**New Concept Conformal Antennas Utilizing Metamaterial and Transformation Optics**

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<td><a href="http://dx.doi.org/10.1109/lawp.2008.2002537">http://dx.doi.org/10.1109/lawp.2008.2002537</a></td>
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<tr>
<td><strong>Publisher</strong></td>
<td>Institute of Electrical and Electronics Engineers</td>
</tr>
<tr>
<td><strong>Version</strong></td>
<td>Final published version</td>
</tr>
<tr>
<td><strong>Accessed</strong></td>
<td>Sun Apr 24 12:30:13 EDT 2016</td>
</tr>
<tr>
<td><strong>Citable Link</strong></td>
<td><a href="http://hdl.handle.net/1721.1/54739">http://hdl.handle.net/1721.1/54739</a></td>
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**Detailed Terms**

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New Concept Conformal Antennas Utilizing Metamaterial and Transformation Optics
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Abstract—In this letter, we show by theoretical analysis and computer simulation that conformal antennas can be designed using metamaterial with inhomogeneous constitutive parameters by applying the electromagnetic coordinate transformation approach, which is the technique used to realize electromagnetic invisibility. We demonstrate that, a source of arbitrary shape and position in the free space can be replaced by an properly designed metamaterial coating with current distributed on the inner surface and would not be detected by outer observers, because the emission of the source can be controlled at will in this way. As examples, we design two conformal antennas by transforming a simple dipole antenna and a standard array antenna separately to illustrate the possible applications of this kind of transformation.

Index Terms—Conformal antennas, metamaterial, transformation optics.

I. INTRODUCTION

In 2006, Pendry et al. proposed the pioneering coordinate transformation concept to arbitrarily control electromagnetic (EM) fields [1]. In his approach, a space consisting of the normal free space can be transformed into a new space with different volume and space-distributed constitutive parameters [1], [3], [4], which could be realized by artificial metamaterial, whose permittivity and/or permeability can be designed to continuously change from negative to positive values [5], [6]. Following this approach, some novel EM devices—one example is the famous invisibility cloak—can be realized to obtain unusual EM behaviors [7]–[20]. In this letter, we further illustrate that such coordinate transformation can even be applied to a space containing EM sources. The closed-form solution obtained from a full wave analysis that combines the coordinate transformation and Green’s function principle shows that in this case, not only the permittivity and permeability tensors, but also the EM sources can be transformed at will. In particular, a source of arbitrary shape and position in the free space can be replaced by another source, given access to a properly designed metamaterial coating, without being detected by outer observers. As examples to illustrate the possible applications of this kind of transformation, we designed two conformal antennas by transforming a simple dipole antenna and a standard array antenna, separately. The calculations show that the metamaterial coatings carrying specific currents have the same radiation patterns as the initial antennas’ in the zones of interest. The method proposed in this letter provides a brand-new approach in the development of antennas.

II. FORMULATIONS

We start from considering a general coordinate transformation between the initial and the transformed coordinate systems \((x', y', z')\) and \((x, y, z)\) by

\[
\begin{align*}
\tau' &= F(\tau) \quad \text{or} \\
x' &= f(x, y, z), \quad y' = g(x, y, z), \quad z' = h(x, y, z).
\end{align*}
\]

Here \(\tau' = x' \hat{x} + y' \hat{y} + z' \hat{z}\), \(\tau = x \hat{x} + y \hat{y} + z \hat{z}\), and \(F\) represents a deformation mapping from coordinate system \((x', y', z')\) to \((x, y, z)\) on a closed domain \(V\), of which the boundary is matched to free space (e.g., \(\tau = F(\tau)|_{\partial V}\)). The relation between the two operators \(\nabla = \hat{x} \partial / \partial x + \hat{y} \partial / \partial y + \hat{z} \partial / \partial z\) and \(\nabla' = \hat{x'} \partial / \partial x' + \hat{y'} \partial / \partial y' + \hat{z'} \partial / \partial z\) is given by

\[
\nabla \times A = \text{det}(\nabla') \nabla \times \left[ (\nabla')^{-1} \cdot A \right] \quad \text{(2)}
\]

\[
\nabla \cdot A = \text{det}(\nabla') \nabla \cdot \left[ (\nabla')^{-1} \cdot A \right] \quad \text{(3)}
\]

where \(\nabla = \partial (f, g, h) / \partial (x, y, z)\) is the Jacobian matrix [3], [4]. Substituting (2) and (3) into Maxwell’s equations, we obtain the desired EM constitutive parameters in terms of the constants in the initial coordinate

\[
\hat{\varepsilon} = \text{det}(\nabla') \hat{\varepsilon} \cdot (\nabla')^{-1} \quad \text{(4)}
\]

\[
\hat{\mu} = \text{det}(\nabla') \hat{\mu} \cdot (\nabla')^{-1} \quad \text{(5)}
\]

\[
\rho(\tau) = \text{det}(\nabla') \rho'(F(\tau)) \quad \text{(6)}
\]

\[
\mathbf{J}(\tau) = \text{det}(\nabla') \mathbf{J}'(F(\tau)) \quad \text{(7)}
\]

Manuscript received May 12, 2008; revised June 10, 2008. First published July 18, 2008; current version published December 05, 2008. This work is sponsored by the Chinese National Science Foundation under Grants 60531020 and 60671003, the NCET-07-0750, the Ph.D. Programs Foundation of MEC (No. 20070335120), the China Postdoctoral Science Foundation under Grant No. 20060390331, the ONR under Contract N00014-01-1-0713, and the Department of the Air Force under Air Force Contract F19628-00-C-0002.

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Digital Object Identifier 10.1109/LAWP.2008.2002537 1536-1225/$25.00 © 2008 IEEE
The surface current, current, and charge in the transformed coordinate can also be described with the mapping matrix \( \mathbf{F} \)

\[
\mathbf{J}_s (\tau') = \mathbf{J}^T \cdot \mathbf{J}_s' (\mathbf{F}(\tau')) \\
\mathbf{I} (\tau') = \mathbf{F}^{-1} (\mathbf{F}(\tau')) \cdot q (\tau') = q' (\mathbf{F}(\tau')).
\]

(8)

Note that Maxwell’s equations still remain their form invariance in the new coordinates \((x', y', z')\), but the permittivity, permeability, charge density and current density will be with different forms, and the total charge \(q\) and total current \(I\) satisfy conservation law under the transformation. To evaluate the electromagnetic field in the transformed coordinates on domain \(V\) which contains sources \(\mathbf{j}_s (\tau_0)\) and \(\rho (\tau_0)\), we introduce the vector potential \(\mathbf{A} (\mathbf{F} = \nabla \times \mathbf{A})\) and scatter potential \(\phi (\mathbf{F} = \hat{\omega} \mathbf{A} - \nabla \phi)\). By applying gauge condition \(\nabla \cdot \left( \mathbf{F}^{-1} \cdot \mathbf{A} \right) - \hat{\omega} q_0 e_{\text{t}} \phi = 0\) (where \(T = \mathbf{F}^T / \det (\mathbf{F})\) is the metric tensor), the partial differential equation of the vector potential can be obtained, and thereby the exact expression of the electric field can be written as Green’s function as

\[
\mathbf{E} = \hat{\omega} q_0 e_{\text{t}} \cdot \left( \mathbf{j} + \frac{\nabla \nabla}{k^2} \right) \cdot \mathbf{F}^{-1} \cdot \mathbf{j} (\tau_0) - e^{2k|\mathbf{r}' - \mathbf{r}_0|} \frac{1}{4\pi|\mathbf{r}' - \mathbf{r}_0| \det (\mathbf{F})} \mathbf{F} \cdot \mathbf{j} (\tau_0)
\]

(9)

with \(\mathbf{r}' = \mathbf{F} (\tau)\) and \(\mathbf{r}_0 = \mathbf{F} (\tau_0)\)

The above analysis implies that, by applying the coordinate transformation \(\mathbf{F}\), the point \(\mathbf{r}' = \mathbf{F} (\tau_0)\) in the initial coordinate will be transformed to \(\mathbf{r} = \mathbf{F} (\tau_0)\) in the new coordinate. Thus looking from the outside of the transformed region, a source located at \(\mathbf{r} = \mathbf{r}_0\) seems to radiate at \(\mathbf{r} = \mathbf{F} (\mathbf{r}_0)\). Then theoretically, by choosing appropriate transformation \(\mathbf{F}\), a given source can be transformed into any required shape and position. This principle can be applied in the design of active EM devices, especially antennas.

III. EXAMPLES

Pendry et al. suggested that with certain transformation, the electromagnetic field in a spherical region \(r < R_2\) can be compressed into an annulus region \(R_1 < r < R_2\), to form an invisibility cloak [1]. Here we consider a similar situation, but the mapping \(\mathbf{F}\) is selected as follows:

\[
\frac{x'^2}{a^2 (r)} + \frac{y'^2}{b^2 (r)} + \frac{z'^2}{c^2 (r)} = 1
\]

(10)

with \(a (r) = R_2 (r - R_1)/(R_2 - R_1)\), and \(b (r) = (R_2 - d/2) (r - R_1)/(R_2 - R_1) + d/2\) (Here \(d\) is a constant).

Under this outer boundary of the annulus \((r = R_2)\) still matches the free space, which is similar to the cloaking case, however, the thing different is that a line with a length \(d\) with respect to the initial axes \((x', y', z')\), instead of the origin, is transformed to the spherical inner surface \(r = R_1\).

Suppose there is a dipole with length \(d\) located at the origin, as shown in Fig. 1(a). After the proposed transformation, the line current carried by the dipole will be mapped to the surface current on the inner boundary \((r = R_1)\), and in the spherical region \(R_1 < r < R_2\), the electric field radiated by the dipole will be squeezed into the annulus \(R_1 < r < R_2\). We can comprehend this from another perspective: suppose there are some currents distributed along the \(\theta\) direction on the inner surface \(r = R_1\), and the region \(R_1 < r < R_2\) is filled with this transformed medium. Looking from the outer space \(r > R_2\), a detector will only ‘see’ a dipole of length \(d\) pointing in the \(z\) direction and the radiation field is completely the same as that of the dipole. This also provides a simple way to understand Pendry’s cloaking [1]. In Pendry’s transformation, a point in the initial space is transformed to the inner spherical surface in the new space. Therefore, the currents distributed on the inner spherical surface \(r = R_1\) simply behave as a point with neither net charges nor net dipole moment to outer observers. That’s why under Pendry’s transformation the current on the inner surface cannot radiate power and is also invisible for detections. Fig. 1(b) displays the surface current \(\mathbf{J}_s = -\hat{n} I_0/(2\pi R_1 \sin \theta)\) uniformly distributed along \(\varphi\) direction on a spherical surface which works equivalently to a dipole under the aforementioned transformation (In fact, as long as the total current \(\int_0^{2\pi} 2\pi R_1 \sin \theta (\mathbf{J}_s \cdot \hat{\theta}) \, d\varphi\) is equal to \(I_0\), the electric far field pattern will not be affected no matter how the current is distributed on the surface). It should be noticed that the \(\varphi\) component of the surface currents is zero in the transformed domain. It is easy to understand that at \(r = R_1\) only the current in the \(\theta\) direction can produce radiation while current in the \(\varphi\) direction will make no contribution to the radiation, because looking from the outside of the annulus, a current in the \(\varphi\) direction will only act like one point source on the line.
The electric fields in the transformed space can be obtained from (9). The working frequency is set at 2 GHz, while the inner ($R_1$) and outer radius ($R_2$) of the spherical shell are 0.05 and 0.1 m, respectively. To compare above two cases, the radiations of the initial dipole and the transformed antenna consisting of the metamaterial coating carrying the spherical surface current, as well as a subtraction between them are shown in Fig. 2(a)–(c), respectively, and we can notice that the field distribution outside the spherical region ($r > R_2$) are exactly the same. Therefore a conformal antenna with the same radiation pattern as a dipole but with a spherical shape is obtained.

We next consider how to map a circular plane of diameter $d$ to a spherical surface, which would yield an equivalent conformal array antenna. Suppose this finite plane is in the $y$-$z$ plane and the transformation take a similar form

$$\frac{x'^2}{b^2(r')} + \frac{y'^2}{a^2(r')} = 1$$

(11)

with $a(r) = R_2(r - R_1)/(R_2 - R_1)$, and $b(r) = (R_2 - d/2)(r - R_1) / (R_2 - R_1) + d/2$.

This transformation maps the circular plane with respect to the initial axes ($x', y', z'$) to a spherical surface $r = R_{1}$. Suppose there is a dipole array of $N$ elements pointing in the $y$ direction and placed along the $x$ axis in the initial space (within the plane of diameter $d$). Under this transformation, the currents of the dipole array will be mapped to the surface current on $r = R_{1}$. In other words, detected from outer domain $r > R_2$, it will appear that the emission is produced by this dipole array. Fig. 3(a) is the schematic of the transformation given in (11), where $N$ is assumed to be 3. The currents distributed on $r = R_{1}$ which will behave as three dipoles (depicted in Fig. 3(a) by red crosses) when the region $R_{1} < r < R_2$ is composed of the proposed transformed metamaterial can be calculated with (8) and are shown in Fig. 3(b).

With (9), we also calculate the electric field distributions of three dipoles in the initial space and the equivalent surface current in the transformed space, which is shown in Fig. 4(a) and (b), respectively, and the subtraction between them is again plotted in Fig. 4(c). The working frequency is 2 GHz, and the parameters are set as $R_{1} = 0.05$ m and $R_2 = 0.1$ m.

Design of conformal antennas is always an approach of interest to microwave engineers, creating antennas that conform to a surface whose shape is determined by considerations other than electromagnetic; for example, aerodynamic or hydrodynamic. The above two specific cases indicate the basic principle for the design of conformal antennas using coordinate transformation. Different from the traditional method based on Huygens’ principle which requires to simultaneously realize both the electric and magnetic currents on the aperture, here we simply use a metamaterial radome to control the current, and consequently the radiation without introducing non-practical perfect magnetic conductor or magnetic current. Not restricted to the proposed spherical cases, the virtual sources can be replaced by the currents on an arbitrary surface as long as we find an appropriate mapping.

IV. CONCLUSION

In summary, coordinate transformation is not restricted to source-free cases. The transformation on domains containing EM sources can also be studied by manipulating the Maxwell’s equations. Under transformations, not only the space but also the
sources can be transformed, and given access to proper metamaterials, the initial source of almost any shape and location can be replaced by another source with the same radiation properties. This makes the realization of new concept conformal antennas as illustrated in this letter.

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