption for the weekend.

5.2.3.2 Misconfigured ECUs

A second example comes from the monitored FOB at Fort Polk. Within the same
sleeping quarters two ECUs were set in opposition to each other, with one set to
heat mode and the other set to cool mode while the building was unoccupied. The
NILM was able to detect the transient pattern of a heater and an air-conditioner
each cycling on/off. Figure 5-13 shows the real power streams of the two-phase
distribution system for this sleeping quarter over an 8-hour period during which the
outside temperature remained relatively constant between 70°F-75°F. In this figure,
the transient signatures for the heater and A/C cycling are identified. The NILM
reveals a limit-cycle type operation where the the two ECUs “dual,” with the heater
operating and increasing temperature for approximately 16 minutes and the A/C
responding to decrease temperature for about 24 minutes. Thus, every hour during
this otherwise idle period represents an energy waste of 4.3 kWh, with the heater
drawing around 10kW (5 kW per phase) when on and the compressor about 4 kW
(2kW per phase). For the run-time shown in Figure 5-13 alone, user negligence
contributed up to 40 kWh of energy inefficiency.
5.2.4 Bottom-Up Fault Detection and Diagnostics

The two top-down monitoring examples of Section 5.2.3 display the utility of NILM in identifying energy efficiency improvements through a reduction in user negligence. In contrast, bottom-up methods are adept at detecting and diagnosing machinery faults (FDD) as monitoring occurs at the subsystem level [77]. Once FDD is performed, the implications on top-level optimizations, e.g. building energy use or occupant comfort, can be assessed to determine the proper course of action.

Using conventional monitoring techniques, bottom-up commissioning requires machinery sensors on all systems of interest. However, the NILM affords virtual sub-metering on any load with a detectable transient. This provides the opportunity for bottom-up methods without the complicated network of machine sensors. In the example here, data collected by the NILMs was used to perform FDD on an HVAC system at Fort Polk and to estimate the energy implications of a missed detection.

5.2.4.1 ECU Fault

On the morning of March 28, 2014 at Fort Polk, a wall-mounted ECU faulted when the supply fan ceased to work. This caused a change in the characteristic signature of the ECU unit, and thus appeared as a previously unidentified load on the NILM. Specifically, two deviations from the known on and off transient characteristics oc-
occurred, which allowed the NILM users to detect the fault.

Figure 5-14 shows a comparison of full on/off cycle data collected a few days prior to the fault (Figure 5-14a) and just following the fault (Fig. 5-14b). As noted in the figures, a change in the off transient was detected as the fan off signature was missing from all transients following the fault. Further, the power consumed by the ECU after the fault was approximately 600 W (300 W per phase) less than before. Compared to a healthy ECU, the fault resulted in power consumption dropping from about 4 kW (2 kW per phase) to around 3.4 kW. This difference is equal to the consumption of the supply fan.

Without the supply fan circulating the cool air out of the ECU could only cool
the room through unforced ventilation, a significantly less effective method than the forced convective cooling with the fan. For a 5-hour period, the hottest part of the day during March 29th, the broken ECU had a cumulative on-time of 3.1 hours. During that same period, a healthy ECU operating in a different sleeping quarter and at the same temperature set point operated for only 1.4 hours total, less than half the time of the broken ECU. Thus, due to the machinery failure, the broken ECU required almost double the energy of the normally functioning ECU.

Without the NILM, this broken ECU may have gone unnoticed as the room was still cooled to a comfortable temperature, just at a significantly larger energy cost. With the NILM however, the unit commander knows that replacement of the ECU can enact an improvement in long-term FOB energy efficiency.

5.2.5 Implications

Each of these examples represents value-added information for actionable feedback towards improving whole facility energy efficiency. For the unit commanders at Army FOBs, acting on this information results in energy savings translating directly into a reduced demand for fuel convoys, and a concomitant reduction in casualties. For an industrial facility or commercial building manager, the NILMs instead provides energy efficiency insight towards lowering utility bills and increased profits; for the environmentally conscious homeowner, the NILM gives positive reinforcement towards reducing their carbon footprint. Thus, while the Army FOB camps provided the environment for these NILM research and demonstration projects, the monitors, software platforms, and energy-saving commissioning and FDD techniques described here are easily extendable across many sectors and useful for a variety of optimization goals.

5.3 US Coast Guard: Equipment Monitoring

Modern Navy, Coast Guard, and commercial maritime crew sizes continue to shrink as there is a shift to “optimally” and minimally manned crews completing more complex and varied mission sets. Smaller crews rely on sensors and automatic operation to
perform a host of duties once completed manually. This generates a substantial
need for monitoring systems to ensure proper operation of equipment and maintain
safety at sea. These systems require a significant infrastructure of sensors, wires, and
intermediate panels or data collation sites. Because conventional monitoring systems
rely on a substantial, distributed hardware installation, communications losses and
sensor failures can become commonplace and crippling. Reduced manning may also
mean reduced repair hours, and crews with complex but difficult to maintain sensor
systems may effectively be left without needed monitoring equipment.

The NILM poses interesting possibilities for shipboard use and maintenance [78].
In particular, the NILM can serve as a “shipboard automatic watchstander” or SAW
for tracking machinery operation. This case study demonstrates the operation of a
NILM as a watchstander aid during underway operation of USCG SPENCER, a 270
foot Famous-class cutter.

5.3.1 Shipboard Automatic Watchstander

The NILM offers several important benefits to both increasing the precision and au-
tomation of Coast Guard watchstanders. First, NILM systems can discern machinery
status and automatically generate a log of operation. Second, they can compare ma-
chinery operation and sequencing, reflecting the demands of the crew, to a known
operational status to relay to decision makers crew fatigue and operational tempo.
Third, the NILM can ensure that operational procedures are followed and that auto-
matic functions of machinery are operating as designed to improve or maintain the
life of machinery. Because NILM systems require limited access from an aggregate
measurement in the power system, they provide a single robust monitoring point that
doesn’t rely on complex networks of sensors.

5.3.2 Automatic Logging

In the USCG the current method for keeping machinery logs is manual entry. This
approach relies heavily on accurate human observation and annotation. Logs are for-
warded to maintainers and operational commanders, and accurate log keeping is an
important function for the USCG. Logs are critical for recording operational history and supporting maintenance decisions, and are entered as official legal documents. Generally, watchstanders maintain a “rough log” which is a handwritten document containing times of events and operations including fuel transfers, machinery status changes (starts and stops) and other key events. This is then periodically transferred to a typed document, an overall method that is clearly open to flaws. Watchstanders can be extremely taxed while making normal rounds on equipment. Verifying operation, safety, performing maintenance, training new crew members, and performing casualty response are just some of the watchstander’s normal duties. Accurate log keeping can become an afterthought in stressful or repetitive situations. Manual logging also poses the possibility of distracting the watchstander from the equally important task of monitoring machinery health, possibly allowing for a casualty to go unnoticed.

This case study presents results from a SAW based on nonintrusive monitoring technology for automatically logging start and stop times of machinery operation. This technology reduces the impact of human error and potentially allows human watchstanders to focus on more important and less repetitive tasks. As budget constraints tighten and technologies increase to allow for remote operation of systems as well as increased automation, crew sizes have decreased, in some cases to 50% of manning on legacy assets. Each remaining crew member performs a new multitude of tasks. It is not uncommon for a single crew member to be responsible for monitoring machinery health through frequent rounds, wipe up oil, complete oil viscosity tests, check oil levels, check temperatures, verify pressures, start generators, pump sewage, refill head tanks, and other duties. A SAW creating automatic logs could improve safety and efficiency by decreasing the amount of time a crew member has to spend logging machinery operation manually. Additionally, precision could be increased through logging of exact times and ensuring that no or relatively few events are missed.

Hourly tracking of operations underlies the USCG’s maintenance planning, as many maintenance tasks are based on accumulated operating time, e.g., for major
overhauls, oil changes, and other cyclical maintenance. Accurate, automated tracking could greatly improve maintenance planning, decreasing costly corrective maintenance completed after casualties. Also, current systems rely on maintainers receiving aggregated reports from operators on a bi-annual or annual basis. Infrequent information flow easily creates disparities between projected hours and actual operational hours and creates a gap in planning. Automated tracking could ease data collation and access for decision making.

5.3.2.1 A Bellwether for Crew Performance

Certain operations pose increased risk. These “special evolutions” include events such as flight operations, anchoring, maneuvering close to shallow waters, towing, battle quarters, refueling at sea, and law enforcement operations, among other higher risk
evolutions. For these evolutions, vessels institute a condition of operation called the Restricted Maneuvering Doctrine (RMD) that sets additional precautions to mitigate risk. This doctrine is a balance, in that a majority of the crew receive complex or additional duties, creating a potentially fatiguing burden. As crew fatigue increases, the likelihood for mishaps increases. Whenever possible operational commanders should be aware of cumulative time spent at RMD to properly evaluate risk when assigning missions.

There is currently no objective metric to measure fatigue. In the naval community, the USCG employs the GAR model which evaluates crew fatigue on a subjective 1-10 scale. This metric is difficult to evaluate objectively. The aviation community, on the other hand, has a more objective metric, accounting hours of operation and requiring hours of rest [79].

5.3.2.2 Ensuring Compliance with Operating Procedures

When setting RMD, certain pieces of equipment are generally energized and an equipment status is prescribed. Knowing this status and equating it to RMD, a SAW could sense the amount of time a vessel spends at RMD, providing operational commanders a hard metric for crew fatigue when evaluating risk and gain for missions. Also, the SAW can evaluate compliance with prescribed operating procedures and detect deviations in crew performance. Each piece of machinery has a specified or “standard operating procedure” (SOP). These SOP’s contain step by step instructions on machinery alignment and operation. In several systems, the order of operations is extremely important to ensure that catastrophic damage does not occur. For instance, the reverse osmosis feedwater pumps must be started before high pressure pumping commences. Deviations remove cooling and impellers or high pressure pistons could be destroyed. Similarly, diesel engines must be prelubed before starting to ensure lubrication of parts. If a NILM can detect these sequences to prevent or warn an operator when they have missed a step in the sequence, millions of dollars in costly corrective maintenance could be saved across the USCG’s fleet assets. Also, deviations from SOP could potentially serve as an additional indicator of crew fatigue.
5.3.3 Installation on the USCGC SPENCER

To explore these possible uses, a SAW system was installed on the USCGC SPENCER (WMEC-905) shown in Figure 5-16 from November 2014 to December 2014. USCGC SPENCER is a 270ft Famous Class cutter stationed in Boston, MA. Two nonintrusive systems were installed, one on the #2 Main Propulsion Diesel Engine (MPDE) auxiliary supply panel in the engine room, and another on the main exhaust fan for the engine room. These monitoring systems collected data during underway operations to test the potential for automatic event logging and centralized data analysis from the ship power system to classify the status of the vessel and its machinery.

The machinery plant of the cutter consists of three ALCO V-18 propulsion diesel engines and two electric diesel generators rated for 475KW as well as an emergency generator rated for 500KW. It carries a crew of approximately 100 and maintains a rigorous schedule of over 185 days deployed per year [80].
Figure 5-17: Standard Coast Guard exhaust fan.

The installed nonintrusive monitors observed the exhaust fan pictured in Figure 5-17 and the #2 MPDE auxiliary supply panel. Mission critical loads fed from this supply panel include the #2 Main Propulsion Diesel Engine (MPDE) prelube pump, the #2 “C” Controllable Pitch Propeller Pump, the MPDE lube oil heater, and the MPDE Jacket Water Heater. The location and placement of the monitoring boxes can be seen in Figure 5-18. By observing data from these monitors, the machinery plant status can be reconstructed, as shown in the next section. This reconstruction can be compared with required operating procedures. For example, the exhaust fan should be turned on prior to the MPDE starting in order to ventilate the space. The fan is deactivated when the MPDE is not running to keep the engine warm while offline.

The CPP “C” pump motor is a 3 phase motor nominally rated at 440V, 13.6 Amperes, and 10 hp. Figure 5-19 shows the motor. The MPDE prelube pump motor is a 440 V 3 phase 4.9 ampere and 3 hp motor and can be seen in Figure 5-20. The two heaters connected to the system, the MPDE jacket water heater and the MPDE lube oil sump heater, are both 440 V, 3 phase resistive heaters. The JW heater is rated at 9KW and the lube oil sump heater is rated at 12 KW.

The monitored equipment works separately and together to ensure that the MPDE functions correctly. For example, the monitored prelube pump runs continuously when the engine is offline, but does not run while the engine is online. The Lube Oil heater will automatically energize when required and then turn off when temperatures
Figure 5-18: USCGC SPENCER engine room. Nonintrusive monitors are installed forward of the #2 MPDE just above the monitored panel.

Figure 5-19: CPP “C” pump motor that supplies pressure to vary the pitch on the blades of the propeller. These pumps are energized when RMD is set and the vessel enters a time of increased risk and fatigue for the crew.
Figure 5-20: The 3 hp motor for the MPDE prelube pump. It is continuously energized when the MPDE is off and automatically stops when the engine is started. By monitoring its status (on/off) the engine’s status can be inferred.

are adequate, maintaining oil temperature between 90 and 120 degrees Fahrenheit). The jacket water (JW) heater works in the same fashion, automatically energizing when required. When the engine shuts down, the prelube pumps turn on, the JW heater turns on, and the exhaust motor should be turned off by the crew. When the engine starts, the prelube pumps turn off, the JW heater turns off and the exhaust motor should be turned on.

The controllable pitch propeller is powered by a hydraulic loop. Hydraulic pressure is sent through a hollow shaft to the blades of the propeller, altering blade angle to quickly alter speed. Hydraulic pumps control the amount of hydraulic oil sent to the propellers to change pitch (by changing pitch the speed/direction of ship movement is controlled). The “C” Controllable Pitch Propeller (CPP) pump is unique in that it is energized for “Special Evolutions” that require that RMD be set. By energizing the “C” pumps, the operators are given greater handling performance and faster response.

During special evolutions the restricted maneuvering doctrine (RMD) is set and a prescribed machinery status is initiated. The nonintrusive SAW can detect machinery status by identifying the transients and recognizing equipment used uniquely during RMD. High level mission commanders could receive automatically logged summaries of times and durations when operational tempo increased. This could move the
surface fleet towards the aviation model where given a certain number of hours would equate to a certain level of crew fatigue. It is not uncommon for watchstanders to go without rest due to special evolutions combined with normal routine.

The next section illustrates the findings of a prototype SAW examining underway data obtained from the USCGC SPENCER.

5.3.4 Signal Processing and Transient Identification

The SAW’s functionality is critically dependent on its ability to disaggregate and identify transients of interest. This signal processing problem of extracting individual transients from aggregate data is an intellectually exciting and mathematically tractable problem for power systems of the size found on SPENCER, for example. Aggregate power data for a window of time aboard the SPENCER is shown in Fig. 5-21. The data clearly shows a complex mix of events occurring on the ship power system, and hints at the challenges in disaggregating transients.

Careful examination of the ship’s data reveals that start/stop events can be identified given exemplars representing individual load transients. During the cruise summarized by Figure 5-21, the cutter participated in an extended training period during which it made frequent port calls. This made monitoring interesting, with many transient load activations. The data from 10 December 2014 is one example, shown in
Figure 5-22: Data retrieved from monitoring on 10 December, 2014.

Figure 5-22 below.

For example, on this day from 0000 local time until 0600, the ship is in-port on shore power, with a collection of loads operating that would be typical for "bravo status," i.e., the ship is active but not underway. The step function in power is the jacket water (JW) heater turning on and off. The prelube pump is also running. Figure 5-23 shows the first crew action for getting underway, the starting of the engine shown in Figure 5-23 at 0601. At this time, the prelube pump is deactivated in preparation for engine start.

At 0601 on SPENCER, nothing on the observed panel is operating. The MPDE is on at this time, providing its own lubrication with an attached shaft-driven pump. The electrical support loads are off, therefore, at this time. As described earlier, also on this panel is the CPP “C” pump which is energized when the cutter enters a special operational status of perceived higher risk, or RMD. The first “on” event for this can be seen at 0720 where the pump energizes as shown in Figure 5-24. This corresponds to the cutter leaving port, and RMD condition.

The data from the CPP can be highly telling as it relates directly to a condition of steaming of the vessel, the setting and securing of RMD. From the data, one can extrapolate that the cutter was at RMD from 0720 to 0903, 0919 to 1055, and 1426
Figure 5-23: The MPDE starting as observed by the nonintrusive SAW. Note that there is a progression as the heating elements turn off once the start sequence initiates. The prelube pump remains energized until after the start sequence is completed to ensure lubrication during start (approximately 2-3 additional seconds).

Figure 5-24: Characteristic CPP on and off event. The CPP motor is rated for 13.6A.
Figure 5-25: This figure shows the data taken from 10 December 2014 from the SPENCER SAW.

to 1607. For that day alone, the cutter was at a heightened state of readiness for 5 hours. This is a telling metric for mission commanders and planners and shows that there is a high probability of fatigue for this crew on this day. In evaluating the risk for an additional potential evolution, this metric could be crucial to weighing the risk and gain of a proposed mission. These start and stop times match manually logged start and stop times. Figure 5-25 shows the data on MPDE start and stop times as well as CPP times taken from the NILM box sensing of the prelube pump status and the CPP pump status.

Nonintrusively acquired and interpreted power data can be more reliable than human entry. Human entry relies upon an already overtaxed watchstander to log items. This leaves a high probability that during high stress or high tempo times, the log becomes an estimate at best, at worst a distraction to a watchstander trying to maintain equipment. An example of this is missed entries in the log. Taking the log from 10 December for an example, the SAW was able to identify two key events (the setting of RMD denoted by starting the CPP “C” pumps) that were not logged in the watchstander’s log. Thus the NILM offers a way to deconflict the work of the watchstander while still providing an accurate log, in this case more reliable than one created by human entry. It is important to note that the NILM also provides exact
time data whereas the logs were off from the NILM data by up to 15 minutes.

When the MPDE is stopped, there is a similar sequence of relevant transients and load activations. The prelube pump should start immediately upon engine stop. Other loads associated with the MPDE (JW heater and lube oil heater) will not start immediately as these are controlled by temperature thermostats. The engine stopping can be seen in Figure 5-26. Then, approximately 15 minutes later, the heater loads activate as shown.

The SAW is able to identify sequences and ensure prerequisites for proper load activation and operation are met. On Famous Class cutters the prelube pumps are continually running. However on many ships, such as the USCG 210ft Reliance Class cutters, prelubing must be done manually before starting the MPDE’s or increased wear will develop on the MPDE. This requires a human input that may be skipped if the operator is not following the SOP correctly. An installed NILM would be able to sense the prelube pump and ensure it is started before starting the MPDE. This has many applications as many systems work in this manner where prerequisites should be met before other steps are taken or damage can occur to the system. On newer ships, many of these fail safes are built into the systems. For example, on the newest USCG cutter, the WMSL, the controls software will not allow start of the MPDE without prelube to a specified pressure; however on legacy class cutters this function does not exist and they rely on human input, which, especially during high stress
Figure 5-27: Image of unusual readings from CPP pump after maintenance.

situations, can result in errors. The SAW can be used to ensure proper steps are followed, producing a warning signal if proper sequencing is not observed.

The nonintrusive SAW also offers opportunities for tracking machinery health. There are characteristic start up and steady state signatures associated with each piece of machinery. If these signatures change, then there may be an identifiable maintenance issue. For example, pump damage can occur when pumps are run without a pumping medium (run “dry”). This situation occurred with a CPP pump onboard SPENCER during the cruise under observation here. After performing maintenance, the CPP pump was started and run without a medium for several seconds (system was purged of fluid during maintenance). Figure 5-27 shows power fluctuations possibly caused by loss of suction in the pump. By identifying these events, the nonintrusive monitor can be used for health monitoring.

Another example of this is when the cutter moors (enters port) or leaves port. During these evolutions, there are rapid calls for rudder and propeller commands. These rapid movements can be seen in unusual patterns in the CPP’s power draw as the motor is worked aggressively. This can cause damage to the pump or motor beyond normal expectations and, depending on conditions, could indicate that operators should be encouraged to decrease command frequency. At a minimum, these records can be used as a kind of “odometer” to indicated the potential need for maintenance. Figure 5-28 shows these heavy use patterns.
5.3.5 Case Study Results

Each piece of machinery on the ship can be characterized on initial installation of the SAW during a training phase. There are a variety of methods for acquiring training data. During the training phase, for example, readings are taken on three phases A-B-C while loads on-board the ship are activated or observed during dock-side operation. Power signatures are recorded in real and reactive power and higher current harmonics, associated as fingerprints for each load of interest. Different machinery draws different amounts of real and reactive power and harmonics consistent with the different physical tasks performed by different machines. Each piece of equipment may also exhibit unique turn-on transients. For example, Figure 5-29a shows the real and reactive power demanded during the startup transient of a CPP pump. For comparison, Figure 5-29b shows the turn-on transient of a lube-oil heater. These distinctive, predictable, and reproducible waveforms can serve as fingerprints for recognizing and disaggregating load operating schedule by examining the aggregate power feed to the loads, even when several loads are operating at the same time.

Some machines operate with strong periodicities, such as heaters that have a period of operation where they are on for a relatively constant amount of time and then...
off for a constant and relatively predictable amount of time for certain underway conditions. Other machines follow a predictable sequence of events, e.g., if one piece of machinery starts, another should start at a given interval later, e.g. the pumps in a reverse-osmosis water system. Through knowledge of proper system operation and prediction of events, an expert system can be developed that uses non intrusively observed power transients to identify not only particular loads but also particular cycles of operation or ship state, such as an engine start. The Wattsworth programming environment can be used to flexibly implement an expert system that analyzes and summarizes ship state and condition based on observed load transients and operation. First, by running a load identification filter over an incoming set of data, load events can be identified and tagged. Streams of tagged events can be further analyzed to identify sequences of load operation that correspond to correct or improper use of a multi-load system. These analyses can be summarized automatically as log reports, providing high accuracy automated replacements for human generated logs, unburdening the crew of this labor. For example, Figure 5-30 shows an actual log report from a SPENCER watchstander during a recent underway cruise. The SAW onboard SPENCER automatically generated the log shown in Figure 5-31. Note the similarities and the more exact times found by the NILM system.

Additional metrics can be parsed from this data. For example, fuel oil transfer pumps periodically transfer diesel fuel to a ready service tank feeding propulsion and power generating prime movers. These fuel pumps deliver a relatively consistent flow rate. The SAW is capable of tracking the operating time of the fuel pump electrically, and then deriving the implied fuel transferred to the service tank, essentially
MACHINERY LOG

U.S. Coast Guard Cutter SPENCER (WMEC 905) Date: 10 DEC 14

WATCH OFFICER’S REMARKS:

0000-0400
Vessel is moored at the above location. Ship's status is B-12. Electrical power, potable water, and sewage discharge are being supplied via shore-tie. Reviewed Tag-Out Log and the following machinery is listed as OOC: Oily water separator system, Bridge window heater STBD center, #2 MG set, VCT suction valve, Clutch control PLTHS pushbutton and STBD CPP L/O Heater. All other machinery is IAW the Midnight Machinery Status sheet. 0345 Carried out the watch routine.

0400-0800
Vessel is moored as before. 0425 Energized the pre-lube pumps for both SSDG’s. 0430 Started both SSDG’s and secured the pre-lube pumps. 0500 Shifted from shore power to ship’s power. 0501 Paralleled the #1 SSDG to the main bus. 0535 Conducted round of the ship and the pier, all secure. 0600 Started BMDE’s. 0630 Shifted BMDE’s from E-MAN to ECC Auto. 0700 Completed Light-Off Schedule. 0720 Set the Special Sea Detail. Set RMD in the Engine Room. 0735 Clutched in BMDE’s, placed in PHC Auto. 0745 Carried out the watch routine.

0800-1200
Vessel is moored as before. 0814 Vessel U/W. 0825 Conducted round of the E/R, all secure. 0855 Secured from Special Sea Detail, secured from RMD in the E/R. 0905 Secured BCPP C Pumps. 0906 Energized BMDE and SSDQ L/O spinners. 0911 Set Restricted Maneuvering Doctrine and Set GE. 0922 Energized BCPP C Pumps. 0924 Energized #1 and #2 Fire Pumps. 1055 Secured from GE and Secured from Restricted Maneuvering Doctrine. 1056 Secured #1 and #2 Fire Pumps. 1057 Secured BCPP C Pumps. 1057 Carried out the watch routine.

Figure 5-30: The machinery log generated manually by the ship’s crew by logging events and times.

automating the tracking of fuel consumption. Currently, fuel transfer amounts are discovered through manual soundings or an Automatic Tank Level Indicator (TLI) on newer vessels. This approximation from the SAW can be a check of these readings. In heavy weather, manual soundings and TLI readings are extremely unreliable and difficult to achieve due to the motion of the vessel. In rough seas the NILM is capable of providing the most accurate fuel consumption estimate. Several other metrics like this can be developed as well, including machinery hours (an important maintenance factor), crew fatigue from hours at heightened alert, proper sequencing and alignment of multi-pump systems like RO, and metrics on days underway.

The robust nature and simplicity of the NILM system offers several advantages to the distributed sensor network currently used by USCG, USN and commercial fleets. Communications losses are common place in distributed systems with long cable runs, large numbers of complex sensors, and complex communications systems.
Figure 5-31: Automatic machinery log generated by a SAW onboard SPENCER.

involving repeaters. Compared to these systems, the nonintrusive approach requires much less maintenance, requires less equipment, and is a fraction of the price to purchase and to install.

5.3.6 Implications

Observation from the USCGC SPENCER field data indicates that nonintrusive power monitoring can have an important role in ship operation and maintenance. Here, we observed a single important breaker panel with eight systems during a month of underway operation. The nonintrusive SAW accurately tracked all systems. The SAW also developed derived metrics using “expert” knowledge of the combined operation of ship systems. For example, the SAW tracked MPDE auxiliaries to determine when the MPDE was online and offline as well as track the usage of the CPP “C” pumps. By tracking the auxiliaries systems of the MPDE, order of operations can be verified to ensure health of the machinery as well as proper start up and securing procedures.
Using this information, top level commanders can easily see the exact state of the vessel, underway, at RMD, or other modes of operation. Work is currently underway to install a NILM system on the USCGC SPENCER to monitor the entire, ship-wide machinery status by placing the NILM at the ship's central power distribution panel. In preliminary observation, loads were observed turning on and off, similar to the observations from the single panel experiment described here. Future work is aimed at expanding the ability of the NILM to detect events in more complex aggregate data streams, and produce comprehensive logs and reports for the entire ship.
Appendix A

Documentation

This appendix covers the installation and operation of non-intrusive power monitors and the usage of the NILM Manager web platform. This appendix is available in its entirety in the NILM Manager Help section. From a standalone system visit http://nilm.standalone/help or from any Internet connected device visit http://www.wattsworth.net/help. Appendix A.1 provides quick start guides to common operations. This covers the installation and configuration of non-contact and contact power meters as well as smart plugs. Appendix A.2 is a comprehensive guide to all of the Wattsworth hardware and software arranged as follows:

Hardware Configuration  Setup and install contact or non-contact power meters

Software Configuration  Configure data capture with one or more power meters

Smart Plugs  Setup and use smart plugs with a NILM system

Administration  Manage databases, processes, and global settings

NILM Explorer  View data streams in the web browser plotting interface

NILM Filter  Run custom python scripts that create new data streams

NILM Analyzer  Run custom python scripts that generate HTML reports

NILM Finder  Find and identify loads using exemplars
Processes Automate NILM filters and analyzers

Command Line Interface Low level command line tool to interact with the NILM
Quickstart Guide To

Setting up a Contact Meter

1. Install current and voltage sensors

Configure the resistor settings for the current sensors

The LEM current sensors are converted to voltages by a resistive load on the meter circuit board. The value of this load is set by a series of DIP switches for each current sensor. See Setting up a Contact Meter for details on setting the DIP switches. The load resistance should be set to spread the expected signal as widely as possible across the +/- 5V input range. The upper limit on the load resistance is specified in the LEM datasheet. See LA 55-P datasheet for an example.

Connect the LEM current sensors and mount the meter

The voltage sensor wires and current sensors must be installed by a trained electrician. Make sure all equipment is fully de-energized and tagged out before installation. It is best practice to install the voltage sensors on a separate breaker so the meter can be de-energized without shutting off other appliances. Use the illustration in Setting up a Contact Meter to determine the mapping of voltage and current sensor phases to the LabJack indices. This information will be required Step 3.

2. Setup the ethernet connection

Pick a network topology

**Single Meter:** If there is only one contact meter in the installation, it should be directly connected to the host computer’s built-in ethernet port or to a USB to ethernet converter. No special configuration of the LabJack IP address is required. The host computer interface must be a unique address on the same subnet. With a LabJack set to factory defaults the host address should be 192.168.1.200. see an example

**Multiple Meters:** If multiple contact meters connect to the same host there are two possible network configurations. Both require reconfiguration of the LabJack IP address.

**Switched Subnet:** In this topology the meters and the host computer connect to a common network switch. The meters and the host computer must be on the same subnet and each LabJack must have a unique address. see an example

**Multiple Interfaces:** In this topology each meter connects directly to the host computer either to a built-in ethernet port or through a USB to ethernet converter. Each meter and its host interface share a subnet and must have unique addresses. see an example

Configure the LabJack IP address

The LabJack settings are configured with LJStream. This is a Windows only application. Check the company website for the latest release or download the local copy of LabJack-2015-11-19.exe. The Windows machine can be configured to talk to the LabJack over ethernet or the LabJack can be physically removed from the meter and connected to the Windows machine by USB.
Configure the Host IP address

The host computer IP address is configured with Network Connections. One way to access Network Connections is through the Dash (see example). This will bring up a dialog with all of the current network connections. Select the interface used by the LabJack and follow the steps in Network Configuration to change the IP address settings.

3. Configure the host computer

Set up a secondary hard drive

The NILM database (NilmDB) should be stored on a separate hard drive if possible. This protects the main system from being completely filled by NilmDB and becoming unstable (although a properly configured meters.yml should prevent the database from growing too large). Placing NilmDB on a separate drive also makes it possible to get data off a meter by simply removing the drive and replacing it with a new one. See Setting Up Storage for more details.

Add configuration to meters.yml

Open meters.yml (on the Desktop) in a text editor or simply double click the file icon to use the default editor. Copy the template and follow the instructions in Setting up a Contact Meter. Note: If you are configuring multiple meters, each meter needs a unique name (meter1, meter2, ... meterN). Adjust the template configuration accordingly.

Configure BIOS for Auto-Boot

NILM’s installed at remote sites should be configured to restart if power is lost and later restored (auto-boot). By default the BIOS will leave a computer off if power is lost, requiring a manual button press to turn the system back on. Each BIOS is different but most can be configured by holding F12 or DEL during system boot. It is best practice to install an uninterruptible power supply (UPS) with the meter both to reduce the chance of power failure and to record current and voltage signals during the power glitch for later diagnostics. Make sure the UPS is configured to restart automatically if it is discharged entirely before power is restored.

4. Verify the configuration

Check meters.yml

Use nilm-check-config to check meters.yml for syntax errors and configuration warnings. Run this command from a terminal window (how to access the terminal). Make sure there are no errors and that you fix or fully understand any warnings. The configuration check also displays the amount of storage required. It is best practice to use only 80% or less of the available space even if NilmDB is on on a separate drive. This keeps space available for data generated by filters or snapshots of interesting data that would otherwise be erased by the keep settings in meters.yml.

Check the sensors

Use nilm-scope to check the sensors. Run this command from a terminal window (how to access the terminal). Check the relative phases of the current and voltage to make sure the sensor indices in meters.yml are correct. Note that the currents will not line up exactly with the voltages if the power factor is less than unity. This is common when there are large motors or other inductive loads on a phase.
5. Start capturing data from the meter

Start nilm-capture service

Start (or re-start) the nilm-capture service using the terminal (how to access the terminal).

Check the system logs

Check the files in /var/log/nilm periodically for error messages. See NILM System Logs for details.

6. View meter data from the website

Refresh the web manager

Open the Installation Administration page, select the "Database" tab, and click Refresh twice. This will update the web interface with the new meter. You should the new meter and its data streams appear in the navigation tree. See Managing the NILM Database for more details.

Plot meter data

Open the Data Explorer and select one or more streams from the new meter. Click Start Live Update to view the latest data and verify that the data is being captured and processed correctly. Edit meters.yml to fix any of the following errors:

- If the ratio of \( P \) and \( Q \) are wrong adjust the phase's sinefit-rotation angle.
- If current or voltage scales are incorrect adjust the respective sensor_scales. Each phase can be fine tuned by using an array of scale factors instead of a single value.
- If the amplitude of prep is wrong but the current and voltage are correct adjust the nominal-rms-voltage setting.

See Configuring a Contact Meter for more details. Note that you must restart the nilm-capture service for changes in meters.yml to take effect.
Quickstart Guide To
Setting up a Non-Contact Meter

1. Install the non-contact sensors

Select a sensor configuration

Select the type of sensor platform you want to use. The Flex Sensor is an all-in-one platform that is ideal for multiple conductor powerlines where the location of each conductor inside the bundle is not known. The D-A-Y board is ideal for monitoring multiple physical conductors or where the location of each conductor in a wire bundle is known. In general the D-A-Y board package provides a more flexible solution and is the recommended platform. The non-contact sensor (D-Board) has four input ports. Sensor boards (A Boards) can connect directly to these input ports. Each A Board provides a current and a derivative of voltage signal. Connecting a sensor to each input port provides a total of four current measurements and four derivative of voltage measurements. This is the recommended configuration. If you want a different combination of sensor inputs or want true voltage rather than derivative of voltage you can use a Y Board to adjust the sensor configuration. The Y-Board connects to any input port on the D-Board and provides two connection ports for sensors (A-Boards). A set of jumpers selects which signals are passed back to the D-Board. See the close up of the jumper configuration diagram here.

Attach sensors

If using the D-A-Y board platform, attach the A-Boards to the powerline with zip ties. Multiple A-Boards can be connected with a single zip tie or each board can be connected individually as shown in the example figures. Make sure each board is connected securely to ensure accurate measurements. Connect the ribbon cable plugs to the D-Board before putting the D-Board in its enclosure. Once all cables are seated, connect the USB cable and seal the D-Board in its enclosure. If using the Flex Board secure the sensor to the powerline two zip ties, one at the base and the other around the flexible arms.

2. Configure the host computer

Set up a secondary hard drive

The NILM database (NilmDB) should be stored on a separate hard drive if possible. This protects the main system from being completely filled by NilmDB and becoming unstable (although a properly configured meters.yml should prevent the database from growing too large). Placing NilmDB on a separate drive also makes it possible to get data off a meter by simply removing the drive and replacing it with a new one. See Setting Up Storage for more details.

Add configuration to meters.yml

Open meters.yml (on the Desktop) in a text editor or simply double click the file icon to use the default editor. Copy the template and follow the instructions in Configuring a Non-Contact Meter. Note: If you are configuring multiple meters, each meter needs a unique name (meter1, meter2, ... meterN). Adjust the template configuration accordingly.

Configure BIOS for Auto-Boot
Meters deployed to remote sites should be configured to restart if power is lost and later restored (auto-boot). By default the BIOS will leave a computer off if power is lost, requiring a manual button press to turn the system back on. Each BIOS is different but most can be configured by holding F12 or DEL during system boot. It is best practice to install an uninterruptible power supply (UPS) with the meter both to reduce the chance of power failure and to record current and voltage signals during the power glitch for later diagnostics. Make sure the UPS is configured to restart automatically if it is discharged entirely before power is restored.

3. Verify the configuration

Check meters.yml

Use `nilm-check-config` to check meters.yml for syntax errors and configuration warnings. Run this command from a terminal window (how to access the terminal). Make sure there are no errors and that you fix or fully understand any warnings. The configuration check also displays the amount of storage required. It is best practice to use only 80% or less of the available space even if NilmDB is on on a separate drive. This keeps space available for data generated by filters or snapshots of interesting data that would otherwise be erased by the keep settings in meters.yml.

Check the sensors

Use `nilm-scope` to check the sensors. Run this command from a terminal window (how to access the terminal). Check that the magnetic sensors have strong signals and show a diverse response to currents on different phases. Adjust the sensor location if the signal is low or the sensor responses appear too similar. Check that the voltage sensor has a strong and stable signal. If you are using an A-Board connected directly to the meter the signal will look like a "messy" sine wave. If you are using a Y-Board with integration the signal should be a "clean" sine wave. The legend labels the sensors by type. Make sure the magnetic sensor channels are labeled "current" and the voltage sensor channel is labeled "voltage". Any channel not in the meters.yml configuration will be labeled "--unused--". Note that all channels are stored in the sensor data stream regardless of sensor type.

4. Calibrate the non-contact sensors

Run the `nilm-calibrate` program

Use `nilm-calibrate` to finish setting up the non-contact meter. Run this command from a terminal window (how to access the terminal). Calibration requires a NILM smart plug and a resistive load like an incandescent light bulb and a micro USB cable.

5. Start capturing data from the meter

Start `nilm-capture` service

Start (or re-start) the `nilm-capture` service using the terminal (how to access the terminal).

Check the system logs

Check the files in `/var/log/nilm` periodically for error messages. See NILM System Logs for details.

6. View meter data from the website
Refresh the web manager

Open the Installation Administration page and click the local repository button. On the Repository Management page, select the "Database" tab, and click twice. This will update the web interface with the new meter. You should see the new meter and its data streams appear in the navigation tree. See Managing the NILM Database for more details.

Plot meter data

Open the Data Explorer and select one or more streams from the new meter. Click Start Live Update to view the latest data and verify that the data is being captured and processed correctly. If the data is correct but noisy or shows significant "cross talk" between phases try adjusting the sensor position and recalibrating. If the data looks incorrectly calibrated try increasing the duration of the calibration and/or the power of the calibration load. You can re-calibrate the system at any time by running nilm-calibrate.
Quickstart Guide To
Smart Plugs

1. Hardware Setup

Configure Wireless Router

The plugs will work with most commercial routers. The plug documentation provides detailed instructions on configuring a TP-Link modem.

Connect Plug

Before using a plug it must be configured over USB. Power up the plug by placing it in an outlet and connect it to the NILM using a micro USB cable. The status LED will alternate between green and blue. Wait until the LED is solid green before continuing to step 2. See a closeup view of the USB connection here.

2. Configure the Plug

Plug Command Line Interface (CLI)

From a terminal window, open up the plug command line interface by running the command below (how to access the terminal). NOTE: If multiple plugs are connected to the same NILM over USB then you must specify the /dev/NODE name of the plug. See USB Plugs for details.

```bash
1 $ nilm-plug --cli
2 /dev/smart_plug, 115200 baud
3 ^C to exit
4 --------
5 Wattsworth WEMO(R) Plug v1.0
6 [help] for more information
7
8 >
```

Disabling Calibration Mode optional

If the plug is configured as a calibration load it will not operate as a smart plug until you explicitly stop the calibration. Run the commands shown below. (documentation for calibrate, config, restart)

```bash
1 > calibrate stop
2 > config set standalone false
3 > restart
```
This will restart the plug and you will have to enter the command line interface by running the `nilm-plug --cli` command again.

Configuring WiFi Parameters

The plugs will work on most standard WiFi networks. They will operate on 802.11a/b/g with WPA2, WEP or no encryption. WPA2 is recommended for the best security. Run the following commands replacing `network_name` and `network_password` with the appropriate values. Ignore the password setting if your network is not protected. (documentation for `config`)

```
$ config set wifi ssid network_name
$ config set wifi pwd network_password
```

This is all that's needed to get the plug on your network. To check the plug connectivity run the following commands to view debug output from the plug as it connects to the network: (documentation for `debug`, `wifi`)

```
$ debug 5
$ wifi on
```

You should see several AT commands and ultimately a success message with an IP address. This should match the address reservation on the wireless modem as configured in Step 1. Alternatively you can look at the plug log which should end with an entry similar to the following: (documentation for `log`)

```
$ log read
$ ... other entries ...
$ 3 [2016-03-04 20:26:55]: Joined [MIT] with IP [18.111.127.86]
```

3. Using the Plug

Control from a terminal window with `nilm-plug`

Once the plug is configured for the wireless network it can be disconnected from the NILM and placed in any outlet within range of the WiFi access point. After the plug has connected to the network you can interact with it from a terminal window using `nilm-plug`. This command lets you read the power meter data, and set the relay.

Control with Python scripts

An application programming interface (API) is available in Python. See Plug API for full details. Python scripts using the API can be executed directly from the command line or built into NILM Filters and Reports.
Quickstart Guide To
Adding Custom Data

1. Format Data and Add Timestamps

NiLM data is organized as rows of timestamped measurements. A measurement may be multiple columns. All values must be numeric. No string sequences are allowed. For example a three axis accelerometer could generate three columns of data corresponding to X, Y, and Z measurements, or a weather station might record barometric pressure, windspeed, wind angle, and temperature. The first column of each row must be a microsecond Unix timestamp. Each timestamp must be unique and the set must be monotonic and ascending. All values must be space separated. The example below shows sample timestamped data with five floating point values:

<table>
<thead>
<tr>
<th>Timestamp</th>
<th>Column 1</th>
<th>Column 2</th>
<th>Column 3</th>
<th>Column 4</th>
<th>Column 5</th>
</tr>
</thead>
<tbody>
<tr>
<td>1360262088608397</td>
<td>0.0543</td>
<td>0.3804</td>
<td>0.5181</td>
<td>0.0017</td>
<td>0.1648</td>
</tr>
<tr>
<td>1360262088625069</td>
<td>0.0864</td>
<td>0.5944</td>
<td>0.6732</td>
<td>0.2295</td>
<td>0.7166</td>
</tr>
<tr>
<td>1360262088641741</td>
<td>0.1411</td>
<td>0.6335</td>
<td>0.2040</td>
<td>0.2584</td>
<td>0.0136</td>
</tr>
<tr>
<td>1360262088658413</td>
<td>0.7833</td>
<td>0.1320</td>
<td>0.0495</td>
<td>0.1560</td>
<td>0.1157</td>
</tr>
<tr>
<td>1360262088675085</td>
<td>0.2791</td>
<td>0.7644</td>
<td>0.2437</td>
<td>0.2997</td>
<td>0.1657</td>
</tr>
<tr>
<td>1360262088691756</td>
<td>0.8472</td>
<td>0.3904</td>
<td>0.1049</td>
<td>0.8328</td>
<td>0.4186</td>
</tr>
</tbody>
</table>

2. Create a New Database Stream

Stream Naming Convention

Data is stored in uniquely named streams. The name has two components, group_name and file_name. These are separated by a forward slash similar to a Unix path name:

/group_name/file_name

Streams are indexed according to these names. Streams store a fixed number of columns of a particular datatype. See the NilmDB reference for a full list of valid data types. The naming convention is type_columns where columns is the number of values in a sample not including the timestamp. The data in Step 1 above could be stored in a stream with the following data format:

float32_5

Create Group Stream

If you want to have your dataset appear in the same group as other streams already on the system, use the same group name as these other streams. If you want your dataset in its own group you will need to create an additional group stream. Use the nilmtool create command replacing group_name with a unique lowercase alphabetic string as shown below:

1 $ nilmtool create /group_name/info uint8_1

Create Data Stream

Determine the datatype and the number of columns (not including the timestamp) for the stream. If you are unsure of the datatype use float32. Create the stream replacing group_name, file_name, and columns with the appropriate values.
1. $ nilmtool create /group_name/file_name float32_columns

3. Write Data to the Stream

Determine Start and End Timestamps

Data is stored as bounded intervals. In order to add raw data to a stream you must specify the interval of time that it covers. The minimum valid interval is first timestamp in the data to one microsecond past the last timestamp in the data. For example the data in Step 1 could be inserted with the following interval:

   start: 1360262088608397   end: 1360262088708429

Write the Data

Use the `nilmtool insert` command to write the data into the new stream as shown below replacing `data.txt` with the timestamped data created in Step 1 and the appropriate timestamps for start and end:

   1 $ nilm-insert /group_name/file_name -s start -e end < data.txt

4. Decimate Stream (optional)

In order to plot streams using NILM Explorer they must be decimated. This roughly doubles the disk space required by the stream so if you do not need to plot it, skipping this step will save space. Use the `nilm-decimate-auto` command as shown below:

   1 $ nilm-decimate-auto /group_name/file_name

5. Configure Stream Attributes

Open the Administration window and refresh the database twice. If you do not see the new stream make sure that the `group_name` matches an existing group or if you wanted to create a new group make sure you added the group stream in Step 2. Select the new file and update the stream attributes, in particular select the plottable checkbox if you want to use it in NILM Explorer. See Administration for more details.
Hardware Setup

Introduction

Non-Intrusive Load Monitors (NILM) collect data using one or more hardware meters. There are two different kinds of meters: contact and non-contact. The contact system uses commercial current and voltage sensors and should be installed by an electrician. The non-contact system uses electromagnetic field sensors to measure current and voltage without touching the powerline. The contact system is more accurate but expensive and difficult to install. The non-contact system can be installed quickly and easily but requires an additional calibration step. A single NILM can manage one or more of either type of meter.

Contact Meter

The contact meter uses LEM voltage and current sensors. The sensors are digitized by a UE9 LabJack. The LabJack has multiple input channels. The sensor to LabJack channel mapping (index) is shown in the figure below. The current sensors connect to the PCB with Molex plugs. Trace the twisted cable from the plug to the panel mounts and label the outside of the box before installing the system. This will make it easier to assign the correct channel mappings.

Connections

The sensors must be scaled correctly to convert the measurements to volts and amps. The voltage scale factor is set in hardware to 0.0919 and the current scale factor can be calculated using the formula in the figure below. alpha_LEM is the Conversion ratio found on the LEM sensor datasheet. This is usually on the order of 1000. See LA 55-P datasheet for an example. R is the load resistance set by the channel DIP switches (see the chart below).

Conversion Factors
Write down the LabJack index to sensor mapping and the scale factor required for each sensor. Once the meter is installed and connected to the host machine, enter these values into `meters.yml`. See Setting up a Contact Meter for details.

Non-Contact Meter

The non-contact meter uses magnetic and electric field sensors to indirectly measure the current and voltage in a powerline. This system is easier to install than a contact meter but requires an additional calibration step. There are two different non-contact sensor hardware platforms: The Flex Board and the D-A-Y Boards.

Flex Board

The Flex Board is an all-in-one platform with both sensors and a microcontroller for data acquisition. The main PCB has an electric field sensor, and a magnetic field sensor. There is also compensation circuitry to provide an integrated electric field output which is proportional to the line voltage. The magnetic sensor also contains a PTAT (proportional to absolute temperature) sensor. The flexible arms hold four more magnetic sensors. The microcontroller samples all eight sensor outputs and provides the values over USB. The sensor indices are provided in the figure below. Unless there is a need for a hardware integrated signal, the raw electric field output (index 0) with digital integration is the recommended configuration.
D-A-Y Boards

The other non-contact platform is a suite of three separate boards. The standard configuration is a data acquisition (D) Board and at least as many analog sensor (A) boards as phases (e.g., 3-phase system = 3 or more A Boards). Each A-Board has a current sensor and a "derivative of voltage" sensor. The figure below shows the channel to sensor mapping when A-Boards are connected directly to the D-Board. Only one of the four A-Boards is used by the NILM to determine the line voltage. Once you have configured the meter in meters.yml, use the nilm-scope utility to determine which A-Board has the strongest reading and use its index as the voltage: sensor_index in meters.yml.

<table>
<thead>
<tr>
<th>Index</th>
<th>Header</th>
<th>Type</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>0</td>
<td>Δ Voltage</td>
</tr>
<tr>
<td>1</td>
<td>0</td>
<td>Current</td>
</tr>
<tr>
<td>2</td>
<td>1</td>
<td>Δ Voltage</td>
</tr>
<tr>
<td>3</td>
<td>1</td>
<td>Current</td>
</tr>
<tr>
<td>4</td>
<td>2</td>
<td>Δ Voltage</td>
</tr>
<tr>
<td>5</td>
<td>2</td>
<td>Current</td>
</tr>
<tr>
<td>6</td>
<td>3</td>
<td>Δ Voltage</td>
</tr>
<tr>
<td>7</td>
<td>3</td>
<td>Current</td>
</tr>
</tbody>
</table>

D-Board index to sensor mapping. Each A-Board measures current and the derivative of voltage.

Securely connect each A-Board to the power cable using a zip tie as shown. The accuracy of the meter depends on the stability of this connection. If the A-Boards rotate after installation, the meter will need to be recalibrated. The quality of the output depends on how well the sensors are positioned. If the location of the conductors is visible, try to align each A-Board to a separate conductor. If the conductor geometry is not known, use the nilm-scope utility once you have set up the meter in meters.yml to determine optimal sensor placement. Loads on each phase should excite a different "mix" of the sensors.
Using the Y Board

The non-contact meter can adapt to a wide variety of installation types through the use of the Y Board adapter. The Y Board multiplexes two A Boards into a single pair of channels and provides optional hardware integration. The left-hand figure below shows a cartoon of the Y Board schematic. Zero ohm 0603 jumpers are used to select which of the six available inputs are placed on each output (S1 and S2).

*Note: only use one jumper per channel*

![Y Board schematic](image)

**Y Board configured for V1 and integrated V1 output**

**Y Board jumper pinout. Use 0603 zero ohm resistors**

Calibration

Non-contact meters must be calibrated before they can collect current and voltage measurements. You will need a resistive load, a smart plug and a micro-USB cable. The resistive load should be greater than 200W- incandescent light bulbs work well. Once you have chosen a load and the sensors are installed, configure the meter in the `meters.yml` file as described in Setting up a Non-Contact Meter. To calibrate the meter, open a terminal window and run `nilm-calibrate` with the name of the meter in `meters.yml` (e.g., `meterX`):

```
$ nilm-calibrate meterX
```

The script will first provide a summary of the meter configuration. If this looks correct, answer `y`. Any other key will cancel the calibration process. Plug the smart plug into an outlet and connect it to the computer with the USB cable. The status light will alternate between blue and green. Once it is solid green, answer `y` at the prompt for programming the plug. If you already have a plug in calibration mode you can answer `n` and reuse the plug for this calibration. If an error occurs programming the plug wait until the plug LED is solid green and try again.
Once the plug is programmed (or the step is skipped) you will be instructed to connect the load to the first phase. Connect the smart plug to any outlet and then connect the load. Once the load is turning on and off, hit [ENTER]. Do not hit [ENTER] until the smart plug is turning on and off.

If the meter is configured for multiphase operation you will be prompted to move the plug to an outlet on each additional phase. Do not worry about identifying which outlet is wired to which phase. The calibration program will automatically detect if you have connected the load to a previous phase and prompt you to move it.

Once the calibration program has run a sufficient number of measurements you will be asked if you want to save the results. Choose y to commit the calibration or n to discard. If you do not save the results the previous calibration values will be used (if available).

After calibration you may have to start the data capture manually, if you do the script will instruct you to run the following command:

```
1 $ sudo service nilm-capture start
```

The meter LED will turn blue when it is actively recording data.
Software Setup

Introduction

The NILM Software suite provides a complete set of tools to acquire, process, and manage high bandwidth NILM datasets. The following sections cover the software installation and configuration. Usage of particular components of the software suite are covered separately by topic from the main help page.

For advanced use see the NILM command line interface for a full listing of available NILM programs and commands.

Installation

The NILM software suite is divided into data acquisition tools and the web manager. The data acquisition tools can be installed on any Ubuntu distribution (verified up to 15). The web manager is only supported on Ubuntu 14.04.3 LTS (Trusty Tahr). The system requires upstart support which is a proprietary Ubuntu init protocol, therefore the system will not run on other Linux distros. The software is installed off a USB stick. To create the installation media, format a USB stick with a single ext4 partition and copy over the contents of the installer folder which can be found on the Desktop of any NILM system. See Storage Setup for details on partitioning and formatting a drive.

Install Full Software Suite

Install a fresh copy of Ubuntu 14.04.3 on the system with username nilm. Once the installation is complete restart the computer and insert the NILM USB stick. Open a terminal window and change to the NILM USB stick directory. Then run the install script as shown below:

```
1 $ cd /media/nilm/<name of usb stick>
2 $ bash install.sh
```

This will take a while to run. When it is complete you should see the following:

```
-------Install Complete--------
***RESTART YOUR MACHINE***
Configure meters in meters.yml on the Desktop
Go to http://nilm.standalone to manage this system
```

If this does not appear, an error occurred. Check the log output for details and correct the error then run the script again.

Configuration

The NILM is completely configured by the meters.yml located on the Desktop. This file lists the configurations for each connected power meter. Both contact and non-contact meters can be set up in this file. A single NILM can run multiple meters of either type. Meters are listed sequentially as meter1 to
meterN. Any changes to this file will only on a reboot or manually restarting the nilm-capture service.

Some settings may not be changed after a meter is initialized (eg the number of phases), others may be changed at any time (eg the amount of data to keep on disk). The next two sections explain how to configure both types of power meters.

Setting up a contact meter

The contact meter should be installed before it is configured. Make careful note of the current sensor connections and their relative orientations. Run the command below to check the communication link between the computer and the meter.

```
1 $ ping <LabJack IP Address> -c 4
```

This should return with a line similar to

```
--- 192.168.1.209 ping statistics ---
4 packets transmitted, 4 received, 0% packet loss, time 2998ms
rtt min/avg/max/mdev = 0.026/0.031/0.035/0.006 ms
```

Open meters.yml in a text editor and copy over the example configuration below. If there is already a meter1, give this meter a unique index (eg meter2). If you reuse a meter name, for example change meter1 from a contact meter to a non-contact meter, or change the meter from 2 phase to 3 phase operation, you must either rename or completely flush the previous meter's data streams from the Nilm database. See command line tools for details on moving and renaming streams in NilmDB.

Example Configuration

Note that all fields are required. Details about each field are itemized below the example. Standard defaults are provided but sensor_scales must be set for your specific installation (see contact meter hardware). The nilm-scope utility is useful for ensuring the channel mappings and sinefit rotations are correct.
meter1:
  
  type: contact
  enabled: true  # set to false to disable this meter
  ip_address: 192.168.1.209  # default LabJack address
  phases: 3  # 1 - 3

  sensors:
    voltage:
      sensor_indices: [3, 4, 5]  # maps to phase A, B, C
      sensor_scales: 0.0919  # built-in constant
      sinefit_phase: A  # [A, B, C] voltage used by sinefit
      nominal_rms_voltage: 120  # used to scale prep to watts

  current:
    sensor_indices: [0, 1, 2]  # maps to phase A, B, C
    sensor_scales: XX  # set by resistors and LEM, see har:
    sinefit_rotations: [0, 120, 240]  # relative to sinefit_phase voltage

  streams:
    sinefit:
      decimate: true  # if [false] only the base stream w:
      keep: 1m  # how much data to keep as [amount]!
      iv:
        decimate: true  # h: hours, d: days, w: weeks
        keep: 1w  # m: months, y: years
        if [false] no data will be saved
      prep:
        decimate: true
        keep: 3w

Contact Meter Fields:

  type  This should be set to contact
  enabled  true/false if false, no data is captured from this meter
  ip_address  The IP address of the LabJack. This defaults to 192.168.1.209 but can be set to
              another value using the LabJack software (Window’s only). When more than one
              Contact NILM is used or if the 192.168.1.0 subnet is unavailable you must change
              this default value. Note that each LabJack must be on it’s own subnet. See Network
              Configuration for more details.
  phases  A value between 1 and 3. This depends on the power system being monitored.

Sensor Configuration
Voltage

  sensor_indices  These are the voltage sensor LabJack channels. The sensors are connected to
                  channels 3 4 and 5. The order of this list is used to name Phases A, B, and C. When
you are installing the system note the phase connection and order this list accordingly. See the figure in Contact Meter Connections for the voltage sensor connections.

**sensor_scales**
The scaling coefficient to convert sensor output to Volts. This is hardwired to 0.0919. Separate scaling factors may be applied to each sensor by using an array instead of a single value: \([X_A, X_B, X_C]\) where X is the scale factor for each phase.

**sinefit_phase**
\(A, B, C\) The phase used by the sinefit processor.

**nominal_rms_**
This is used to scale prep to approximate power (Watts)

**Current**

**sensor_indices**
These are the current sensor LabJack channels. The sensors are connected to channels 0, 1, and 2. The order of this list should match the order used in the voltage configuration. See the figure in NEMO Channel Connections for the current sensor connections.

**sensor_scales**
The scaling coefficient to convert sensor output to Amps. See the figure in NEMO Configuration for details on calculating this value. Separate scaling factors may be applied to each sensor by using an array instead of a single value: \([X_A, X_B, X_C]\) where X is the scale factor for each phase.

**sinefit_rotation**
The phase difference in degrees from the sinefit_phase voltage for each phase (note that the coefficient for the phase used by sinefit should be a 0 in this array)

**Stream Configuration**

The **streams** configuration block determine how much data is retained for each stream and whether or not the stream is decimated as it is collected. Once the NILM has been running for a few hours the nilm-cleanup command line tool can be used to estimate how much space the database will take up given the amount of data the streams are configured to store. It is very important to make sure the total size required by the database will fit on your storage drive.

**decimate**
**true/false** Whether or not the stream should be decimated. This makes the stream plottable in the web interface but roughly doubles the amount of space required to store this data. There is also some network overhead associated with decimation so if you are experiencing high processor load try disabling this for some streams.

**keep**
How much data to keep for this stream. The is specified as a coefficient and unit. Valid units are h for hours, w for weeks, m for months, and y for years. Set to false to discard the stream data.

Setting up a non-contact meter

There are many different configurations for the non-contact sensors. See Non-Contact Sensors on the Hardware help page for detailed information on connecting and configuring the sensor hardware. The nilm-scene utility can be helpful in finding optimal installation sites for the non-contact sensors.

Open **meters.yml** in a text editor and copy over the example configuration below. If there is already a meter1, give this meter a unique index (eg meter2). If you reuse a meter name, for example change meter1 from a contact meter to a non-contact meter, or change the meter from two phase to three phase...
operation, you must either rename or completely flush the previous meter's data streams from the Niilm
database. See command line tools for details on removing and renaming streams in NiilmDB.

```
meter1:
  type: noncontact
  enabled: true
  serial_number: meterXXXX
  phases: 2
  sensors:
    voltage:
      sensor_index: 0
      digitally_integrate: true
      nominal_rms_voltage: 120
    current:
      sensor_indices: [1,3,5,7]
      #sensor_indices: [1,2,3,4,5]
    calibration:
      duration: 30
      watts: 200
      has_neutral: true
    streams:
      sinefit:
        decimate: true
        keep: 1m
        iv:
        decimate: true
        keep: 1w
      iv:
      decimate: true
      keep: 1w
    iv:
    decimate: true
    keep: 3w
    sensor:
      keep: false
```

Non-Contact Meter Fields:
- **type**: This should be set to `noncontact`
- **enabled**: `true`/false if false, no data is captured from this meter
- **serial_number**: This is printed on the DBoard meter case. See DBoard Setup for more information.
- **phases**: A value between 1 and 3. This depends on the power system being monitored.
**Sensor Configuration**

### Voltage

<table>
<thead>
<tr>
<th><strong>sensor_index</strong></th>
<th>This is the index of the electric field sensor to used to calculate the effective voltage waveform. Use nilm-scope to determine which electric field sensor has the strongest signal and use its index here.</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>digitally_integrated</strong></td>
<td>true/false If the sensor specified in sensor_index does not have hardware integration, set this to true. See non-contact sensors for information on hardware versus software integration</td>
</tr>
<tr>
<td><strong>nominal_rms_voltage</strong></td>
<td>The rated line voltage. This is used to scale the voltage output</td>
</tr>
</tbody>
</table>

### Current

| **sensor_indices** | These are the magnetic sensor indices. Place all available sensors in this array. There must be at least as many sensors as phases. The order does not matter. |

### Calibration

| **duration** | Time in seconds to run the calibration load on each phase. Longer durations can improve calibration results especially in environments with many background loads. Do not use less than 30 seconds on a production system. |
| **watts** | The power draw of the calibration load. This is used to scale the prep output |
| **has_neutral** | true/false If the system has a neutral bus (most common), set this to true. |

---

**Stream Configuration**

The stream configuration block determine how much data is retained for each stream and whether or not the stream is decimated as it is collected. The sensor stream is the raw output from the DBoard and is always eight channels whether or not all eight sensor inputs are used. Once the NILM has been running for a few hours the nilm-cleanup command line tool can be used to estimate how much space the database will take up given the amount of data the streams are configured to store. It is very important to make sure the total size required by the database will fit on your storage drive.

| **decimate** | true/false Whether or not the stream should be decimated. This makes the stream plottable in the web interface but roughly doubles the amount of space required to store this data. There is also some network overhead associated with decimation so if you are experiencing high processor load try disabling this for some streams. |
| **keep** | How much data to keep for this stream. The is specified as a coefficient and unit. Valid units are h for hours, w for weeks, m for months, and y for years. Set to false to discard the stream data. |

---

**Storage Setup**

This section explains how to properly format and configure an extra hard drive for a NILM system. It is usually a good idea to place the Nilm Database on a separate hard drive. This prevents the database from filling the primary drive to the point where the system become unusable and also makes it easy to retrieve collected data from an installation by simply swapping out the extra harddrive.
**Formatting a drive** After installing the drive and booting the system, the first step to use the drive is to place a usable filesystem on it. There are many tools that can be used for this but one of the easiest is GParted. This program must be run as root. From the command line type the following:

⚠️ Be very careful with gparted, formatting the primary drive will destroy the installation

```bash
sudo gparted
```

Select the extra drive from the dropdown menu as shown. Generally the extra drive should be `/dev/sdb` but this is not always the case. If the drive already has multiple partitions this most likely means it is the primary drive.

Carefully select the device node for the extra drive.

Create a new msdos partition table. This will erase the drive.

Select **Device > Create Partition Table** to bring up the Create Partition dialog. Select **msdos** and click **Apply**. Select **Partition > New** to bring up the New Partition dialog. Add a new **ext4** partition to the drive and assign it the full extents of the disk (this is the default). Click **Add** to close the dialog. Finally click **Apply** to format the disk and then close the program.

Add an **ext4** partition to fill the disk.

To use the drive for the Niim database it must be mounted to the correct location in the filesystem. Edit `/etc/fstab` in a word processor and add the following line where `/dev/sdX1` is the name of the drive you just formatted. The number one refers to the first (and only) partition. Note that you will need to run the
Run the following commands to mount the drive and setup the permissions. Use `df` to verify the configuration:

1. `sudo service nilm-capture stop` #stop data capture if it is already run;
2. `sudo mount -a`
3. `sudo chown -R nilm:nilm /opt/data` #assign the drive to the nilm user
4. `df -h`

The output from `df` should look similar to that below:

<table>
<thead>
<tr>
<th>Filesystem</th>
<th>Size</th>
<th>Used</th>
<th>Avail</th>
<th>Use%</th>
<th>Mounted on</th>
</tr>
</thead>
<tbody>
<tr>
<td>/dev/sdal</td>
<td>1.8T</td>
<td>5.3G</td>
<td>1.7T</td>
<td>1%</td>
<td>/</td>
</tr>
<tr>
<td>other mount points</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>/dev/sdcl</td>
<td>917G</td>
<td>72M</td>
<td>871G</td>
<td>1%</td>
<td>/opt/data</td>
</tr>
</tbody>
</table>

If you have already configured your meters and want to start collecting data, run:

```
1 $ sudo service nilm-capture start
```

Network Setup

The LabJacks in contact meters require an ethernet connection. If you need more ethernet ports than the computer has available, use a USB to ethernet adapter. While most adapters should work out of the box, the recommended adapter is the **TU2-ET100** from TRENDnet. After you connect the contact meter to the computer note the MAC address of the USB adapter. This is found on the backside of the TU2-ET100 as shown in the figure below. Open the network connection editor and configure the interface for the MAC address used by the NILM. Each interface has a unique MAC address and it is helpful to rename the connection to "NILM" or "Web" depending on the role of the interface. For interfaces connecting to the web, set the IPv4 address method to **DHCP** from the **IPv4 Settings** tab.
Find the MAC address for the LabJack connection. On the TU2-ET100 this is on the bottom sticker.

Configure the network interface for the MAC address associated with the LabJack.

For interfaces connected to a contact meter select the IPv4 Settings tab and set Method to manual. Click Add and enter an IP address on the same subnet as the LabJack. Unless you have set up an advanced configuration the IP address should share the first three numbers as the LabJack and use a different final number. For example, the default LabJack address is 192.168.1.209 and a valid host IP address would be 192.168.1.200. The Netmask should be 24 or 255.255.255.0 and the Gateway should be left blank. Note that each interface must be on a separate subnet. If you need more than one contact meter you will have to assign a different IP address to the additional LabJack devices. This is done with the commercial configuration tool available through the LabJack website.

Assign an address in the same subnet as the LabJack

Select the local routing check box in the Routes dialog
For multiple LabJack installations address them as 192.168.X.209 where X is different for each device (between 1 - 255). After you assign the IP address click and select the checkbox for local routing only as shown in the figure. This prevents web bound traffic from getting sent to the LabJack. Once you have completed the IP address configuration click to close the network configuration dialog. Open a terminal and enter the following command to reconfigure the network interfaces to use the new values:

1 $ sudo service network-manager restart

Cluster Setup

The NILM system can be managed by a Wattsworth Cluster. If the system is connected to a cluster, it cannot be managed locally. Using the local NILM Manager site (nilm.standalone) while connected to a cluster will corrupt the NILM filters and analyzers. There are two different types of clusters: VPN and Peer-to-Peer. The VPN cluster is managed by a central server which provides secure remote access to any NILM with an Internet connection. The Peer-to-Peer cluster allows one NILM to manage another NILM. This configuration can be used to manage a “headless” NILM from another NILM that has the Manager framework installed.

1) Stop Local Manager: Before joining a cluster, make sure that the local NILM Manager cron tasks are disabled. Do this by commenting out the NILM Manager lines. See the comments in the crontab for more details. To edit the crontab open a terminal and run the following command:

1 $ crontab -e

2) Select a Cluster Type: Decide which type of cluster you want to join. The VPN cluster requires an Internet connection and the Peer-to-Peer cluster only requires a network connection between the two NILMs.

2a) Join a VPN Cluster: Open a terminal and enter the following commands below. This will require you to enter the cluster administrator’s password so have it ready before you begin.

1 $ cd ~/Desktop/cluster #switch to the cluster folder on the Desktop
2 $ sudo ./join-cluster.sh cluster_name

The cluster_name is the fully qualified domain name (FQDN) of the cluster server. Omit this argument to see a list of available clusters. Wait for about a minute and run the command:

1 $ ifconfig
This will display all the current network interfaces. Look for an interface that begins with tun usually this will be tun0. Find the IP address for this interface, it will look like 10.x.x.x. Write this down, you will need it for the next step. If this command has no output this means the NILM was not able to join the cluster VPN. To debug VPN problems, run the command below and fix any errors that are displayed:

1 #FOR DEBUGGING ONLY#
2 #run this if there is no tun interface and fix any errors that occur#
3 $ sudo openvpn /etc/openvpn/client.conf

2b.) Join a peer-to-peer Cluster: You must establish a network connection between the two NILMs. Connect the systems with an ethernet cable and assign both NILM's static IP addresses on the same subnet. Record the IP address of the managed NILM for the next step.

3.) Add the NILM: Log in to the Cluster NILM Manager site as an administrator and open up the admin panel. Click Add Repository to bring up the New Repository dialog. Fill in the name, description and location fields. Uncheck the “default URL” box to display the custom URL text boxes. The NilmDB URL should be X.X.X.X/nilmdb and the Niim Manager URL should be X.X.X.X/nilmun where x.x.x.x is the IP address (which is found using the steps above).

4.) Leave the Cluster: If you want to remove the NILM from the cluster delete it from the Server tab in the Global Administration panel. See Global Administration for details.

4a.) Leave a N cluster

1 $ cd ~/Desktop/cluster #switch to the cluster folder on the Desktop
2 $ sudo ./leave-cluster.sh <vpn-name>

Then re-enable the local NILM Manager cron tasks by uncommenting the lines commented out in Step 1

Secondary Setup
The NILM supports a secondary drive that can be used to copy datasets from the primary database or preview data collected from another NILM system. Any storage device can be used as a secondary drive including internal SATA drives, USB flash drives, and eSATA drives. The drive must be an ext4 volume. See Storage for details on using GParted to format a drive. Ubuntu often automounts removable media, if it does click the eject button on the Desktop to unmount the volume. Compare the output of the following command before and after you connect the drive to determine the assigned device name:

```bash
1 $ ls /dev/sd*
```

When the drive is connected the output should include an extra /dev/sd<letter>1 where <letter> is b,c,d etc. This is the device name. Now mount the volume to the secondary disk location:

```bash
1 $ sudo mount /dev/sdXX /opt/secondary
2 $ sudo chown -R nilm:nilm /opt/secondary #update drive permissions
```

Restart the apache web server to initialize the secondary system:

```bash
1 $ sudo apache2ctl restart
```

Once Apache restarts you will be able to access the backup server at http:\/\slash\slashnilm.secondary\slashnilmdb. To view the data using the NILM Manager website refresh the secondary database from the administration interface. See NILM Administration: Database Tab for details. Also, any nilmtool commands can be used on the secondary server. The most useful commands are the following:

```bash
1 $ nilm-copy-wildcard -u localhost/nilmdb -U nilm.secondary/nilmdb /meterX
2 $ nilm-copy-rename -u localhost/nilmdb -U nilm.secondary/nilmdb /meterX/
```

The first will copy all streams associated with meterX to the secondary volume using the same name. The second command renames the streams which can be helpful when using a single drive to backup multiple NILM’s each with a meterX group. Run either command with the -h flag to see a full list of options. When you are done copying streams, run the following commands to stop the secondary server and unmount the drive:

```bash
1 $ sudo umount /opt/secondary
2 $ sudo apache2ctl restart
```
Smart Plugs

Introduction

The NILM smart plug is a WiFi-enabled plug with a software controlled relay and solid state power meter. These plugs can be controlled over a wireless network or by USB. There are three main tools to interact with these plugs. The easiest tool is the command line nilm-plug utility which can control most plug features over USB or WiFi. For more advanced operation the plug has a terminal mode that is accessed using nilm-plug --cli. See Plug CLI for more details. Finally there is a set of python modules for scripting and integration with NILM filters. See Plug API for more details. In order to use the plugs on a network a wireless access point should be set up with MAC address reservations and static IP bindings for each plug. See the next section for details on configuring a wireless access point.

Wi-Fi Setup

Any standard wireless access point can be used to interact with NILM smart plugs. This documentation covers the TP-Link TL-WR841N. A similar sequence of steps should work on most devices. When setup for the first time the router will advertise a default SSID. The network name and password can be found on the back of the router as shown the figure below. Open a browser and navigate to http://tplinkwifi.net. Authenticate with username [admin] and password [admin].
Change the wireless network name (SSID). Do not use spaces in the name. If you are configuring multiple access points that will be in close proximity make sure each has a unique name. Make sure the mode supports 802.11a, b and g. This is the default. The broadcast SSID checkbox may be disabled if you do not want to advertise the presence of the network. This helps prevent people casually trying to connect to the network. Note that this does not improve the security of the network. If you change the name of the network you will have to reconnect to the new SSID once the router restarts.

While not strictly necessary it is strongly recommended to enable wireless security. The plugs work best with WPA2 Personal. The authentication should be set to PSK (pre-shared key) and AES encryption. Select a strong password and save the settings. You will have to reconnect to the network using the new password.
Recommended security settings for the wireless access point.

The NILM smart plugs are controlled using their IP addresses. Wireless networks by default assign random addresses to each client. The router must be configured to assign a consistent fixed address to each plug. Each plug as a unique MAC address which must be entered into the router to reserve an address. The first step is to make sure DHCP services are enabled on the router and set to a range of addresses that do not overlap with any other networks on the machine including contact meters. The default address space should work well for most configurations. The router will use a pool of the addresses in this space to assign to clients as they connect. This range is specified in the boxes highlighted below. You will need to assign IP addresses to the plugs that are outside of this range. Here the DHCP server will use addresses above * .100 leaving * .2-* .99 available for reservations. Note that * .0 and * .1 are reserved and should not be used for plugs.

Configuring DHCP services on the wireless access point.

Create and address reservation for each plug and record the mapping so that you will know which plug is attached to which address. Note that the format for the MAC address field is XX-XX-XX-XX-XX-XX. The first three octets are the organization identifier (OUI) and are the same for all the plugs. The last three are unique for each plug. The MAC address is labeled on the case of each plug.
Create address reservations for each plug. The address should not be in the DHCP dynamic address range.

Connect the host NILM either with WiFi or to one of the local (yellow) ethernet ports on the back of the router. If it is connected to the WAN port (blue) the NILM will not be able to communicate with the plugs.

Once the NILM and plugs are configured you should see a status similar to the figure below. All of the plugs (recognizable by their OUI) should have reserved addresses and the computer should have a leased address.

The DHCP Client List shows the current address assignments. Plugs should have a reserved address (Permanent).

```
nilm-plug

The easiest way to interact with the NILM smart plug is with the nilm-plug command line utility. It can be used with USB or WiFi connected plugs. The program takes two arguments, an action and a device_address. If a single plug is connected over USB the address can be omitted because the system can find the plug automatically. When multiple plugs are connected by USB or plugs are connected over WiFi the address must be specified. For plugs connected by USB the address is /dev/ttyACM#, where # is a number dynamically assigned to the plug by the operating system. Run ls /dev/ttyACM* before and after connecting the plug. The new entry is the plug's device_address. The device_address for wirelessly connected plugs is their IP address.
```

Read plug data
nilm-plug --read [--file filename] [plug_address]

This command retrieves meter data from the plug and stores the result in a comma separated text (CSV) file. If no file is specified the output is written to the file plug.data in the current directory. If the file exists, data is appended to the end. Each row of data has eight values specified below:

<table>
<thead>
<tr>
<th>ts</th>
<th>vrms</th>
<th>irms</th>
<th>watts</th>
<th>pavg</th>
<th>pf</th>
<th>freq</th>
<th>kwh</th>
</tr>
</thead>
<tbody>
<tr>
<td>ts Timestamp in milliseconds since 1970 (UNIX time)</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
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<tr>
<td>vrms RMS voltage (V)</td>
<td></td>
<td></td>
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<td></td>
<td></td>
</tr>
<tr>
<td>irms RMS current (A)</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>watts Current power usage (W)</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>pavg 30 second average of power usage (W)</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>pf Power Factor</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>freq Line Frequency (Hz)</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>kwh Energy used since last plugged in (kWh)</td>
<td></td>
<td></td>
<td></td>
<td></td>
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<td></td>
</tr>
</tbody>
</table>

The plug collects data in one minute packets. The timestamp for each packet is displayed as it is retrieved from the plug. For plugs connected wirelessly only the most recent data packet is available. If a wireless plug is queried before a new packet is ready it will return an empty packet and the output file will remain unchanged. If a plug is connected by USB, the read command returns all of the data packets stored on the SD Card. If the output file already exists, only new data is appended to the end of the file. This command is designed to be run iteratively with each plug using a separate output file.

If a plug is read wirelessly it still stores data to the SD Card which can be retrieved later over USB. This allows you to query the plug over an intermittent WiFi connection and fill in any missing data packets once the plug is connected by USB.

Erase plug data (USB only)

nilm-plug --erase [plug_address]

This command erases all data from the plug's SD Card. Data can only be erased when a plug is connected by USB.

Read and erase plug data (USB only)

nilm-plug --read_erase [--file filename] [plug_address]

This command is identical to running read and then erase. This is the recommended command to use with USB plugs to prevent the SD card from filling up with data that has already been retrieved.

Control plug relay

nilm-plug --relay on|off [plug_address]

This command turns the plug on or off. If the requested relay state matches the current relay state this command is ignored. This works for both USB and WiFi plugs.

Display help and examples

nilm-plug --help
This command displays usage examples and a copy of this documentation.

**Plug API**

The Plug Application Programming Interface (API) allows you to control NILM smart plugs from Python scripts. Before you can use the API in a script you must import the nilmplug module:

```python
from nilmplug import plug
```

This module contains a single object `Plug`. The constructor takes two arguments, the `device_address` and a flag to indicate whether this address is a USB device. The code below shows examples of both plug types:

```python
# manage the plug over a USB cable
myplug = plug.Plug("/dev/NODE", usb=True)

# OR manage the plug over wifi
myplug = plug.Plug("192.168.1.XX")
```

The API provides methods to read meter data, control the relay and set the LED color over USB or WiFi.

**Read plug data**

```python
myplug.get_data(last_ts=0)
```

This method returns a numpy array of data. The columns are described [here](#). If the plug has no new data this will return an empty array. The optional argument `last_ts` limits the returned data to samples after this timestamp. This can be helpful when you don't want to erase the data after reading it. Setting this value to the last timestamp received from the previous read will return only new data. Omitting this parameter will return all data on the SD card.

**Control plug relay**

```python
myplug.set_relay(value)
```

This method controls the plug relay. The parameter `value` must be either "on" or "off". This method returns 0 on success or -1 on error. Errors can be caused by a poor WiFi connection.

**Control plug LED**

The method controls the multicolor LED. By default the LED is green when the plug is on and running normally, blue when it is actively connected over USB, and red if an error has occurred.
The red, green, and blue parameters are 8 bit values (0–255). Many online references provide common RGB color combinations. The blink value sets the blink rate in milliseconds. Set to 0 to disable blinking (solid).

Erase plug data (USB only)

```
1  my_plug.erase_data()
```

This method removes all data from the plug’s SD card. This method can only be used with USB connected plugs.

Plug CLI

NILM smart plugs provide a complete command line interface accessible with a standard terminal emulator. The nilm-plug program provides a built-in terminal interface that is started by using the --cli flag:

```
$ nilm-plug --cli
/dev/smartplug, 115200 baud
^C to exit
--------------------
Wattsworth WEMO(R) Plug v1.0
[help] for more information
$>
```

The following sections explain the commands available through this interface. You can also use the help in the CLI to see a brief summary of command options.

```
calibrate - start or stop calibration mode
```

Usage

```
calibrate stop|start on_time off_time
```

Description

Run the plug in calibration mode. This disables data collection and toggles the relay with a duty cycle of on_time and off_time milliseconds. This is used to calibrate non-contact power meters. Use the stop flag followed by the restart command to return the plug to normal operation. This is a persistent setting which means that a plug will remain in calibration mode until set otherwise.

Arguments
action stop|start
on_time duration the plug is on in milliseconds
off_time duration the plug is off in milliseconds

**config - get or set a configuration parameter**

**Usage**

```
config action parameter [value]
```

**Description**

Retrieve or set the plug configuration parameters. Parameters are persistent and stored on the SD card.

If a blank SD card is inserted into a plug the default parameters are empty strings unless otherwise specified. The last three parameters are used to support DHCP environments where neither the plug or the NILM IP addresses are fixed. If you are using IP address reservations as recommended in WiFi Setup, these parameters should be left blank.

**Arguments**

- **action**: get|set
- **parameter**: configuration parameter, see list below
- **value**: new value of parameter, leave blank to clear parameter setting

**Parameters**

- `wifi_ssid`: wireless network name
- `wifi_pwd`: wireless network password. Leave blank for open network. *(write only)*
- `standalone`: [true|false] If true, do not attempt to connect to a wireless network. Default is true
- `serial_number`: unique string to identify the plug
- `nilm_id`: the NILM associated with this plug *(optional)*
- `nilm_ip`: the IP address of the associated NILM *(optional)*
- `mgr_url`: management website URL *(optional)*

**Example**

```
1 > config set wifi_ssid nilmplug
2 Set [wifi_ssid] to [nilmplug]
3 > config get serial_number
4 plugAD49
```

**data - read or clear the data**

**Usage**

```
data action
```

**Description**

Use this command to retrieve data packets stored on the SD card. The data is returned in the binary format described below and should only be used in scripts, not for printing to the terminal. If you want
to view data from the command line, use the `meter` command. Use the `erase` flag to erase the data file.

**Arguments**

`action` [read|erase]

**Structure**

Data is returned in packet chunks with the binary format shown below. End of file (EOF) is signaled by a packet containing the character `x` in every byte. See the plug.py source code for an example of how to parse this data structure in python.

```c
//binary structure returned by [data read] command
#define PKT_SIZE 30
#define PKT_TIMESTAMP_BUFSIZE 20
typedef struct power_pkt_struct {
    int32_t vrms[PKT_SIZE];  //RMS voltage
    int32_t irms[PKT_SIZE];  //RMS current
    int32_t watts[PKT_SIZE];  //watts
    int32_t pavg[PKT_SIZE];  //Average power (30s window)
    int32_t freq[PKT_SIZE];  //Line frequency
    int32_t pf[PKT_SIZE];  //Power factor
    int32_t kwh[PKT_SIZE];  //kWh since turn on
    char timestamp[PKT_TIMESTAMP_BUFSIZE];  //YYYY-MM-DD HH:MM:ss
    uint8_t status;  //struct valid flag
} power_pkt;

//end of file signal returned by [data read] command
char* EOF = (char*)malloc(sizeof(power_pkt));
memset(&EOF, 'x', sizeof(power_pkt));
```

**Usage**

`rtc` get|set year month date dw hour min sec

**Description**

Get or set the value of the real time clock. The battery backed `rtc` is used to timestamp data collected by the plug. Query the current time using get, or set the time and specify the full date, see the arguments below:

**Arguments**
get

return the current time formatted as a string. If the battery fails this will report a corrupt date.

set

set the clock value, all of the following parameters must be set to valid values for this command to execute successfully.

year

year as a two digit number 2016 = 16

month

two digit value 0-12

date

two digit value 0-31

dw

day of week 0-7

hour

two digit value 0-24

min

minute as a two digit value 0-59

sec

second as a two digit number 0-59

Example

1 > rtc set 16 02 01 01 03 16 51
2 Set time to: 2016-02-01 03:16:51
3 > rtc get
4 Time: 2016-02-01 03:16:51

log - read or clear the log

Usage

log action

Description

The SD card records a persistent log of plug events. This includes network connectivity, general errors, and system restarts. A [general reset] occurs when the plug is connected to power and a [software reset] is indicates the restart command was used. Use the clear flag to erase the log file.

Arguments

action [read|erase]

Example

1 > log read
2 ...
3 [2016-01-29 14:59:06]: general reset
4 [2016-01-31 03:41:41]: no requests from NILM, resetting WiFi
5 [2016-01-31 03:42:00]: Joined [nilmplug] with IP [192.168.0.11]
6 [2016-01-31 03:44:25]: software reset

relay - control the plug relay

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Usage

relay action

Description
Control the plug relay to turn the connected appliance on or off. Executing this command with the existing relay state has no effect.

Arguments
action on|off

Advanced Commands
The following commands are specialized diagnostic tools that are less commonly used. They are listed alphabetically

**collect_data** - start or stop power logging

Usage

collect_data action

Description
Start or stop data collection from the power meter. By default the plug collects data from the power meter. This command can be useful for debugging communication with the solid state meter hardware.

Arguments
action [true|false]

**debug** - set debug level

Usage

level

Description
Controls the verbosity of console information. Set to 5 to see AT command traffic to the ESP8266. This is useful for diagnosing network connectivity issues.

Arguments
level [0-5] Default is 0 (lowest). Level >=3 show wireless TX messages. Level >=4 echo ESP8266 AT traffic

Example
The wireless interface is controlled by a separate ESP8266 module which communicates with the main processor through a UART with AT commands. The following shows the output of a successful wireless bootup. Note that the output of this debug session also displays the plug MAC address
(CIFSR: STAMAC). This should be labeled on the plug case but if it is not present use the combination of these two commands to find it.

```
1 > debug 4
2 debug level: 4
3 > wifi on
4 AT+RST
5 OK
6 ok
7 c\xfec\xcfRs\rfgj\xd7\xe2\jd3j\xeaj\xf3\x82k\xfaf\xd2fW\xf2@
8 Ai-Thinker Technology Co. Ltd.
9
10 ready
11 AT+CWMODE=1
12 OK
13 ok
14 AT+CWJAP="nilmplug","topsecret"
15 OK
16 AT+CIFSR
17 +CIFSR:STAIP,"192.168.0.11"
20 OK
21 AT+CIPMUX=1
22 OK
23 AT+CIPSERVER=1,1336
24 OK
25 Joined [nilmplug] with IP [192.168.0.11]
26 wifi on
27 >
```

**Usage**

```
echo - turn echo on or off
```

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Description
Turn the prompt echo on or off. This can be useful when interacting with the plug via scripts. This value is not persistent and defaults to on.

Arguments
action on|off

**led - set the led**

Usage
led red green blue blink

Description
Set the LED color and control the blink rate. This overrides the default color but any change to the system (eg, error or USB connect event) will change the LED back the system setting. This is not a persistent setting, it resets to the system default on powerloss.

Arguments
red [0-255]
green [0-255]
blue [0-255]
blink blink rate in milliseconds, set to 0 for no blink. Maximum value is 65536.

**ls - view files on SD Card**

Usage
ls no arguments>

Description
View SD card file statistics, similar to the standard linux ls command. There should be three files.

The timestamp is the last modified date as recorded by the plug RTC. The files are:

log.txt system log
config.txt persistent configuration settings
power.dat data collected by the plug power meter in binary format

Example

```plaintext
1 > ls
2 FILE SIZE DATE
3 log.txt 29445 16/01/31 03:44
4 config.txt 197 16/01/28 19:41
5 power.dat 825984 16/01/31 03:43
```
memory - show memory statistics

Usage

memory no arguments>

Description

The plug firmware dynamically allocates memory using a set of reserved blocks similar to a heap.
This command is useful for debugging memory allocation. A steadily increasing allocation
percentage indicates a memory leak in the code.

Example

1 > memory
2 Allocated 200 of 11200 bytes (1%)
3 Largest free block: 1000 bytes
4 Smallest free block: 200 bytes

meter - view plug meter

Usage

meter no arguments>

Description

Displays the last full data packet collected by the meter. If the meter is not collecting data an error
message is displayed instead. This is a convenience function for debugging see data command for
retrieving meter data.

Example

1 > meter
2 **this data may be up to a minute behind**
3
4 voltage    119.25
5 current    0.51
6 watts      59.62
7 avg pwr    55.30
8 freq       59.59
9 pf         0.95
10 kwh       0.81

restart - software reset

Usage
**restart bootloader**

**Description**
This command issues a soft reset to the processor. The optional bootloader flag restarts the processor in SAM-BA bootloader mode. This should only be used when the plug needs to be reflashed over USB.

**Arguments**
- bootloader: boot into SAM-BA firmware this should only be used for reflashing the plug

---

**version**

**Usage**
```
version no arguments>
```

**Description**
Print the firmware version and compilation date. The firmware version is set by the VERSION_STR define in inc/monitor.h.

**Example**
```
1 > version
2   Firmware [v1.1]
3   Date: [Jan 5 2016 17:08:53]
```

---

**wifi**

**Usage**
```
wifi action
```

**Description**
Turn the wifi system (ESP8266) on or off. The wifi system is turned on a system boot if wifi_ssid!="" and standalone=false. Issuing this command with the on will reset the wifi module and attempt to connect to the specified network. Use in conjunction with the debug command to diagnose network connectivity issues.

**Arguments**
- action: on|off
Administration

Introduction

There are two interfaces for administration. The system administration interface and the global administration interface. The system interface is used to configure and manage NILM systems. The global interface is used to manage the manager site itself (this website).

The system administration interface is accessible from the dashboard (or click here to open it in a new tab). From the main administration page find the installation you are interested in and click the Manage button. If you are on a standalone system there will only be one installation listed. If you are on a clustered system there may be multiple installations listed. Once you select a particular installation you will see that installation’s administration page.

The global administration interface is accessible from the admin link on the page header (or click here to open it in a new tab). Note that you must have admin privileges to view this interface and the header link will be hidden if you do not have access. The global interface allows you to configure user accounts and add or remove NILM systems. This interface is available on all manager sites but is most useful on cluster managers and not standalone systems.

System Administration

The System Administration interface is used to configure a particular NILM system. Access this interface by selecting the Administration tile from the dashboard and then clicking the Manage button on a NILM system. This button will only be available on NILM’s you administer. The interface has four main tabs, Setup, Database, Processes, and Cloud. Each of these tabs are explained below.

Setup Tab

This tab configures general information about the NILM and user permissions. See the figure below for an example. The Name, and the Serial # must be unique, other general information fields must be present but not necessarily unique. On a standalone system most of this information is not important, but on a cluster this helps identify a particular machine. You must uncheck Use default URL’s and configure a custom address when adding a NILM to a cluster- see Wattsworth Clusters for details. If you would like to set a live meter view instead of the Dashboard as the site homepage, check Show on Live Panel, then select a meter dataset to display. Any user that has permissions on this NILM will see this meter in their live panel. Users who do not have permissions on this NILM will not be affected. Any changes to these settings will only take effect if you click the Save Settings button.
Permissions are configured on the righthand side of the interface. There are three levels, Administrator, Owner, and Viewer. Administrators are the highest level and Viewers are the lowest. Each level has the following permissions:

- **Administrator**: access system administration interface, run processes (filters and analyzers), view data
- **Owner**: run processes (filters and analyzers), view data
- **Viewer**: view data

To add a user to a permission group, click the button next to the permission. To remove a permission click the next to the user's name. To change a user's permission level, remove the current permission and add them back to the desired level.

System Administration Setup Tab. Configure general information and user permissions.

Database Tab
This tab provides information about the NILM database and has numerous tools for configuring the data streams. The interface is divided into three sections: General Information, Database Tree, and Group/File Configuration.

**General Information**: The top section shows general information about the database. The Version is the NilmDB software version and the URL is the location of the database. This will be a localhost URL on a standalone system and will be an IP address on a cluster system. The button updates the interface with the latest values from the database. The system automatically refreshes every half hour but in some cases it is helpful to force a refresh (for example when adding and configuring new meters). The Disk Usage chart shows how much space is used by NILM data in orange and how much space is used by the rest of the system in blue. The keep settings in meters.yml should be set appropriately so the disk does not fill completely with NILM data. The Plot Resolution slider configures how many samples are displayed in in NILM Explorer plots. Higher plot resolution requires more bandwidth and processing time on the NILM system. In general standalone systems should be configured for highest bandwidth and
clustered systems should be configured for a bandwidth that is appropriate for their network connection. Adjusting this slider automatically updates the server. Adjust this slider as you work with a plot to find an appropriate setting.

**Database Tree:** The left panel shows a tree view of the database. Database groups are listed below the NilmDB node. Clicking on the triangle next to a group toggles visibility of the files beneath it. Clicking a group or a file will select the node and display configuration options for it in the **Group/File Configuration** panel. The **Add Group** button adds a new empty group to the database. Group names must be unique. Groups can only be added when a connection to the NilmDB system is available which may be intermittent on a cluster system depending on the quality of the network connection.

![Database Tree Screenshot](image)

**System Administration Database Tab. View and Configure the NILM database.**

**Group/File Configuration:** The center panel is reserved for group and file configuration options. Select a group or file to configure by clicking it in the **Database Tree**. If you change any values click the **Save Changes** button to submit the changes, or click **Reset** to change all values back to their current state. To remove a group or file click the **Delete** button. This completely erases all of the data in the group or file and is not reversible. To prevent accidental deletion, click the **Lock** button. This removes the option to delete the file or group. To delete a locked object you must manually erase each stream in the group or file from the command line using **nilmtool destroy**.

When a group is selected the interface will look like the left hand figure below. The group name must be unique and the description should be a short sentence or phrase. The time range is the maximum extent of the files in this group, and the size is the sum of the file sizes. The **Hidden** checkbox controls whether the group is visible in the NILM Explorer interface.
When a file is selected the interface will look like the right hand figure below. The summary information at the top shows the extents of the data, number of samples and size on disk. Note that the total time is covers the intervals with data which may be much than the Time Range than the extents if there are gaps in the data. The keep settings in meters.yml track the Total Time parameter and not the Time Range.

The Database Path is the NilmDB stream name for the file. The Move button allows you to move the file to a different group. This should only be used for static datasets. Do not move active files, that is, inputs or outputs to a NILM process or raw streams like prep or sinefit.

The file Name must be unique in the group. Abbreviate as is an optional field that is added to the plot legend in NILM Explorer. If it is blank the legend will just be the stream name. Below these fields is an array of entries to configure each column (stream) of data in the file. Select Plottable to display the stream in NILM Explorer. Select Discrete to plot the data as vertical bars instead of a line graph. Name must be unique in the file. Units should be an SI value or descriptive word like "event". NILM Explorer requires that all datasets on an axis share the same unit. If unit is left blank the stream will only be plottable with other blank unit streams. The Offset and Scale fields are floating point values that can apply a linear transform to the data. The formula for the transform is:

\[ y = (x\text{-offset}) \times \text{scale} \]

The transform is applied "live", that is the underlying data is never changed. The transform is used both for NILM processes (filters and analyzers) and in NILM Explorer. Default Min and Default Max fix the auto scale bounds to the specified values. If left blank the plot will autoscale to the extents in the plotted dataset. This is useful if you want autoscale to provide a consistent scale to help building an intuition of what is "large" and "small". Otherwise zooming into any dataset and clicking autoscale will make the result fill the plot window. You must click Save Changes before selecting any other file or group from the Database Tree otherwise your changes will be lost.
Global Administration

The global administration interface is used to add users or NILM’s to the system. This is primarily used on cluster systems although the interface is available on standalone systems as well. To access this interface your user account must have administrative privileges. The interface is composed of three tabs, Servers, Users, and Data Views. Each of these tabs is described below.

Server Tab
The server tab is used to add NILM’s to the system. The only type of NILM that can be added to this version of the manager is a Repository. Click to access the new repository dialogue. Full details on adding NILM’s to a cluster using this interface are in Wattsworth Cluster. To remove a NILM from the system click the icon. This will remove the NILM from active management by the system but will not erase any data or settings on the NILM itself. You can add and remove the same NILM multiple times using this interface without any problems. The Status icon indicates whether the NILM is online (green) or not available (red).

User Tab
The user tab allows you to add, edit, and remove user accounts from the system. Note that any account you add you must manually confirm by clicking the button next to the user account. Usually the confirmation would be done by the user through an e-mail but this version of NILM Manager does not have an e-mail server. The Engineer attribute is not currently used. The Admin attribute controls whether the account has administrative privileges (i.e. the ability to use this interface). Note this is not related to any privileges an account has on a particular NILM.

Data Views Tab
This tab displays all of the stored dataviews on the system. You can edit the name and description of the views by clicking the icon and delete it by clicking the icon.
NILM Explorer

Introduction

NILM Explorer is an interactive plotting tool that provides visualizations of remote datasets using very little network bandwidth. This interface seamlessly combines data from one or more remote NILM systems and is capable of plotting data at any time scale. The interface works best with a three button mouse (left, right and scroll wheel), although a touch pad can be used. The interface consists of three main panels, the Dataset Explorer, Navigation Plot, and Main Plot. The figure below labels each panel on the interface. The sections below describe these panels in detail.

Dataset Explorer

The dataset explorer shows all the plottable datasets for all the NILM’s managed by the system. If this is a standalone system there will only be one NILM listed. On a cluster multiple NILM’s are separated by dark grey title bars. Select which NILM’s are displayed by using the button next to the search bar.

The groups on each NILM are listed below the NILM title bar. Click the button to expand a group and show its files. Each file can in turn be expanded to show the streams it contains. Streams have three radio buttons that control their visibility on the plot. By default all streams are off meaning they are not displayed. Plot a stream by selecting either the Left or Right radio buttons.
Left and Right refer to left and right Y-axes of the plot. When at least one stream is selected for plotting both the Navigation and Main Plot panels will appear. Multiple streams may be plotted simultaneously from any file, group or even other NILM's. However only streams must share the same unit to be plotted on the same axis. Radio buttons are automatically disabled if the stream's unit does not match the current axis unit. When a stream is displayed on the plot an @ is displayed next to the stream, file and group name. Clicking this icon on the stream will remove it from the plot. Clicking this on the file will remove any of the file's streams from the plot, and clicking it on the group will remove any stream from any the group's files from the plot. This is a quick way to clear a plot with many streams displayed.

The Dataset Explorer interface

The first stream to be displayed sets the bounds of the plots. The x-axis is set to the full range of data in the stream and the y-axis is set to either the range of the data or to the streams Default Min and Default Max values if set (see Stream Configuration for this setting). If you want the plot to track the latest data select **Start Live Update**. This will lock the time axis of the Navigation Plot to the last hour and the Main Plot to the last twenty minutes. Click **Stop Live Update** to disable time axis tracking.

**Navigation Plot**

The Navigation Plot shows a fixed overview of the data and highlights the portion displayed in the Main Plot. The y-axis is fixed to the autoscale values of the data (either the range of the plotted data or the Default Max and Default Min of the streams). In the default navigation mode is clicking and dragging on the plot selects the subset of data displayed in the Main Plot window. This mode is animated in the left hand figure below. The mode can be changed by clicking the ![search](image) and selecting **Lock Navplot Selection**. When this box is checked the time range of the selection is locked. Clicking and dragging the selection window changes the fixed time range displayed in the Main Plot. This mode is animated in the right hand figure below.
Navigation Plot in default mode. Click and drag to select a portion of data to display in the Main Plot.

Navigation Plot with Lock Navplot Selection checked. Click and drag to move the selection window across the data.

To change the time range of data displayed in the Navigation Plot, zoom to the desired time range in the Main Plot, click the button and select Sync Navplot to View. This will set the Navigation Plot time range to the Main Plot time range.

Main Plot

The Main Plot interface supports pan and zoom on three axes (left and right y axis and the x axis). Click and drag to pan, and scroll to zoom. The plot is divided into four regions as shown in the figure below. The zoom and pan controls operate differently depending on which region the cursor is in. When the cursor is in the center of the plot, pan and zoom operates simultaneously on all the axes.

The Main Plot interface is divided into four zones. When the cursor is close to an axis the zoom and pan controls operate only on that axis.
When the cursor is placed close to an axis, the pan and zoom only operate on that axis. This is indicated visually by a yellow highlight on the isolated axis. The three animations below show demonstrations of (a) isolating the time axis, (b) isolating the y-axis, and (c) operating all axes simultaneously. In general, it is easier to navigate datasets with isolated axes rather than zooming or panning all axes together. If the cursor is moved on top of the axis icon, a yellow highlight appears on the axis. Clicking this icon will autoscale the axis.

On the time axis, this means the bounds will change to cover all of the data from all currently plotted streams. On the y axes, this means the bounds will adjust to the maximum range of either the plotted samples or the Default Min/Default Max settings of the streams. The cursor must remain in the plot grid to pan or zoom, moving the cursor outside the axes will disable the plot controls.

A.) Isolated zoom on the time axis.
B.) Isolated zoom on the y axis.
C.) Simultaneous zoom on both axes.

The cursor will automatically highlight datapoints on the plot with a circle overlay. This can be helpful to determine the resolution of a particular plot. The button in the plot header toggles the cursor tooltip. The tooltip displays the numeric value of the data as the cursor moves over a plot. This is useful for determining the exact value of a sample.

The date label below the Main Plot automatically adjusts according to the range of data plotted. Click the date to bring up the time selection overlay shown below. This allows you to specify a particular time range of data. Click the date field to open up a calendar view or use the mouse wheel to scroll individual fields. The overlay is translucent so you can see the data adjusting as you specify the date. If the end time is before the start time, the selection is invalid, and no change will be made to the plot.
The plot menu is accessed by clicking the button in the header bar. This expands a dropdown menu with options to Open, Save, and Download plots. To open a previously saved plot, select Open and find the desired plot in the dialogue. The search feature filters plots on description and title. Click a plot figure to open it. To save a plot select Save and enter a title and description. The installation drop down box is for categorizing plots by location. On a standalone system there is only one installation, but on a cluster system there will be multiple installations listed. Note the saved plots are lightweight indexes to the underlying datasets. Depending on the keep settings of the datastreams plots using live datasets may be erased. It is recommended to archive sections of datasets you would like to keep to a separate stream that will not be erased by the cleanup routine.

The Download menu allows you to retrieve the raw data behind a plot as a comma separated value (CSV) file. Each file must be downloaded separately since the timeseries differ between files. The downloaded file has an informational header that describes the dataset. An example datafile is shown below.

```
# Source: Archive
# Bucket archive
#
# group: LEES' Compressor
# file: prep
# database:
#   url: http://bucket.vpn.wattsworth.net/nilmdb
#   path: /no-leak/prep
#
# start: 2013-02-12 13:21:05 -0500
# end: 2013-02-12 13:21:10 -0500
# total time: less than a minute
# total rows: 281
#
# The raw data file can be retrieved at the following URL:
#   http://bucket.vpn.wattsworth.net/nilmdb/stream/extract?path=....
#
# to import in matlab run:
#   nilm = importdata('thisfilename.txt')
#
# nilm.textdata: this help text
# nilm.data: the data
#
# The data has 2 columns with the following format:
#
# Column 1: Timestamp (microseconds)
# Column 2: P1 (W)
#
```

Data continues below....
In many cases the plotted dataset is too large to download over an HTTP (web) connection. In this case the download file will provide instructions for using nilmtool commands on the terminal to retrieve the raw data. nilmtool retrieves all streams in a file and the data is not scaled. The file provides equations to scale the streams according to their scale and offset settings.

# Source: Archive
# Bucket archive
# group: LEES' Compressor
# file: prep
# database: http://bucket.vpn.wattsworth.net/nilmdb
# path: /no-leak/prep
# start: 2013-02-12 14:34:53 -0500
# end: 2013-02-13 23:29:51 -0500
# total time: 1 day
# total rows: 2969842 <= OVER 2 MILLION ROWS
# The raw data file can be retrieved at the following URL:
# http://bucket.vpn.wattsworth.net/nilmdb/stream/extract?path=...
# There is too much data to download. If you really need this data you can extract it directly using nilmtool
# The data has 9 columns with the following format:
# (Column 1): Timestamp (microseconds)
# (Column 2): P1 (W)  [y=(x-0.0)*-1.0)]
# (Column 3): 01 (prep)  [y=(x-0.0)*1.0)]
# (Column 4): P3 (prep)  [y=(x-0.0)*1.0)]
# (Column 5): Q3 (prep)  [y=(x-0.0)*1.0)]
# (Column 6): P5 (prep)  [y=(x-0.0)*1.0)]
# (Column 7): 05 (prep)  [y=(x-0.0)*1.0)]
# (Column 8): P7 (prep)  [y=(x-0.0)*1.0)]
# (Column 9): 07 (prep)  [y=(x-0.0)*1.0)]
# This file can be run directly as a script
# Usage: nilmtool --url http://bucket.vpn.wattsworth.net/nilmdb extract ...

The file can be run directly as a bash script which will dump the timestamped file data to standard output.

Redirect this to a file to save the data. Note that raw data can be very large, be careful with your disk usage and the network bandwidth when retrieving datasets with nilmtool.

1 #print data to the terminal
2 $ bash ~/Downloads/nilm_data.txt
3 1360697693233225 6.951723e-01 -2.935897e-01 9.620408e-01 ... 
4 1360697693249891 1.101132e-02 4.109371e-01 -1.420663e-02 ... 
5 1360697693266557 2.287447e-01 1.076953e-01 4.715213e-01 ... 
6 1360697693283223 -5.571978e-01 -6.638092e-04 7.577136e-01 ... 
7 .... data continues ... 
8 #save data to text file
9 $ bash ~/Downloads/nilm_data.txt > saved_data.txt
NILM Filter

Introduction

Filters are the NILM’s data processing engine. Unlike static datasets which have a known fixed size, NILM datasets are constantly growing and are generally too large to operate on as a single array. Filters are iterative code blocks that allow for efficient processing on these large datasets. The tutorials below introduce the basic concepts. See the labeled sections for more detailed information.

Tutorial 1: Hello World

This example is an introduction to the NILM Filter tool. In this example you will build a basic median filter to smooth a dataset. This example will show you how to create a new filter, set up bindings, and test the filter in the development environment. To get started, click the NILM Filter [tile on the dashboard to load the Filter Listing page.

*Filter Listing:* Filters are listed by Title and Description. Filters can either be public or private. The Editing column shows the permission setting. Private filters can only be edited by their author while public filters can be edited by any user. The current permission is displayed as a private [ or public [ icon. Click the button to toggle the permission setting. To other users private filters are marked with a [ icon. The private and public setting only applies to editing. Any filter can be installed on any NILM by a user with at least owner privileges on the NILM. Click the [Create a new filter button to enter the New Filter Page.

*New Filter Page:* Enter a name and description for the filter. The name must be unique and the description should be a short sentence that describes what the filter is doing. Filters have one or more input data sources. Input sources are generic hooks that are bound to data streams at runtime. Enter "source" in the input text box and click [Add]. The input will be added to the filter. If you mistyped the entry click the [ next to the input and type the input name again. You can add more inputs the same way, but for now just use a single input. *Do not* click the "Resample streams" check box. Filters produce one or more output data streams. The output streams are stored in a single file that is dynamically created on the NILM at runtime. When run in the development environment this output file is stored temporarily by default (although it can be stored permanently). When a filter is run as a NILM Process the output file is stored permanently. For this filter add a single output named "filtered". Click [Add] to add the output stream to the filter. Click [Create Filter] to enter the Filter Development Environment.

*Filter Development Environment:* The development interface is divided into two main panels each with two tabs. The left panel is a code editor and the right panel provides options for configuring and testing the filter. Select the **Setup** tab on the right panel.
Filter Setup

Filters run on a particular NILM. In order to test the filter in the development environment you must pick an available NILM and associate the filter inputs with data streams on this NILM. Select an available NILM from the combo box. If this is a standalone installation there will only be one entry. If this is a cluster installation there may be multiple NILMs listed. After you select a NILM, bind the filter inputs to data streams that are available on the NILM. This filter only has one input which we will bind to a P1 stream. Start by selecting a data group. For this tutorial select a meter group that has available data. Then select the Prep A file and P1 stream. Next we need to configure the output stream. The output will be a filtered copy of the input so the units should match the input stream. P1 is in watts so enter "W" in the unit field. We want to plot the filter output so select the plottable checkbox. This will notify the filter engine that the output must be decimated. Click to update the filter with these new settings. Whenever you adjust the settings in the Setup tab you must click this button to apply the changes. A green success message appears at the top of the tab once the save operation is complete. The setup tab also lets you add or remove inputs and outputs to the filter. This has the same effect as adding inputs and outputs on the New Filter Page. A filter must have at least one input and one output. Now you can begin writing code for the filter.

Code: Filter

NILM filters are written in Python 2.7. If you are new to Python, there are many books on the subject as well as several good websites. O’Reilly’s "Learning Python" and "Programming Python" are great introductory texts. Websites come and go, at the time of this writing, Code Academy is a good resource to learn Python and many other languages. Filters rely on numpy and scipy for most signal processing routines. The online documentation for these tools is excellent. O’Reilly’s "Python for Data Analysis" provides a good introduction to these tools and many Python data processing packages.

Select the Filter tab in the code editor. Lines 1-3 are auto generated from the filter name and description. Add the import statement in line 5 to your filter. This imports the medfilt function from Numpy. Lines 8-17 are auto generated from the Setup tab settings. These lines should match the auto
generated comments in your filter exactly. If the comments do not match check to make sure you have
not selected "Resample Streams" and that your input is named source and output is named filtered.
Correct any errors and save the changes. This comment block will automatically update. When the filter is
first created the body of the filter function is empty. Copy lines 18–29 and paste it in place of the
#TODO...pass lines to complete the function.

```python
""" Median Filter
Windowed median filter
""

from scipy.signal import medfilt

def filter(data, interval, args, insert_func, state):
    """--[Auto-Generated: Do Not Remove or Modify]
    data is a python array where each element
    is a numpy array of timestamped values
    (timestamps are 64 bit microseconds)
    Access data in input array with these names:
    source: _i_source
    Access data in output array with these names:
    filtered: _o_filtered
    --"
    
    #filter parameters
    WINDOW_SIZE = 25
    #shorthand to access timestamps and values
    ts = data[_i_source][:, 0]
    vals = data[_i_source][:, 1]
    #run the median filter
    result = medfilt(vals, WINDOW_SIZE)
    #add timestamps to the result array by
    #stacking it together with the ts array
    output=np.hstack((ts[:, None], result[:, None]))
    #insert the timestamped data into the output stream
    insert_func(output)
```

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How it works: NILM data streams can be very large (e.g., billions of samples). In order to process large data sets on a machine with limited resources, we have to break the data into discrete chunks. The NILM Filter engine handles this data chunking transparently allowing developers to write code that assumes all the data is available as a continuous array. The framework defines two functions that must be specified by the developer: filter and initialize. Within filter, the data can be processed like a traditional array. The data processing engine calls filter iteratively with chunks of input data.

This example applies a windowed median filter. The median filter algorithm is imported from Numpy in line 5. Line 19 defines WINDOW_SIZE which is a parameter to medfilt. Explicitly defining tunable constants is a good way to make your code more readable and easier to maintain. Lines 21–22 set up local variables from the input data. The data parameter is a list of Numpy arrays from each input. This filter has only one input so a numerical index would be straightforward, but it is best practice to retrieve inputs from data using the logical index generated by the filter framework, _i_source. The next index operation is into the Numpy array. The Numpy array has two columns, timestamp (0) and value (1). The [:, X] notation is shorthand for “all rows of a specific column”. This initializes ts to a 1D array of timestamps and vals to a 1D array of input values.

Line 24 applies the median filter. This is the same code used for processing “standard” continuous arrays of data. The filter engine makes it possible to port standard signal processing algorithms directly to a chunk-processing architecture. Line 27 applies timestamps to the median filtered data so it can be stored as an output stream. The median filter is time invariant so the output has the same timestamps as the input. Line 29 inserts the median filtered data into the output stream. insert_func takes one argument, an array of timestamped values to save. Output timestamps must be monotonically increasing. This means each element of the array must have a unique timestamp that is greater than the timestamps before it. In this case, the timestamps are copied from the input stream, so we are guaranteed to meet this requirement. Click ✈️ Save Code when you have finished entering the code. Whenever you have unsaved changes to the code, an ✖️ will appear next to the tab with changes. Important: You must save changes before running the filter or leaving the page, otherwise any changes will be lost.

Testing the Filter

Once you have finished writing the processing code, it's time to test the filter on a sample dataset. Select the Test tab from the right panel. The tab is divided into two sections. The top section has filter controls and displays the console output. The bottom section is a truncated NILM Explorer interface. Filter inputs and outputs are listed below the plot window. The inputs are listed by name with the associated stream in brackets. Plot the source[Pl] stream on the left axis. Pan and zoom the plot to a short (less than a minute) section of data. The filter will run against the plotted time range only so selecting a smaller amount of data will make the filter run faster. Once you have selected a suitable range, click the ▶️ Run button to start the filter. The console output will display
information as the filter runs including the output of any print statements. If an error occurs the console will display the python debug dump. Fix any errors and run the filter again. When the filter finishes successfully the console status will display Complete!

When the filter is finished the outputs will be plottable. Plot the filtered output on the same axis as the input. If the axis is disabled the units do not match with the input. Go back to the Setup tab and set the output stream units to match your input (W). Depending on how much data your filter processed, the output may require decimation. This happens automatically but takes some time. If the decimation isn’t complete you will see an * next to the stream in the plot legend. Pan or zoom the plot to refresh the view until the decimation process is complete. The figures below show output from this filter with different WINDOW_LENGTH settings. The development environment makes it easy to quickly iterate and tune your filters. When you are satisfied with its performance you can set the filter up as a NILM Process to continuously on input data.

Median filter example using a window size of 15

Median filter example using a window size of 55

Tutorial 2: Calculating Power

This filter calculates instantaneous power from current and voltage inputs. Since this filter has multiple inputs we will resample the input array to a single time series which makes the data easier to process with standard signal processing techniques.

Resampled inputs: When a filter has multiple inputs you have the option of resampling them to a common time series. The filter engine can automatically interpolate the inputs and create a composite input array. The resampled input is a two dimensional numpy array where the first column is the time stamp and each subsequent column corresponds to a filter input. See Filter Inputs for more information. The filter engine requires a master stream to establish the time series. This is usually the highest bandwidth stream, although some applications may require a different choice.

Filter Setup
Create a new filter with two inputs labeled current and voltage and select the "Resample streams" check box. Add one output labeled power. From the filter setup panel, attach input streams to the bindings from a raw NILM file and make the output plottable in units of watts (W) and save your changes.

Select the current input as the master stream. A note on performance: resampling adds overhead which can slow down filters with highbandwidth inputs. In this example a faster implementation would be to use a single bulk input on the raw NILM file. See the Filter Inputs section for information on bulk inputs.

Code: Filter

Select the Filter tab in the code editor. Lines 1-3 are auto generated from the filter name and description. Lines 6-18 are auto generated from the Setup tab settings. These lines should match the auto generated comments in your filter exactly. If the comments do not match check to make sure you have selected "Resample Streams" and that your inputs are named current and voltage. Correct any errors and save the changes. This comment block will automatically update. When the filter is first created the body of the filter function is empty. Copy lines 16-19 and paste it in place of the #TODO...pass lines to complete the function.

```python
def filter(data, interval, args, insert_func, state):
    power = data[:, _i_current] * data[:, _i_voltage]
    time = data[:, 0]
    output = np.hstack((time[:, None], power[:, None]))
    insert_func(output)
```

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How it works: The data parameter is a 2D Numpy array. Column 0 is the timestamp and the subsequent columns are the input stream values. The resampling engine linearly interpolates the inputs to a single timeseries so the inputs appear to be simultaneously sampled. This makes the power calculation very straightforward. Line 16 computes the power directly by multiplying the current and voltage columns of the array. Using logical indices for the data array makes the code self commenting and easier to maintain if you later want to add or rearrange the inputs.

The output array is created by stacking the input timestamps with the power array in line 18. This inserted into the output stream in line 19.

After you have entered this code, save the changes and run the filter against a short section of input data. Notice the ripple at twice the line frequency.

Testing: Changing to 3 Phase

Many industrial systems use three phase power to avoid this ripple. This filter can be easily adapted to measure three phase power. Delete the filter inputs and add the following six inputs IA, IB, IC, VA, VB, VC. Bind these inputs to their respective streams in the raw file and save the changes. Notice the comment section in the filter function updates with the new configuration. Copy the new filter code below:
def filter(data, interval, args, insert_func, state):
    # data is a 2D numpy array, each row is a sample
    column[0]: 64 bit timestamp (us)

    Access data in input array with these names:
    I1: _i_IA
    V1: _i_IB
    I2: _i_IC
    V2: _i_VA
    I3: _i_IB
    V3: _i_VC

    Access data in output array with these names:
    PT: _o_PT

    pA = data[:,_i_I1]*data[:,_i_V1]
pB = data[:,_i_I2]*data[:,_i_V2]
pC = data[:,_i_I3]*data[:,_i_V3]
pT = p1+p2+p3
time = data[:,0]
output = np.hstack((time[:,None],pT[:,None]))
insert_func(output)

The output from this filter is shown below. Notice that the power is relatively constant. Try adjusting this
filter to have multiple outputs for PA, PB, PC. These outputs will look similar to the single phase power
plot.
Instantaneous power for a single phase system

Instantaneous power for a three phase system

So far we have only seen filters compute instantaneous metrics, many times we are interested in
cumulative metrics like energy consumption or average power. Computing these types of metrics requires
a new type of filter tool called state. See the next tutorial for information on how to build stateful filters.

Tutorial 3: Energy Consumption

This filter computes cumulative energy consumption from a prep input. This requires maintaining a
persistent running sum. The filter engine maintains persistent variables through the state object. This
object is initialized prior to the first filter run and then passed in as an argument to the filter function.

Filter State: State provides a type of "memory" between runs of the filter function. The state is passed
into filter as a parameter. The state object stores persistent data in slots. Slots must be initialized
and before they can be used. Once a slot is initialized any data type can be stored into it and retrieved
later. Slots can be used many ways but the recommended design pattern is as follows:

State Workflow:
1. Create state slots for each persistent variable in the initialize function
2. At the start of the filter function, retrieve state objects into local variables
3. Manipulate the local copies of the state objects
4. At the end of the filter function, return local copies back to the state

Step 4 is not necessary for mutable objects because Python passes them by reference. Immutable
objects like lists, and numbers must be returned explicitly since they are passed by value. When in doubt,
return local variables to the state.

Filter Setup
Create a new filter with one input labeled prep. Do not select the "Resample streams" check box. Add one output labeled energy. From the filter setup panel, attach a P1 prep stream to the input binding. Make the output plottable in units of kilowatt hours (kWh) and save your changes.

Code: Initialize

Select the Initialize tab in the code editor. Lines 1–3 are auto generated from the filter name and description. When the filter is first created the body of the initialize function is empty. Copy lines 6–9 and paste it in place of the #TODO...pass lines to complete the function.

```python
1 """ Initialization for Energy Integrator
2 """ Tutorial filter for energy
3 """

4
def initialize(state):
5 #1.) ---initialize state slots---
6 state.initializeSlot("C",0)
7 state.initializeSlot("last_ts",None)
8 state.initializeSlot("last_y",None)
```

How it works: This function runs before the data chunks are passed through filter. This is step 1 of the State Workflow. Slots in state are created by called initializeSlot. This function takes two parameters, a unique string identifier and the initial value for the slot. This filter uses three state slots: C is the integration offset. It is initialized to 0 which means the output energy stream will start at 0. The next two slots, last_ts and last_y are the last timestamp and value of the previous data chunk. These two slots are initialized with None to indicate they don't have a valid initial value. The next section describes how these state variables are used.

Code: Filter

Select the Filter tab in the code editor. Lines 1–3 are auto generated from the filter name and description. Add the import statement in line 5 to your filter. This imports the cumtrapz integration function from Numpy. Lines 8–17 are auto generated from the Setup tab settings. These lines should match the auto generated comments in your filter exactly. If the comments do not match check to make sure you have not selected "Resample Streams" and that your input is named source and output is named filtered. Correct any errors and save the changes. This comment block will automatically update. When the filter is first created the body of the filter function is empty. Copy lines 18–49 and paste it in place of the #TODO...pass lines to complete the function.

```python
1 """ Energy Integrator
2 """ Tutorial filter for energy
3 """
```

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from scipy.integrate import cumtrapz

def filter(data, interval, args, insert_func, state):
    """--[Auto-Generated: Do Not Remove or Modify]
    data is a python array where each element
    is a numpy array of timestamped values
    (timestamps are 64 bit microseconds)
"

    Access data in input array with these names:
    prep: __i_prep

    Access data in output array with these names:
    energy: __o_energy

    #2.) --- retrieve state into local variables---
    last_ts = state.retrieveSlot("last_ts")
    last_y = state.retrieveSlot("last_y")
    C = state.retrieveSlot("C")

    # shorthand to access timestamps and values
    ts = data[__i_prep][:,0]
    y = data[__i_prep][:,1]

    #3.) --- run data processing---
    if(last_ts is None):
        last_ts = ts[0]
    if(last_y is None):
        last_y = y[0]

    # append last values to current arrays
    ts = np.insert(ts,0,last_ts)
    y = np.insert(y,0,last_y)

    # integrate 'y' with respect to 'ts'
    # scale output to kWh
    kwh = cumtrapz(y,ts/(1e6*60*60*1e3))

    # the integration is offset by the previous run of the filter function
    kwh += C
41 #4.) ---return local variables to the state---
42 state.updateSlot("C",kwh[-1])
43 state.updateSlot("last_ts",ts[-1])
44 state.updateSlot("last_y",y[-1])
45
46 result = np.hstack((ts[1:,None],kwh[:,None]))
47 insert_func(result)

How it works: This example is more complex than the previous two, but it consists of several simple steps. The first section of this code (lines 19–22) retrieves the state slots into local variables which is step 2 of the State Workflow. Next, lines 24–25 provide shorthand variables into the data array so we can easily access the timestamps (ts) and values (y).

Lines 27–41 perform the data processing which is step 3 of the State Workflow. Lines 28–32 initialize last_ts and last_y if this is the first chunk of data. The reason for these variables is somewhat subtle. The output of a numerical integration is one element shorter than the input. This might seem insignificant, but the filter function executes iteratively and loosing a value with each iteration will cause the output (energy) to lag the input (power). To keep the streams in sync, the input timestamps and power are padded with the last value of the previous input arrays. This is done in lines 34–35 with the call to np.insert. Lines 38–41 calculate the energy integral. The cumtrapz is imported from the Numpy integration library in line 5. This function performs efficient trapezoidal integration. The integral is offset by C which is the value of the energy integral from the last data chunk. Without this addition the integral would "reset" to 0 with every data chunk.

Lines 45–47 complete step 4 of the State Workflow. The slots are updated from the local variable values with calls to updateSlot. Finally, the energy array is timestamped and passed to insert_func for insertion into the output stream.

Testing
The figures below show the filter output over two different time intervals. Gaps in the input stream propagate to the output stream. If a filter has multiple input streams the output is only computed over the intersection of available input data. The state is maintained across gaps in the input data so the filter code does not need to explicitly check for areas of missing data. If you do want to check for breaks in the data use the args["isEnd"] flag, see args documentation for details.
Calculating energy from power using a stateful filter.

Gaps in the input data do not affect filter state.

Reference

Inputs

Filters have one or more inputs. For example, a filter that computes power would have two inputs—voltage and current. Inputs are hooks that are associated with data sets on the NILM at runtime. Hooks allow the same filter to be used multiple times with different datasets. This makes the code more efficient and reusable. For example instead of designing a three phase median filter, an instance of the filter from Tutorial 1 could be scheduled for each phase. In design mode, the filter inputs are bound to datasets in the Setup tab. First select a NILM to run the filter from the dropdown box at the top of the tab (default is Primary). Specify the binding by selecting the Group, File, and Stream for each input using the dropdown boxes. An input is fully specified when all three boxes have a valid selection. The filter will not run if any of its inputs are not fully specified. Filter inputs can be removed by clicking the trashcan icon to the right of the combo boxes and new inputs can be added by typing a name in the text box below the current inputs and clicking the + icon. All inputs must have unique names. The figure below shows an example of the filter input binding interface:

Specifying filter inputs. All inputs must be specified before a filter can run.

Inputs can be presented to the filter either as a list individual Numpy arrays or a single resampled Numpy array. Arrays are 2D structures where column 0 is a microsecond timestamp and columns 1–N are the data. The filter receives data through the data argument. If resampling is not enabled (default), this argument is a Python list of Numpy arrays as shown in the figure below. This example shows a three input
filter. The input arrays are different lengths because NILM streams do not necessarily have the same sampling rate. Over a one minute time range for example, prep data will have 3600 samples while sensor data will have up to 480K samples (when using a contact NILM).

The data argument for a three input filter without resampling. Example indexing schemes for accessing different parts of the data.

To facilitate indexing into the data array the filter engine provides index tags for each input. These tags are inserted into the comments field below the filter declaration. They are formatted as _i_inputname. Using index tags instead of integers make the code easier to read and less brittle if inputs are added or removed later. Some common indexing techniques are shown in the figure above.

For many algorithms it is more convenient to have synchronously sampled inputs. The filter resample feature provides exactly this capability. In this mode, a single master stream (selected by the user) is used as the base timeseries and the other filter inputs are interpolated to fit these timestamps. In general the highest bandwidth stream should be selected as the master to reduce the effects of aliasing. The figure below has the same three inputs as before but uses resampling to collapse the inputs into a single array. In the first case, input 2 is the master so inputs 1 and 3 have additional interpolated samples to match this higher bandwidth time series. In the second case, input 1 is the master so inputs 2 and 3 are decimated (and interpolated) to match the lower bandwidth time series. Index tags are provided and should be used to index into the column of each sample. The righthand figure below shows some common indexing examples.
The data argument for a resampled three input filter. Using _i_input2 as the master stream. Other inputs are interpolated.

Resampling is useful for combining inputs from different files, but if the inputs all come from the same file resampling is not necessary since the datasets already share a common timeseries. When you are using more than one stream from a file it can be faster and more convenient to use a bulk input. Specify a bulk input by selecting --all-- from the stream dropdown box (the first entry). Bulk inputs provide every stream from the file. Without resampling the input data will look similar to the figure below. As with normal inputs, use the logical indexing variables to locate each input array in data.

Like normal inputs, bulk inputs can be resampled. However care must be taken when indexing into this array because the logical index variables are pointers to the base of the bulk input block. See the figure below for an example.
two bulk inputs (input1 and input3)
resampled using input1 as the master.

Outputs
Filters produce one or more outputs. These outputs are stored in a single file that is dynamically managed by the NILM. When a filter runs in the development environment, the NILM creates a fresh output file each time the filter runs. When you are satisfied with the filter's performance it can be scheduled to run as a process. Process filters are assigned a persistent output file which is then available for plotting in the [explorer] view and can be used as inputs to other filters or analyzers.

The filter output setup is below the filter input controls. Each filter output has optional plot settings. Selecting the [discrete] option plots the output as sticks rather than a continuous line. The output must be plottable to be shown (some outputs might not make sense to plot so they can be hidden from view by unchecking this option). The units, scale factor, and offset options are optional and can be adjusted later using the standard NILM administration interface. Like filter inputs, outputs can be removed by clicking the trashcan icon and new outputs can be added using the controls below the current outputs.

After you make any changes to the filter setup you must click [Save Changes] to put them into effect
NILM Analyzers

Introduction

Analyzers produce reports from NILM data. Before working with Analyzers make sure you fully understand NILM Filters. Analyzers iterate over input data exactly the same as filters but have an additional post processing step to generate an HTML report document. Reports can contain both text and graphics. Analyzers can be installed as a NILM processes to automatically generate reports as new data arrives. Reports generated by processes are accessible from the Report Groups dashboard tile.

Tutorial 1: Hello World

Analyzers use NILM data to produce reports. This example reports the average of a dataset. To get started, click the NILM Analyzer tile on the dashboard to load the NILM Analyzer Listing.

NILM Analyzer Listing: Analyzers are listed by Title and Description. Analyzers can either be public or private. The Editing column shows the permission setting. Private analyzers can only be edited by their author while public analyzers can be edited by any user. The current permission is displayed as a private or public icon. Click the button to toggle the permission setting. To other users private analyzers are marked with an icon. The private and public setting only applies to editing. Any analyzer can be installed on any NILM by a user with at least owner privileges on the NILM. Click the button to enter the NILM Analyzer Listing.

New Analyzer Page: Enter a name and description for the Analyzer. The name must be unique and the description should be a short sentence that describes what the analyzer is doing. Analyzers have one or more input data sources. Input sources are generic hooks that are bound to data streams at runtime. Enter "source" in the input text box and click +M. The input will be added to the analyzer. If you mistyped the entry click the X next to the input and type the input name again. You can add more inputs the same way, but for now just use a single input. Do not click the "Resample streams" check box. Click to enter the NILM Analyzer Page.

NILM Analyzer Page: The NILM Analyzer interface is divided into two main panels each with three tabs. The left panel is a code editor and the right panel provides options for configuring and testing the analyzer. Select the Setup tab on the right panel.

Analyzer Setup

Analyzers run on a particular NILM. In order to test the analyzer during development you must pick an available NILM and associate the analyzer inputs with data streams on this NILM. Select an available NILM from the combo box. If this is a standalone installation there will only be one entry. If this is a cluster installation there may be multiple NILMs listed. After you select a NILM you must bind the analyzer inputs to data streams that are available on the NILM. This analyzer only has one input which we will bind to a
P1 stream. Start by selecting a data group. For this tutorial select a meter group that has available data. Then select the Prep A file and P1 stream. Click to update the analyzer with these new settings. Whenever you adjust the settings in the Setup tab you must click this button to apply the changes. A green success message appears at the top of the tab once the save operation is complete. The setup tab also lets you add or remove inputs to the analyzer. This has the same effect as adding inputs on the New Analyzer Page. An analyzer must have at least one input. Now you can begin writing code for the analyzer.

Code: iteration

Select the Iteration tab in the code editor. Lines 1-3 are auto generated from the Analyzer name and description. Lines 6-12 are auto generated from the Setup tab settings. These lines should match the auto generated comments in your analyzer exactly. If the comments do not match check to make sure you have not selected “Resample Streams” and that your input is named source. Correct any errors and save the changes. This comment block will automatically update. When the analyzer is first created the body of the iteration function is empty. Copy lines 13-28 and paste it in place of the #TODO...pass lines to complete the function.
Compute the average of a dataset

**def iteration(data, interval, args, state):**

```
data is a python array where each element is a numpy array
of timestamped values (timestamps are 64 bit microseconds)

Access data in input array with these names:

- `source`: `i_source`

```

# shorthand to access values in `_i_source`
vals = data[[_i_source][:, 1]]

# local variables initialized from the state
avg = state.retrieveSlot("avg")
count = state.retrieveSlot("count")

# compute the local average
local_avg = np.mean(vals)
if(avg==None):
    avg = local_avg
else:
    # ... or compute the weighted average
    avg = avg*count/(count+len(vals)) + \n        local_avg*len(vals)/(count+len(vals))

# update the state from the local variables
state.updateSlot("count",count+len(vals))
state.updateSlot("avg",avg)
```

*How it works:* The analyzer iteration function is very similar to the filter function in NILM Filters. You should already be comfortable with NILM Filters. In line 14 we extract the values from the input stream into val. The data parameter is a list of Numpy arrays from each input. This analyzer has only one input so a numerical index would be straightforward, but it is best practice to retrieve inputs from the data list using the logical index generated by the analyzer framework, `_i_source`. The next index operation is into the Numpy array. The Numpy array has two columns, timestamp (0) and value (1). We are only interested in the values so we strip out the second column and store it in the local vals variable.
In lines 16–17 we retrieve the analyzer state into local variables. This analyzer has two state slots, \texttt{avg} and \texttt{count}. \texttt{avg} stores the average and \texttt{count} stores the number of samples in the average. Lines 18–25 perform the averaging computation. The Numpy built-in \texttt{np.mean(x)} is used to compute the average of the \texttt{vals} array. If this is the first data chunk through the analyzer the \texttt{avg} state variable will be \texttt{None} and we simply store the \texttt{local_avg} as the \texttt{avg} (line 21). If this is not the first data chunk, \texttt{avg} will be the average of the previous samples and we have to take the weighted combination of the previous average with the average of the new data. This is done in lines 24–25.

In lines 27–28 the state slots are updated from the local variables. \texttt{count} is incremented by the length of the \texttt{vals} array and \texttt{avg} is set to the new average.

\textbf{Code: Support}

Select the \texttt{Support} tab in the code editor. Lines 1–3 are auto generated from the Analyzer \texttt{name} and \texttt{description}. This tab defines two functions: \texttt{initialize} and \texttt{analyze}. The \texttt{initialize} function runs \texttt{before} the data is processed by \texttt{iteration}. Like NILM Filters, this function is used to set up state slots. This analyzer has two slots, \texttt{avg} and \texttt{count}. The value for \texttt{avg} is unknown until the data has been processed so this slot is initialized to \texttt{None}. The \texttt{count} slot is used to store the total number of samples in the average and is initialized to \texttt{0}.

The \texttt{analyze} function runs \texttt{after} the data is processed by \texttt{iteration}. This function can use the values stored in \texttt{state} to compute statistics on the data and produce plots with the \texttt{matplotlib} library. For this tutorial we simply print the average and number of samples processed.

```python
    """ Initialization for Average
    Compute the average of a dataset
    """

    def initialize(state):
        state.initializeSlot("count",0)
        state.initializeSlot("avg",None)

    def analyze(state, saveFigure, args):
        #retrieve state into local variables
        avg = state.retrieveSlot("avg")
        count = state.retrieveSlot("count")
        #display result in the terminal
        print "Processed %d values"%count
        print "The average is: %f"%avg
```

\textbf{Code: Report}
Select the **Report** tab in the code editor. This is the report template. Reports are written using Markdown which is a simplified version of HTML. See [markdown syntax](#) for details. Lines 1–3 are autogenerated from the analyzer name and description. Lines 5–6 display our result. State values are injected into the report with double braces. Any state variable with a string representation can be injected into a report.

Click ![Save Code](#) when you have finished entering the code for all three tabs.

```markdown
1 Average
2 -------------------
3 Compute the average of a dataset
4
5 Processed {{count}} values
6 The average is {{avg}}
```

**Testing the Analyzer**

Once you have saved the code it is time to test the analyzer on a sample dataset. Select the **Test** tab from the right panel. The test tab is divided into two sections. The top section has analyzer controls and displays the console output. The bottom section is a truncated NILM explorer interface. Analyzer inputs are listed below the plot window. Plot the source stream on the left axis. Pan and zoom the plot to a short (less than a minute) section of data. Once you have selected a suitable range click the ![Enabled](#) button to lock the plot. Click ![Run](#) to start the analyzer. The console output will display information as the analyzer runs including the output of any print statements. If an error occurs the console will display the python debug dump. Fix any errors and run the analyzer again. When the analyzer finishes successfully the console status will update to **Complete!**

After the analyzer has run successfully select the **Output** tab on the right. This tab displays the analyzer report. You should see the number of values processed and the overall average. Try changing the report template or the time range in the plot and run the analyzer again. Remember to click the save code button to commit any changes.

**Tutorial 2: Pump Health**

This analyzer example generates diagnostics for an air compressor. Air compressors maintain the pressure in a tank. During normal operation the compressor runs intermittently. If there is a leak in the system the frequency of runs will increase. If the compressor itself has a fault the duration of the runs will increase since the compressor is less efficient. By plotting a histogram of runtimes we can detect these types of error conditions before they become a critical failure. The input to this analyzer is a stream of pump turn on and off events identified by [NILM Finder](#).
Source data for Tutorial 2. The pump transients are identified by NILM Finder.

The runtime histogram indicates pump health.

Analyzer Setup

This analyzer requires two inputs but both of the inputs are part of the same file so we can use a single bulk input binding. Create a new Analyzer and add a single input, Events. **Do not** click the "Resample streams" check box. From the setup tab bind the input to the --all-- stream on the events file generated by NILM Finder, and save the changes.

```
Events
  Group: Pump
  File: Events
  Stream: --all--
```

Use --all-- to create a **bulk input** from all streams in the file.

Code: Iteration

Select the Iteration tab in the code editor. Lines 1–3 are auto generated from the Analyzer name and description. Lines 6–12 are auto generated from the Setup tab settings. These lines should match the auto generated comments in your analyzer **exactly**. If the comments do not match check to make sure you have not selected "Resample Streams" and that your **input** is named events. Correct any errors and save the changes. This comment block will automatically update. When the analyzer is first created the body of the iteration function is empty. Copy lines 13–38 and paste it in place of the #TODO...pass lines to complete the function.

```python
""
Cycling Systems Analysis
2 Create histograms of runtime
3 ""
4
def iteration(data, interval, args, state):
5 """--[Auto-Generated: Do Not Remove or Modify]
6    data is a python array where each element is a numpy array
7    of timestamped values (timestamps are 64 bit microseconds)
8 pass
""
```
Access data in input array with these names:

Events: _i_Events

#indices into bulk input _i_events

ON = 1; OFF = 2

#local variables initialized from the state

turn_on_time = state.retrieveSlot("turn_on_time")

is_on = state.retrieveSlot("is_on")

runtimes = state.retrieveSlot("runtimes")

#compute runtimes

for d in data[_i_Events]:

    if(d[OFF]):

        if(is_on):

            runtimes.append((d[0]-turn_on_time)/1e6)

            is_on = False

        else:

            print "double turn OFF at ",timestamp_to_human(d[0])

    if(d[ON]):

        if(is_on):

            runtimes.append((d[0]-turn_on_time)/1e6)

            is_on = True

if(args["isEnd"] and is_on):

    #machine must be off at the end of an interval

    is_on = False

    print "forcing off at end of interval"

#update the state from the local variables

state.updateSlot("turn_on_time",turn_on_time)

state.updateSlot("is_on",is_on)

state.updateSlot("runtimes",runtimes)
**How it works:** Line 14 sets up logical indices for the bulk input events. In lines 16–18 we retrieve the analyzer state into local variables. This analyzer uses three state slots: `turn_on_time` is the timestamp from the last ON event, `is_on` is the pump state (true/false), and `runtimes` is an array of the pump runtimes in seconds. Lines 20–34 loop over the input to calculate the pump runtimes. A runtime starts with a turn on event and ends with a turn off event. Each element in the input array is an event (ON or OFF). If the event is an OFF event (line 21) and `is_on` is true (line 22) this is the end of a runtime. The runtime is the difference between `turn_on_time` and the time of the OFF event. This is converted to seconds and appended to the `runtimes` array (line 24). Line 25 sets `is_on` to False to indicate the pump is off.

If the event is an ON event (line 29) `turn_on_time` is set to the event time (line 33) and `is_on` is set to true (line 34). Two additional clauses catch spurious transients. If the pump is off according to `is_on`, and another OFF event occurs, a warning is printed to the console and the event is ignored (line 28). Similarly, if the pump is on according to `is_on` and another ON event occurs a warning is printed (line 32) and `turn_on_time` is set to the more recent ON event (because the execution falls through to line 33).

Line 35 forces `is_on` to false at the end of an interval. This check is necessary because the data stream is intermittent. Ideally we would have continuous data but in reality sensors fail periodically so we have some gaps in the event stream. If the pump is on when the sensor stops recording we will have an ON event with no matching OFF. Without this check the runtime will extend until the sensor is back online and has recorded another OFF transient. Finally lines 40–42 update the state slots from the local variables.

Code: Support

Select the Support tab in the code editor. Lines 1–3 are auto generated from the Analyzer name and description. The initialize function defines the three state slots. `runtimes` is initialized to an empty array, `is_on` is initialized to false because we assume the pump is off before the event stream starts. If it is actually on we ignore the first OFF transient (line 27 in iterate) and start tracking runtimes with the first ON transient. The `turn_on_time` is left blank since we can’t provide a valid initial value.
Initialization for Cycling Systems Analysis
Create histograms of runtime

```
def initialize(state):
    state.initializeSlot("runtimes",[])
    state.initializeSlot("is_on",False)
    state.initializeSlot("turn_on_time", None)

def analyze(state, saveFigure, args):
    # retrieve state into local variables
    runtimes = state.retrieveSlot("runtimes")
    # compute histogram of runtimes
    (hist, bins) = np.histogram(runtimes, bins=15)
    center = (bins[:-1]+bins[1:])/2
    # create a matplotlib figure with histogram
    plt.figure()
    plt.plot(center, hist)
    plt.xlabel("Runtime (secs)")
    plt.ylabel("Counts")
    # store total number of runs
    state.initializeSlot("count", len(runtimes))
    # save figure for use in report
    saveFigure(fig, "runtimes")
```

The `analyze` function generates a histogram plot from the `runtimes` array. In line 12 the runtime state slot is retrieved into a local variable. Lines 14-15 compute the histogram using Numpy's built-in `histogram` function. See the numpy documentation for a full list of arguments. This function returns the counts per bin in `hist` and the bin edges in `bin`. To plot the count per bin we compute the bin centers in lines 15. `center` and `hist` have the same length so they can be plotted together. Analyzers use `matplotlib` to generate graphics. Matplotlib's `pyplot` module is imported as `plt`. Line 17 creates a new figure and line 18 plots the histogram in this figure. Lines 18-19 set up the plot labels. Line 22 initializes a new state slot to store the total number of runtimes. This slot is used to populate the report template. Line 24 uses the `saveFigure` function to store the plot image so it can be used in the report template. This function takes two arguments, the figure and a unique string identifier.

Code: Report

Select the **Report** tab in the code editor. Lines 1-3 are auto generated from the Analyzer name and
Cycling Systems Analysis

### Histogram of runtime duration

Total number of runs: \{\text{count}\}

\{\text{insertFigure("runtimes")}\}

Testing the Analyzer

Select the Test tab from the right panel. Plot the turn ON and turn OFF events on the left axis and select a region of time to run the analyzer over. Notice there are several gaps in the data indicating times when the NILM was offline. Even if you expect to have an uninterrupted dataset it is always best to design the analyzer to support these kinds of gaps (eg with check at line 35 of \text{analyze}). Click \text{Run} to start the analyzer. Select the Report tab to see the result. The histogram becomes smoother as more pump runtimes are included in the analysis. Try to display the max and min runtimes in the report. Experiment with different numbers of bins in \text{np.histogram} and different lengths of input data. Remember to click \text{Save Code} to update changes before running the analyzer again.

Tutorial 3: Energy Dashboard

Analyzers use the matplotlib package to provide powerful plotting and graphical presentation tools. Matplotlib’s pyplot is imported by default as \text{plt}. The code below shows how to create a basic graph using these tools.

\begin{verbatim}
fig = plt.figure()
x = np.arange(0,2*pi)
y = np.sin(x)
plt.plot(x,y)
#save the figure
saveFigure(fig,"example")
\end{verbatim}
NILM Finder

Introduction

The NILM Finder uses exemplar pattern matching to identify load transients. Exemplars are short sections of a waveform that correspond to a load turn on or turn off event. Users identify and label exemplars and can then run a load identification filter across a dataset to extract matching transients. The exemplar engine uses a cross correlation algorithm to determine match events. An exemplar can consist of multiple streams (eg P1, Q1, P3, etc) but they must all be part of the same file.

Exemplar Groups

Exemplars are classified into groups. The NILM Finder page lists available exemplar groups. Click a group to enter the exemplar matching page (shown in the figure below). You can create a new exemplar group by clicking the blue button at the bottom of the group list. Each group must have a unique name. The button deletes the group.

Identify Loads

The Exemplar Matching interface has three main panels labeled in the figure below. Start by finding an isolated transient in the data using the embedded NILM Explorer interface (click the link for details about this interface). A transient exemplar can consist of multiple streams but all streams must be in the same file. Once you have zoomed in to just the section of data corresponding to a transient enter the name of the transient (eg Fridge On) in the Exemplar List and click + Add. Click the name of an exemplar to display a thumbnail of the transient. Click the name again to hide the thumbnail. Edit displays the transient waveform in the NILM Explorer interface where you can change the bounds of the transient and add or remove streams. Once you are done adjusting the transient click Save to update the exemplar with the new transient waveform. Click Remove to delete an exemplar from the group.
Identify transients:

Exemplar name

Off Exemplars Left Right
+ Laser On 0 Edit Remove
+ Laser Off 0 Edit Remove
+ Compressor On 0 Edit Remove
+ Compressor Off 0 Edit Remove

Exemplar List

Find Loads  Save Output

Match Loads

After you have built a list of exemplars you can then search a dataset for matches. The exemplar matching engine runs across the range of data plotted in the NILM Explorer interface. The exemplars do not have to be part of the dataset you are matching against but the target file must have all of the streams required by the exemplar. Therefore if a transient is defined as a section of P1 and Q1 waveforms it can be used to match any prep file that also has P1 and Q1 streams. Click Find Loads to start the exemplar matching engine. Once the process has completed you can plot the identified exemplars on the left or right axis by selecting the appropriate radio button in the Exemplar List. By default the matches are only stored in a temporary stream, if you want to save the match results click Save Output and select a destination group and file name before running the matching engine.

An off transient defined by P1, Q1 and Q3.

Transients should be 30 seconds or less and all

NILM Finder automatically identifies loads based on exemplar transients. Matched

253
streams must be in the same file. exemplars are plotted as vertical pipes.
Process Manager

Introduction

Filters and Analyzers can be installed as NILM processes and run automatically. The NILM Process Manager shows currently installed processes and allows users to schedule new processes on demand.

The NILM process framework is based around NilmRun, a remote execution service integrated with the NILM. The nilmrn server provides command line tools but these are only for advanced diagnostics and debugging.

The Process Manager interface is available to any user with privileges on the NILM but only admins and owners can schedule new processes. admins can remove currently executing processes using the Administration interface.

Process List

The Process Manager overview shows all installed processes. On a standalone system the only NILM listed will be the local device, but on a cluster this view will contain process listings from all of NILM’s in the cluster. The Process column shows the type of process (Filter or Analyzer) and the name. The Owner is the name of the user who installed the process. Nilm is the serial number of the NILM holding the process. Status provides information about the state of the process. A green icon ● indicates a running process and a red icon ○ indicates an inactive process. Processes may be inactive for several reasons.

The process may be waiting for more data, finished if it is a one shot process, or halted with an error condition. If the process has failed with an error the return code is displayed in brackets.

Processes can be scheduled to execute as one shot or to repeat as new data becomes available. Repeat processes are indicated with a ✅ in the Repeat column. Click 🔄 to view the console output from a process. The ✖️ button uninstalls the process from the NILM.

Click the date below the Main Plot to open the Date Selector Overlay
New Processes

To install a process click the New Process button at the bottom of the Process Manager page. There are two different types of processes, filters and analyzers. See NILM Filters and NILM Analyzers for more details. Select which type of process you would like to install. Next specify the start and end times for the process. There are several different time options. The start time can be set to Earliest available or to a specific date. If there is a large amount of data in the input streams and you only want to process new data going forward, set the start time to the current date. The end time can also be set to a specific date or to Latest Available. If you select Latest Available then you can also select Repeat Process which will continue to run the process indefinitely as new data becomes available. Selecting all three check boxes will process all data that is currently available and all future data as it arrives.

Process just the data bounded by the start and end times.

Filter Process

Select "filter" from the Process Type combo box to display the filter specific configuration options. Select the filter and the NILM you want to run it on. Any filter can be installed on any NILM. Filters have one or more inputs. These must be bound to data streams that are available on the NILM. If the filter was designed on the same NILM, the stream binding will be populated with the values used in the filter editor. Finally you must create an output file for the process. Clicking the button brings up the file selector. Click the group where you want to store the file and enter a name for the file.

Once all of the settings are correct click Create Filter Process. The process will be automatically installed on the NILM and started. You will be redirected to the Process Manager page where you can check the status of the new process.
Analyzer Process

Select "analyzer" from the Process Type combo box to display the analyzer specific configuration options. Select the analyzer and the NILM you want to run it on. Any analyzer can be installed on any NILM. Analyzers have one or more inputs. These must be bound to data streams that are available on the NILM. If the analyzer was designed on the same NILM, the stream binding will be populated with the values used in the analyzer editor.

Next you must configure the report group structure. The group must have a unique name and description. The group should also be correlated with an installation. The installation should match the NILM where the process will be installed. The analyzer is run repeatedly across the data to generate reports which are stored in this group. The Create Report Every setting controls the frequency of reports and the Each Report Covers setting controls how much data is processed by each report. The figure below shows how these settings can be combined to create several different types of report structures. The units for these settings can be set to minutes, hours, or days.

Once all of the settings are correct click Create Analyzer Process. The process will be automatically installed on the NILM and started. You will be redirected to the Process Manager page where you can check the status of the new process.
Filter Process configuration panel
NILM Command Line Interface

Introduction

Command-line arguments can often be supplied in both short and long forms, and many arguments are optional. The following documentation uses these conventions:

- An argument that takes an additional parameter is denoted `-f FILE`.
- The syntax `-f FILE`, `--file FILE` indicates that either the short form (-f) or long form (--file) can be used interchangeably.
- Square brackets ([ ]) denote optional arguments.
- Pipes (A | B) indicate that either A or B can be specified, but not both.
- Curly braces ({ }) indicate a list of mutually-exclusive argument choices.

Many of the programs support arguments that represent a NilmDB timestamp. This timestamp is specified as a free-form string, as supported by the `parse_time` client library function, described in Section 3.2.2.4 of the NilmDB reference guide. Examples of accepted formats are shown in Table 3-19 on page 133 of that document.

NILM Diagnostics

`nilm-capture` is the global NILM service that manages data capture from all of the meters (contact and non-contact). This service is automatically managed by the NILM. The rest of the functions are diagnostic utilities that are useful when setting up an installation. `nilm-scope` provides a realtime waveform viewer similar to an oscilloscope. `nilm-calibrate` calibrates non-contact meters. `nilm-check-config` verifies the meters.yml syntax, checks if the specified meters are correctly connected, and estimates the disk usage required by the keep settings. `usbstream` prints non-contact USB meter data to standard output and `ethstream` does the same for the contact meters. The tools are designed to be used for temporary measurements while a user is setting up the system. All of these tools will disable `nilm-capture` while they are running. Finally, `NILM logs` describes the structure and location of log files generated by the NILM. These logs are useful for diagnostics and debugging installed systems.

```
nilm-capture - NILM system service
```

Usage

```
sudo service nilm-capture action
```

Description

This program controls the entire NILM acquisition and signal processing pipeline. It runs as a system
service. When nilm-capture is running data is collected from the meters, processed and stored as streams into NilmDB. When this service is not running the meters are idle and available for use by other diagnostic utilities. nilm-capture will automatically start on system boot. Stop data capture by issuing the stop action. After any change to the meters.yml file you must restart the daemon.

**Arguments**

**action**

start|stop|restart|status (specify a single action)

**Example**

```
$ sudo service nilm-capture restart #reload the meters.yml file and start
```

### nilm-scope - View sensor waveforms

**Usage**

```
nilm-scope meter -c
```

**Description**

NILM scope can display the sensor waveforms for either a non-contact or contact meter in realtime. For a contact installation this can help determine the phase pairings between the current and voltage sensors and for a non-contact installation this can help when placing the sensors to ensure strong magnetic and electric field pickup. The program requires two parameters, the meter name from the meters.yml configuration file and a list of channels to display. A legend is automatically built using the configuration in meters.yml.

**Arguments**

meter

meter name from meters.yml (meter1,meter2, etc)

-c CHANNELS

Space seperated list of channel indices to plot [0-5] for contact meters and [0-7] for non-contact meters

**Example**

```
$ nilm-scope meter1 -c 2 4 #display channels 2 and 4 from meter1
```
Usage

nilm-check-config

Description

This command verifies the syntax of meters.yml. This command should be run after any change to the meters.yml file to ensure that the configuration is valid. If the syntax is valid, it then checks if the specified meters are connected to the NILM. Finally, it calculates the disk space required by the keep settings and displays the estimated disk usage. If more space is required than currently available, adjust the keep settings for the meter streams and run this command again.

Arguments

none

Example

1 $ nilm-check-config  # syntax error in meters.yml
2 [CONFIGURATION_ERROR]: meter1 error in [streams][sinefit][keep] bad synt:
3
4 $ nilm-check-config  # no syntax errors, but warning that meter1 is missin:
5 [CONFIGURATION_WARNING]: meter1 device [meter0012] is not connected
6 This configuration will require -176.68 GiB
7 This is 41% of the available space on the disk

Usage

nilm-calibrate - Calibrate non-contact meters
\texttt{nilm-calibrate} \texttt{meter}

\textit{Description}

This command calibrates a non-contact meter. The meter must be configured in \texttt{meters.yml}. The calibration routine requires you to connect a smart plug to an outlet on each phase. Before running this command make sure you have a smart plug, micro USB cable, and a resistive load like an incandescent lightbulb. Configure the \texttt{meters.yml \texttt{calibration \textit{section}}} \texttt{with the load \texttt{watts} and calibration \texttt{duration} in seconds. Longer durations generally improve the calibration result. In general use around 30 seconds for a house and 90 seconds or more a ship or larger building. The calibration wattage should be at least 5\% of the background load with higher wattages producing more reliable calibration results. If the power system does not have a neutral bus (eg on a ship) set \texttt{has_neutral} to \texttt{false} otherwise leave it as \texttt{true}. This command can be used to calibrate a meter multiple times so you can experiment with different load sizes and calibration durations until the result is accurate.

\textit{Arguments}

\texttt{\textit{meter}}

\texttt{\textit{meter} name from \texttt{meters.yml} (\textit{meter1},\textit{meter2}, etc)}

\textit{Example}

Before running this command make sure the \texttt{meters.yml} file is configured for this meter. In particular adjust the \texttt{calibration \textit{section}} to match your setup. See \textit{Setting Up a Non-Contact Meter} for details on configuring \texttt{meters.yml}

\begin{verbatim}
meter1: ...other configurations... calibration:  
duration: 30 # length of calibration in seconds  
watts: 200 # power consumed by calibration load  
has_neutral: true # [false] if the system has no neutral bus ...
...other configurations...
\end{verbatim}

Once you have configured \texttt{meters.yml} run \texttt{nilm-calibrate} as shown below:
1 $ \textit{nilm-calibrate} \text{ meter1}
2
3 Calibrating meter1
4 + The power system has 2 phases and neutral
5 + Digitally integrating sensor 0 \textit{for} voltage measurement
6 + Using sensors 1,3,5,7 \textit{for} current measurements
7 + Calibration load is 200W and will run for 30 seconds
8 + The reference voltage is 120V rms
9 + The meter serial number is [meter0001]
10 Is this correct? (y/n) y \#answer n to cancel calibration
11 Set up a smart plug \textit{for} calibration? (y/n) y \#smart plug must be connected
12 #... calibration continues ...

\begin{quote}
\textbf{usbstream} - Stream raw sensor data non-contact meter (D-Board)
\end{quote}

\textbf{Usage}

\textbf{usbstream} meter

\textbf{Description}

This command returns timestamped sample data from a non-contact meter D-Board. The meter must be configured in \texttt{meters.yml} before running this command. All eight channels are sampled at 3kHz and printed to standard output. The first column is a Unix microsecond timestamp. This command does not apply any scaling or calibration to the sensor values, the output is the raw ADC reading. This command stops the \texttt{nilm-capture} process.

\textbf{Arguments}

meter

meter name from \texttt{meters.yml} (meter1,meter2, etc)

\textbf{Example}
\$ usbstream meter1
14574759674477951 -7071 551 -7090 501 -7048 483 -16247 -16248
1457475967447551 -7071 558 -7087 501 -7048 483 -16246 -16249
1457475967447885 -7069 566 -7088 504 -7049 486 -16247 -16249
1457475967448218 -7067 561 -7089 505 -7046 478 -16248 -16249
1457475967448551 -7066 557 -7084 502 -7045 479 -16247 -16250
1457475967448884 -7064 561 -7082 504 -7046 484 -16248 -16251
```
^C caught signal [2], stopping # hit Ctrl-C to stop
1 closed usb sensor
```

$usbstream meter1 > output.dat # save values to a file

---

**ethstream** - Stream raw sensor data from contact meter (LabJack)

**Usage**

```
ethstream [options]
```

**Description**

This command returns raw sample data from a LabJack UE9. The contact meter sensors are connected to channels 0–6 on the LabJack. See [Contact Meter](#) for a mapping of sensors to LabJack channels. There are many options to this command but the most useful for NILM debugging is `-a address, -C channels, and -L to force LabJack mode. The default sample rate is 8kHz. The full options are listed below. Use the `-x` flag to show complete usage examples. Before running this command you must manually stop the nilm-capture service. When you are done manually interacting with the LabJack, restart the nilm-capture service.

**Arguments**

- `a, --address string` host/address of device (192.168.1.209)
- `n, --numchannels n` sample the first N ADC channels (2)
- `C, --channels a,b,c` sample channels a, b, and c
- `r, --rate hz` sample each channel at this rate (8000.0)
- `L, --labjack` Force LabJack device
- `t, --timers a[:A],b[:B]` set LabJack timer modes a,b and optional values A,B
- `T, --timerdivisor n` set LabJack timer divisor to n
- `N, --nerdjack` Force NerdJack device
- `d, --detect` Detect NerdJack IP address
- `R, --range a,b` Set range on NerdJack for channels 0-5,6-11 to either 5 or 10 (10,10)
- `g, --gain a,b,c` Set LabJack AIN channel gains: 0,1,2,4,8 in -C channel order
- `o, --oneshot` don't retry in case of errors
- `f, --forceretry` retry no matter what happens
- `c, --convert` convert output to volts/temperature
- `H, --converthex` convert output to hex
- `m, --showmem` output memory stats with data (NJ only)
-l, --lines num    if set, output this many lines and quit
-h, --help         this help
-v, --verbose      be verbose
-V, --version      show version number and exit
-i, --info         get info from device (NJ only)
-X, --examples     show ethstream examples and exit

Example

1 $ ethstream -a 192.168.1.209 -C 0,1,2 -L #record channels 0,1,2 (current sen

NLM Logs - System logging

Description

The NILM processes record logging information to a set of log files located in /var/log/nilm. The
logs are automatically rotated daily and compressed. Logs older than 10 days are removed. View the
logs using tail. Each meter has a log and the supervisor NILM daemon has a log.

   supervisor.log
   Global data NILM system events. This log is produced by the nilm-capture service.

   meterX.log
   Individual meter events. Each of these logs is produced by the nilm-capture-daemon threads
   spawned by the global nilm-capture service.

Example

The logs are flat text files but due to their large size it is often easiest to view them using tail which
displays the last 10 lines of a file (the most recent log events). Use the -f flag to follow the file and
display new logging events as they are recorded.

Supervisor Correct Operation: Supervisor log indicates that a capture process has been spawned for
meter1

1 $ tail /var/log/nilm/supervisor.log
2 2016-03-09 09:06:56,524:INFO:STDOUT:-------- Starting Supervisor --------
3 2016-03-09 09:06:56,589:INFO:STDOUT:[supervisor]: waiting 2 minutes to avoi
4 2016-03-09 09:06:57,591:INFO:STDOUT:[supervisor]: starting capture for [met

Supervisor Error Condition: Supervisor log indicates that meter 1 is empty
$ tail /var/log/nilm/supervisor.log
2016-03-07 13:01:27,386:INFO:STDOUT:-------- Starting Supervisor --------
2016-03-07 13:01:27,387:INFO:STDOUT:[CONFIGURATION_ERROR]: meters.yml is em
2016-03-07 13:01:27,388:INFO:STDOUT: see [http://nilm.standalone/help/s...
2016-03-07 13:01:27,388:INFO:STDOUT:## Configuration has errors.
2016-03-07 13:01:27,388:INFO:STDOUT:## Run [nilm-check-config] to verify me

Meter Correct Operation: Meter log indicates that data capture has started on meter1

$ tail /var/log/nilm/meter1.log
2016-03-09 11:57:11,374:--------------starting capture on meter1----------
2016-03-09 11:57:11,374:--------------starting capture on meter1----------
2016-03-09 11:57:16,768:[meter1]: beginning interval

Meter Error Condition: Meter log indicates that the non-contact meter (D-Board) is not connected

$ tail /var/log/nilm/meter1.log
2016-03-09 11:56:51,378:--------------starting capture on meter1----------
2016-03-09 11:56:51,378:--------------starting capture on meter1----------
2016-03-09 11:56:51,735:[meter1]: beginning interval

Error Condition:
2016-03-09 11:56:51,735:[meter1]: beginning interval
2016-03-09 11:56:51,735:#### ERROR ####
2016-03-09 11:56:51,735:[meter1] Cannot find USB meter with serial number [ 
2016-03-09 11:56:51,735:check USB connection or set enabled=False in m 
2016-03-09 11:56:51,735:could not open port /dev/serial/by-id/usb-MIT_

nilmtool

Tools for interacting with the nilm database are wrapped in nilmtool, a monolithic multi-purpose
program that provides command-line access to most of the NilmDB functionality. Global operation is
described first followed by specific documentation for each subcommand.

```bash
nilmtool - Multipurpose NilmDB management tool
```

Usage

```
nilmtool [-h] [-v] [-u URL] {help, info, create, rename, list, intervals, 
metadata, insert, extract, remove, destroy} ...
```

Description

Multipurpose tool that provides command-line access to most of the NilmDB functionality. The
command-line syntax provides the ability to execute sub-commands: first, global arguments that affect
the behavior of all subcommands can be specified, followed by one subcommand name, followed by arguments for that subcommand. Each defines its own arguments and is documented independently.

Arguments

- **u** URL, **--url** URL
  (default: http://localhost/nilmdb/) NiimDB server URL. Must be specified before the subcommand.

subcommand ...

The subcommand to run, followed by its arguments. This is required.

- **h**, **--help**
  Print a help message with usage information and details on all supported command-line arguments.
  This can also be specified after the subcommand, in which case the usage and arguments of the subcommand are shown instead.

- **v**, **--version**
  Print the nilmtool version.

Environment Variables: Some behaviors of nilmtool subcommands can be configured via environment variables.

**NILMDB_URL**
  (default: http://localhost/nilmdb/) The default URL of the NiimDB server. This is used if --url is not specified, and can be set as an environment variable to avoid the need to specify it on each invocation of nilmtool.

**TZ**
  (default: system default timezone) The timezone to use when parsing or displaying times. This is usually of the form America/New_York, using the standard TZ names from the IANA Time Zone Database.

```
nilmtool help — Print help for a subcommand

Usage

   nilmtool help [-h] subcommand

Description

   Print more specific help for a subcommand. nilmtool help subcommand is the same as nilmtool subcommand --help.
```

```
nilmtool info — Server information

Usage

   nilmtool info [-h]

Description

   Print server information such as software versions, database location, and disk space usage.

Example
```
nilmtool info

Client version: 1.9.7
Server version: 1.9.7
Server URL: http://localhost/nilmdb/
Server database path: /home/nilmdb/db
Server disk space used by NilmDB: 143.87 GiB
Server disk space used by other: 378.93 GiB
Server disk space reserved: 6.86 GiB
Server disk space free: 147.17 GiB

Usage

nilmtool create

Usage

nilmtool create 

Description

Create a new empty stream at the specified path and with the specified layout.

Arguments

PATH
Path of the new stream. Stream paths are similar to filesystem paths and must contain at least two components. For example, /foo/bar.

LAYOUT
Layout for the new stream. Layouts are of the form <type>_<count>. The <type> is one of those described in Section 2.2.3 of the NilmDB Reference Guide, such as uint16, int64, or float32. <count> is a numeric count of how many data elements there are, per row. Streams store rows of homogeneous data only, and the largest supported <count> is 1024. Generally, counts should fall within a much lower range, typically between 1 and 32. For example, float32_8.

Usage

nilmtool rename

Usage

nilmtool rename

Description

Rename or relocate a stream in the database from one path to another. Metadata and intervals, if any, are relocated to the new path name.

Arguments

OLDPATH
Old existing stream path, e.g. /foo/old

NEWPATH
New stream path, e.g. /foo/bar/new
Notes

Metadata contents are not changed by this operation. Any software tools that store and use path names stored in metadata keys or values will need to update them accordingly.

**nilmtool list** - List streams

**Usage**

```bash
nilmtool list [-h] [-E] [-d] [-s TIME] [-e TIME] [-T] [-l] [-n] [PATH [PATH ...
```

**Description**

List streams available in the database, optionally filtering by path, and optionally including extended stream info and intervals.

**Arguments**

- **PATH**
  (default: "") If paths are specified, only streams that match the given paths are shown. Wildcards are accepted; for example, /sharon/* will list all streams with a path beginning with /sharon/. Note that, to prevent wildcards from being interpreted by the shell, they should be quoted at the command line; for example:
  ```bash
  1 $ nilmtool list "/sharon/*"
  2 $ nilmtool list "*raw"
  ```
  - **-E, --ext**
    Show extended stream information, like interval extents, total rows of data present, and total amount of time covered by the stream's intervals.
  - **-T, --timestamp-raw**
    When displaying timestamps in the output, show raw timestamp values from the NilmDB database rather than converting to human-readable times. Raw values are typically measured in microseconds since the Unix time epoch (1970/01/01 00:00 UTC).
  - **-l, --layout**
    Display the stream layout next to the path name.
  - **-n, --no-decim**
    Omit streams with paths containing the string "--decim-", to avoid cluttering the output with decimated streams.
  - **-d, --detail**
    In addition to the normal output, show the time intervals present in each stream. See also nilmtool intervals in Section 3.2.3.7 of the NilmDB Reference Guide, which can display more details about the intervals.
  - **-s TIME, --start TIME**
    Starting timestamp for intervals (free-form, inclusive).
  - **-e TIME, --end TIME**
    Ending timestamp for intervals (free-form, noninclusive).

**nilmtool intervals** - List intervals

**Usage**

Description
List intervals in a stream, similar to nilmtool list --detail, but with options for calculating set-differences between intervals of two streams, and for optimizing the output by joining adjacent intervals.

Arguments
PATH
List intervals for this path.
-d, --diff DIFFPATH
(default: none) if specified, perform a set-difference by subtract the intervals in this path; that is, only show interval ranges that are present in the original path but not present in DiffPath.

-s TIME, --start TIME
Starting timestamp for intervals (free-form, inclusive).
-e TIME, --end TIME
Ending timestamp for intervals (free-form, noninclusive).
-T, --timestamp-raw
(default: min) (default: max) When displaying timestamps in the output, show raw timestamp values from the NiImDB database rather than converting to human-readable times. Raw values are typically measured in microseconds since the Unix time epoch (1970/01/01 00:00 UTC).
-o, --optimize
Optimize the interval output by merging adjacent intervals. For example, the two intervals [1 → 2) and [2 → 5) would be displayed as one interval [1 → 5).

nilmtool metadata - Manage stream metadata

Usage
nilmtool metadata [-h] PATH [-g [KEY ...] | -s KEY=VALUE [...] | -u KEY=VALUE [...] | -d [KEY ...]]

Description
Get, set, update, or delete the key/value metadata associated with a stream.

Arguments
PATH
Path of the stream for which to manage metadata. Required, and must be specified before the action arguments.

Action Arguments: These actions are mutually exclusive.

-g [KEY ...], --get [KEY ...]
(default: all) Get and print metadata for the specified key(s). If none are specified, print metadata for all keys. Keys are printed as key=value, one per line.
-s [KEY=VALUE ...], --set [KEY=VALUE ...]
Set metadata. Keys and values are specified as a key=value string. This replaces all existing metadata on the stream with the provided keys; any keys present in the database but not specified on the command line are removed.
-u [KEY=VALUE ...], --update [KEY=VALUE ...]
Update metadata. Keys and values are specified as a key=value string. This is similar to --set, but only adds or changes metadata keys; keys that are present in the database but not specified on the
command line are left unchanged.
-d [KEY ...], --delete [KEY ...]
  (default: all) Delete metadata for the specified key(s). If none are specified, delete all metadata for
the stream.

Example

1 $ nilmtool metadata /temp/raw --set "location=Honolulu, HI" "source=NOAA"
2 $ nilmtool metadata /temp/raw --get
3 location=Honolulu, HI
4 source=NOAA
5 $ nilmtool metadata /temp/raw --update "units=F"
6 location=Honolulu, HI
7 source=NOAA
8 units=F

nilmtool insert -- insert data

Usage


Description

Insert data into a stream. This is a relatively low-level interface analogous to the /stream/insert HTTP
interface described in Section 3.2.1.13 on the NilmDB Reference Guide. This is the program that should
be used when a fixed quantity of text-based data is being inserted into a single interval, with a known
start and end time. If the input data does not already have timestamps, they can be optionally added
based on the start time and a known data rate. In many cases, using the separate nilm-insert
program is preferable, particularly when dealing with large amounts of pre-recorded data, or when
streaming data from a live source.

Arguments

PATH
  Path of the stream into which to insert data. The format of the input data must match the layout of
  the stream.

FILE
  (default: standard input) Input data filename, which must be formatted as uncompressed plain text.
  Default is to read the input from stdin.

-q, --quiet
  Suppress printing unnecessary messages.

Timestamping: To add timestamps to data that does not already have it, specify both of these arguments.

The added timestamps are based on the interval start time and the given data rate.

-t, --timestamp
  Add timestamps to each line

-r RATE, --rate RATE
  Data rate, in Hz

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Start Time: The start time may be manually specified, or it can be determined from the input filename, based on the following options.

- `-s` TIME, `--start` TIME
  Starting timestamp for the new interval (free-form, inclusive)
- `-f`, `--filename`
  Use filename to determine start time

End Time: The ending time should be manually specified. If timestamps are being added, this can be omitted, in which case the end of the interval is set to the last timestamp plus one microsecond.

- `-e` TIME, `--end` TIME
  Ending timestamp for the new interval (free-form, noninclusive)

Usage

`nilmtool extract` - Extract data

Usage


Description

Extract rows of data from a specified time interval in a stream, or output a count of how many rows are present in the interval.

Arguments

- `PATH`
  Path of the stream from which to extract data.
- `-s` TIME, `--start` TIME
  Starting timestamp to extract (free-form, inclusive)
- `-e` TIME, `--end` TIME
  Ending timestamp to extract (free-form, noninclusive)

Output Formatting

- `-B`, `--binary`
  Output raw binary data instead of the usual text format. For details on the text and binary formatting, see the documentation of HTTP call `/stream/insert` in Section 3.2.1.13.
- `-b`, `--bare`
  Omit timestamps from each line of the output.
- `-a`, `--annotate`
  Include comments at the beginning of the output with information about the stream. Comments are lines beginning with #.
- `-m`, `--markup`
  Include comments in the output with information that denotes where the stream's internal intervals begin and end. See the documentation of the markup parameter to HTTP call `/stream/extract` in Section 3.2.1.14 for details on the format of the comments.
- `-T`, `--timestamp-raw`
  Use raw integer timestamps in the --annotate output instead of human-readable strings.
- `-c`, `--count`
  Instead of outputting the data, output a count of how many rows are present in the given time interval. This is fast as it does not transfer the data from the server.

`nilmtool remove` - Remove rows of data
Usage

```
nilmtool remove [-h] -s TIME -e TIME [-q] [-c] PATH [PATH ...]
```

Description

Remove all data from a specified time range within the stream at /PATH/. Multiple streams may be specified, and wildcards are supported; the same time range will be removed from all matching streams.

Arguments

- **PATH**
  
  Path(s) of streams. Wildcards are supported. At least one path must be provided.

- **-s TIME**, **--start TIME**
  
  Starting timestamp of data to remove (free-form, inclusive, required).

- **-e TIME**, **--end TIME**
  
  Ending timestamp of data to remove (free-form, non-inclusive, required).

Output Format

- **-q**, **--quiet**
  
  By default, matching path names are printed when removing from multiple paths. With this option, path names are not printed.

- **-c**, **--count**
  
  Display a count of the number of rows of data that were removed from each path.

Example

```
1 $ nilmtool remove -s @1364140671600000 -e @1364141576585000 -c "/sh/raw*"
2 Removing from /sh/raw
3 7239364
4 Removing from /sh/raw-decim-4
5 1809841
6 Removing from /sh/raw-decim-16
7 452460
```

```
nilmtool destroy - Destroy a stream
```

Usage

```
nilmtool destroy [-h] [-R] [-q] PATH [PATH ...]
```

Description

Destroy the stream at the specified path(s); the opposite of nilmtool create. Metadata related to the stream is permanently deleted. All data must be removed before a stream can be destroyed.

Wildcards are supported.

Arguments

- **PATH**
  
  Path(s) of streams. Wildcards are supported. At least one path must be provided.

- **-R**, **--remove**
  
  If specified, all data is removed before destroying the stream. Equivalent to first running
The following section documents a variety of programs useful for processing and interacting with NILM data. Each program begins with the prefix `nilm-`.

Many of these programs are filters that process input from one or more source streams into a destination stream. Only regions of time that are present in the source, and not yet present in the destination, are processed. These programs can therefore be re-run with the same command-line arguments multiple times, and they will only process the newly available data each time.

### nilm-copy

**Copy data between streams**

**Usage**

```
```

**Description**

Copy data and metadata from one stream to another. The source and destination streams can reside on different servers. Both streams must have the same layout.

**Arguments**

- **-u URL, --url URL**
  (default: http://localhost/nilmdb/) NILMDB server URL for the source stream.
- **-U DESTURL, --dest-url DESTURL**
  (default: same as URL) NILMDB server URL for the destination stream. If unspecified, the same URL is used for both source and destination.
- **-D, --dry-run**
  Just print intervals that would be processed, and exit.
- **-F, --force-metadata**
  Metadata is copied from the source to the destination. By default, an error is returned if the destination stream metadata conflicts with the source stream metadata. Specify this flag to always overwrite the destination values with those from the source stream.
- **-n, --nometa**
  Don't copy or check metadata at all.
- **-s TIME, --start TIME**
  (default: min) Starting timestamp of data to copy (free-form, inclusive).
- **-e TIME, --end TIME**
  (default: max) Ending timestamp of data to copy (free-form, noninclusive).

**SRCPATH**

Path of the source stream (on the source server).

**DESTPATH**

Path of the destination stream (on the destination server).
nilm-copy-wildcard – Copy multiple streams

Usage

```
```

Description

Copy data and metadata, from multiple streams, between two servers. Similar to nilm-copy, except:

- Wildcards and multiple paths are supported in the stream names.
- Streams must always be copied between two servers.
- Stream paths must match on the source and destination server.
- If a stream does not exist on the destination server, it is created with the correct layout automatically.

Arguments

Most arguments are identical to those of nilm-copy (reference it for more details).

`PATHS`

Path(s) to copy from the source server to the destination server. Wildcards are accepted.

Example

```
2 Source URL: http://bucket/nilmdb/
3 Dest URL: http://pilot/nilmdb/
4 Creating destination stream /bp/startup/info
5 Creating destination stream /bp/startup/prep-a
6 Creating destination stream /bp/startup/prep-a-decim-4
7 Creating destination stream /bp/startup/prep-a-decim-16 ... etc
```

nilm-decimate – Decimate a stream one level

Usage

```
```

Description

Decimate the stream at SRCPATH and write the output to DESTPATH. The decimation operation is described in Section 2.4.1; in short, every FACTOR rows in the source are consolidated into one row in the destination, by calculating the mean, minimum, and maximum values for each column.

This program detects if the stream at SRCPATH is already decimated, by the presence of a decimate_source metadata key. If present, subsequent decimations take the existing mean, minimum, and maximum values into account, and the output has the same number of columns as...
the input. Otherwise, for the first level of decimation, the output has three times as many columns as
the input.

See also nilm-decimate-auto (Section 3.4.2.5) for a simpler method of decimating a stream by
multiple levels.

Arguments

-\texttt{-u URL, \--url URL}
  (default: http://localhost/nilmdb/) NilmDB server URL for the source stream.
-\texttt{-U DESTURL, \--dest-url DESTURL}
  (default: same as URL) NilmDB server URL for the destination stream. If unspecified, the same
  URL is used for both source and destination.
-\texttt{-D, \--dry-run}
  Just print intervals that would be processed, and exit.
-\texttt{-F, \--force-metadata}
  Overwrite destination metadata even if it conflicts with the values in the “metadata” section
  below.
-\texttt{-s TIME, \--start TIME}
  (default: min) Startingtimestamp of data to decimate (free-form, inclusive).
-\texttt{-e TIME, \--end TIME}
  (default: max) Endingsubmission of data to decimate (free-form, noninclusive).
-\texttt{-f FACTOR, \--factor FACTOR}
  (default: 4) Set the decimation factor. For a source stream with \(n\) rows, the output stream will have
  \(n/\text{FACTOR}\) rows.

\texttt{SRCPATH}
Path of the source stream (on the source server).

\texttt{DESTPATH}
Path of the destination stream (on the destination server).

\texttt{Metadata:} The destination stream has the following metadata keys added:

- \texttt{decimate\_source}
  The source stream from which this data was decimated.
- \texttt{decimate\_factor}
  The decimation factor used.

\begin{center}
\textbf{nilm-decimate-auto} – Decimate a stream completely
\end{center}

Usage


Description

Automatically create multiple decimation levels using from a single source stream, continuing until
the last decimated level contains fewer than 500 rows total. Decimations are performed using nilm-
decimate (Section 3.4.2.4). Wildcards and multiple paths are accepted. Destination streams are
automatically named based on the source stream name and the total decimation factor; for example, /test/raw-decim-4, /test/raw-decim-16, etc. Streams containing the string
"-decim-" are ignored when matching wildcards.

Arguments
-\texttt{-u URL, --url URL} \\
  (default: http://localhost/nilmdb) NiImDB server URL for the source and destination streams.
-\texttt{-F, --force-metadata} \\
  Overwrite destination metadata even if it conflicts with the values in the "metadata" section above.
-\texttt{-f FACTOR, --factor FACTOR} \\
  (default: 4) Set the decimation factor. Each decimation level will have 1/\texttt{FACTOR} as many rows as the previous level.
\texttt{PATH} [...]
  One or more paths to decimate. Wildcards are accepted.

\texttt{nilm-insert} - insert data from an external source

Usage

Description
Insert a large amount of text-formatted data from an external source like eth-stream. This is a higher-level tool than nilmtool insert in that it attempts to intelligently manage timestamps. The general concept is that it tracks two timestamps:

1. The data timestamp is the precise timestamp corresponding to a particular row of data, and is the timestamp that gets inserted into the database. It increases by data_delta for every row of input. data_delta can come from one of two sources. If \texttt{--delta} is specified, it is pulled from the first column of data. If \texttt{--rate} is specified, data_delta is set to a fixed value of 1/RATE.

2. The clock timestamp is the less precise timestamp that gives the absolute time. It can come from two sources. If \texttt{--live} is specified, it is pulled directly from the system clock. If \texttt{--file} is specified, it is extracted from the input file every time a new file is opened for read, and from comments that appear in the files.

Small discrepancies between data and clock are ignored. If the data timestamp ever differs from the clock timestamp by more than max_gap seconds:

- If data is running behind, there is a gap in the data, so the timestamp is stepped forward to match clock.
- If data is running ahead, there is overlap in the data, and an error is returned. If \texttt{--skip} is specified, then instead of returning an error, data is dropped and the remainder of the current file is skipped.

Arguments
-\texttt{-u URL, --url URL} \\
  (default: http://localhost/nilmdb) NiImDB server URL.
-D, --dry-run
Parse files and print information, but don't insert any data. Useful for verification before making changes to the database.
-s, --skip
Skip the remainder of input files if the data timestamp runs too far ahead of the clock timestamp. Useful when inserting a large directory of existing files with inaccurate timestamps.
-m SEC, --max-gap SEC
(default: 10.0) Maximum discrepancy between the clock and data timestamps.

Data timestamp
-r RATE, --rate RATE
(default: 8000.0) data_delta is constant 1/RATE (in Hz).
-d, --delta
data_delta is provided as the first number on each input line.

Clock timestamp
-l, --live
Use the live system time for the clock timestamp. This is most useful when piping in data live from a capture device.
-f, --file
Use filename and file comments for the clock timestamp. This is most useful when reading previously saved data.
-o SEC, --offset-filename SEC
(default: -3600.0) Offset to add to timestamps in filenames, when using --file. The default accounts for the existing practice of naming capture files based on the end of the hour in which they were recorded. The filename timestamp plus this offset should equal the time that the first row of data in the file was captured.
-O SEC, --offset-comment SEC
(default: 0.0) Offset to add to timestamps in comments, when using --file. The comment timestamp plus this offset should equal the time that the next row of data was captured.

Path and Input
PATH
Path of the stream into which to insert data. The layout of the path must match the input data.
INFILE [ ... ]
(default: standard input) Input data filename(s). Filenames ending with .gz are transparently decompressed as they are read. The default is to read the input from stdin.

Usage


Description
Perform the spectral envelope harmonic coefficient calculation described in Section 4.3.3. Two source streams are provided, one with the raw current data and one with marked zero crossings, typically created by nilm-sinefit (Section 3.4.2.10). The filter processes regions of time that are present in both source streams, and not present in the destination stream.
Arguments

-u URL, --url URL
    (default: http://localhost/nilmdb/) NilmDB server URL for the source stream.
-U DESTURL, --dest-url DESTURL
    (default: same as URL) NilmDB server URL for the destination stream. If unspecified, the same
    URL is used for both source and destination.
-D, --dry-run
    Just print intervals that would be processed, and exit.
-F, --force-metadata
    Overwrite destination metadata even if it conflicts with the values in the “metadata” section
    below.
-s TIME, --start TIME
    (default: min) Starting timestamp of data to filter (free-form, inclusive).
-e TIME, --end TIME
    (default: max) Ending timestamp of data to filter (free-form, noninclusive).

Preprocessor Arguments

-c COLUMN, --column COLUMN
    Column number in SRCPATH to use for the raw data. The first data column is 1.
-q NHARM, --nharm NHARM
    (default: 4) Number of odd harmonics Nharm to compute and store. For example, Nharm = 2
    will store P1, Q1, P3, and Q3.
-N NSHIFT, --nshift NSHIFT
    (default: 1) Number of shifted FFTs Nshift to compute, per period of the raw data. If the input
    frequency is 60 Hz, the data rate of the preprocessor output is Nshift x 60 Hz.
    Note that the calculation used by the similar Kalman-filter preprocessor, described in [54], is
    equivalent to Nshift = 2.
-r DEG, --rotate DEG
    (default: 0.0) Apply the additional rotation φextra to the FFT output, in degrees. Typically used
    to account for known phase offset between voltage and current. This is equivalent to adding a
    lag of φextra degrees to the zero crossing data.
    This is also useful for three-phase systems. For example, the zero crossings can be calculated
    once with nilm-sinefit on φA voltage. Then, nilm-prep can be run on φA, φB, and φC currents
    using rotations of 0, 120, and 240 degrees. The order in which to apply these shifts will depend
    on the phase ordering in the measured system.
-R RAD, --rotate-rad RAD
    (default: 0 rad) Like --rotate, except specified in radians instead of degrees.

SRCPATH
    Path of the raw source stream, for example, /foo/raw.
SINEPATH
    Path of the sinefit source stream, for example, /foo/sinefit.
DESTPATH
    Path of the prep output, for example, /foo/prep. The destination stream must have 2 · Nharm
    columns.

Metadata: The destination stream has the following metadata keys added:

prep_raw_source
    The source stream of the raw data from which these envelopes were calculated.
prep_sinefit_source
The source stream of the marked zero crossings used for this data.

prep_column
  The column number of the raw data in the raw data source.

prep_rotation
  The applied rotation $\phi_{extra}$ for this data, in radians. prep_nshift The number of shifted FFTs for this data.

### nilm-sinefit - Sinusoid fitting

#### Usage

```
```

#### Description

Perform the 4-parameter sinefit fit calculation described in Section 4.3.2. Given a rough estimate of the frequency, this filter looks at successive windows of approximately 3 - 4 periods of the input waveform. For each window, it computes the least-squares best fit sinusoid.

At each of the positive zero crossings ($\phi = 0$) of the fit, the timestamped values $f_0$, $A$, and $C$ corresponding to the subsequent period are stored. The output stream will have one row of output per period of the input stream. The window sliding algorithm is designed to ensure that zero crossings do not occur near the window boundaries in order to reduce error. The fitted sinusoid is checked against frequency and amplitude limits. If the fit falls outside the given bounds, no data points are inserted into the destination stream for that particular window.

#### General Arguments

- `-u URL`, `--url URL`
  (default: http://localhost/nilmdb/) NilmDB server URL for the source stream.
- `-U DESTURL`, `--dest-url DESTURL`
  (default: same as URL) NilmDB server URL for the destination stream. If unspecified, the same URL is used for both source and destination.
- `-D`, `--dry-run`
  Just print intervals that would be processed, and exit.
- `-F`, `--force-metadata`
  Overwrite destination metadata even if it conflicts with the values in the "metadata" section below.
- `-s TIME`, `--start TIME`
  (default: min) Starting timestamp of data to filter (free-form, inclusive).
- `-e TIME`, `--end TIME`
  (default: max) Ending timestamp of data to filter (free-form, noninclusive).

#### Sinefit Arguments

- `-c COLUMN`, `--column COLUMN`
  Column number in SRCPATH to use for the source data. The first data column is 1.
- `-f FREQ`, `--frequency FREQ`
  (default: 60.0) Rough estimate of the input frequency, used only to determine the size of the
window to analyze and to set defaults for the minimum and maximum frequency. Given an
average sampling rate $fs$ of the input data, the sine wave fit is performed against windows of $N = 3.5 \cdot fs/FREQ$ points.

```plaintext
-m MIN_FREQ, --min-freq MIN_FREQ
  (default: $fest/2$) Minimum valid frequency $fO$ of the fitted sinusoid.
-m MAX_FREQ, --max-freq MAX_FREQ
  (default: $fest - 2$) Maximum valid frequency $fO$ of the fitted sinusoid.
-a MIN Amp, --min-amp MIN Amp
  (default: 20.0) Minimum valid amplitude $A$ of the fitted sinusoid.
```

**SRC PATH**
Path of the raw source stream, for example, /foo/raw.

**DEST PATH**
Path of the fitted output parameters, for example, /foo/sinefit.

**Metadata:** The destination stream has the following metadata keys added:

- **sinefit_source**
  The source stream of the raw data used to fit these parameters.
- **sinefit_column**
  The column number used from the source stream.

---

**Advanced Command Line Tools**

These tools provide low level access to the NLM and are not required for normal system use. Be
very careful running these commands.

**Nilm Database**

The primary NLM database is run as a daemon process and does not require any user interaction.
However the primary database or any other database can be run from the command line using the
`nilmdb-server` command. Like any complex data storage system, NilmDB is subject to corruption
if not shutdown properly. The command line utility `nilmdb-fsck` is designed to verify database
consistency and fix most problems that might arise. The primary cause of database corruption is a
powerloss while the system is recording data. The management daemon automatically runs fsck
when a corrupt database is detected. Therefore, this command should be used only on secondary or
backup databases. To prevent NLM data from over flowing the available space the system
automatically removes old data based off keep settings in `meters.yml`. The cleanup service can be
run manually using `nilm-cleanup`.

```
nilmdb-server - Standalone NilmDB server
```

**Usage**

```
```
Description

Run the standalone NilmDB server. Note that the NilmDB server is typically run as a WSGI process as described in Section 3.1.1.3. This program runs NilmDB using a built-in web server instead.

Arguments

-v, --version
Print the installed NilmDB version.
-a ADDRESS, --address ADDRESS
(default: 0.0.0.0) Only listen on the given IP address. The default is to listen on all addresses.
-p PORT, --port PORT
(default: 12380) Listen on the given TCP port.
-d DATABASE, --database DATABASE
(default: ./db) Local filesystem directory of the NilmDB database.
-q, --quiet
Silence output.

Debug Options

-t, --traceback
Provide tracebacks in the error response for client errors (HTTP status codes 400 - 499).
Normally, tracebacks are only provided for server errors (HTTP status codes 500 - 599).
-y, --yappi
Run under the yappi profiler and invoke an interactive shell afterwards. Not intended for normal operation.

Usage

nilmdb-fsck DATABASE

Description

Check database consistency, and optionally repair errors automatically, when possible. Running this may be necessary after an improper shutdown or other corruption has occurred. This program will refuse to run if the database is currently locked by any other process, like the Apache webserver; such programs should be stopped first.

Arguments

DATABASE
Local filesystem directory of the NilmDB database to check.
-f, --fix
Attempt to fix errors when possible. Note that this may involve removing intervals or data.
-n, --no-data
Skip the slow full-data check. The earlier, faster checks are likely to find most database corruption, so the data checks may be unnecessary.
-h, --help
Print a help message with usage information and details.
-v, --version
Print the installed NilmDB version. Generally, you should ensure that the version of nilmdb-fsck is newer than the NilmDB version that created, or last used, the given database.
**nilm-cleanup** - Clean up old data from streams

**Usage**

```
```

**Description**

Clean up old data from streams, using a configuration file to specify which data to remove. The configuration file is a text file in the following format:

```
1 [/stream/path]
2 keep = 3w # keep up to 3 weeks of data
3 rate = 8000 # optional, used for the --estimate option
4 decimated = false # whether to delete decimated data too
5 [*/prep]
6 keep = 3.5m # or 2520h or 105d or 15w or 0.29y
```

Stream paths are specified inside square brackets ([ ]) and are followed by configuration keywords for the matching streams. Paths can contain wildcards. Supported keywords are:

- **keep**
  - How much data to keep. Supported suffixes are h for hours, d for days, w for weeks, m for months, and y for years.

- **rate**
  - (default: automatic) Expected data rate. Only used by the --estimate option. If not specified, the rate is guessed based on the existing data in the stream.

- **decimated**
  - (default: true) If true, delete decimated data too. For stream path /A/B, this includes any stream matching the wildcard /A/B-decim*.
  - If specified as false, no special treatment is applied to such streams.

**Arguments**

- **-u URL, --url URL**
  - (default: http://localhost/nilmdb/) NilmDB server URL.

- **-y, --yes**
  - Actually remove the data. By default, nilm-cleanup only prints what it would have removed, but leaves the data intact.

- **-e, --estimate**
  - Instead of removing data, print an estimated report of the maximum amount of disk space that will be used by the cleaned-up streams. This uses the on-disk size of the stream layout, the estimated data rate, and the space required by decimation levels. Streams not matched in the configuration file are not included in the total.

**CONFIGFILE**

- Path to the configuration file.

**Notes**

The value keep is a maximum amount of data, not a cutoff time. When cleaning data, the oldest data in the stream will be removed, until the total remaining amount of data is less than or equal to keep. This means that data older than keep will remain if insufficient newer data is present; for example, if new data ceases to be inserted, old data will cease to be deleted.
Nilm Run

NilmRun includes a command line program that allows the server to be run in a standalone mode, using a built-in web server. Additionally, a set of tools is offered for running, listing, and removing processes.

**nilmrun-server** - Standalone NilmRun server

**Usage**

```
```

**Description**

Run the standalone NilmRun server. Note that the NilmRun server is typically run as a WSGI process, as described in Section 3.1.2.3. Running it in standalone mode may be insecure, as no access control or authentication is supported.

**Arguments**

- `-v`, `--version`
  - Print the installed NilmRun version.
- `-a ADDRESS`, `--address ADDRESS`
  - (default: 0.0.0.0) Only listen on the given IP address. The default is to listen on all addresses.
- `-p PORT`, `--port PORT`
  - (default: 12381) Listen on the given TCP port.
- `-q`, `--quiet`
  - Silence output.

**Debug Options**

- `-t`, `--traceback`
  - Provide tracebacks in the error response for client errors (HTTP status codes 400 - 499). Normally, tracebacks are only provided for server errors (HTTP status codes 500 - 599).

**nilmrun-ps** - List processes

**Usage**

```
nilmrun-ps [-h] [-v] [-u URL] [-n]
```

**Description**

List processes on a remote NilmRun server. Shows overall system information as well as detailed information about each process.

**Arguments**

- `-u URL`, `--url URL`
  - (default: http://localhost/nilmrun/) NilmRun server URL. For servers that require authentication, it can be included in the URL in the form http://user:password@host/.
- `-n`, `--noverify`
  - Disable SSL certificate verification.

**Environment Variables**

284
NILMRUN_URL
(default: http://localhost/nilmrun/) The default URL of the NilmRun server.

Output
The output of nilmrun-ps includes overall system information about the number of running processes, CPU usage, and memory usage on the server. Output fields are described below:

**PID**
Process ID.

**STATE**
Process status. This is "alive" if the process is still running, "done" if it has exited successfully, and "error" if it has exited with an error.

**SINCE**
Date and time that the process was started.

**PROC**
Number of operating system processes associated with this NilmRun process.

**CPU**
CPU usage of this process as a percentage of a single CPU core.

**LOG**
Length, in bytes, of the stored output for the process. This output can be retrieved when the process is removed with nilmrun-kill.

Example

```
$ nilmrun-ps
procs: 2 nilm, 157 other
cpu: 29% nilm, 96% other, 200% max
mem: 623 MiB used, 3965 MiB total, 16%
```

```
<table>
<thead>
<tr>
<th>PID</th>
<th>STATE</th>
<th>SINCE</th>
<th>PROC</th>
<th>CPU</th>
<th>LOG</th>
</tr>
</thead>
<tbody>
<tr>
<td>76d81854-feca-11e2-9b2c-000000002559</td>
<td>alive</td>
<td>08/06-15:00:30</td>
<td>2</td>
<td>1337</td>
<td></td>
</tr>
<tr>
<td>8168f08f-feca-11e2-87fe-00000000255c</td>
<td>alive</td>
<td>08/06-15:00:48</td>
<td>1</td>
<td>4505</td>
<td></td>
</tr>
</tbody>
</table>
```

**nilmrun-run** - Run a command on a NilmRun server

**Usage**

```
```

**Description**

Run a command on a NilmRun server. By default, this program will poll the command's output log and display it while waiting for the process to exit.

**Arguments**

- `-u URL`, `--url URL`
  (default: http://localhost/nilmrun/) NilmRun server URL. For servers that require authentication, it can be included in the URL in the form http://user:password@host/.

- `-n`, `--noverify`
  Disable SSL certificate verification.

**Remote Program**
-d, --detach
  Run process and return immediately, without printing the command output. The process must
  be later removed with nilmrun-kill.

CMD [ARG [...]]
  Remote command to execute, with arguments.

Environment Variables

NILMRUN_URL
  (default: http://localhost/nilmdb/) The default URL of the NilmRun server.

```
nilmrun-kill - Kill/remove a process
```

Usage

```
```

Description

Kill or remove a process from the NilmRun server. This terminates all system-level processes that
are running and removes the entry from the NilmRun process listing. Stored log output of the
command, if any, is displayed after the process is removed.

Arguments

-u URL, --url URL
  (default: http://localhost/nilmrn/) Nilmrun server URL. For servers that require authentication, it
can be included in the URL in the form http://user:password@host/.

-n, --noverify
  Disable SSL certificate verification.

Remote Program

-q, --quiet
  Omit display of the command's final output log.

PID [...]  
  One or more process IDs to remove. Process IDs should be those listed by nilmrun-ps.

Environment Variables

NILMRUN_URL
  (default: http://localhost/nilmdb/) The default URL of the Nilmrun server.
Appendix B

Implementation

This appendix contains design files, bill of materials, and selected source code for the hardware associated with this work. There are four sections in this appendix. Appendix B.1 covers the Flex Sensor. The Flex Sensor source code works on the D-Board hardware described in [11] with adjustments to the Makefile as described in the code README. Appendix B.2 covers the NILM Smart Plug. The board design is a drop in replacement for the control PCB in the Belkin WeMo. There are two hardware versions deployed as of this writing. They can be distinguished by the labeling on the front face of the plug. Plugs with “Belkin” work without modification, plugs with “wemo” require a custom interconnect cable described in the assembly section. Appendix B.3 covers the NILM Board, a single board computer designed to run the NILM software. The NILM Board a combined microcontroller and Freescale iMX6 platform that runs the NILM host software. This board uses an analog input channel for the sensor. It is recommended to use a commercial single board computer (eg Raspberry Pi) with the Flex Sensor since this sensor has an onboard ADC and connects over USB. Finally, Appendix B.4 covers server configuration for the currently deployed management cluster. These are implemented on a set of Dell servers running the Xen hypervisor.


Figure B-1: Mylar pickup consists of an FPC connector (left) and four sensors (right)

### B.1 Flex Sensor

The flex sensor integrates multiple magnetic sensors and an electric field sensor with an ARM microcontroller to provide a complete set of non-contact measurements to a NILM system. The sensor uses USB for both power and communication making it easy to connect to any standard computing platform including embedded devices, laptops, and desktop machines. The sensor enumerates as two TTY serial devices. The first serial device is for sensor data and the second interface is for I/O control of the button and LED which is used by embedded NILMs to provide feedback to the end user. Any standard serial program can be used to communicate with the sensor. The software designed in this thesis uses Python’s pySerial package which is an open source serial module available on Window’s, OS X, and Linux platforms.

The hardware consists of two components, the host PCB and a flexible Mylar pickup. The pickup connects to the host board with a friction fit FPC connection. The connection provides electrical connectivity but does not mechanically affix the pickup to the board. An adhesive should be applied to the pickup in order to assure a solid connection with the host PCB. Additionally, it is best practice to passivate both boards to prevent electrical shorts or corrosion of the circuits in a deployed environment.

The following pages present schematics, bills of material and CAD renderings for both the host PCB and Mylar pickup.
Figure B-2: Flexible Mylar pickup

Figure B-3: Flex sensor host PCB
Figure B-4: Flex sensor prototype. The sensor (right) is coated in Plasti Dip for electrical passivation and increased mechanical resilience.
Flex Sensor PCB Design

LED DATA

LED GRN

ATSAM454BA-MU-ND

+5V

IN

OUT

BYRFNC

C1

2

GND

U2

TLV7023

D1

+5V

C4

3

GND

BYRFNC

C5

LED_DATA

100m

U1

28085

VDD

D1

DOUT

Q2

S2312BDE-T1-E3

LED_DATA

+5V

R22

1k

C10

100m

C11

100m

C12

100m

U4B

VDDCORE

VDDCORE

VDDCORE

GND

GND

GND

+5V

Q3

+5V

C4

P80AD4

P81AD5

P82AD6

P83AD7

+5V

R10

10k

R11

10k

R12

10k

J1

VCC

SWDO/TMS

nRESET

SWCLK/TCK

GND

SWOTDDO

TCX00-30P-FP-NL

+5V

C7

100n

C8

100n

C9

100n

+5V

Q5

+5V

C13

2p2

220

168-1-ND

+5V

VDD

VDD

VDD

0.05 Header

+5V

ADVREF

VDDIN

VDDOUT

NRST

NRST

4

GND

GND

GND

WM1.MPC-CT-ND

WM1.MPC-CT-ND

+5V

J5

USB

USB

USB

USB

USB

USB

USB

USB

USB

USB

USB

USB

USB

USB
B.1.2 Selected Firmware Files

Listing B-1: /src/main.c: System initialization and main loop.

```
#include <efc.h>
#include <pmc.h>
#include <sysclk.h>
#include <udi_cdc.h>
#include <wdt.h>
#include <board.h>
#include <pio.h>
#include <twi.h>
#include "analog.h"
#include "buffer.h"
#include "debug.h"
#include "led.h"
#include "usb.h"
#include "pots.h"

void usbledupdate(void);
static void buttonhandler(void);

int main(void) {
    // Switch over to the crystal oscillator
    sysclkinit();
    // Disable the built-in watchdog timer
    wtd_disable(WDT);
    // Board LED's
    //piosetoutput(PIOA,PIOPA7,HIGH,DISABLE,DISABLE);
    //pioset(PIOA,PIO_PA7);
    // Initialize peripherals
    usb_init();
    analog_init();
    led_init();
    // Button
    pmc_enable_periph_clk(IDPIOA);
    pio_set_input(PIOA, BUTTON_PIN, PIO_PULLUP);
    pio_handler_set(PIOA, IDPIOA, BUTTON_PIN, PIO_IT_EDGE, buttonhandler);
    pio_enable_interrupt(PIOA, BUTTON_PIN);
    NVIC_EnableIRQ(PIOAIRQn);
    // Default LED state
    led_set(IO_LED, LED_OFF, 0);
    led_set(DATA_LED,LED_GREEN,0);

    for (;;) {
        // Transmit data if we can
        while(udi_cdc_multi_is_tx_ready(DATA_PORT)) {
            uint16_t data;
            if(pop(&data) != BUFFER_OK) // buffer empty
                break;
            udi_cdc_multi_write_buf(DATA_PORT, &data, sizeof(data));
        }
    }
```
if (bufferfull()) {
    led_set(DATA_LED, LED_RED, 0);
}
// Receive data in our free time
uint8_t c;
// First check DATA_PORT interface
if (udi_cdc_multi_is_rx_ready(DATA_PORT)) {
    c = udi_cdc_multi_getc(DATA_PORT);
    if (c < 0) {
        print("Read error");
    }
    switch(c){
    case DATA_START:
        analog_start();
        led_set(DATA_LED, LED_BLUE, 0);
        break;
    case DATA_STOP:
        analog_stop();
        led_set(DATA_LED, LED_LT_GREEN, 0);
        break;
    case DATA_BOOTLOADER:
        // Clear GPWM to boot from ROM instead of flash
        efc_perform_command(EFC0, EFC_FCMD_GPB, 1);
        break;
    default:
        //led_set(IOLED, LED_BLUE, 0);
        print("unknown command");
    }
    // Next check USERIO_PORT interface
    if (udi_cdc_multi_is_rx_ready(USERIO_PORT)) {
        c = udi_cdc_multi_getc(USERIO_PORT);
        if (c < 0) {
            print("Read error");
        }
        switch(c){
        case IO_RGBLED:
            usb_led_update();
            break;
        default:
            //led_set(IO_LED, LED_BLUE, 0);
            print("unknown command");
        }
    }
}

static void button_handler(void){
    static int b_state = -1; // button starts out unknown
    // grab the USB port
    while(!udi_cdc_multi_is_tx_ready(USERIO_PORT)) {
        // if its pressed AND the state is NOT pressed
        if (pio_get(PIOA, PIO_INPUT, BUTTON_PIN) == 0 && b_state!=1){
            udi_cdc_multi_putc(USERIO_PORT,'p');
            pio_set(PIOA, PIO_PA7);
            b_state = 1; // new state is pressed
        }
        // if its released AND the state is NOT released
        else if(b_state!=0){
            udi_cdc_multi_putc(USERIO_PORT,'r');
            pio_clear(PIOA, PIO_PA7);
            b_state=0; // new state is released
        }
    }
void usb_led_update(void) {
    // expect 4 bytes to specify new LED setting
    // [RED, GREEN, BLUE, BLINK]
    uint8_t red, green, blue, blink;
    while(!udi_cdc_multi_is_rx_ready(USERIO_PORT));
    red = udi_cdc_multi_getc(USERIO_PORT);
    while(!udi_cdc_multi_is_rx_ready(USERIO_PORT));
    green = udi_cdc_multi_getc(USERIO_PORT);
    while(!udi_cdc_multi_is_rx_ready(USERIO_PORT));
    blue = udi_cdc_multi_getc(USERIO_PORT);
    while(!udi_cdc_multi_is_rx_ready(USERIO_PORT));
    blink = udi_cdc_multi_getc(USERIO_PORT);
    led_set(IO_LED, red, green, blue, blink);
}

Listing B-2: /src/analog.c: ADC data capture and digital filtering.

Git repository: http://git.wattsworth.net/nilm/iv-sensor
Filename: /src/analog.c
Revision: master

// ADC runs at 96 kHz per channel. There are 8 channels.
// Data is low-pass filtered by a zero-phase FIR filter which
// passes frequencies below 660 Hz and rejects above 1.5 kHz.
// Result is decimated by 32x and output at 3 kHz per channel.
// Raw ADC values are between 0 and 4095 inclusive.
// We subtract 2048 and the filter applies a DC gain of 8,
// so output values are nominally between -16384 and 16383.
// The filter L-infinity norm is 1.035, so pathological inputs
// can produce outputs ever so slightly outside of this range
// (but they will still fit comfortably in signed 16 bits).

// Frequency Filter gain (/8)
// 60 Hz  0.9967
// 180 Hz  0.9951
// 300 Hz  0.9938
// 420 Hz  0.9915
// 540 Hz  0.9801
// 660 Hz  0.9443
// 1500 Hz  0.0501

#define NUMCHANNELS 8

#include <adc.h>
#include <arm_math.h>
#include <buffer.h>
#include <pio.h>
#include <pmc.h>
#include <sysclk.h>
#include <tc.h>
#include "analog.h"
#include "led.h"
#include "fir_filter.h"

//----------two current production boards----------
#if (D_BOARD)
    // mapping depends on sensor configuration
    static enum adc_channel_num_t channels[NUMCHANNELS] = {4,5,6,7,8,2,9,3};
#else (FLEX_SENSOR)
    static enum adc_channel_num_t channels[NUMCHANNELS] = {0,3,2,9,8,5,4,6};
#endif

295
#error "Define D_BOARD or FLEXSENSOR (see README)"
#endif

// Stage 1: decimate 8 times with a 16-tap FIR.
#define DEC1 8
#define NTAPS1 16
static const ql5_t coeffsl[NTAPS1] = 
    { 2305, 2296, 4354, 6819, 9420, 11818, 13661, 14663, 14663, 13661, 11818, 9420, 6819, 4354, 2296, 2305
};
static q15_t buffer1[NUM_CHANNELS][2*NTAPS1];

// Stage 2: decimate 4 times with a 32-tap FIR.
#define DEC2 4
#define NTAPS2 32
static const q15_t coeffss[NTAPS2] = 
    { 64, 147, 234, 261, 139, -195, -715, -1257, -1529, -1196, 0, 2105, 4880, 7823, 10297, 11710, 11710, 10297, 7823, 4880, 2105, 0, -1196, -1529, -1257, -715, -195, 139, 261, 234, 147, 64
};
static q15_t buffer2[NUM_CHANNELS][2*NTAPS2];

// The output format consists of the eight 16-bit channel values
// followed by the alignment word 0x807F and a 16-bit status word.
// (Note that it is never possible for 0x80 or 0x7F to be the
// most significant byte of the channel value or status word.)
static volatile int fifo_running;
static uint16_t status_mask;
static int fifo_write(uint16_t value) {
    int r = push(value);
    if (r != BUFFER_OK) {
        status_mask |= ERROR_FIFO;
    }
    return r;
}

void analog_init(void) {
    // Enable the switch
    pmc_enable_periph_clk(ID PIOA);
pio_set_input(PIOA, PIO_PA23, PIO_PULLUP);

    // Initialize the ADC
    pmc_enable_periph_clk(ID_ADC);
    adc_init(ADC, sysclk_get_cpu_hz(), 20000000, ADC_STARTUP_TIME_0);
    adc_configure_timing(ADC, 0, ADC_SETTLING_TIME_0, 1); // "fast"

    // Setup ADC channel sequence
    adc_configure_sequence(ADC, channels, NUM_CHANNELS);
    adc_start_sequencer(ADC);
    for (int i = 0; i < NUM_CHANNELS; ++i)
        adc_enable_channel(ADC, i); // by *sequence #, not channel #
    adc_enable_interrupt(ADC, 1 << channels[NUM_CHANNELS-1]);
    NVIC_EnableIRQ(ADC_IRQn);

    // Trigger from timer 0
    pmc_enable_periph_clk(ID_TCO);
tc_init(TCO, 0, TC_CMR_TCLKS_TIMER_CLOCK1 // source clock (CLOCK1 = MCLK/2)
        | TC_CMR_CPCTRIG // up mode with automatic reset on RC match
TC_CMR_WAVE // waveform mode
TC_CMR_ACPA_CLEAR // RA compare effect: clear
TC_CMR_ACPC_SET; // RC compare effect: set
tc_write_ra(TCO, 0, 1);
tc_write_rc(TCO, 0, 625); // frequency = (120MHz/2)/625 = 96 kHz
adc_configure_trigger(ADC, ADC_TRIG_TIO_CH_0, 0);

// Start everything
adc_start(ADC);
tc_start(TCO, 0);
}

void analog_start(void) {
    flush();
    status_mask = 0;
    fifo_running = 1;
}

void analog_stop(void) {
    fifo_running = 0;
    flush();
}

void ADC_Handler(void) {
    static uint32_t sample_index; // counts up forever

    // voltage detection variables
    #define WINDOW_SIZE 1000
    #define VOLTAGE_THRESH 100000
    static int32_t window_index = 0;
    static int32_t last_mean = 0;
    static int32_t raw_bucket = 0;
    static int32_t sgr_bucket = 0;
    static int32_t signed_result = 0;

    for (int i = 0; i < NUM_CHANNELS; i++) {
        q15_t adc = adc_get_channel_value(ADC, channels[i]) - 2048;
        // TODO: make ADC error logging PER-CHANNEL.
        if (adc < -2000 || adc > 2000)
            status_mask |= (1 << i);
        buffer1[i][sample_index & (2*NTAPS1-1)] = adc;
    }

    // Update the switch status
    if (pio_get(PIOA, PIO_INPUT, PIO_PA23) == 0)
        status_mask |= SWITCH_PRESSED;

    // We distribute the computational load of running FIR filters
    // so that the USB interrupt never gets delayed too long.
    // Let N = sample_index. Run stage 1 on channel N % 8.
    // If N % 4 = 0, run stage 2 on channel (N/4) % 8.
    // This computation is hard-coded for NUM_CHANNELS = DEC1.
    // Quantities DEC1, DEC2, NTAPS1, NTAPS2 must be powers of 2.

    // STAGE 1
    int base = (sample_index / DEC1) * DEC1;
    int channel = sample_index & (NUM_CHANNELS-1);
    q15_t result = fir_filter(coeffs1, NTAPS1, buffer1[channel], base);
    buffer2[channel][(base / DEC1) & (2*NTAPS2-1)] = result;

    // STAGE 2
    if (!(sample_index & (DEC2-1))) {
        base = (sample_index / DEC1 / DEC2) * DEC2;
        channel = (sample_index / DEC2) & (NUM_CHANNELS-1);
        result = fir_filter(coeffs2, NTAPS2, buffer2[channel], base);
    }

    // Output result to the FIFO.
If the status word is successfully written, clear it.

```c
if (fifo_running) {
    if (channel == 0) {
        if (fifo_write(0x807F) == BUFFER_OK &&
            fifo_write(status_mask) == BUFFER_OK) {
            status_mask = 0;
        }
    }
    // If the buffer is full, stop writing data to the buffer.
    // The host will have to issue a new "start" command to resume.
    if (fifo_write(result) != BUFFER_OK) {
        fifo_running = 0;
    }
}

//--------voltage detection code-----------
if(channel==0){
    signed_result = result;
    raw_bucket+=signed_result;
    if(last_mean!=0)
        sqr_bucket+=\(\text{signed_result}-\text{last_mean}\)^2\(\text{signed_result}-\text{last_mean}\);
    window_index++;
    if(window_index>=WINDOW_SIZE){
        // run the voltage detection routine
        if(last_mean!=0){
            if((sqr_bucket/\text{WINDOW SIZE})>=\text{VOLTAGE THRESH})
                led_set(GREEN_LED,LED_GRN_ON);
            else
                led_set(GREEN_LED,LED_GRN_OFF);
        }
        // update the mean
        last_mean = raw_bucket/\text{WINDOW SIZE};
    }
    // reset the buckets and index
    raw_bucket = 0;
    sqr_bucket = 0;
    window_index = 0;
}
//--------end voltage detection code--------
++sample_index;
```
# Makefile for Atmel SAM4S using cmsis and GNU toolchain.
# The variables $(SRC), $(INC), $(LIB) are defined in path.mk.
include path.mk

# Object file location and linker script
OBJ = $(SRC:%.c=obj/%.o) $(LIB)
LD_SCRIPT = asf/sam/utils/linker_scripts/sam4s/sam4s4/gcc/%.ld

# Compiler and linker flags. Here be dragons.
CFLAGS += -mlittle-endian -mthumb -mcpu=cortex-m4
CFLAGS += -g -03 $(INC:%=-I%) -std=c99 -Wall
CFLAGS += -DARM_MATH_CM4 -D'_SAM4S4B_ -DBOARD=USER_BOARD'
LFLAGS = $(CFLAGS) -T$(@:bin/%.elf=$(LD_SCRIPT))
LFLAGS += -Wl,--entry=Reset_Handler -Wl,-gc-sections

# Targets
.PHONY: all clean gdb
.SECONDARY: $(OBJ)
all: bin/flash.bin bin/flash.elf

clean:
   -rm -rf obj bin
gdb: bin/flash.elf
   @arm-none-eabi-gdb
bin/%.bin: bin/%.elf
   arm-none-eabi-objcopy -O binary $< $@
gbin/%.hex: bin/%.elf
   arm-none-eabi-objcopy -O ihex $< $@
binary elf: $(OBJ)
   @mkdir -p $(dir $@)
   $(info LD $@)
   @arm-none-eabi-gcc $(LFLAGS) -o $@ $(OBJ)
obj/%.o: %.c
   @mkdir -p $(dir $@)
   $(info CC $<)
   $(@:bin/%.elf=$(OBJ))

B.2 NILM Smart Plug

The NILM smart plug is a retrofitted Belkin WeMo. The stock control PCB is removed and replaced with a custom PCB that adds several additional features. With the custom control PCB the plug can store up to four years of power measurements and accurately timestamp each measurement using a battery backed real time clock. The smart plug connects to a NILM over USB or WiFi and can both transmit power data and receive commands to turn on and off the plug or set the RGB LED to a particular color or pattern. The stock control PCB only reports the power usage of the plug, but the solid state power meter chip (Figure B-7) actually collects many more metrics. The custom control PCB unlocks these additional metrics recording
not only wattage but also line frequency, voltage, current, and power factor. The following figures show the design and construction of the custom PCB and how it fits into the WeMo plug. See Appendix A.2.3 for documentation on configuring and using these smart plugs with a NILM system.
Figure B-7: The WeMo uses a solid state power meter board that communicates with the control PCB by optically isolated UART.

Figure B-8: Assembled smart plug with custom control PCB.
## WEMO Control Board BOM

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<th>Production P/N_NK</th>
<th>Production Description_NK</th>
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Sub-Total 14.37524  
Production loss 0.71876  
Supplier Shipping Cost 0.60000  
**PARTS TOTAL 15.69400**
Cable Pinout for Version 2

* No connection between 7 and 1

Connector: 455-1199-ND
Pin: SZH-002T-P0.5
WEMO Plug Version 1 (original)

Connect with existing cable

WEMO Plug Version 2 (new)

Side B to control board
Side A to plug PCB
B.2.4 Selected Firmware Files

Listing B-4: firmware/src/wifi.c: Driver for ESP8266. AT+ Command logic for wifi interface

Git repository: http://git.wattsworth.net/nilm/wemo-firmware
Filename: firmware/src/wifi.c
Revision: master

```
#include <asf.h>
#include <stdio.h>
#include "string.h"
#include "wifi.h"
#include "monitor.h"
#include "conf_membag.h"

//wifi rx and tx data structures

//resp-buf: uart interrupt fills this buf
// when rx_wait==true & data_tx_status==TX_IDLE
//resp_complete_buf: short string we expect wifi module
// to respond with before the timeout
uint8_t *respbuf=NULL;
uint32_t respbufidx=0;
char *respcompletebuf;

//I/expected response of command to ESP8266
bool rx_wait=false; //we are waiting for response
bool rx_complete=false; //flag set by UART int when rx_complete_str matches

int data_tx_status = TX_IDLE;
//index into incoming data buffer (data from another server)
// this is local to wifi module because the core only gets
// the buffer after the full flag is set
uint32_t wifi_rx_buf_idx = 0;

//**declared in header b/c monitor calls this when NILM IP addr changes
//int wifi_send_ip(void);
int wifi_send_data(int ch, const uint8_t* data, int size);
//try to set the baud to 9600 since they come from the factory at 115200
int wifi_set_baud(void);

int wifi_init(void){
    uint32_t BUFSIZE = MDBUFSIZE;
    uint8_t tmp; //dummy var for flushing UART
    char *buf;
    char *tx_buf;

    if(respbuf==NULL){
        resp_buf=coremalloc(RESPBUFSIZE);
    }
    if( respcompletebuf==NULL){
        respcompletebuf=coremalloc(RESPCOMPLETEBUFSIZE);
    }
    if(wifi_rx_buf==NULL){
        wifi_rx_buf=coremalloc(WIFI_RX_BUFSIZE);
    }
    if (wemo_config.standalone){
        printf("warning: wifi_init called in standalone mode\n");
        return 0;
    }
```

307
I/initialize the memory

buf = core_malloc(BUFSIZE);
tx_buf = core_malloc(BUFSIZE);

// set up the UART

static usart_serial_options_t usart_options = {
   .baudrate = WIFI_UART_BAUDRATE,
   .charlength = WIFI_UART_CHAR_LENGTH,
   .paritytype = WIFI_UART_PARITY,
   .stopbits = WIFI_UART_STOP_BITS
};
gpio_configure_pin(PIO_PA9_IDX, (PIO_PERIPH_A | PIO_DEFAULT));
gpio_configure_pin(PIO_PA10_IDX, (PIO_PERIPH_A | PIO_DEFAULT));
pmc_enable_periph_clk(ID_WIFI_UART);
sysclk_enable_peripheral_clock(ID_WIFI_UART);
usart_serial_init(WIFI_UART,&usart_options);

// flush any existing data
while(usart_serial_is_rx_ready(WIFI_UART)){
   usart_serial_getchar(WIFI_UART,&tmp);
}

// Trigger from timer 0

pmc_enable_periph_clk(ID_TCO);
tc_init(TCO, 0, // channel 0
   | TC_CMRA_CTRL
   | TC_CMRA_CTRL_WAVE // waveform mode
   | TC_CMRA_CTRL_ACPA_SET // RC compare effect: set
   | TC_CMRA_CTRL_ACPB_CLEAR // RA compare effect: clear
);

TC0->TC_CHANNEL[0].TC_RA = 0; // doesn't matter
TC0->TC_CHANNEL[0].TC_RC = 64000; // sets frequency: 32kHz/32000 = 1 Hz
 NVIC_SetPriority(TC0_IRQn,1); // high priority
 NVIC_EnableIRQ(TC0_IRQn);
tc_enable_interrupt(TCO, 0, TC_IER_CPCS);

// reset the module

if(wifi_send_cmd("AT+RST","ready",buf,BUFSIZE,1)==0){
   printf("Error reseting ESP8266\n");
   core_free(buf);
   core_free(tx_buf);
   // if the baud rate was wrong try to set it to 9600
   // wifi_set_baud(); **disabled on production firmware**
   return -1;
}

// set to mode STA

if(wifi_send_cmd("AT+CWMODE=1","OK",buf,BUFSIZE,1)==0){
   printf("Error setting ESP8266 mode\n");
   core_free(buf);
   core_free(tx_buf);
   return 0;
}

// try to join the specified network

snprintf(tx_buf,BUFSIZE,"AT+CWMAP="%s","%s",
         wemo_config.wifi_ssid,wemo_config.wifipwd);
if(wifi_send_cmd(tx_buf,"OK",buf,BUFSIZE,20)==0){
   printf("no response to CWMAP\n");
   core_free(buf);
   core_free(tx_buf);
   return -1;
}

// make sure the response ends in OK
uint8_t len = strlen(buf);
if(len>2 || strcmp(&buf[len-2],"OK")!=0){
   snprintf(tx_buf,BUFSIZE,"failed to join network [%s]: [%s]\n",
            wemo_config.wifi_ssid, buf);
printf(txbuf);
corelog(tx buf);

//f ree memory
core free(buf);
core free(tx buf);
return -1;

}
/see if we have an IP address
wifi sendcmd("AT+CIFSR","OK",buf,BUFSIZE,2);
if(strstr(buf,"ERROR")==buf){
printf("error getting IP address\n");

I/free the memory
corefree(txbuf);
corefree(buf);

return -1;

}
/try

to parse the response into an IP address

I/expect 4 octets but *not* 0.0.0.0
int al,a2,a3,a4;
if(!(sscanf(buf,"+CIFSR:STAIP,\"%d.%d.%d.%d\"",&al,&a2,&a3,&a4)==4 && al!=O)){
printf("error, bad address: %s\n",buf);
//free the memory
corefree(txbuf);
core-free(buf);
return -1;

}

/save

the IP to our config

snprintf(buf,BUFSIZE,"%d.%d.%d.%d",al,a2,a3,a4);
memset(wemoconfig.ipaddr,OxO,MAXCONFIGLEN);
strcpy(wemo config.ipaddr,buf);

/set

the mode to multiple connection

wifi sendcmd("AT+CIPMUX=l","OK",buf,BUFSIZE,2);
/start a server on port 1336
wifi sendcmd("AT+CIPSERVER=1,1336","OK",buf,BUFSIZE,2);
//if we know the NILM IP address, send it our IP
if(strlen(wemoconfig.nilmipaddr)!=O){
if(wifisend_ip()==TX ERR_MODULE_RESET){
return TXERRMODULERESET;

}
}else{
/get the NILM IP address from the manager
/once we know the NILM address we send it ours
coregetnilmipaddr();

aa}
I/log the event
snprintf(buf,BUFSIZE,"Joined [%s] with IP [%s]",
wemoconfig.wifissidwemoconfig.ip_addr);
printf("\n%s\n",buf);
core_log(buf);
//free the memory
core free(tx buf);
corefree(buf);
return 0;
}

1'

1n1

Vc

int wifisendip(void){
int TXBUFSIZE = LGBUFSIZE;
int PAYLOADBUFSIZE = LGBUFSIZE;
int r;
char *tx_buf,*payload_buf;
txbuf = coremalloc(TXBUFSIZE);
payloadbuf = core malloc(PAYLOADBUFSIZE);
snprintf(payloadbuf,PAYLOADBUFSIZE,
"{\ "se rial -numbe r\": \ "%s \", \ ip-add r\": \ %s\ }"
wemoconfig.serialnumber,wemo_config.ipaddr);
snprintf(txbuf,TXBUFSIZE,

309


"POST /config/plugs/update HTTP/1.1\r\n"  
"User-Agent: WemoPlug\r\n"  
"Host: NILM\r\nAccept:*/*\r\n"  
"Connection: keep-alive\r\n"  
"Content-Type: application/json\r\n"  
"\r\n",  
strlen(payload_buf),payload_buf);  
//send the packet!  
r = wifi_transmit(wemo_config.nilm_ip_addr,80,tx_buf);  
core_free(tx_buf);  
core_free(payload_buf);  
return r;  
}  
}

int wifi_set_baud(void){  
core_log("setting ESP8266 baudrate to 9600");  
//reconfigure UART for 115200  
static uart_serial_options_t usart_options = {  
    .baudrate = 115200,  
    .charlength = WIFI_UART_CHAR_LENGTH,  
    .paritytype = WIFI_UART_PARITY,  
    .stopbits = WIFI_UART_STOPBITS  
};  
//send baudrate command  
char* cmd = "AT+CIOBAUD=9600";  
usart_serial_init(WIFI_UART,&usart_options);  
usart_serial_writepacket(WIFI_UART,(uint8_t*)cmd,strlen(cmd));  
//terminate the command  
usart_serial_putchar(WIFI_UART,'\r');  
usart_serial_putchar(WIFI_UART,'\n');  
//wait 1 second  
tc_start(TC0, 0);  
rxWait=true;  
while(rxWait);  
//reconfigure UART for 9600  
usart_options.baudrate = WIFI_UART_BAUDRATE;  
usart_serial_init(WIFI_UART,&usart_options);  
printf("reset baudrate\n");  
}

int wifi_transmit(char *url, int port, char *data){  
int BUFSIZE = MD_BUFSIZE;  
char *cmd;  
char *buf;  
int r;  
//allocate memory  
cmd = core_malloc(BUFSIZE);  
buf = core_malloc(BUFSIZE);  
//sometimes the port stays open, so check for both  
//conditions  
char *success_str = "4,CONNECT";  
char *connected_str = "ALREADY CONNECT";  
//open a TCP connection on channel 4  
snprintf(cmd,BUFSIZE,"AT+CIPSTART=4,\"TCP\"",url,5);  
wifi_send_cmd(cmd,"4,CONNECT",buf,100,5);  
//check if we are able to connect to the NILM  
if strstr(buf,"ERROR\n\nUnlink")==buf{  
printf("can't connect to NILM\n");  
core_free(cmd);  
core_free(buf);  
return TX_BAD_DEST_IP;  
}  
//if we are still connected, close and reopen socket  
if strstr(buf,connected_str)==buf{  
    wifi_send_cmd("AT+CIPCLOSE=4","Unlink",buf,100,1);  
}  
}
now try again

wifi_send_cmd(cmd,"Linked",buf,100,2);
}
//check for successful link
if(strstr(buf,success_str)!=buf){
    printf("error, setting up link\n");
    core_free(cmd);
    core_free(buf);
    return TXERROR;
}
//send the data
if((r=wifisend_txt(4,data))!=0){
    printf("error transmitting data: %d\n",datatxstatus);
    core_free(cmd);
    core_free(buf);
    return r;
}
//connection is closed *after* we receive the server's response
//this is processed by the core and we discard the response
wifi_send_cmd("AT+CIPCLOSE=4","Unlink",buf,100,1);
core_free(cmd);
core_free(buf);
return r; //success!

//**** These are the accessor functions to transmit data ***//
int wifi_send_txt(int ch, const char* data){
    return wifi_send_raw(ch,(uint8_t*)data,strlen(data));
}

int wifi_send_raw(int ch, const uint8_t* data, int size){
    int BUFFER_SIZE=1000;
    int i=0;
    int r;
    char *tx_buf;
    tx_buf = coremalloc(MDBUFSIZE);
    for(i=0;i<size;i+=BUFFER_SIZE){
        if(i+BUFFER_SIZE<size)
            r=wifisend_data(ch,&data[i],BUFFER_SIZE);
        else
            r=wifisend_data(ch,&data[i],size-i);
        if(r!=TX_SUCCESS){ //exit early
            core_free(tx_buf);
            return r; //fail!
        }
    }
    core_free(tx_buf);
    return r;
}

//**** Private method that actually sends data ***//
int wifi_send_data(int ch, const uint8_t* data, int size){
    int cmd buf size = MD_BUF_SIZE;
    char *cmd;
    int timeout = 7; //wait 7 seconds to transmit the data
    //allocate memory
    cmd = coremalloc(cmd buf size);
    snprintf(cmd,cmd buf size,"AT+CIPSEND=%d,%d\r\n",ch,size);
    data tx status=TX_PENDING;
    rx_wait=true;
    resp buf idx = 0;
    memset(resp buf,0x0,RESP_BUF_SIZE);
    memset(wifi rx buf,0x0,WIFI_RX_BUF_SIZE); //to make debugging easier
    wifi rx buf idx=0;
    uart_serial_write_packet(WIFI_UART,(uint8_t*)cmd,strlen(cmd));
    delay_ms(250); //wait for module to be ready to accept data
usart_serial_writepacket(WIFI_UART,(uint8_t*)data,size);

//now wait for the data to be sent
while(timeout>O){
    //start the timer
    tc_start(TCO, 0);
    //when timer expires, return what we have in the buffer
    rx_wait=true; //reset the wait flag
    while(rx_wait && data_tx_status!=TX_SUCCESS);
    tc_stop(TCO,0);
    //the success flag is set *before* we receive the server's response
    //core_process_wifi_data receives the response but discards it
    if(data_tx_status==TX_SUCCESS){
        data_tx_status=TX_IDLE;
        rx_wait = false;
        //free memory
        core_free(cmd);
        return TXSUCCESS;
    }

    timeout--;
}

//check if this is a timeout error
if(strlen((char*)resp-buf)==0){
    printf("timeout error\n");
    core_log("timeout error");
    data_tx_status = TX_TIMEOUT;
} else if(strcmp((char*)resp_buf,"\r\nready\r\n")==0){
    //module reset itself!!!
    printf("detected module reset\n");
    core_log("module reset");
    data_tx_status = TX_ERR_MODULE_RESET;
} else { data_tx_status=TX_ERROR;
    core_log("TX error: ");
    core_log((char*)resp_buf);
    data_tx_status = TX_ERROR;
}

//free memory
core_free(cmd);
return data_tx_status;

int wifi_send_cmd(const char* cmd, const char* resp_complete, char* resp, uint32_t maxlen, int int timeout){
    uint32_t rx_start, rx_end;
    //clear out the response buffer
    memset(resp,0x0,maxlen);
    memset(respbuf,0x0,RESPBUFSIZE);
    //setup the rx complete buffer so we know when the command is finished
    if(strlen(resp_complete)>RESPocomplete_BUF_SIZE-3){
        printf("resp_complete, too long exiting\n");
        return -1;
    }
    strcpy(resp_complete_buf,resp_complete);
    strcat(resp_complete_buf,\"\n\n\n");
    //enable RX interrupts
    usart_enable_interrupt(WIFI_UART, US_IER_RXRDY);
    NVIC_SetPriority(WIFI_UART_IRQn,2);
    NVIC_EnableIRQ(WIFI_UART_IRQn);
    //write the command
    rx_wait=true; //we want this data returned in resp_buf
    rx_complete =false; //reset the early complete flag
    usart_serial_writepacket(WIFI_UART,(uint8_t*)cmd,strlen(cmd));
    //terminate the command
    usart_serial_putchar(WIFI_UART,\'\r\');
struct uart_config
{
    int baudrate;
    char parity;
    int stopbits;
    int data_bits;
    int flowcontrol;
    char *device_file;
};

uart *uart_new(struct uart_config *config)
{
    uart *u = (uart *)malloc(sizeof(uart));
    if (u == NULL)
        return NULL;

    u->config = *config;
    u->status = UART_INIT;
    u->transmit_buffer = (char *)malloc(u->config->baudrate);
    if (u->transmit_buffer == NULL)
        free(u);
    return u;
}

uart *uart_init(uart *u, int fd)
{
    int res;

    if ((res = ioctl(fd, TIOCFanity, 0)) == -1)
        return NULL;

    u = uart_new(&u->config);
    if (u == NULL)
        return NULL;

    u->fd = fd;
    return u;
}

uart *uart_open(void)
{
    return uart_init(uart_new(&uart_config), 0);
}

uart *uart_close(uart *u)
{
    if (u == NULL)
        return NULL;

    if (u->fd != 0)
    {
        close(u->fd);
        free(u->transmit_buffer);
    }

    free(u);
    return NULL;
}

int uart_putchar(uart *u, int c)
{
    if (u == NULL)
        return -1;

    // Wait for the UART to be idle
    while (uart_get_status(u) & UART_BUSY)
        continue;

    // Write the character to the UART buffer
    if (uart_putchar(u, c) == 0)
        return 0;

    // Wait for the character to be transmitted
    while (uart_get_status(u) & UART_TRANSMITTING)
        continue;

    return 1;
}

int uart_putchar(WIFI_UART, '\n');

// Wait for [timeout] seconds
while(timeout>0){
    // Start the timer
    tc_start(TCO, 0);
    // When timer expires, return what we have in the buffer
    rx_wait=true; // Reset the wait flag
    while(rx_wait);
    tc_stop(TCO,0);
    if(rx_complete) // if the uart interrupt signals rx is complete
        break;
    timeout--;
}
// Now null terminate the response
resp_buf[resp_buf_idx]=0x0;
// Remove any ECHO
if(strstr((char*)resp_buf,cmd)!=(char*)resp_buf){
    printf("bad echo: %s\n",resp_buf);
    return 0;
}

rx_start = strlen(cmd);
// Remove leading whitespace
while(resp_buf[rx_start]=='\r'||resp_buf[rx_start]=='\n')
    rx_start++;
// Remove trailing whitespace
rx_end = strlen((char*)resp_buf)-1;
while(resp_buf[rx_end]=='\r'||resp_buf[rx_end]=='\n')
    rx_end--;
// Make sure we have a response
if(rx_end<=rx_start){
    printf("no response by timeout\n");
    return 0;
}

// Copy the data to the response buffer
if((rx_end-rx_start+1)>maxlen){
    memcpy(resp,&resp_buf[rx_start],maxlen-1);
    resp[maxlen-1]=0x0;
    printf((char*)resp_buf);
    // Truncated output!
}
else{
    memcpy(resp,&resp_buf[rx_start],rx_end-rx_start+1);
    // Null terminate the response buffer
    resp[rx_end-rx_start+1]=0x0;
}
return rx_end-rx_start;

ISR(TCO_Handler)
{
    // Clear the interrupt so we don't get stuck here
    tc_get_status(TCO,0);
}

ISR(UART0_Handler)
{
    uint8_t tmp, i;
    // State machine vars for handling RX'd data
    static int rx_bytes_recvd = 0;
    static bool rx_in_prog = false;
    static int rx_bytes_expected = 0;
    static int rx_chan = 0;
    char *action_buf;
    int ACTION_BUF_SIZE = MD_BUF_SIZE;
usart_serial_getchar(WIFI_UART,&tmp);
//if debug level is high enough, print the char
if(wemo_config.debug_level>=DEBUG_INFO)
coreputc(NULL,tmp);
//check whether this is a command response or
//new data from the web (unsolicited response)
if(rx_wait && data_tx_status==TX_PENDING){
if(resp_buf_idx==RESP_BUF_SIZE){
printf("error!\n");
return; //ERROR!!!!!
}
resp_buf[resp_buf_idx++]=(char)tmp;
//check for completion_str to indicate completion of command
//this is just a speed up, we still timeout regardless
//of whether we find this string
if(resp_buf_idx>4){
if(strlen((char*)resp_buf,resp_complete_buf)==
(char*)&resp_buf[resp_buf_idx-strlen(resp_complete_buf)]){
rx_complete = true; //early completion!
rxd = false;
}
}
else if(rx_wait && data_tx_status==TX_PENDING){
//we are transmitting, no need to capture response,
//after transmission we receive SEND OK\n, responses
//are captured by wifi_rx_buf and processed by the core
//just wait for SEND OK\n, use a 9 char circular buffer
if(resp_buf_idx<8){
for(i=0;i<8;i++)
resp_buf[i]=resp_buf[i+1];
resp_buf[8]=tmp;
if(strlen("SEND OK\n",(char*)resp_buf)==
data_tx_status==TX_SUCCESS;
}
else{ //data_tx_status == TX_IDLE
//this is unsolicited data, incoming from Internet,
//process into wifi_rx_buf and pass off to the core
//when the reception is complete
if(wifi_rx_buf_full){
printf("error, wifi_rx_buf must be processed by main loop!\n");
return; //ERROR!!!!
}
if(wifi_rx_buf_idx==WIFI_RX_BUF_SIZE){
printf("too much data, wifi_rx_buf full!\n");
//empty the buffer
wifi_rx_buf_idx = 0;
return; //ERROR!!!!
}
//store the data in the rx buffer
wifi_rx_buf[wifi_rx_buf_idx++]=(char)tmp;
//if a reception is in progress...
if(rx_in_prog){
rx_bytes_recvd++;
if(rx_bytes_recvd==rx_bytes_expected){
//data is ready for processing, set flag so main loop
//runs core_process_wifi_data
wifi_rx_buf_full=true;
wifi_rx_buf_idx=0;
rx_in_prog = false;
return;
}
}
//otherwise check for control sequences....
if(wifi_rxbuf_idx>6 && !rx_in_prog){
    //check for incoming data
    char dummy;
    if(sscanf(wifi_rxbuf,\"\r\n+IPD,%d,%d:%c\", 
        &rx_chan,&rx_bytes_expected,&dummy)==3){
        rx_in_prog = true;
        rx_bytes_recvd = 1; //reset the RX counter so we know when we have all the data
        return;
    }
    //check for link and unlink
    actionbuf = core_malloc(ACTION_BUFSIZE);
    if(sscanf(wifi_rxbuf,\"%d,%s\r\n\",&rx_chan,actionbuf)==2){
        if(strcmp(actionbuf,\"CONNECT\")==0){
            core_wifi_link(rx_chan);
            wifi_rxbuf_idx=0;
        }
        else if(strcmp(actionbuf,\"CLOSED\")==0){
            core_wifi_unlink(rx_chan);
            wifi_rxbuf_idx=0;
        }
    }
    if(wifi_rxbuf_idx>20){
        if(strcmp(&wifi_rxbuf[wifi_rxbuf_idx-2],\"\r\n\")==0){
            wifi_rxbuf_idx = 0;
            printf("flushed wifi_rxbuf, out of sync\n");
        }
    }
    core_free(actionbuf);
    return;
}

//****NOTE: error when startup misses a character so wifi_rxbuf is out of sync**
flag is set

***************/

power_sample wemo_sample;
uint8_t wemo_buffer[30];
//take 30 byte buffer from WEMO and fill power sample struct
uint8_t process_sample(uint8_t *buffer);

void wemo_init(void){
//allocate memory for the server buffer
//set up the power meter UART
static usart_serial_options_t usart_options = {
  .baudrate = WEMO_UART_BAUDRATE,
  .charlength = WEMO_UART_CHAR_LENGTH,
  .paritytype = WEMO_UART_PARITY,
  .stopbits = WEMO_UART_STOP_BITS
};
gpio_configure_pin(PIO_PB2_IDX, (PIO_PERIPH_A | PIO_DEFAULT));
pmc_enable_periph_clk(ID_WEMO_UART);
sysclk_enable_peripheral_clock(ID_WEMO_UART);
usart_serial_init(WEMO_UART,&usart_options);
NVICSetPriority(WEMO_UART_IRQ,4); //lowest priority
NVIC_EnableIRQ(WEMO_UART_IRQ);
}

uint8_t process_sample(uint8_t *buffer){
//process 30 byte data packet buffer
uint8_t checksum = 0;
uint8_t bytes[3];
int32_t vals[9];
int i;
//1.) check for header and length
if(buffer[0]!=0xAE || buffer[1]!=0x1E){
  return false;
}
//2.) compute checksum
for(i=0;i<29;i++){
  checksum += buffer[i];
}
checksum = (-checksum)+1;
if(checksum!=buffer[29]){ //check checksum
  core_log("bad checksum");
  return false;
}
//3.) Parse raw data into values
  // Data is 3 byte signed LSB
for(i=0;i<9;i++){
  bytes[0] = buffer[3*i+2];
  bytes[1] = buffer[3*i+3];
  bytes[2] = buffer[3*i+4];
  if((bytes[2]&0x80)==0x80){ //sign extend top byte
    vals[i] |= 0xFF<<24;
  }
} //4.) Populate the power struct
wemo_sample.vrms = vals[2];
wemo_sample.irms = vals[3];
wemo_sample.watts= vals[4];
wemo_sample.pavg = vals[5];
wemo_sample.pf = vals[6];
wemo_sample.freq = vals[7];
wemo_sample.kwh = vals[8];
//5.) Set the valid flag
B.3 NILM Software Stack

The NILM software stack can run on a wide variety of hardware platforms from commodity desktop and laptop machines to low cost embedded single board computers (SBC). There are two main variants of the software stack: standalone and embedded. The standalone suite is designed for relatively high power desktop or laptop machines with a keyboard, mouse and monitor. This configuration provides a local distribution of NILM Manager for data visualization and control which means there is no dependency on an Internet connection.

The embedded version is a stripped down software stack optimized to run on...
resource constrained embedded systems. This variant does not have a local distribution of NILM Manager and must have a network connection to a NILM Manager instance in order to run. Embedded systems usually do not have input/output devices like a mouse, keyboard, or monitor, so this stack uses a locally hosted web page for configuration. When the system is in configuration mode, users can connect to the “Wattsworth Config” ssid and visit www.wattsworth.net to view and edit the system settings. The flex sensor LED indicates the state of the system. The colors are as follows:

**Solid Green** Normal operation: System is in run mode, and securely connected to a NILM Manager server

**Blinking Red** Error: System is in run mode but has a configuration error

**Blinking Orange** Busy: System is booting or switching between modes

**Solid Blue** Configuration mode. Connect to “Wattsworth Config” WiFi network to manage the system.

The flex sensor button is used for basic input tasks. When the system is in run mode, press the button once to transition to configuration mode. Press and hold the button for three seconds to shut down the system. When the system is shutting down, the LED will blink red quickly. When the LED turns off it is safe to unplug the system.

The standalone software stack has been verified on Ubuntu 14 LTS. The core data capture, analysis and storage software has been verified on Ubuntu 15. Currently the NILM Manager software only runs on Ubuntu 14. The embedded stack is tightly coupled to the hardware platform and has been deployed on a custom built single board computer as well as the Raspberry Pi 2 (Figure B-9). The custom single board computer was designed as a reference embedded NILM, but as commercial single board computers have improved this has reduced the need for a custom design. The full schematics and bill of materials for the custom NILM Board are included at the end of this appendix for completeness.
B.3.1 Data Capture

The NILM software stack is primarily designed to capture and store data collected by contact or non-contact (flex sensor) power meters. Both the standalone and embedded stacks implement a similar data capture service illustrated in Figure B-10. The source code for all data capture processes can be found in /opt/nilmcapture. All file names listed in this section are relative to this folder. When the system boots, the OS spawns a supervisor process (nilmcapture/supervisor.py). The supervisor loads the system configuration from the meters.yml file, and spawns a capture process (nilmcapture/captured.py) for each meter that is present and calibrated. If any capture process stops due to an error, the supervisor tries to restart it. If all of the capture processes fail, the supervisor assumes the database is corrupt and runs nilmdb-fsck before restarting the capture processes.

B.3.1.1 Standalone Capture

The capture processes differ between the standalone and embedded implementations. The standalone software supports both contact and non-contact sensors and also allows storing more types of data than the embedded implementation. This section covers the standalone capture and the following section covers the embedded capture. Figure B-10 shows the standalone capture implementation. The capture process first
Figure B-10: NILM data capture. The supervisor process manages a capture process for each meter on the NILM.

creates a data reader object. The class of this reader depends on whether the meter is contact (ethernet_sensor) or non-contact (usb_sensor). The capture process starts the reader as a new process and runs in a loop requesting blocks of data from the reader as it becomes available. Each block runs through several data processing stages. The raw (ADC counts) data is first reconstructed to current (amps) and voltage (volts). For a contact sensor the conversion values are specified in meters.yml, and for a non-contact sensor these values are calculated during calibration. The reconstruct function is implemented in nilmcapture/reconstructor.py. The data is then passed through sinefit (/opt/nlmttools/nlmttools/sinefit.py) to detect the line frequency and zero crossings. Both the reconstructed data and the sinefit data are then passed to prep. Prep (nilmcapture/auto_prepper.py) is implemented as a stateful object instead of a NILM filter to facilitate streaming decimation. The algorithm is identical to the NILM filter version found in /opt/nlmttools/nlmttools/prep.py.
The result of each data processing step can be optionally inserted into the database depending on the settings in meters.yml.

On average, the capture process consumes data faster than it arrives (a requirement for realtime processing), but it only polls for new data once it has finished processing a block. Depending on the system architecture the kernel may not have sufficient internal buffers to store incoming sensor data while the capture process is working on a block. To prevent a buffer overflow in the kernel, capture relies on a reader object to continuously poll the kernel for sensor data. The reader has sufficient buffer space to hold the data until capture is ready for it. The reader implementations are discussed below.

**Contact Sensor**  Figure B-11a illustrates the reader structure for contact sensors.

The contact sensors use a LabJack UE9 data acquisition board. Following the diagram
from the bottom up, data acquisition board connects to the NILM via Ethernet. The kernel’s network drivers expose the connection as a device node to user space. A pre-compiled binary, ethstream, connects to the board using a socket to the device node and streams data from it. The reader spawns a thread that continuously polls ethstream for new data. This data is accumulated in a thread-safe queue. capture retrieves data from the reader by calling the get_block function which dequeues a block of data. If a sensor error has occurred the reader returns a None element to capture which causes it to shut down. The supervisor detects this and restarts the capture process which in turn re-initializes the sensor to clear the error. The only error that is likely to occur is a buffer overrun which happens when the reader thread is not polling the sensor frequently enough. This indicates that the system has too many processes running. If this happens frequently, reduce the number of processes running (eg NILM filters or analyzers), or switch to a faster hardware platform.

Non-contact Sensor Figure B-11b illustrates the reader structure for non-contact sensors. The data flow is similar to the contact sensor reader described above. The main difference is that the non-contact sensors connect to the NILM by USB instead of Ethernet. Like Ethernet, the kernel drivers expose the connection as a device node to user space. However instead of a network connection, the device is a serial line (TTYACM). The reader polling thread connects to the device node using the pySerial module included in the default Python installation. The rest of the data flow is identical to the contact sensor.

B.3.1.2 Embedded Capture

The data capture process is structured differently in the embedded software stack because embedded systems do not have the processing power to run a full sinefit and prep toolchain in Python. The embedded stack uses a similar supervisor but has a different capture process as illustrated in Figure B-12. A separate compiled binary written by David Lawrence runs the prep algorithm directly on the sensor data. This “s-prep” data is fed into the capture process by block. Since the prep transform is
if (not streams_exist?): build_streams(meter_config)

reader = run("sensor_prep")
# runs as long as sensor keeps sending data
for block in reader:
    # unit voltage vector
    \[ \mathbf{v} = \mathbf{v}/|\mathbf{v}| \]
    # unmix currents with calibration matrix
    pq_currents = sensors*cal_matrix
    # rotate P and Q by calibrated sinefit angle
    pq_currents += sinefit_angles
    # align to voltage vector
    pq_currents /= \mathbf{v}
    # save data to prep stream
    insert(prep_stream, pq_currents)

Figure B-12: Embedded data capture

linear, the calibration matrix can be applied directly to s-prep with the same result as if it was applied to the time domain sensor data. The advantage of applying the calibration to s-prep is that this stream arrives at a much lower data rate than the time domain data (60 Hz vs 3kHz). Two rotations are then applied. The ratio of P and Q for each phase are corrected by the sinefit rotation angle computed during calibration, and the ratio of P and Q is aligned to the electric field sensor. This pair of rotations is equivalent to running sinefit.

The prep output is stored in the database. Unlike the standalone software stack, there is no option to store intermediate data streams like raw or sinefit as these are never directly computed.
B.3.2 Embedded Management

The embedded stack runs a global management daemon which controls the system operation. This daemon is illustrated in Figure B-13. When the system boots this daemon is started automatically (in the standalone stack the supervisor is started automatically).

**Configuration** The daemon first checks to see if the system has been configured. If not, it switches to configuration mode and starts a WiFi access point at “Wattsworth Config”. The user connects to the access point and configures the system with information about the wireless network to use (SSID and password), a name and description of the installation, and an e-mail to associate with the NILM owner. Once this information is entered, the daemon restarts the system.

**Network Setup** If the daemon detects that the configuration values are present and valid, it attempts to connect to the specified network. If this is unsuccessful, it sets the flex sensor LED to blinking red and waits for the user to press the flex sensor button to enter to configuration mode.

**Registration** If the network connection is successful, the daemon sets up an encrypted virtual private network (VPN) with the NILM Manager server. The keys for this connection are pre-installed on the system. Once it has joined the VPN, the daemon checks to see if the NILM has been registered with the manager. If this is the first time the NILM has connected to the manager, it registers by sending the e-mail address of the NILM owner as entered by the user during system configuration. The manager then associates the NILM with the user’s account. If the e-mail does not belong to an existing account, the manager sends the user an e-mail with instructions how to create an account and claim the NILM.

**Calibration** After connecting to the NILM Manager server, the daemon checks if its meters have been calibrated. If not, it starts a calibration server instance and waits for the user to connect the NILM Manager to begin the calibration.
If the meters are calibrated, the daemon starts the supervisor process described in Appendix B.3.1.
System Boots

wattsworthd.py

restart on configuration complete

configured? no local access point with DNS wattsworth.net → localhost

yes

configure network interfaces

connected? no Flash red LED

yes join VPN at vpn.wattsworth.net using pre-installed certificates

registered? no POST owner e-mail to www.wattsworth.net

yes

calibrated? no owner has account?

run calibration server

calibration complete

yes run supervisor.py

associate NILM with user account

create account and send e-mail

no

4

yes

Figure B-13: Embedded system management

326
Network and USB

Gigabit Ethernet

USB Host

Bypass Caps for Micro and SDRAM

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Date: 4/22/2016
File: C:Users\NTWK_USB.SchDoc
Drawn By: 3 4 5 6
**NOTE THIS IS THE WRONG CHIP** Use XMEGA128A1U
STORAGE

mSATA

SD Card

uSD Card: bootable volume, not user accessible
SD Card: auxiliary storage, user accessible
mSATA: auxiliary storage, not user accessible
### NILM Board BOM

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**Total:** $354.90 USD
**B.4 Server Architecture**

Creating a secure and reliable infrastructure to manage the remote energy monitors requires more than a web server with VPN software. NILM Manager is in fact a cluster of seven separate servers, illustrated on the following page. These servers work together to provide a complete suite of management tools. In our experimental implementation, these servers run as virtual machines (VM’s) on two Dell R320 servers with Xen hypervisor. All VM’s are paravirtualized Ubuntu 14.0 images. The servers are named according to their roles, described next.

**B.4.1 Firewall**

The firewall is the only machine with a public network connection. Incoming traffic is analyzed against a set of rules that determines whether the particular packet is allowed and where it should be routed. The firewall VM does not run any services itself making it easier to secure against attack.

**B.4.2 Backbone**

The backbone manages communication between servers in the management node and remote NILM’s. NILM’s authenticate with the backbone using SSL certificates. Certificates (unlike passwords) allow for two-way authentication meaning NILM’s verify the identity of the management node and vice versa. This prevents impostor management nodes from accessing NILM’s and rogue NILM’s from accessing the management node. Once a NILM authenticates, the backbone assigns it an IP address and hostname which uniquely identifies it on the VPN. Other servers on the management node can access the NILM by requesting its IP address from the backbone using a domain name resolution service (DNS).
B.4.3 Web

The web server hosts the NILM Manager website. The firewall directs all inbound HTTP requests to this VM using port address translation. This protects the web server from unsolicited (and potentially malicious) traffic. One of the advantages to deploying the web server in a VM is that resources can be scaled with user demand. If web traffic increases, the Xen Hypervisor can reassign processor cores and memory to handle the additional load [81].

B.4.4 Metrics

Metrics runs Nagios [60] and Ganglia [82] monitoring services. Nagios periodically checks the health of remote NILM’s and Ganglia provides a trending report of memory usage, CPU load, and other metrics for each NILM machine. This enables rapid detection and diagnosis of faults in deployed NILM systems. Additionally it provides profiling information that helps in designing hardware for future NILM’s based on their real world usage.

B.4.5 Archive

Archive holds NILM data for long term storage. This server is used to backup valuable data sets collected by deployed NILM’s. The archive server is useful for testing and evaluating different data processing techniques as the machine has significant hardware resources as well as a reliable network connection (neither of which can be assumed for remote NILM’s).

B.4.6 Devops

Devops (a portmanteau of “development” and “operations”) provides configuration management for remote NILM’s. All of the settings, packages, and scripts needed by a NILM are stored on this server using Puppet, an open source management tool [83]. Puppet automatically mirrors updates to these files to every NILM on the VPN ensuring they have consistent and up-to-date configurations. Without such a
service any update to a setting or script would have to be manually applied to each NILM- a tedious and error prone process.

**B.4.7 Git**

This server hosts git repositories [84] for all the software developed for NILM’s and NILM Manager. Git provides version controlled storage and enables collaborative work on the NILM code base.

Together these servers create a reliable and secure infrastructure for managing NILM systems. They permit access to remote database storage located at different monitoring sites. Visualizations or other results of data analysis can be returned from a remote monitor. Python or Octave-style analysis code can be transmitted to remote monitors to provide new analytical capabilities or requests. In both directions, network bandwidth is minimized, as large data streams never have to be transmitted from the remote monitoring sites. The next two sections describe how this infrastructure makes it possible to view and process almost unlimited amounts of NILM data with very little exchange of information over a network.
Physical Hardware

Physical Servers implement a private cloud using XEN

Private Cloud

Network  | ip subnet  | DNS space
----------|------------|------------
LAN       | 10.10.0.X/24 | *.vpn.wattsworth.net
NILM's    | 10.10.1.X/24 | *.nilm
admin     | 10.10.100.X | -

New NILM vpn is 10.10.2.X/24 under subdomain *.vpn.wattsworth.net
Each NILM is assigned a domain name nilm000X where X-hex character that is installed in bind when the NILM is registered to the VPN

firewall  | 10.10.0.1
metrics   | 10.10.0.2
git       | 10.10.0.3
dnsmasq   | 10.10.0.16
nilm-archive | 10.10.0.14
backbone  | 10.10.0.15
web       | 10.10.0.14
mail      | 10.10.0.5
archive   | 10.10.0.6
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