

$$1. \quad E(\vec{v}, \vec{r}) = \frac{1}{2} m \vec{v} \cdot \vec{v} + \frac{1}{2} \alpha x^2 + \frac{1}{2} \beta (y - y_0)^2$$

$$p(\vec{v}, \vec{r}) \propto e^{E(\vec{v}, \vec{r})/kT}$$

FACTORS INTO A PRODUCT OF TERMS,  
EACH OF WHICH CAN BE NORMALIZED BY INSPECTION

$$p(\vec{v}, \vec{r}) = \left[ \frac{1}{\sqrt{2\pi kT/m}} e^{-\frac{v_x^2}{2kT/m}} \right] \left[ \frac{1}{\sqrt{2\pi kT/m}} e^{-\frac{v_y^2}{2kT/m}} \right] \left[ \frac{1}{\sqrt{2\pi kT/m}} e^{-\frac{v_z^2}{2kT/m}} \right] \\ \times \left[ \frac{1}{\sqrt{2\pi kT/\alpha}} e^{-\frac{x^2}{2kT/\alpha}} \right] \left[ \frac{1}{\sqrt{2\pi kT/\beta}} e^{-\frac{(y-y_0)^2}{2kT/\beta}} \right] \left[ \frac{1}{L} \right]$$

$$a) \quad p(v_x) = \frac{1}{\sqrt{2\pi kT/m}} e^{-\frac{v_x^2}{2kT/m}}$$

$$b) \quad p(y) = \frac{1}{\sqrt{2\pi kT/\beta}} e^{-\frac{(y-y_0)^2}{2kT/\beta}}$$

{ BECAUSE THE Z INTEGRAL  
IS OVER p NOT v.

$$c) \quad Z_1 = (2\pi kT)^{5/2} (\alpha \beta m^3)^{-1/2} L m^3 / h^3, \quad Z(N, L, T) = Z_1^N / N!$$

$$d) \quad F = -kT \ln Z \quad \bar{F} = \frac{\partial F}{\partial L} \Big|_{N, T} = -\frac{kT}{Z} N \frac{Z}{L} = -\frac{NkT}{L}$$

$$\bar{F} \text{ IS DEFINED AS A TENSION} \Rightarrow \underline{f_z = -\bar{F} = \frac{NkT}{L}}$$

$$e) \quad S = -\frac{\partial F}{\partial T} \Big|_{N, L} = k \ln Z + kT \frac{1}{Z} \frac{\partial Z}{\partial T} = k \ln Z + \frac{5}{2} N k$$

THUS CONSTANT S (ADIABATIC)  $\Rightarrow$  CONSTANT Z

$$\Rightarrow T_i^{5/2} \beta_i^{-1/2} = T_f^{5/2} \beta_f^{-1/2}$$

$$\underline{T_f = T_i \left( \beta_f / \beta_i \right)^{1/5}}$$

(2)

$$2. \quad V = V_1 e^{(T/T_1 - P/P_1)} \rightarrow \ln V/V_1 = T/T_1 - P/P_1$$

$$P(T, V) = P_1 (T/T_1 - \ln(V/V_1))$$

$$a) \quad dS = \left. \frac{\partial S}{\partial T} \right|_V dT + \left. \frac{\partial S}{\partial V} \right|_T dV$$

$$\delta Q = T dS \Rightarrow C_V = T \left. \frac{\partial S}{\partial T} \right|_V \rightarrow \left. \frac{\partial S}{\partial T} \right|_V = C_V/T = DT^2$$

$$\left. \frac{\partial S}{\partial V} \right|_T = \left. \frac{\partial P}{\partial T} \right|_V \quad (\text{USING A MAXWELL RELATION}) = P_1/T_1$$

$$dS = DT^2 dT + (P_1/T_1) dV$$

$$S = \frac{1}{3} DT^3 + f(V), \quad f'(V) = \frac{P_1}{T_1} \Rightarrow f(V) = \frac{P_1 V}{T_1} + \text{CONSTANT}$$

$$\underline{S = \frac{1}{3} DT^3 + P_1 V/T_1 + S_0}$$

$$b) \quad C_P = \left. \frac{\delta Q}{dT} \right|_P = T \left. \frac{\partial S}{\partial T} \right|_P \quad \text{BUT WE HAVE } dS \text{ ABOVE}$$

$$\left. \frac{\partial S}{\partial T} \right|_P = \underbrace{\left. \frac{\partial S}{\partial T} \right|_V}_{DT^2} + \underbrace{\left. \frac{\partial S}{\partial V} \right|_T}_{P_1/T_1} \underbrace{\left. \frac{\partial V}{\partial T} \right|_P}_{V/T_1}$$

$$\underline{C_P = \underbrace{DT^3}_{C_V} + \frac{P_1 V T}{T_1^2}}$$

$$c) \quad dF = -S dT - P dV$$

$$\underline{dF = \left(-\frac{1}{3} DT^3 - \frac{P_1 V}{T_1} + S_0\right) dT + P_1 \left(-\ln V/V_1 - T/T_1\right) dV}$$

3. a)

$$\Delta Q_S = -\Delta Q_L$$

$$\int_{T_0}^{1/2} bT^{-2} dT = -\int_1^{1/2} aT^3 dT$$

$$-b \left[ \frac{1}{T} \right]_{T_0}^{1/2} = -\frac{a}{4} \left[ \frac{1}{4} - 1 \right]$$

$$\left(2 - \frac{1}{T_0}\right) = \frac{1}{4} \frac{a}{b} \left(\frac{1}{16} - 1\right) = -\frac{1}{4} \frac{a}{b} \frac{15}{16} = -\frac{1}{4} \frac{128}{15} \frac{15}{16} = -2$$

$$\frac{1}{T_0} = 4, \quad \underline{T_0 = 1/4}$$

b)

$$\Delta S = \Delta S_S + \Delta S_L$$

$$dS = \frac{dQ}{T} = \frac{c dT}{T}$$

$$= \int_{T_0}^{1/2} bT^{-2} dT + \int_1^{1/2} aT^2 dT$$

$$= -\frac{b}{2} \left[ \frac{1}{T} \right]_{1/4}^{1/2} + \frac{a}{3} \left[ \frac{1}{3} T^3 \right]_1^{1/2}$$

$$= -\frac{b}{2} \underbrace{(4-16)}_{-12} + \frac{a}{3} \underbrace{\left(\frac{1}{8} - 1\right)}_{-7/8} = \underline{6b - \frac{7}{24}a}$$