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Nonlinear Behavior of a Shim Coil in an LTS/HTS NMR Magnet With an HTS Insert Comprising Double-Pancake HTS-Tape Coils

Seung-yong Hahn, Min Cheol Ahn, Juan Bascuñán, Weijun Yao, and Yukikazu Iwasa

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Abstract—This paper reports results, experimental and analytical, of the nonlinear behavior of a shim coil in the presence of an HTS coil assembled with double-pancake (DP) HTS-tape coils. The experimental results are from: 1) operation of a 700 MHz LTS/HTS NMR magnet (LH700) consisting of a 600 MHz LTS NMR magnet (L600) equipped with superconducting shim coils and a 100 MHz DP-assembled HTS insert (H100) and; 2) an experiment with a room-temperature (RT) Z1 shim coil coupled to a 50 MHz DP-assembled HTS insert (H50). A field mapping theory with a harmonic analysis is applied to interpret both results. Based on experimental results and analyses, we conclude that the screening-current-induced field (SCF) generated by a DP-assembled HTS insert is primarily responsible for the nonlinear behavior, including strength degradation, of a shim coil.

Index Terms—Double-pancake coils, field homogeneity, HTS insert, LTS/HTS NMR magnet, nonlinear behavior of a shim coil, screening-current-induced field.

I. INTRODUCTION

NUCLEAR magnetic resonance (NMR) phenomenon has been widely used in various applications including chemistry, medicine, and nondestructive testing of nucleic acids such as DNA and RNA or proteins. With the need to analyse more complicated structures of materials by NMR techniques increases, so is the need to increase the field of superconducting NMR magnets. Recently, a field of 22.3 T (corresponding to a 950 MHz $^1$H NMR frequency), to-date the highest, was achieved with an all-LTS (low temperature superconductor) NMR magnets [1]. Despite incessant demands by NMR users for even higher fields, it is generally agreed that 1 GHz is a limit achievable with all-LTS NMR magnets, primarily because of low current-carrying capacities of LTS, even at 1.8 K, in fields above ~24 T. We believe that HTS (high temperature Superconductor) is the only superconductor that even at 1.8 K, in fields above 24 T. We believe that HTS (high temperature Superconductor) NMR magnets [1].

This paper presents the nonlinear behavior of the L600 superconducting shim coils observed during the operation of LH700. Shimming results from LH700 were analysed with a field mapping theory [4]. Based on the results, experiment and analysis, it appeared that the screening-current-induced field (SCF) generated by the 100 MHz HTS insert was primarily responsible for the observed nonlinear behavior of the shim coils. To further study and quantify this nonlinear behavior of the L600 shim coils, a room-temperature (RT) Z1 shim coil was coupled to and tested with the 50-MHz HTS insert (H50) of the Phase 1 350 MHz LTS/HTS NMR magnet (LH350), completed in 2003 [5]. The performance of the Z1 RT shim coil is presented first, followed by its test results and discussion.

II. SHIM COIL PERFORMANCE IN LH700

A. System Configuration of LH700

Fig. 1 shows a schematic drawing of the LH700 where eight shim coils up to the 2nd order (Z1, Z2, X, Y, ZX, ZY, C2, and S2) are installed radially outside the LTS background magnet, L600. Table I summarizes key magnet parameters of L600 and H100 including those eight shim coil strength values that were measured separately without the H100; maximum current allowed through each shim coil is 20 A, though, in the actual operation, we limited the shim coil current up to 18 A for safety. Note that the shim coils were designed and constructed to mitigate field impurity specifically from the L600 so that their strengths were not strong enough to completely remove those from the H100.

B. Degradation of Shim Coil Strength in LH700

In a field mapping of LH700, a $^1$H NMR probe was helically traced over a cylindrical surface of 17 mm diameter and 30 mm long in 12 revolutions. Fig. 2 shows two field mapping results in

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full operation of LH700; Dashed line with a triangle represents a mapping taken before shimming while solid line with a circle after shimming with maximum currents, 18 A, of the \( Z1 \), \( Y \), \( ZX \), and \( ZY \) shim coils and 8 A of the \( X \) shim coil—\( C2 \) and \( S2 \) were not activated. Overall homogeneity within the cylindrical mapping volume was improved from 351 ppm to 172 ppm by shimming though it was still much larger than the target homogeneity of 3 ppm [5].

Table II summarizes three dominant field gradients—\( Z1 \), \( Y \), and \( ZY \)—of the two mappings in Fig. 2; “Before” represents field gradients before shimming; “After” those after shimming; “Shim strength” was calculated by the difference between “Before” and “After” divided by the shim coil current, 18 A. Note that each shim strength in the actual operation was degraded from those measured without the H100 in Table I; the tesseral shim strengths of \( Y \) and \( ZY \) were degraded more than the zonal shim strength of \( Z1 \) in percentage.

### III. TEST OF A \( Z1 \) ROOM-TEMPERATURE SHIM COIL WITH H50

To further investigate the non-linear behavior of a shim coil in a stacked-DP type HTS insert wound with Bi2223 tapes, a Room-Temperature (RT) \( Z1 \) shim coil was designed, constructed, and tested with a 50 MHz HTS insert (H50) which was disassembled from the Phase 1 350 MHz LTS/HTS NMR magnet (LH350) completed in 2003 [6].

#### A. Test Set-Up and Procedure

Fig. 3 shows a schematic to-scale drawing of the RT \( Z1 \) shim coil coupled to the H50. The \( Z1 \) shim coil consists of two geometrically identical loops with opposite directions of operating current. An AWG-18 copper wire of 3.8 m long was used for each current loop to form a single layer with 10 turns and the calculated shim strength at the center of H50 was 1171 Hz/cm/A that corresponded to 0.275 gauss/cm/A. Key parameters of the RT shim coil are presented in Table III. During the test, axial field distribution along the axis of H50 was measured using a search coil moved by a speed-controllable DC step motor.

Test procedure is as follows; 1) The H50 and \( Z1 \) shim coil were placed in an LN\(_2\) dewar without any cryogen at room-temperature and axial field distributions were measured at sequential shim coil currents of \( 0 \rightarrow 5 \rightarrow 0 \rightarrow -5 \) A and \( 0 \rightarrow 1 \rightarrow 0 \rightarrow -1 \) A; 2) The same two sets of tests were repeated while the H50 and \( Z1 \) shim coil were placed in a bath of LN\(_2\) at 77 K. In the 77-K tests, the H50 and \( Z1 \) shim coils were completely
warmed up to room-temperature between the 5-A and 1-A sets of tests to clear the previous charging history.

B. Performance of the Z1 RT Shim Coil

Fig. 4 presents axial field measurements at shim coil currents of a) ±5 A and b) ±1 A with two different temperatures of 300 K and 77 K, respectively, while the H50 was not energized; Solid triangle and solid square indicate the results at 300 K with positive and negative operating currents respectively; Open triangle and open square indicate those at 77 K. The measured Z1 shim strengths at the H50 center from the Fig. 4 are summarized in Table IV; The Z1 shim strengths at 300 K ranged from 1151 to 1218 Hz/cm, which is consistent with the design frequency, 1171 Hz/cm while those measured at 77 K varied more widely from 175 to 673 Hz/cm which were degraded by more than 40% from the design frequency. Note that the non-linear variation of the shim strength measured at 77 K was enhanced as the shim current was reduced (5 → 1 A) because of a corresponding relative strength increase of the Screening Current induced Field (SCF) in the H50. This non-linear variation of the shim strength as well as its strength degradation made it very difficult to completely remove the dominant field gradients of the LH700 as seen in Fig. 2 and Table II. More research on the shim coil performance in the presence of an HTS coil will be required for a high-resolution LTS/HTS NMR magnet where a precise shimming is crucial.

C. Canceling a Z1 Gradient of SCF From the H50

In a bath of LN2, we charged the H50 up to 15 A and then completely discharged it with the intention of generating an SCF in the bore of H50 and canceling the gradient of the SCF by the Z1 RT shim coil. Fig. 5 shows measured axial field, Bz, profiles along the H50 axis with different operating currents of the Z1 shim coil; The open squares represent a Bz distribution before the Z1 shim coil was activated; The solid circles are a

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TABLE III

KEY DESIGN PARAMETERS OF THE RT Z1 SHIM COIL

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<td>Material</td>
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<td>Distance between two loops [mm]</td>
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<tr>
<td>Turns per layer; layer</td>
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<tr>
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<tr>
<td>Total resistance [Ω]</td>
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<tr>
<td>Total wire length [m]</td>
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<tr>
<td>Shim strength [Hz/cm/A]</td>
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TABLE IV

MEASURED AND DESIGNED Z1 RT SHIM STRENGTH VALUES

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<td>Designed [Hz/cm/A]</td>
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Fig. 3. Schematic to-scale drawing of the Z1 RT shim coil coupled to the H50.

Fig. 4. Axial field distribution generated by the Z1 RT shim coil along the H50 axis operated at 300 K and 77 K with shim coil currents of: (a) ±5 A; (b) ±1 A.

Fig. 5. Axial displacement from the H50 center [mm]

(a) Measured data for different currents at 300 K and 77 K.

(b) Measured data for different currents at 300 K and 77 K.
5-A Z1 shim current applied; The solid triangles are a current of 10 A; The solid reverse triangles are with 12 A applied when the Z1 gradient at the H50 center was almost canceled out; The open diamonds indicate a B2 measured after the SCF was induced in the H50.

Table V summarizes the measured Z1 gradient at the H50 center in Fig. 5; the “Shim strength” was defined as the average variation of the Z1 gradient divided by the shim current variation at a given operating condition, e.g. that of “12 A”, 756 Hz/cm/A, was obtained by \((243+1269)/2\). While the change of shim current was every 5 A (0 → 10 A), the shim strengths were not changed much although they were still less than 50% of the measured one at 300 K in Table IV. However, when the change of shim current was 2 A (10 → 12 A), its non-linearity increased similarly as seen in Fig. 4(b) because of a corresponding relative increase in the SCF strength.

In Fig. 5, the B2 measured after the shim current returned to zero, “After test”, is different from that measured before the tests started, “Before test”, because of a temporal instability of the SCF which is explained in detail in [7]. This may cause another problem in finding a frame of reference for shimming. In general, a frame of reference is obtained by subtracting two mappings with opposite currents of Z1, X, and Y shim coils. If the time-dependent SCF is added to the field from shim coils, it may be more difficult to find a frame of reference. Currently, we are devoting our efforts in better understanding the frame-of-reference related issues as well as non-linear behavior of shim coils in an LTS/HTS NMR magnet having a DP-type HTS magnet as an insert.

IV. CONCLUSION
Using a field mapping analysis, we have investigated the non-linear behavior (and below-specs performance) of the L600 superconducting shim coils observed during operation of LH700. To further understand this non-linear behavior of the L600 shim coils in the presence of H100, a room-temperature (RT) Z1 shim coil was coupled to and tested with H50. Based on our investigation, experimental and analytical, of both systems, we may conclude that:

- The primary reason that the dominant field gradients—Z1, Y, ZY—of LH700 could not be completely shimmed out is the non-linear behavior of the L600 superconducting shim coils.
- The screening-current-induced field (SCF) generated by H100 is the primarily source responsible for this unexpected non-linear behavior of the L600 shim coils.
- The non-linear behavior as well as the degradation of a shim coil in a field of a DP-assembled HTS insert was further confirmed by an experiment with a Z1 RT shim coil coupled to the H50.
- The nonlinearity of the Z1 RT shim coil increased as the field of the Z1 RT shim was reduced, apparently because of a corresponding relative increase in the SCF strength.
- A “time-dependent” SCF may compound the problem of shimming because it will be more difficult to find a frame of reference for shimming an LTS/HTS NMR magnet.
- Understanding the non-linear behavior of a shim coil as well as the temporal and spatial characteristics of an SCF is critical to successfully construct an above 1 GHz high-resolution LTS/HTS NMR magnet, particularly if the magnet incorporates an HTS insert assembled with DP coils wound with HTS tapes. Specifically, a set of superconducting shim coils, to be placed in the LTS magnet of such an LTS/HTS NMR magnet, must be designed to mitigate or even eliminate the effects of this nonlinear behavior caused by the HTS insert.

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REFERENCES