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Indications of flow near maximum compression in layered deuterium-tritium implosions at the National Ignition Facility


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An accurate understanding of burn dynamics in implosions of cryogenically layered deuterium (D) and tritium (T) filled capsules, obtained partly through precision diagnosis of these experiments, is essential for assessing the impediments to achieving ignition at the National Ignition Facility. We present measurements of neutrons from such implosions. The apparent ion temperatures $T_{\text{ion}}$ are inferred from the variance of the primary neutron spectrum. Consistently higher DT than DD $T_{\text{ion}}$ are observed and the difference is seen to increase with increasing apparent DT $T_{\text{ion}}$. The line-of-sight rms variations of both DD and DT $T_{\text{ion}}$ are small, $\sim 150 \text{ eV}$, indicating an isotropic source. The DD neutron yields are consistently high relative to the DT neutron yields given the observed $T_{\text{ion}}$. Spatial and temporal variations of the DT temperature and density, DD-DT differential attenuation in the surrounding DT fuel, and fluid motion variations contribute to a DT $T_{\text{ion}}$ greater than the DD $T_{\text{ion}}$, but are in a one-dimensional model insufficient to explain the data. We hypothesize that in a three-dimensional interpretation, these effects combined could explain the results.

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At the National Ignition Facility (NIF) [1], cryogenically layered deuterium (D) and tritium (T) fuel contained in 2-mm-diam carbon-based shells are imploded through laser irradiation of a surrounding high-Z hohlraum [2,3]. The imploding DT fuel assembles and “stagnates” in a configuration with a cold high-density shell surrounding a low-density hot spot. Efficient conversion of shell kinetic energy to hot-spot thermal energy is an essential requirement to achieving ignition at the NIF [4,5]. At peak convergence, this ideally results in a spherically symmetric, cold, dense DT fuel shell with an areal density $\rho R$ of $\sim 1.5 \text{ g/cm}^2$ surrounding a $\sim 5$-keV hot spot with $\rho R \sim 0.3 \text{ g/cm}^2$. Although the word “stagnation” is often used for this phase of the implosion, it is inappropriate as the DT and DD neutron spectra indicate significant remaining kinetic energy. Neutron spectrometers [6–15] provide directional measurements of DT and DD neutron spectra from which yield, burn-averaged ion temperatures $T_{\text{ion}}$ and areal densities $\rho R$ are obtained. Neutron activation detectors (NADs) [16] measure the unscattered DT yield $Y_{\text{DT}}$. In this paper we focus on the DT “temperatures” from a more extensive set of experiments than previously published [2] and conclude that the fuel assembly during burn in layered DT implosions is not well described by detailed one-dimensional (1D) physics models and simulations. The leading hypothesis for the observed discrepancy between the data and the 1D description is significant disordered motion and the highly 3D nature of the assembly at burn.

For a homogeneous stationary DT plasma in thermal equilibrium at ion temperature $T_{\text{thermal}}$, the variance of the DT neutron spectrum (in units of neutron energy) is given by

$$\sigma^2 = \frac{2 T_{\text{thermal}} E_n m_n}{(m_n + m_u)} ,$$

(1)

where $E_n$ is the neutron energy and $m_n$ and $m_u$ are the fusion product masses [17–20]. This has been traditionally used to infer $T_{\text{ion}}$ [21,22]. For DD neutrons the denominator is $m_n + m_{3\text{He}}$, giving a 25% larger relative neutron spectral broadening for the same $T_{\text{thermal}}$ because of the higher average thermal velocity of the reactants. It should be noted that the strong coupling of deuterons and tritons will result in equality of the true ion temperatures. In a recent paper, Murphy [23] articulates that the quantity inferred from the neutron spectrum variance, which we will call apparent $T_{\text{ion}}$, for a homogeneous nonstationary plasma is the sum of the thermal broadening and a macroscopic broadening from the line-of-sight-projected bulk fluid velocity variance $\sigma_v^2$,

$$T_{\text{ion,apparent}} = T_{\text{ion}} + \frac{(m_u + m_X)}{k_B} \sigma_v^2 ,$$

(2)

where $k_B$ is Boltzmann’s constant, $m_X = m_t$ for DT neutrons, and $m_X = m_d$ for DD (see also [24]). If the variance of the bulk velocity dominates over $T_{\text{thermal}}$, then apparent $T_{\text{ion}}$ as inferred from the neutron spectrum variance for DD neutrons will be 80% of the apparent $T_{\text{ion}}$ inferred from DT neutrons. For the implosions studied here, the apparent $T_{\text{ion}}$ is inferred (using the formalism developed in Ref. [20]) from the variance of the neutron spectrum produced in a plasma known to be nonhomogeneous. In this scenario, one has to consider what impact fuel elements at different $T_{\text{thermal}}$ (and possibly different $\sigma_v^2$) have on the primary neutron spectrum. Clearly, there is a
The capability to measure DD $T_{\text{ion}}$ in a DT implosion is a recent development, first reported in Ref. [25] and at the NIF in Ref. [26]. The measurement is now made at the NIF with unprecedented precision and accuracy [10]. The simultaneous measurement of DT and DD neutron yield $Y_{\text{DD}}$ and apparent $T_{\text{ion}}$ in DT implosions is achieved with a suite of three nearly orthogonal, fast neutron time-of-flight (NTOF) detectors [9–11]. These detectors [27] are fielded at polar and azimuthal orthogonal, fast neutron time-of-flight (NTOF) detectors (black crosses) and predicted ratios in apparent $T_{\text{ion}}$ due to a nonthermal contribution from flows according to Ref. [23], assuming a thermal $T_{\text{ion}} = 0$ keV (solid purple line), thermal $T_{\text{ion}} = 1.5$ keV (dot-dashed line), and thermal $T_{\text{ion}} = 2$ keV (double-dot–dashed line).

Figure 1 shows the ratio of the measured apparent DD $T_{\text{ion}}$ to apparent DT $T_{\text{ion}}$ plotted as a function of apparent DT $T_{\text{ion}}$ (different colored points with error bars represent different implosion types, as detailed in the figure caption). A trend in the DD to DT $T_{\text{ion}}$ ratio with increasing apparent $T_{\text{ion}}$ is observed, which appears independent of ablator material and thickness, hohlraum material, and laser pulse shape. A number of possible mechanisms have been proposed that would give rise to a DT $T_{\text{ion}}$ greater than the DD $T_{\text{ion}}$ in these implosions. These include flows [23], species separation [35], and Knudsen tail depletion [36,37]. However, before any such effects are invoked to describe the data, it is important to consider that a difference in measured apparent DT and DD $T_{\text{ion}}$ is also expected based on the spatial and temporal burn weighting of the neutron emission because of the different temperature dependence of the DD and DT reactivities [38].

The neutron spectrum measurements discussed here are all integrated over the burn history of the plasma; measured spectra include neutrons from all regions and times in the nonhomogeneous plasma hot and dense enough for fusion reactions to occur. The fusion burn lasts less than 250 ps, during which time there are strong spatial gradients; the capsule starts out at ~2 mm diameter, is compressed a factor ~25 at the fuel ablator radius, and consists at the time of burn of a dense (many hundreds of g/cm$^3$) cold fuel shell surrounding a central lower-density (many tens of g/cm$^3$) hotspot with temperature that peaks in the center and drops off dramatically towards the hot-spot to high-density-shell interface. Since the DD and DT reactivities increase steeply with increasing temperature, the neutron-based observations weight towards higher temperature. The relatively higher DD reactivity at lower temperature will result in a burn-averaged apparent DD $T_{\text{ion}}$ less than the DT $T_{\text{ion}}$. In addition, the cross section for DD neutron elastic scattering in the dense fuel shell is larger than that for DT neutrons. Given a relatively higher cold fuel $\rho R$ at times with high $T_{\text{ion}}$ than at times with low $T_{\text{ion}}$, this differential attenuation effect integrated over space and time can also contribute to the observed apparent DT $T_{\text{ion}}$ being lower than the DT $T_{\text{ion}}$.

The impact of profile effects on the $T_{\text{ion}}$ ratio is assessed using the HYDRA code [39]. The black crosses in Fig. 1 are results from 1D HYDRA simulations for some of the implosions studied here, where the laser drive has been artificially adjusted for perfectly symmetric capsule illumination (i.e., the radiation field has been smeared around the capsule so that it experiences a uniform radiation drive; see Ref. [40] for more detail). Running the code in this mode effectively eliminates any velocities during burn in the simulation and the resulting simulated $T_{\text{ion}}$ ratio is expected to be almost entirely due to profile effects. The simulations are done postshot and constrained by a requirement to reproduce measured values for, e.g., burn duration $t_{\text{burn}}$, implosion velocity $v_{\text{imp}}$, hot-spot radius $r_{\text{fs}}$, and DSR [40]. For these simulations, $t_{\text{burn}}$ is measured by the $\gamma$ reaction history detector [41], DSR by the neutron spectrometers, and hot-spot size by the neutron imager [42]. Hydrodynamically equivalent convergent ablator implosions are used to determine $v_{\text{imp}}$ [43]. Comparing the simulated black crosses with the data in Fig. 1, it is clear that 1D profile effects alone do not explain the observations.

Bulk fluid flow will impact the measured neutron spectrum, as discussed in the introduction [Eq. (2)] and in Refs. [23,24,44], contributing to the apparent DD $T_{\text{ion}}$ being lower than the DT $T_{\text{ion}}$. The magnitude of this effect is
FIG. 2. Ratios of DT to DD yield as a function of DT $T_{\text{ion}}$. Points without error bars represent the measured DT and DD yields uncorrected for neutron scattering. Framed data points represent estimated birth-yield ratios determined from the measured data using a DSR-dependent correction (plotted vs measured apparent DT $T_{\text{ion}}$), with the same color coding as in Fig. 1. Error bars are statistical only; the systematic error is represented by the dotted curves compared to the dashed curve average for the framed data points. The solid black curve represents the expected birth-yield ratio (plotted vs $T_{\text{ion}}$) calculated using Bosch-Hale reactivities [38] assuming 50%:50% D:T; the dot-dashed black curve is the same for 60%:40% D:T.

illustrated as a function of apparent DT $T_{\text{ion}}$ in Fig. 1, where the solid purple line shows the calculated expected $T_{\text{ion}}$ ratio due to nonthermal motion assuming zero $T_{\text{thermal}}$; the dot-dashed line the $T_{\text{ion}}$ ratio due to nonthermal motion assuming $T_{\text{thermal}} = 1.5$ keV, and the double-dot–dashed line the $T_{\text{ion}}$ ratio due to nonthermal motion assuming $T_{\text{thermal}} = 2$ keV. If we assume the observed temperature difference is due to flow, then the inferred average $T_{\text{thermal}}$ for many of the shots is very low (more than half the shots fall below the double-dot–dashed 2-keV $T_{\text{thermal}}$ line). Correcting for profiles using the $T_{\text{ion}}$ ratio from 1D HYDRA simulations (black crosses in Fig. 1), $T_{\text{thermal}}$ is on average 2.1 keV for implosions with a $T_{\text{ion}}$ ratio lower than predicted from the simulations. Such low $T_{\text{thermal}}$ requires a much higher than previously calculated pressure ($Y_{\text{DT}} \sim P^2 T_{\text{ion}}^2$) [45], and hence hot-spot density, to reconcile measured $T_{\text{burn}}, T_{\text{io}},$ and neutron yields. Higher hot-spot density is inconsistent with x-ray irradiance measurements on these implosions. We conclude that in a 1D model, combined profile and reactivity related effects and flows are insufficient to explain the measured $T_{\text{ion}}$ ratios.

It is also interesting to study the relative DT-DD yields from these implosions. In Fig. 2, measured $Y_{\text{DT}}/Y_{\text{DD}}$ (colored data points) are contrasted with predictions based on Bosch-Hale reactivities [38] assuming a fuel ratio of 50:50 D:T (solid black line) and 60:40 D:T (dot-dashed black line). Weighted average yields from all reporting detectors (NTOF, MRS, and NAD) are used. Note that the data points are plotted versus measured apparent DT $T_{\text{ion}}$, while the theoretical curves assume that the x axis represents $T_{\text{thermal}}$. Due to the high $\rho R$, a significant fraction of neutrons lose energy through scattering on ions in the cold fuel, which has to be considered when measuring the yields. Measured yield is defined as the integral $E_n = 2.2–2.7$ MeV for $Y_{\text{DD}}$ and $E_n = 13–15$ MeV for $Y_{\text{DT}}$ (points without error bars in Fig. 2). Birth yields (framed data points with error bars) are inferred from measured yields using correction factors as a function of DSR determined from MCNPX modeling of a 1D implosion [46,47]. The vertical error bars in Fig. 2 represent the statistical uncertainty in the yield ratio measurement. The systematic uncertainty is represented by the dotted gray curves relative to the dashed curve average for the framed data points. Errors in the DSR measurement are also considered when determining these total statistical and systematic errors in the DSR-corrected yield ratio measurement.

In principle, since the DT/DD reactivity ratio is a strong function of temperature, the yield ratio is another thermometer that can be brought to bear to determine hot-spot plasma conditions [48]. This method requires, however, (i) high accuracy in the birth-yield ratio measurements and (ii) a thorough understanding of the isotopic composition of the fuel. Given the present uncertainties in both of these factors, $T_{\text{thermal}}$ for these implosions cannot be constrained to a meaningful accuracy using this method. In regard to fuel isotope composition, targets for these implosions are filled with a 50:50 mixture of DT gas. However, due to different freezing temperatures for D and T, it is estimated that the solid ice layer in the cryogenic capsules contains 50%:50% D:T, while the composition of the vapor in the central cavity before the implosion is 63%:37% D:T. The mass of the vapor is $\sim 0.8 \mu g$. The estimated total mass of the reacting fuel for these implosions ranges from 4 to 13 $\mu g$, meaning that the effective D fraction should be in the range of 50.8%–52.3% and the corresponding T fraction in the range of 47.7%–49.2%. Taking these best-estimate numbers at face value, the DD yield comes in higher than expected relative to the DT yield for a majority of these implosions. Measured and predicted yields could be reconciled if apparent DT $T_{\text{ion}}$ was inflated due to flows. However, it cannot at present be ruled out that shot-to-shot variations in the fuel isotope composition may be as high as $\pm 10\%$.

Nonhydrodynamic effects such as fuel stratification [35,49,50] and Knudsen tail depletion [36] have been proposed as possible mechanisms that could give rise to a DT $T_{\text{ion}}$ greater than the DD $T_{\text{ion}}$. The fuel stratification hypothesis also implies that the DT yields would be larger relative to DD yields than expected from 1D hydrodynamic simulations [35]. The NIF $Y_{\text{DT}}/Y_{\text{DD}}$ result is in apparent contradiction with this hypothesis. In the Knudsen tail depletion hypothesis, ions from the high-energy tail of the distribution with mean free path much longer than the system scale size are lost from the reacting region before undergoing fusion. This narrows the width of the neutron energy distribution, reducing inferred apparent $T_{\text{ion}}$. At a Knudsen number of 0.05 and thermal $T_{\text{ion}}$ of 5 keV, the expected $T_{\text{ion}}$ ratio due to this effect alone would be 0.95 [37]. However, nominal Knudsen numbers calculated for the neutron-producing compression phase of these implosions are too small for the depletion to be significant at $(1–3) \times 10^{-3}$. Local Knudsen numbers might increase due to turbulence and mix, elevating the impact of this effect [37], but such small-scale turbulence is expected to be reduced by viscosity [51].
Three-dimensional dynamics seeded by laser drive asymmetry, engineering features, ice-layer nonuniformity, etc., are believed to play a substantial role in these implosions [52–55]. Profile or reactivity effects, differential scatter, and nonthermal flows in a realistic 3D implosion model have the potential to explain the DD/DT $T_{\text{ion}}$ ratio measurements without invoking nonhydrodynamic effects. Asymmetry-driven 3D effects can be expected to introduce significant fuel flows. Presuming that the bulk fluid flow is either strictly radial [24] or uniformly turbulent [23], broadening of the neutron spectrum is the same independent of viewing direction. However, given the nature of the assumed asymmetry seeds, highly resolved 3D simulations show strong velocity variance in the implosions and line-of-sight (LOS) variations in apparent $T_{\text{ion}}$. Figure 3 shows the observed variations in the DT (DD) apparent $T_{\text{ion}}$ between the individual measurements in five (three) different LOSs. The measurements conclusively rule out LOS anisotropy above 0.4 keV and no anisotropy trend is seen with increasing apparent DT $T_{\text{ion}}$. Given the almost direct correlation between increasing apparent $T_{\text{ion}}$ and increasing implosion velocity, the lack of a trend indicates that low-mode asymmetries are not amplified when implosion velocity increases.

For DT, the highest observed anisotropy is seen for shot N150318 (rightmost point in Fig. 3), which was purposely imploded with a top-down ±4% laser drive asymmetry to provoke flows in the implosion. The limited LOS coverage may lead to undersampling of the signatures of velocity variance, which is being addressed through the addition of another detector system at the NIF. Improvements in capsule coverage and in the systematic measurement uncertainties are required to explore the $T_{\text{ion}}$ variance in finer detail and to further investigate the 3D dynamics hypothesis. We conjecture that the small line-of-sight variations observed may indicate that flows due to low-mode asymmetries are not responsible for the observed DD/DT $T_{\text{ion}}$ ratios; flows due to high-mode asymmetries, on the other hand, could simultaneously explain the data in Figs. 1 and 3.

Although the implosion dynamics for indirect drive exploding pushers (IDEPs) [56] are very different from cryogenically layered implosion dynamics, it is interesting to compare the measurements and simulations for these types of implosions. For the IDEPs, excellent agreement has been found between measured data and HYDRA simulations, with measured DT and DD yields and $T_{\text{ion}}$ all showing agreement with simulated results. The $T_{\text{ion}}$ ratios of 0.84–0.90 observed for the IDEPs appear to be fully explained by profile effects alone; yield ratios also agree with expectation. Detailed analyses of DT neutron spectra from IDEPs have also shown that an observed non-Gaussian peak shape, due to profile effects, was correctly captured in simulations [57].

Given that neutrons from many different fuel elements at different temperatures and in different states of motion contribute to the measured spectra, a detailed comparison of measured and simulated spectral shape is another potential path to conclusive answers. Further refinements in analysis [58] and measurement techniques are under development, which may allow more sophisticated analysis of higher moments (skew and kurtosis) of the neutron peak in future work.

In summary, measured apparent DT $T_{\text{ion}}$ from cryogenically layered NIF DT implosions are seen to be consistently higher than apparent DD $T_{\text{ion}}$, a discrepancy that increases with increasing $T_{\text{ion}}$. The DD yields are observed to be high relative to DT yields and LOS variations in $T_{\text{ion}}$ measurements are small. Apparent DT and DD $T_{\text{ion}}$ do not match 1D hydrodynamic simulations assuming a central isobaric hot spot. Species separation and non-Maxwellian ion distributions have been proposed as explanations for a DT $T_{\text{ion}}$ greater than the DD $T_{\text{ion}}$; while a contribution from these effects cannot be ruled out, neither effect on its own self-consistently explains the present data. Three-dimensional profile or reactivity effects, differential scatter, and bulk fluid motion have the potential to explain the measurements. Testing this 3D hypothesis requires highly resolved simulations. The present data provide a strong constraint for the 3D simulations in that they must simultaneously recreate large DT to DD $T_{\text{ion}}$ differences (Fig. 1) and small LOS variations (Fig. 3). A complete understanding of implosion dynamics and hot-spot formation will be obtained by bringing to bear all available diagnostic measurements and comparing the results obtained to realistic 3D simulations of the implosions.
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[27] The detectors have fast-response benzylx scintillators as the detecting medium, each coupled to 3 photomultiplier tubes and one photodiode to allow for optimal detection over a large range of yields.
[33] The downscatter ratio is defined as yield in the $E_n = 10-12$ MeV range divided by yield in the $E_n = 13-15$ MeV range: $\rho R \sim 20.4 \times DSR g/cm^2$ (derived from an ensemble of CH simulations; similar work for HDC is expected to be close to the same).
[45] $Y \sim P^2 C_{\text{born}}^2 (\sigma v(T_{\text{ion}}) V_{\text{dynam}}) / (PT_{\text{ion}}+T_{\text{dynam}} V_{\text{dynam}})$. for DT 2 to 7 keV, $\sim V_{\text{dynam}}/T_{\text{ion}}^2$. With constant $V_{\text{dynam}}$ and $T_{\text{ion}}$.
[47] The MCNPX model is made up of a spherical core (radius 35 $\mu$m and DT gas density $\rho = 122.5$ g/cm$^3$), surrounded by a DT shell (35–50 m), with density varied to obtain different values for DSR, and a CH shell (50–55 $\mu$m, $\rho = 250$ mg/cm$^3$). A thermal neutron source with $T_{\text{dynam}} = 4$ keV, Gaussian distributed in space from 0 to 35 $\mu$m, is used in separate DD and DT runs, and escaped neutron spectra are tallied using point detectors. The resulting correction factor is $(Y_{\text{DDmeas}}/Y_{\text{DDdynam}})(Y_{\text{DTmeas}}/Y_{\text{DTdynam}}) = 24.27 \times Y_{\text{DSR}} - 6.93 \times Y_{\text{DSR}} + 1$.
[57] L. Divol (private communication).