Gravity-Capillary Lumps Generated by a Moving Pressure Source

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The nonlinear wave pattern generated by a localized pressure source moving over a liquid free surface at speeds below the minimum phase speed \(c_{\text{min}}\) of linear gravity-capillary waves is investigated experimentally and theoretically. At these speeds, freely propagating fully localized solitary waves, or “lumps,” are known theoretically to be possible. For pressure-source speeds far below \(c_{\text{min}}\), the surface response is a local depression similar to the case with no forward speed. As the speed is increased, a critical value is reached \(c_c \approx 0.9c_{\text{min}}\) where there is an abrupt transition to a wavelike state that features a steady disturbance similar to a steep lump behind the pressure forcing. As the speed approaches \(c_{\text{min}}\), a second transition is found; the new state is unsteady and is characterized by continuous shedding of lumps from the tips of a \(V\)-shaped pattern.

The experiments were carried out in a water tank 7.3 m long and 76 cm wide with water depth of approximately 60 cm. The tank has glass walls and bottom for optical access. The surface tension was measured in situ with a Willhelmy plate and remained at \(\sigma = 73\) dyn/cm throughout the experiments. A pipe with inner diameter \(D = 2.5\) mm was mounted vertically to a carriage that rides on top of the tank. The open end of the pipe was positioned 1 cm above the water surface. The carriage was towed at various speeds by a servomotor with a precision of better than 0.3%. We define a speed parameter, \(\alpha = c/c_{\text{min}}\), where \(c\) is the speed of the pipe-carriage assembly and \(c_{\text{min}} = 23\) cm/s is the minimum phase speed defined above. A pressure disturbance is made on the water surface by connecting a pressurized air line to the 2.5-mm tube. The air flow rate was controlled with a flow metering valve and we define a nondimensional forcing parameter, \(\epsilon = h_0/D\), where \(h_0\) is the depth of the depression created by the air forcing when the carriage is stationary. In these experiments, \(\epsilon = 0.43\). The resulting wave pattern was measured using a high-speed camera combined with a shadowgraph technique.

To understand the qualitative change in the shape of the free surface, Fig. 1 shows patterns that form as the pipe is towed at various speeds. The pictures were taken with the high-speed camera viewing the water surface from above. The images were backlit using a white light source to create contrast; roughly speaking, the dark patterns represent downward sloping faces that are blocked from the light and the bright patterns are ridges or crests that are well illuminated. Each photo is from a separate experiment, and the forcing is moving from right to left. At low speeds, there is a symmetric circular depression located directly beneath the air jet, Fig. 1(a). We call this configuration state I. As the speed is increased, the response becomes asymmetric and a stronger depression forms be-
hind the air jet [Fig. 1(b)]. This trailing disturbance is longer in the cross-stream than the streamwise direction and is qualitatively similar to a depression gravity-capillary lump of finite steepness [15]; as the speed is increased further, the disturbance moves farther behind the air jet [Figs. 1(b)–1(d)]. We refer to this asymmetric pattern as state II. Eventually, as the towing speed approaches \( c_{\text{min}} \), the trailing disturbance completely detaches from the forcing, leading to the formation of a time-dependent V shape as in 1(e). We refer to this pattern as state III. As the towing speed exceeds \( c_{\text{min}} \), the classic wave radiation “wedge” is formed, with waves both in front of and behind the pressure forcing [1(f)].

These images should be considered in conjunction with Fig. 2 which shows the peak depth of the pattern \( h_{\text{min}} \), normalized by \( h_0 \), versus \( \alpha \). Each point in Fig. 2 is from a different experimental run. For small values of \( \alpha \) the response is essentially linear, as in Fig. 1(a). However, at a critical value of the speed parameter, \( \alpha_c = 0.9 \), there is a distinct jump in amplitude which coincides with the transition from the linear, localized, symmetric response (state I) to the nonlinear, extended, asymmetric response (state II). In the vicinity of this transition point, the response exhibits time-dependent behavior, oscillating between state I and II, but the wave pattern appears to become steady again for \( \alpha > \alpha_c \). For \( \alpha = 0.95 \), a second transition is observed; the asymmetric pattern of state II gives way to the time-dependent V-shaped behavior of state III. The wave pattern in state III has a well-defined cycle. Figure 3 shows images of the water surface as the wave passes through one of these cycles. Initially the wave has a V shape as shown in Fig. 3(a). The pattern then stretches out as two disturbances are shed from the tips of the V [3(b) and 3(c)] producing a more localized, linear response [3(d)]. The nonlinear response quickly grows again and the V-shaped pattern is observed once more [3(e) and 3(f)].

Turning now to the theoretical investigation, rather than the full nonlinear viscous water-wave equations, our analysis is based on a simple model equation that combines the main effects governing the response, namely, the interplay of nonlinear and dispersive effects along with viscous damping. On kinematic grounds [18], a forcing disturbance moving along \( x \) with speed near \( c_{\text{min}} \) generates waves with wave vectors \( k = (k, l) \) close to \( k_{\text{min}} = (1, 0) \). For a left-going source as in the experiment, expanding the disper-
sion relation (1) to second order around $k_{\text{min}}$ [19] and adding an imaginary part representing the wave decay rate due to viscous damping [20] yields

$$\omega = -i\bar{v}|k|^2 - \frac{1}{4}\text{sgn}(k)(1 + 2|k| + k^2 + 2l^2). \quad (2)$$

The parameter $\bar{v} = \nu(4g)^{1/4}(\sigma/\rho)^{-3/4}$, $\nu$ being the kinematic viscosity; in cgs units, $\nu = 0.01$, $g = 981$, $\rho = 1$, and $\sigma = 73$, so $\bar{v} = 0.003$. Finally, combining Eq. (2) with a moving pressure forcing, $A_p(\xi, y, \xi = x + \alpha t$, and assuming quadratic nonlinearity [19], the following equation for the free-surface elevation $\eta(\xi, y, t)$ is obtained:

$$\eta_t - \bar{v}(\eta_{\xi \xi} + \eta_{yy}) - \left(\frac{1}{2} - \alpha\right)\eta_{\xi} - \beta(\eta^3)_{\xi} - \frac{1}{4}H(\eta_{\xi \xi} + 2\eta_{yy} - \eta) = A_p \xi. \quad (3)$$

Here, $A$ denotes the peak amplitude of the applied forcing and $H[f] = F^{-1}\{-i\text{sgn}(k)F[f]\}$ stands for the Hilbert transform, with

$$F[f] = \frac{1}{2\pi} \int_{-\infty}^{\infty} f(x)e^{-ikx}dx$$

being the Fourier transform. The coefficient of the nonlinear term in Eq. (3) is set to $\beta = \sqrt{11}/2$.8. This ensures that, for $\bar{v} = 0$ and $\alpha$ slightly below the bifurcation point $\alpha = 1$, free lump solutions of Eq. (3) agree, to leading order, with their weakly nonlinear counterparts of the full water-wave equations [14]; for finite steepness, however, Eq. (3) significantly overpredicts the peak amplitude of solitary waves of potential-flow theory [7]. Nonetheless, as will be seen, Eq. (3) does capture the essential nonlinear features of the wave patterns brought out by the experiment.

The model equation (3) was solved numerically as an initial-value problem, starting from rest and turning on the forcing impulsively. The numerical solution technique used a spectral approximation in space, combined with a predictor-corrector Euler time stepping. In all computations, we used the Gaussian forcing $p(\xi, y) = \exp(-2\xi^2 - 2y^2)$. Several runs were made for values of the forcing amplitude in the range $0.035 \leq A \leq 0.283$ and for forcing speeds below as well as slightly above $c_{\text{min}}$ (0.707 $\leq \alpha \leq 1.047$). For weak forcing ($A < 0.07$), the response reaches steady state at all speeds and is essentially linear: a symmetric depression confined in the vicinity of the forcing is seen when $\alpha < 1$, while a radiating pattern, with relatively shorter waves ahead and longer waves behind the source, is generated for $\alpha > 1$. For stronger forcing ($A > 0.07$), the response remains essentially linear if the forcing speed is well below $c_{\text{min}}$; but, as $\alpha$ is increased, nonlinear effects suddenly come into play above a critical speed $\alpha_c < 1$, where transition to a nonlinear state takes place.

For comparison with the experimental observations discussed above, we choose $A = 0.212$; for this value of $A$, the critical speed $\alpha_c = 0.9$, consistent with the experiment for the forcing amplitude $\epsilon = 0.43$. Figure 4 shows plots of computed wave patterns for six different speeds corresponding to the experimental conditions in Fig. 1. For $\alpha = 0.905$, slightly below $\alpha_c$, the response is essentially linear, consistent with Fig. 1(a). Once the critical speed is crossed, however, the pattern becomes markedly asymmetric, as a lumplike disturbance appears on the downstream side of the forcing; moreover, this transition is accompanied by a jump in the response amplitude, in qualitative agreement with Fig. 2. Increasing $\alpha$ past $\alpha_c$ causes the disturbance to move further downstream, in line with the experimentally observed state II in Figs. 1(b)–1(d). It should be noted, however, that the computed wave patterns oscillate periodically (with period of roughly 1 s) between the finite-amplitude state displayed in Figs. 4(b)–4(d) and a small-amplitude state confined close to the forcing; experimentally, on the other hand, state II exhibits oscillatory behavior only for speeds in the immediate vicinity of $\alpha_c$. Increasing $\alpha$ further, a second transition occurs to a V-shaped nonlinear pattern, Fig. 4(c), consistent with state III in the experiment, Fig. 1(e). This new state, which is unsteady according to both the observations and the computations, involves periodic shedding of lumplike disturbances downstream of the forcing. This is seen more clearly in Fig. 5, which displays snapshots of the computed response for $\alpha = 0.981$ at six times, separated by 0.36 s,
corresponding to the sequence of images in Fig. 3. Finally, for \( \alpha > 1 \) [Fig. 4(f)], the computed response does not involve lumps and is similar to the pattern observed experimentally for speeds above \( c_{\text{min}} \) [Fig. 1(f)].

In summary, we have investigated the free-surface wave pattern generated by a localized pressure source moving at a speed below the minimum phase speed for gravity-capillary waves, \( c_{\text{min}} \). High-speed photographs and numerical results from a simple model equation reveal that fully localized solitary waves, or lumps, can play an important part as \( c_{\text{min}} \) is approached. Specifically we identify three distinct types of behavior. First, at speeds far below \( c_{\text{min}} \), the response is essentially linear; a steady depression is observed that is locally confined and symmetric relative to the forcing, and the response amplitude depends weakly on the forcing speed. Second, at a critical speed close to \( c_{\text{min}} \), transition to a nonlinear steady state occurs; the maximum response amplitude experiences a jump as the wave pattern becomes asymmetric and a steep gravity-capillary lump forms behind the applied forcing. Third, at a speed closer to (but still below) \( c_{\text{min}} \), a new transition takes place to an unsteady nonlinear response involving shedding of these lumps downstream. The problem of gravity-capillary waves is prototypical of dispersive wave systems that feature phase-speed minima at nonzero wave numbers, and these results are likely to have implications in other physical settings [21–23].

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