

1.

$$\vec{\nabla}^2 p = \frac{1}{c^2} \frac{\partial^2 p}{\partial t^2}$$

$$\begin{aligned} \text{L.H.S.} &= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial p}{\partial r} \right) \\ \frac{\partial p}{\partial r} &= \frac{\partial}{\partial r} \left(\frac{A}{r} e^{-i(kr-\omega t)} \right) \\ &= \left(-\frac{A}{r^2} - \frac{iAk}{r} \right) e^{-i(kr-\omega t)} \\ r^2 \frac{\partial p}{\partial r} &= (-A - iAkr) e^{-i(kr-\omega t)} \\ \frac{\partial}{\partial r} \left(r^2 \frac{\partial p}{\partial r} \right) &= (-iAk + (-A - iAkr)(-ik)) e^{-i(kr-\omega t)} \\ \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial p}{\partial r} \right) &= \left(-\frac{Ak^2}{r} \right) e^{-i(kr-\omega t)} \end{aligned}$$

$$\begin{aligned} \text{R.H.S.} &= \frac{1}{c^2} \frac{\partial^2 p}{\partial t^2} \\ &= \frac{1}{c^2} \left(-\frac{A\omega^2}{r} e^{-i(kr-\omega t)} \right) \end{aligned}$$

Using the property, $c = \lambda f = \frac{\omega}{k}$, we can show that the L.H.S. is the same as R.H.S. (QED)

3.(a)

$$I_{ref} = \frac{p_{ref}^2}{\rho c} = \frac{(1 \times 10^{-6} \text{ N/m}^2)^2}{(1000 \text{ kg/m}^3 \times 1500 \text{ m/s})} = 0.67 \times 10^{-18} \text{ Watt/m}^2$$

(b)

$$0.0002 \text{ dyne/cm}^2 \times \frac{10^4 \text{ cm}^2}{1 \text{ m}^2} \times \frac{10^{-5} \text{ N}}{1 \text{ dyne}} = 2 \times 10^{-5} \text{ N/m}^2$$

$$I_{ref} = \frac{p_{ref}^2}{\rho c} = \frac{(2 \times 10^{-5})^2}{(1.21 \times 343)} = 9.63 \times 10^{-13} \text{ Watt/m}^2$$

(c)

$$SL = 10 \log \frac{I}{I_{ref}}$$

For the whisper, $\mathcal{P} = 10^{-10}$ W and for the shout, $\mathcal{P} = 10^{-5}$ W. Assuming that both the shout and the whisper are omni-directional, we can divide by 4π to get the intensities: $I_{whisper} = 7.9^{-12}$ and $I_{shout} = 7.9^{-7}$.

Using the air reference:

$$I_{whisper} = 10 \log \left(\frac{7.9^{-12}}{9.63 \times 10^{-13}} \right) = 9.1 \text{ dB re } 0.0002 \text{ dyne/cm}^2$$

$$I_{shout} = 10 \log \left(\frac{7.9^{-7}}{9.63 \times 10^{-13}} \right) = 59.1 \text{ dB re } 0.0002 \text{ dyne/cm}^2.$$

Using the underwater reference:

$$I_{whisper} = 10 \log \left(\frac{7.9^{-12}}{0.67 \times 10^{-18}} \right) = 70.7 \text{ dB re } 1 \mu \text{ Pa}$$

$$I_{shout} = 10 \log \left(\frac{7.9^{-7}}{0.67 \times 10^{-18}} \right) = 120.7 \text{ dB re } 1 \mu \text{ Pa}$$

(d) If the whole world shouted at once (in the same place),

$$I = (6 \times 10^9) \times 7.9^{-7} \text{ W/m}^2 = 4.74 \times 10^3 \text{ W/m}^2$$

Calculate sound pressure level in dB:

$$SL = 10 \log \left(\frac{4.74 \times 10^3}{9.63 \times 10^{-13}} \right) = 157 \text{ dB re } 0.0002 \text{ dyne/cm}^2$$

$$SL = 10 \log \left(\frac{4.74 \times 10^3}{0.67 \times 10^{-18}} \right) = 218 \text{ dB re } 1 \mu \text{ Pa}.$$

(e) For the rock band:

$$140 \text{ dB} = 10 \log \left(\frac{I}{9.63 \times 10^{-13}} \right)$$

$$I = (9.63 \times 10^{-13}) \times 10^{14} = 96.3 \text{ Watts/m}^2.$$

What is the corresponding sound pressure level (SPL) in water?

$$10 \log \left(\frac{96.3}{0.67 \times 10^{-18}} \right) = 202 \text{ dB re } 1 \mu \text{ Pa.}$$

(f) The rock band would be louder than the whale.

4. (a) From the definition, the intensity of A, I_A satisfies:

$$100 = 10 \log_{10} \frac{I_A}{I_{ref}}, \Rightarrow \frac{I_A}{I_{ref}} = 10^{10}$$

Those of B and C satisfy respectively,

$$\begin{aligned} 100 &= 10 \log_{10} \frac{I_B}{I_{ref}} \Rightarrow \frac{I_B}{I_{ref}} = 10^{10} \\ 90 &= 10 \log_{10} \frac{I_C}{I_{ref}} \Rightarrow \frac{I_C}{I_{ref}} = 10^9 \end{aligned}$$

Therefore, $I_{A+B} = (I_A + I_B)$ gives us

$$\begin{aligned} 10 \log_{10} \left(\frac{I_A + I_B}{I_{ref}} \right) &= 10 \log_{10} \left(\frac{I_A}{I_{ref}} + \frac{I_B}{I_{ref}} \right) \\ &= 10 \log_{10} (2 \cdot 10^{10}) = 10(\log_{10} 2 + 10) \\ &\cong 103.0 \text{ dB re } 1 \mu \text{ Pa} \end{aligned}$$

(b)

$$\begin{aligned} 10 \log_{10} \left(\frac{I_A + I_C}{I_{ref}} \right) &= 10 \log_{10} \left(\frac{I_A}{I_{ref}} + \frac{I_C}{I_{ref}} \right) \\ &= 10 \log_{10} (10^{10} + 10^9) \cong 100.4 \text{ dB re } 1 \mu \text{ Pa} \end{aligned}$$

(c)

$$\begin{aligned} 10 \log_{10} \left(\frac{I_A + I_B + I_C}{I_{ref}} \right) &= 10 \log_{10} \left(\frac{I_A}{I_{ref}} + \frac{I_B}{I_{ref}} + \frac{I_C}{I_{ref}} \right) \\ &= 10 \log_{10} (10^{10} + 10^{10} + 10^9) \cong 103.2 \text{ dB re } 1 \mu \text{ Pa} \end{aligned}$$

5.

$$1. f = 30 \text{ kHz}; \lambda = c/f = 1500/15000 = 0.05\text{m}.$$

$$\tan \theta_{3dB} = (25/1000) \implies \theta_{3dB} = \pm 1.43^\circ$$

$$\theta_{3dB} = \pm \frac{29.5\lambda}{D} = \pm 1.43$$

$$D = \frac{29.5(0.05)}{1.43} = 1.03 \text{ meters}.$$

$$2. DI = 10 \log\left(\frac{\pi D}{\lambda}\right)^2 = 10 \log\left(\frac{1.03\pi}{0.05}\right)^2 = 36 \text{ dB}$$

$$3. SL = 171 + 10 \log \mathcal{P} + DI = 171 + 10 \log(1) + 36 = 207 \text{ dB re } 1 \mu\text{Pa at } 1 \text{ meter}.$$

$$4. \text{ From matlab, } \alpha \approx 7.6 \text{ dB/km}.$$

$$TL = 20 \log r + \alpha r \times 10^{-3} = 20 \log 1000 + 1(7.6) = 60 + 7.6 = 67.6 \text{ dB re } 1 \text{ meter}.$$

$$5. \text{ Use the formula for echo level from Urick (and handout 2): } EL = SL - 2 TL + TS = 207 - 2(67.6) = 72 \text{ dB re } 1 \mu\text{Pa at } 1 \text{ meter}.$$

$$6. \text{ When ship rolls } \pm 10 \text{ degrees, theinsonified area will vary between } \pm (10 + \theta_{3dB}) = \pm 11.5 \text{ degrees in the across track direction. } 1000 \tan(11.5^\circ) = 203 \text{ meters. Hence the ensonified region of the bottom will be up to } \pm 203 \text{ meters wide}.$$

Note also that it takes $2 \times 1000\text{m} \div 1500\text{m/sec} \approx 1.3$ seconds for a sound ping to travel from the ship to the bottom and back. Depending on the roll rate of the ship, there is a good chance the beam will be pointing in a different direction at reception than for transmission of the pulse. This would result in a much weaker detection from one of the sidelobes of the beam pattern, or in no detection at all.

6.(c) Expand $D\rho/Dt$ using the definition of substantial derivative,

$$\frac{D\rho}{Dt} = \frac{\partial\rho}{\partial t} + (\vec{u} \cdot \nabla)\rho$$

and insert in Equation 1 to yield

$$\frac{\partial\rho}{\partial t} + (\vec{u} \cdot \nabla)\rho + \rho(\nabla \cdot \vec{u}) = 0.$$

The last two terms are the result of applying the chain rule to the divergence of a scalar times a vector, i.e.

$$\nabla \cdot (\rho\vec{u}) = (\vec{u} \cdot \nabla)\rho + \rho(\nabla \cdot \vec{u})$$

and we get the result:

$$\frac{\partial\rho}{\partial t} = -\nabla \cdot (\rho\vec{u}).$$

(d) We can neglect the effect of gravity in deriving the wave equation because we are assuming infinitesimal motion. Applying the definition of the substantial derivative Du/Dt and applying Equation 4 yields:

$$\begin{aligned} \rho \left[\frac{\partial u}{\partial t} + (\vec{u} \cdot \nabla)u \right] &= \left\{ -\frac{\partial p}{\partial x} + 0 + 0 \right\} \\ \rho \left[\frac{\partial v}{\partial t} + (\vec{u} \cdot \nabla)v \right] &= \left\{ 0 - \frac{\partial p}{\partial y} + 0 \right\} \\ \rho \left[\frac{\partial w}{\partial t} + (\vec{u} \cdot \nabla)w \right] &= \left\{ 0 + 0 - \frac{\partial p}{\partial z} \right\} \end{aligned}$$

(f) The perturbations for pressure and density are $p = p_0 + p'$, $\rho = \rho_0 + \rho'$. For the three components of velocity we have $u = u_0 + u'$, $v = v_0 + v'$, and $w = w_0 + w'$, however, we are told that $u_0 = v_0 = w_0 = 0$. Hence, the velocity vector \vec{u} is simply $\vec{u}' = u'\vec{i} + v'\vec{j} + w'\vec{k}$. Applying these to the mass equation yields:

$$\begin{aligned} \frac{\partial(\rho_0 + \rho')}{\partial t} &= -\nabla \cdot ((\rho_0 + \rho')\vec{u}') \\ \frac{\partial\rho_0}{\partial t} + \frac{\partial\rho'}{\partial t} &= -\rho_0\nabla \cdot \vec{u}' - \nabla \cdot (\rho'\vec{u}') \end{aligned}$$

Since ρ_0 is constant, $\partial\rho_0/\partial t = \text{zero}$. Further, $\nabla \cdot (\rho'\vec{u}')$ is a second-order term, and can be dropped, yielding:

$$\frac{\partial\rho'}{\partial t} = -\rho_0\nabla \cdot \vec{u}'$$

For the momentum equations, first consider the equation for x :

$$\rho \left[\frac{\partial u'}{\partial t} + (\vec{u}' \cdot \nabla) u' \right] = \frac{\partial(p_0 + p')}{\partial x}$$

$$\rho \left[\frac{\partial u'}{\partial t} + (u' \frac{\partial u'}{\partial x} + v' \frac{\partial u'}{\partial y} + w' \frac{\partial u'}{\partial z}) \right] = \frac{\partial p_0}{\partial x} + \frac{\partial p'}{\partial x}$$

The three terms that comprise the 2nd part of left hand side of this equation are all quadratic, and hence can be dropped. Since p_0 is constant, $\partial p_0 / \partial x$ is zero, and we are left with:

$$\rho \frac{\partial u'}{\partial t} = \frac{\partial p'}{\partial x}$$

We apply the same process to the y and z momentum equations to yield:

$$\rho \frac{\partial v'}{\partial t} = \frac{\partial p'}{\partial y}$$

$$\rho \frac{\partial w'}{\partial t} = \frac{\partial p'}{\partial z}$$

Which can be combined into a single vector equation:

$$\rho \frac{\partial \vec{u}'}{\partial t} = \nabla \cdot p'$$

(g) Differentiate the new mass equation with respect to time

$$\frac{\partial}{\partial t} \left(\frac{\partial \rho'}{\partial t} \right) = \frac{\partial}{\partial t} (-\rho_0 \nabla \cdot \vec{u}')$$

$$\frac{\partial^2 \rho'}{\partial t^2} = -\rho_0 \frac{\partial}{\partial t} (\nabla \cdot \vec{u}') \quad (1)$$

and take the divergence of the momentum equations:

$$\nabla \cdot \left(\rho \frac{\partial \vec{u}'}{\partial t} \right) = \nabla \cdot \left(\frac{\partial p'}{\partial x} \right)$$

$$\rho (\nabla \cdot \frac{\partial \vec{u}'}{\partial t}) = \nabla^2 p' \quad (2)$$

Because $\nabla \cdot (\partial \vec{u}' / \partial t) = \partial / \partial t (\nabla \cdot \vec{u}')$, the right hand side of Equation 1 equals the left hand side of Equation 2, yielding the desired result:

$$\frac{\partial^2}{\partial t^2} \rho' = \nabla^2 p'.$$

(i) Manipulate Equation 3 to solve for p :

$$\rho = \frac{\rho \phi}{1 - p/k}$$

$$\rho(1 - p/k) = \rho_\phi$$

$$k\rho - \rho p = k\rho_\phi$$

$$p = k \left[1 - \frac{\rho_\phi}{\rho} \right].$$

Substitute $k = c^2\rho$ into this equation to yield

$$p = c^2\rho \left[1 - \frac{\rho_\phi}{\rho} \right] = c^2\rho - c^2\rho_\phi$$

and take the derivative with respect to ρ

$$\frac{\partial p}{\partial \rho} = c^2$$

(j) From the chain rule, we can expand $\partial^2\rho'/\partial t^2$:

$$\begin{aligned} \frac{\partial^2\rho'}{\partial t^2} &= \frac{\partial}{\partial t} \left[\frac{\partial\rho'}{\partial t} \right] = \frac{\partial}{\partial t} \left[\frac{\partial p'}{\partial t} \frac{\partial\rho'}{\partial p'} \right] \\ &= \frac{\partial p'}{\partial t} \frac{\partial}{\partial t} \left(\frac{\partial\rho'}{\partial p'} \right) + \frac{\partial\rho'}{\partial p'} \frac{\partial}{\partial t} \left(\frac{\partial p'}{\partial t} \right) \end{aligned}$$

but

$$\frac{\partial}{\partial t} \left(\frac{\partial\rho'}{\partial p'} \right) = 0,$$

so we can drop the first term, and we are left with:

$$\frac{\partial^2\rho'}{\partial t^2} = \frac{\partial\rho'}{\partial p'} \frac{\partial^2 p'}{\partial t^2}.$$

Using our result of c^2 for $\partial p/\partial\rho$, we get:

$$\frac{\partial^2\rho'}{\partial t^2} = \frac{1}{c^2} \frac{\partial^2 p'}{\partial t^2}.$$

Finally, substituting this into Equation 8, we obtain the desired result:

$$\frac{1}{c^2} \frac{\partial^2 p'}{\partial t^2} = \nabla^2 p'$$