

Answer 2.1**Case1. Phosphorus is removed at a constant rate, with removal completed in T_R .**

The removal rate is $\partial C/\partial t = (C_0/T_R)$, such that $C(t) = C_0(1 - t/T_R)$ for $t \leq T_R$, and $C(t) = 0$ for $t > T_R$. From Chapter 2.5 equation (21), $C_e = \int_0^{\infty} \text{RTD}(t) C(t) dt$.

For Plug-Flow, $\text{RTD}(t) = \delta(t - T_R)$, then $C_e = \int_0^{T_R} \delta(t - T_R) C_0(1 - t/T_R) dt = 0$.

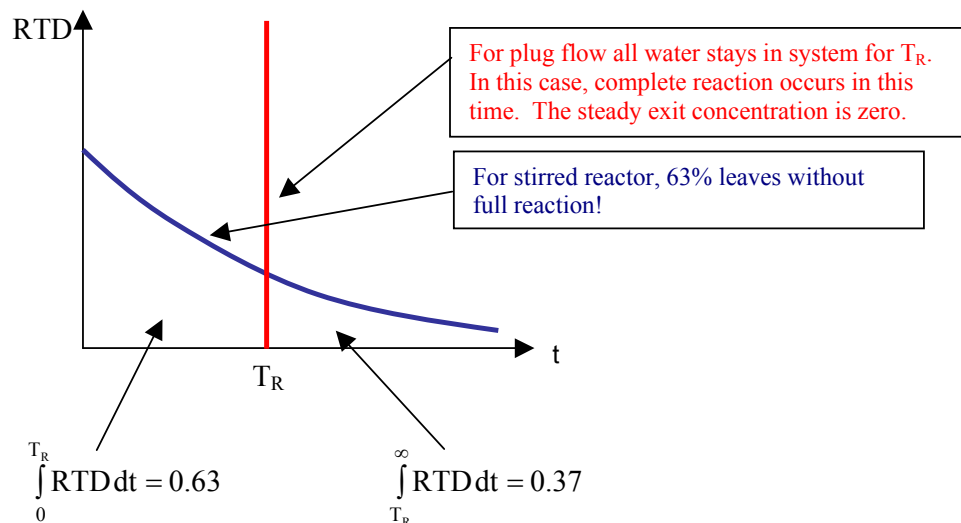
Note the integration is only be carried to $t = T_R$, because for $t > T_R$, $C = 0$.

For a Stirred Reactor $\text{RTD}(t) = \exp(-t/T_R)/T_R$, then

$$\begin{aligned} C_e &= \int_0^{T_R} \exp(-t/T_R) \frac{C_0}{T_R} (1 - t/T_R) dt = \frac{C_0}{T_R} \int_0^{T_R} \left(\exp(-t/T_R) - \frac{t}{T_R} \exp(-t/T_R) \right) dt \\ &= \frac{C_0}{T_R} \left[-T_R \exp(-t/T_R) - T_R \exp(-t/T_R)(-t/T_R - 1) \right] \Big|_0^{T_R} \\ &= \frac{C_0}{T_R} \left[-T_R (\exp(-1) - \exp(0)) - T_R (\exp(-1)(-2) - \exp(0)(-1)) \right] = C_0 \exp(-1) = 0.37 C_0 \end{aligned}$$

Again the integration is carried out only to $t = T_R$, because $C = 0$ for $t > T_R$.

For Plug-Flow the steady exist concentration is zero, indicating 100% removal. For the Stirred Reactor the steady exit concentration is $0.37 C_0$, indicating only 63% removal. So, clearly the Plug-Flow circulation provides better removal.



Case2. **Phosphorus is removed in a first-order reaction with rate, $k = 1/T_R$.**

Following the same procedure above, but with $C(t) = C_0 \exp(-kt)$.

Plug Flow:
$$C_e = \int_0^{\infty} \delta(t - T_R) C_0 \exp(-kt) dt = C_0 \exp(-kT_R) = 0.37 C_0$$

Stirred Reactor:

$$C_e = \frac{C_0}{T_R} \int_0^{\infty} \exp(- (1/T_R + k) t) dt = -\frac{C_0}{T_R} \frac{1}{(1/T_R) + k} \exp(- (1/T_R + k)t) \Big|_0^{\infty} = \frac{C_0}{1 + kT_R}$$

$$C_e = C_0 / (1 + kT_R) = 0.5 C_0$$

Again, Plug-Flow yields a lower exit concentration, and thus achieves higher removal.