

# Objectives (Output) of Reactor Analysis

## CALCS

### 1. Fuel Management Info

- Cycle Length
- Batch Burnups
- Batch Isotopes

### 2. Operating Info

- Excess Reactivity vs Burnup
- Data to Perform Startup Tests
- Target Power Shapes (BWR)
- Control Rod Patterns
- Process Computer Input
- Plant Data Book

### 3. Licensing Data

- Expected and Limiting Power Dists.
- Shutdown Margin
- Reactivity Coeffs
- Ejected and Dropped Rod Effects
- Delayed Neutron Parameters
- Transient and Accident Evaluations
- CHF and LOCA Limits

# Reactor Physics Parameters

- Power Distribution
- Reactivities

**Reaction Rates**  
(or combinations)

## Power Distribution

- Fission Reaction Rate
- $\Sigma_f \phi$

## Reactivity

$$\frac{\text{Production} - \text{Destruction}}{\text{Production}}$$

$$\frac{\Sigma_f \phi - (\Sigma_a \phi + DB^2)}{\Sigma_f \phi}$$

# Reaction Rates

$$= N \sigma \phi$$

$N \equiv$  Nuclide Concentration  
 $= N(x, B)$

$\sigma \equiv$  Cross Section  
 $= \sigma(x, E, B)$

$\phi \equiv$  Flux  
 $= \phi(x, E, B, \text{operating variables})$

$x \rightarrow$  Position  
 $E \rightarrow$  Energy  
 $B \rightarrow$  Burnup of Fuel

# N

-Initially, From Fuel Design

-Balance Equation:

$$\frac{dN}{dt} = -N\sigma\phi$$

$$\frac{dN(x,t)}{dt} = N\sigma\phi - \lambda N + \sum_i N^i \sigma^i \phi + \sum_j \lambda_j N_j$$

$\Phi$

### Neutron Balance Equation

- Choice of Diffusion theory, transport theory, intermediates
- Choice of zero dimensions, one dimension, 2 – D, 3 – D or combinations
- Choice of spatial detail

PDQ – Diffusion Theory (1 – 3D)

Simulate – nodal (1 – 3D)

CASMO and other lattice codes (2 – D)

$\Sigma$

Divide Continuous Energy into a Few Energy Groups!

$\sigma(x, E, B) \rightarrow \sigma_i$  (N operating variables)

$$\sigma_i(N, OpVar) = \frac{\int \sigma(E) \rho(N, E, OpVar) dE}{\int \rho(N, E, OpVar) dE}$$

Unit Cell (Lattice Physics) Code

Leopard – Unit Fuel (Rod) Cells

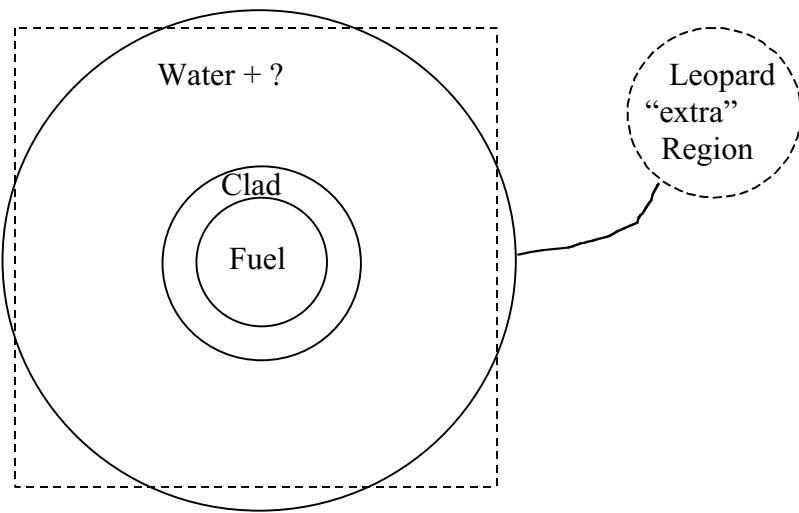
Casmo – Unit Fuel Assemblies

Color set (4 assemblies)

## Unit Cell Codes

1. Since  $\phi$  appears in top and bottom, only E dependance (spectrum), not absolute magnitude, matters
2. Therefore – a single unit cell calculation can represent many places in core (whew!)
3. Most include depletion ( $\frac{dN}{dt}$ )
4. Most come with multigroup of  $\sigma$  libe
5. Since approximations are used, code and libe are matched set (but not so much today)

# Unit Cell Geometry



## Unit Assy

Fuel Cells  
Water Slots  
Control Rods  
Instrumentation Holes  
Can  
Poison PIN Cells

# Effects to consider in Unit Cell Code

## 1. Energy

- Fission Spectrum
- Fast Fission
- Slowing Down
- Leakage During Slowing Down
- Resonance Capture
- Thermal Flux Spectrum
- Self – Shielding

## 2. Space

- Unit Pin Cells (= Lattice)
- Non – Lattice Region
- Effect on Resonance Capture
- Fast Advantage Factor
- Thermal Disadvantage Factor

# Effects to Consider in Unit Cell Code

## Leopard

1. ENERGY      0 – 10 MEV 172 thermal (0 – 0.625 ev)  
                  Fast (0.625 ev – 10 Mev)

- Fission Spectrum – U-235
- Fast Fission Homogeneous
- Slowing down B-1
- Leakage during slowing down – buckling
- Resonance capture – norm to hellstrand
- Thermal flux spectrum – wigner wilkins
- Self shielding – thermal → ABH by group  
                  Res → implicit in hellstrand  
                  Fast → none

2. SPACE

- Unit Pin Cells (=Lattice)
- Non – Lattice Region – Homogeneous
- Effect on Resonance Capture -  $\sqrt{\frac{S}{M}}$
- Fast Advantage Factor = 1.0
- Thermal Disadvantage Factor – ABH

# Effects to Consider in Unit Cell Code

## CASMO

1. ENERGY                  0 – 10 MEV        40 groups  
    70 groups
  - Fission Spectrum U-235
  - Pu-239
  - Fast Fission – Transp. Th.
  - Slowing Down – Space-Energy Together
  - Leakage During Slowing Down – Buckling
  - Resonance Capture- interp. On T and  $\sigma_p$
  - Thermal Flux Spectrum – Numerical
  - Self – Shielding – Transport Theory
2. SPACE
  - Unit Pin Cells ( = Lattice)
  - Non – Lattice Region – Explicit assy
  - Effect on resonance Capture – Equiv. Th
  - Fast Advantage Factor – Transp. Th
  - Thermal Disadvantage Factor – Trans. Th.

## Input to Unit Cell Codes

- Geometry
- Materials
- Temperatures
- Depletion Parameters
  - Power Level
  - Mechanism to obtain criticality  
(usually buckling or poison)

## Output from Unit Cell Codes

Macroscopic few group cross sects.

Microscopic few group cross sects.

Nuclide number densities

Fluxes

Reaction rates

Neutron balance

$K_{\infty}$

$K_{EFF}$

## Cross – Sections

### Macros

- Good only for conditions calculated (unless corrected)
  - Soluble born
  - Temperatures
- Can be used for Depletion

### Micros

- Good for wide variety of conditions
- Can be used for depletion
- Can be used to estimate reactivity of absent capture nuclides

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LRM Proof of Efficacy; graph: Enrichment vs Core AVE EOFPL Burnup.

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Please see pp. 4.3-83, 4.3-67, and 4.3-102 in  
"Reference Safety Analysis Report -- RESAR-3."  
Westinghouse Nuclear Energy Systems, April 1973.

Also see 15.2-1, 15.1-39 and 15.1-42 in "Amendment 4" of the above  
document, May 1974.

## **CONTROLLING CHARACTERISTICS IN POSTULATED INCIDENTS**

<u>POSTULATED INCIDENT</u>	<u>CONTROLLING CORE CHARACTERISTICS</u>
Rod withdrawal, misoperation	Control rod worth MTC Doppler
Boron Dilution	Boron Worth
Incidents causing a change in it temperature	MTC
Steam line break	Rod worth MTC
Rod ejection	Rod worth Delayed neutron fraction Prompt neutron lifetime Doppler

MTC = Moderator Temperature Coefficient

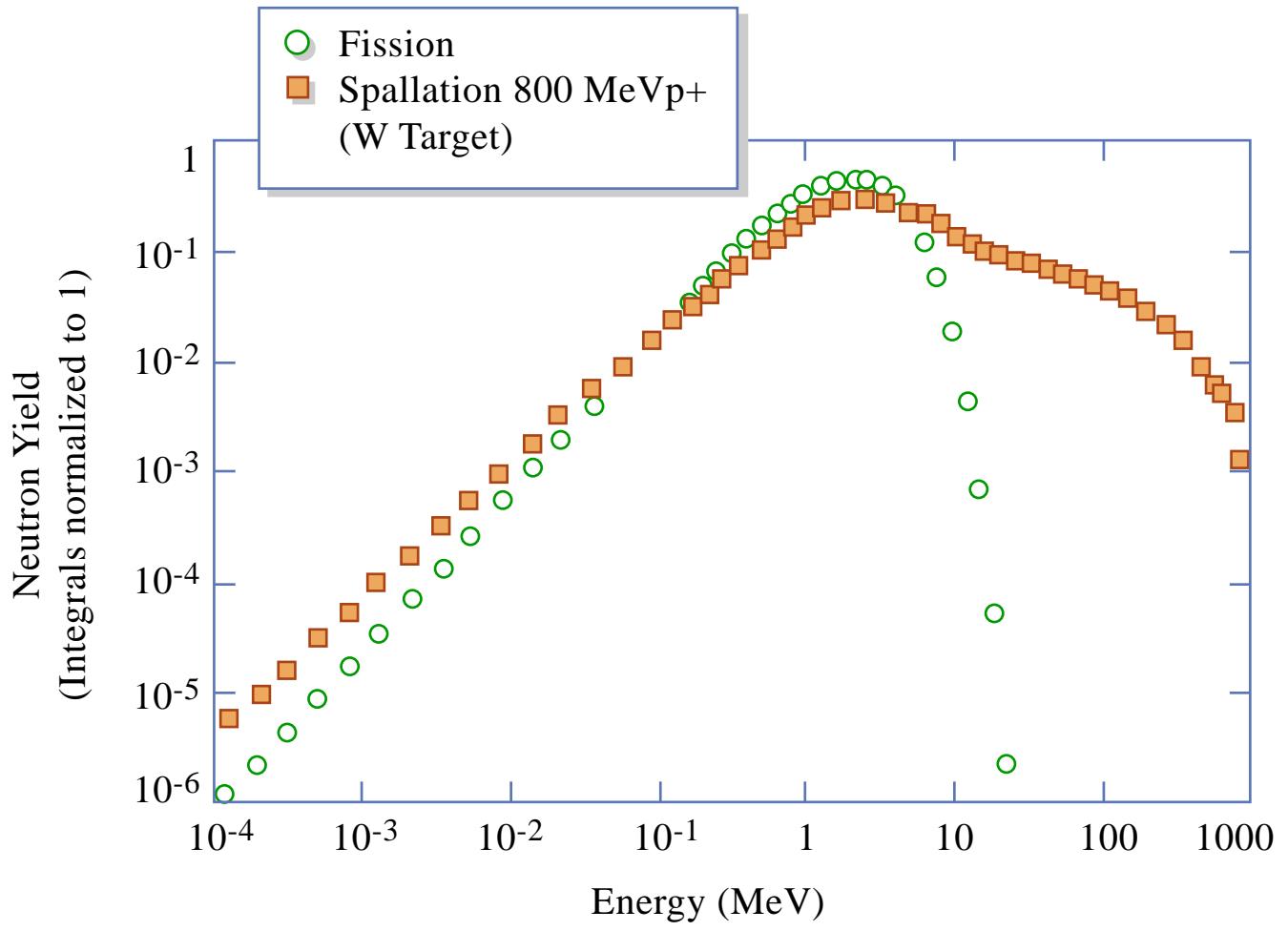


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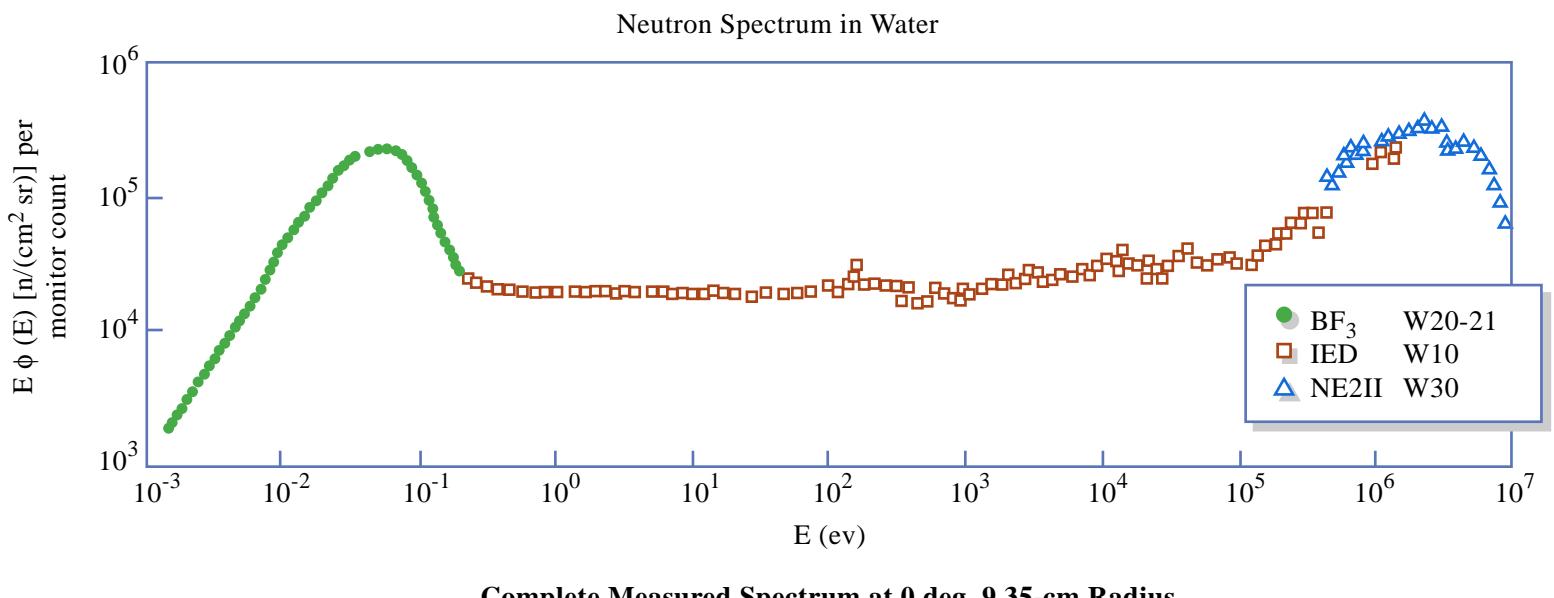


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Please see Waris, Abdul, and Hiroshi Sekimoto.

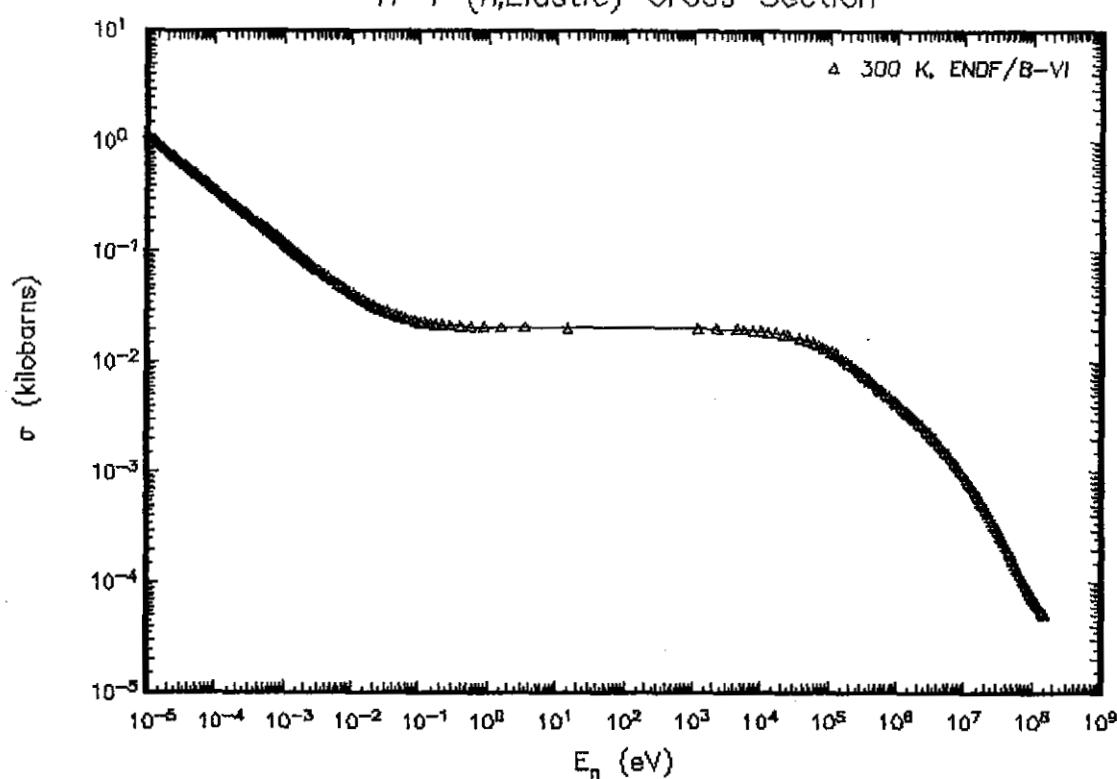
"Characteristics of Several Equilibrium Fuel Cycles of PWR."

*Journal of Nuclear Science and Technology* 38 (2001): 521-522.

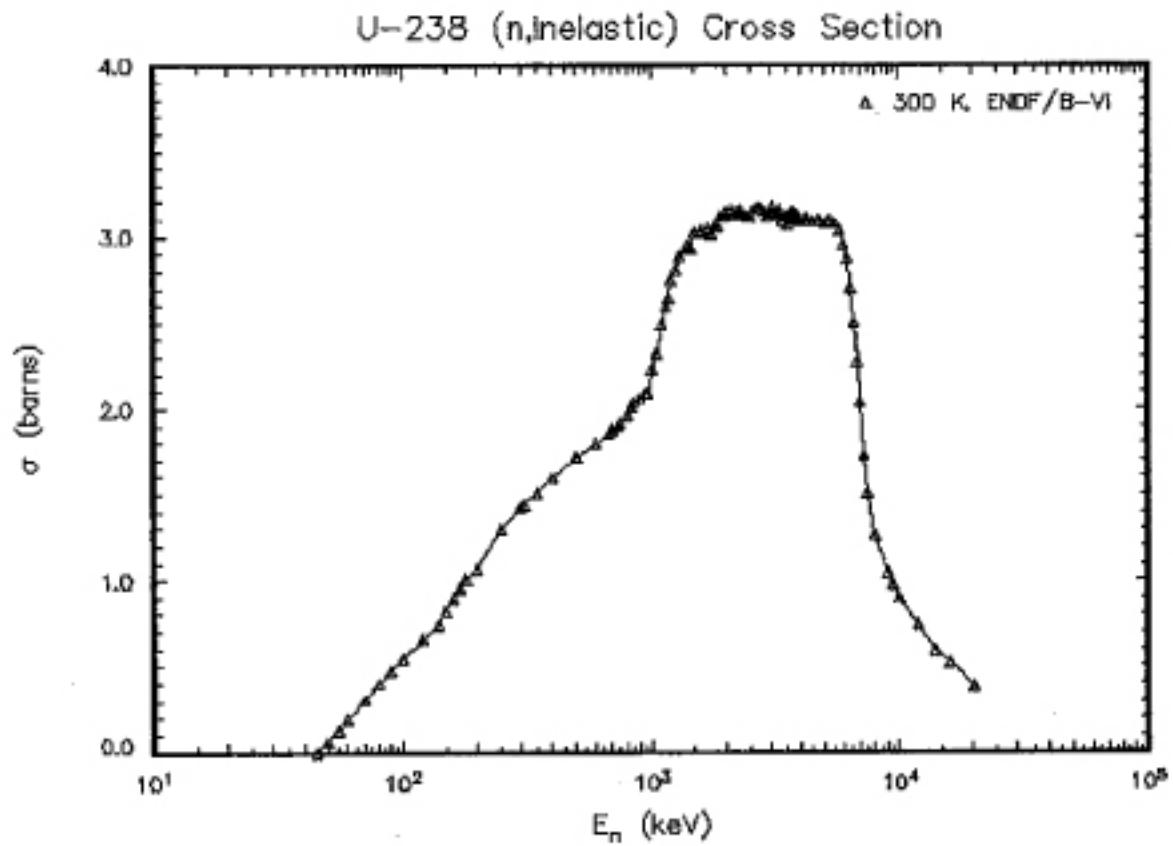
<[http://wwwsoc.nii.ac.jp/aesj/publication/JNST2001/NO.7/38\\_517-526.pdf](http://wwwsoc.nii.ac.jp/aesj/publication/JNST2001/NO.7/38_517-526.pdf)>

### H-1 ( $n$ ,Elastic) Cross Section

△ 300 K, ENDF/B-VI



31-JAN-2003



31-JAN-2003

1/31/03

Classic Naval Reactors  
4 Group Structure

Classic Commercial  
2 Group Structure

ENERGY GROUP STRUCTURES

BOUNDS

MICRO	MACRO	EDIT-A	EDIT-B	2D	PDQ	UPPER	LOWER	WIDTH	
1- 1		1->	1	1	1	10.00000	6.06550	3.93450	MeV
2- 2	2					6.06550	3.67900	2.38650	
3- 3	3					3.67900	2.23100	1.44800	
4- 4	4					2.23100	1.35300	0.87800	
5- 5	5					1.35300	0.82100	0.53200	
6- 6	6->			2	2	821.00000	500.00000	321.00000	keV
7- 9	7					500.00000	111.00000	389.00000	
10- 14	8					111.00000	9.11800	101.88200	
15- 15	9					9.11800	5.53000	3.58800	
16- 21	10->			3	3	5.53000	0.14873	5.38127	
22- 23	11					148.73000	48.05200	100.67799	eV
24- 24	12					48.05200	27.70000	20.35200	
25- 25	13					27.70000	15.96800	11.73200	
26- 26	14					15.96800	9.87700	6.09100	
27- 27	15					9.87700	4.00000	5.87700	
28- 28	16->				4	4.00000	3.30000	0.70000	
29- 29	17					3.30000	2.60000	0.70000	
30- 30	18					2.60000	2.10000	0.50000	
31- 31	19					2.10000	1.85500	0.24500	
32- 32	20					1.85500	1.50000	0.35500	
33- 33	21					1.50000	1.30000	0.20000	
34- 34	22					1.30000	1.15000	0.15000	
35- 36	23					1.15000	1.09700	0.05300	
37- 39	24					1.09700	1.02000	0.07700	
40- 41	25					1.02000	0.97200	0.04800	
42- 42	26					0.97200	0.95000	0.02200	
43- 44	27					0.95000	0.85000	0.10000	
45- 46	28					0.85000	0.62500	0.22500	
47- 49	29->	2	4	5	2	0.62500	0.35000	0.27500	
50- 52	30					0.35000	0.28000	0.07000	
53- 54	31->				6	0.28000	0.22000	0.06000	
55- 55	32					0.22000	0.18000	0.04000	
56- 56	33					0.18000	0.14000	0.04000	
57- 57	34->				7	0.14000	0.10000	0.04000	
58- 58	35					0.10000	0.08000	0.02000	
59- 60	36					0.08000	0.05800	0.02200	
61- 62	37->				8	0.05800	0.04200	0.01600	
63- 64	38					0.04200	0.03000	0.01200	
65- 67	39					0.03000	0.01500	0.01500	
68- 70	40					0.01500	0.00000	0.01500	

### Spontaneous Fission and ( $\alpha$ ,n) Neutron Yields of Selected Isotopes

Isotope	Total Half Life (yr)	Spontaneous	Fission	SF	( $\alpha$ ,n) in	Reaction Oxide
		SF Half-Life (yr)	Neutrons per SF	Neutrons Yield (n/g-s)	$\alpha$ -decay Half-Life (yr)	Neutron Yield (n/g-s)
$^{232}\text{Th}$	$1.41 \times 10^{10}$	$>1 \times 10^{21}$	2.14	$>6 \times 10^{-5}$	$1.41 \times 10^{10}$	$2.2 \times 10^{-5}$
$^{232}\text{U}$	71.7	$8 \times 10^{13}$	1.71	1.3	71.7	$1.49 \times 10^4$
$^{233}\text{U}$	$1.59 \times 10^5$	$1.2 \times 10^{17}$	1.76	$8.6 \times 10^{-4}$	$1.59 \times 10^5$	4.8
$^{234}\text{U}$	$2.45 \times 10^5$	$2.1 \times 10^{16}$	1.81	$5.02 \times 10^{-3}$	$2.45 \times 10^5$	3.0
$^{235}\text{U}$	$7.04 \times 10^8$	$3.5 \times 10^{17}$	1.86	$2.99 \times 10^{-4}$	$7.04 \times 10^6$	$7.1 \times 10^{-4}$
$^{236}\text{U}$	$2.34 \times 10^7$	$1.95 \times 10^{16}$	1.91	$5.49 \times 10^{-3}$	$2.34 \times 10^7$	$2.4 \times 10^{-2}$
$^{238}\text{U}$	$4.47 \times 10^9$	$8.2 \times 10^{15}$	2.01	$1.36 \times 10^{-3}$	$4.47 \times 10^9$	$8.3 \times 10^{-5}$
$^{237}\text{Np}$	$2.14 \times 10^6$	$1.0 \times 10^{18}$	2.05	$1.14 \times 10^{-4}$	$2.14 \times 10^6$	0.34
$^{238}\text{Pu}$	87.74	$4.77 \times 10^{10}$	2.22	$2.59 \times 10^3$	87.74	$1.34 \times 10^4$
$^{239}\text{Pu}$	$2.41 \times 10^4$	$5.48 \times 10^{15}$	2.16	$2.18 \times 10^{-2}$	$2.41 \times 10^4$	38.1
$^{240}\text{Pu}$	$6.56 \times 10^3$	$1.16 \times 10^{11}$	2.16	$1.02 \times 10^3$	$6.56 \times 10^3$	$1.41 \times 10^2$
$^{241}\text{Pu}$	14.35	$(2.5 \times 10^{15})$	2.25	$(4.94 \times 10^{-2})$	$5.90 \times 10^5$	1.3
$^{242}\text{Pu}$	$3.76 \times 10^5$	$6.84 \times 10^{10}$	2.15	$1.72 \times 10^3$	$3.76 \times 10^5$	2.0
$^{241}\text{Am}$	433.6	$1.05 \times 10^{14}$	2.27	1.18	433.6	$2.69 \times 10^3$
$^{242\text{m}}\text{Am}$	152	$9.5 \times 10^{11}$	2.34	$1.35 \times 10^2$	152	33.1
$^{243}\text{Am}$	$7.38 \times 10^3$	$3.35 \times 10^{13}$	2.42	3.93	$7.38 \times 10^3$	$1.34 \times 10^2$
$^{240}\text{Cm}$	26.8 days	$1.9 \times 10^6$	2.39	$6.93 \times 10^2$	26.8 days	$2.53 \times 10^7$
$^{241}\text{Cm}$	32.4 days	$(1.6 \times 10^{12})$	(2.50)	$(8.57 \times 10^1)$	32.4 days	$1.72 \times 10^5$
$^{242}\text{Cm}$	163 days	$6.56 \times 10^6$	2.52	$2.1 \times 10^7$	163 days	$3.76 \times 10^6$
$^{243}\text{Cm}$	28.5	$(1.2 \times 10^{11})$	(2.69)	$(1.22 \times 10^3)$	28.5	$5.00 \times 10^4$
$^{244}\text{Cm}$	18.1	$1.35 \times 10^7$	2.69	$1.08 \times 10^7$	18.1	$7.73 \times 10^4$
$^{245}\text{Cm}$	$8.48 \times 10^3$	$(4.0 \times 10^{12})$	(2.87)	$(3.87 \times 10^1)$	$8.48 \times 10^3$	$1.24 \times 10^2$
$^{246}\text{Cm}$	$4.73 \times 10^3$	$1.81 \times 10^7$	3.18	$9.45 \times 10^6$	$4.73 \times 10^3$	$2.24 \times 10^2$
$^{252}\text{Cf}$	2.646	85.5	3.757	$2.34 \times 10^{12}$	2.731	$6.0 \times 10^5$

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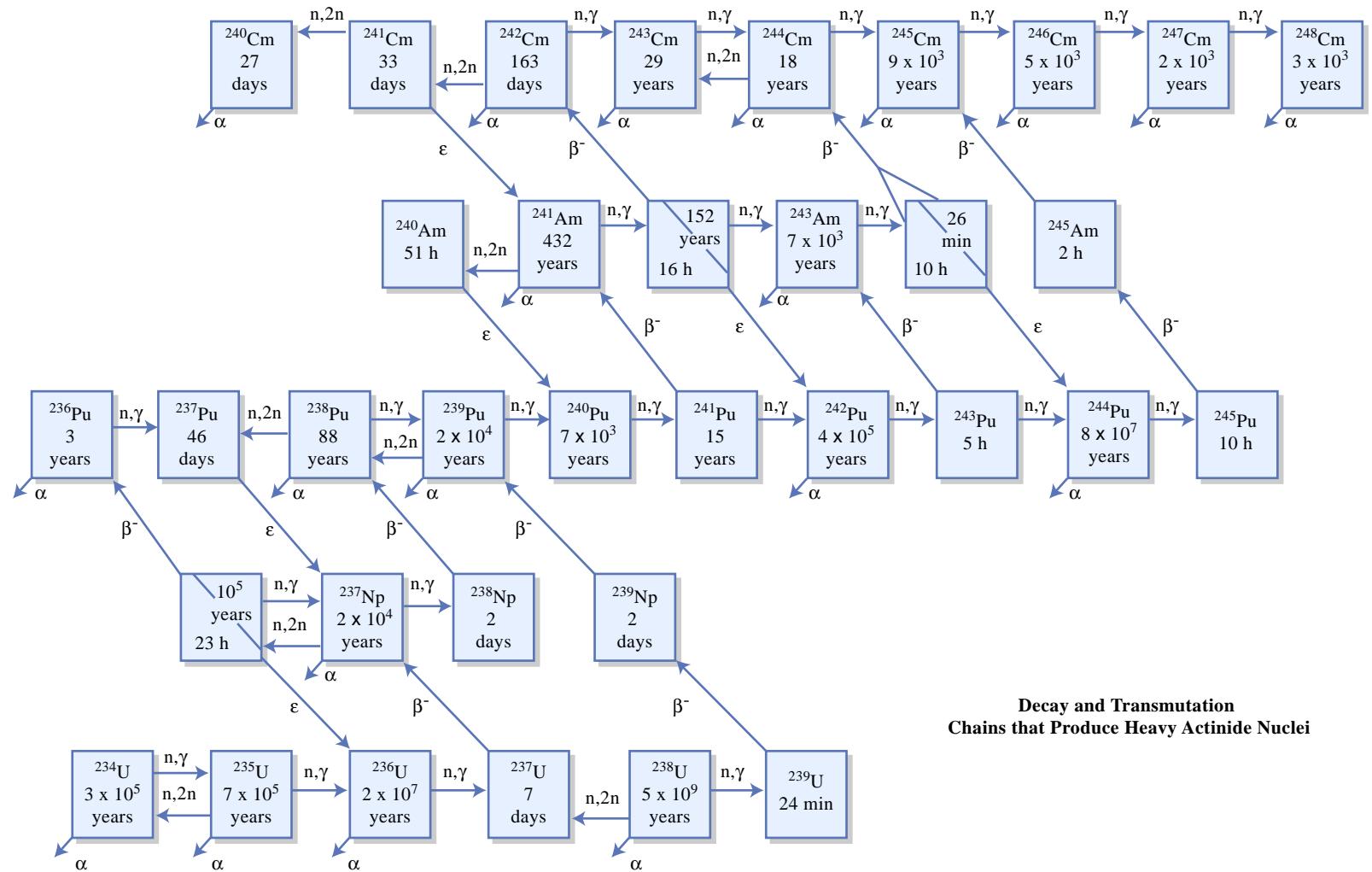
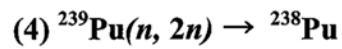
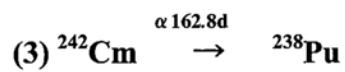
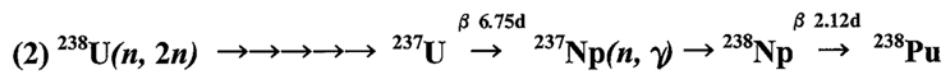
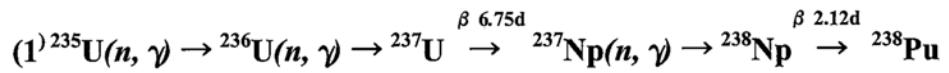


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## POSSIBLE PATHS TO $^{238}\text{Pu}$



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Please see: *Nuclear Technology* 91 (1990): 323, 324, and 326.