A 4Gb/s/ch 356fJ/b 10mm equalized on-chip interconnect with nonlinear charge-injecting transmit filter and transimpedance receiver in 90nm CMOS

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This paper presents a transceiver for fast and energy-efficient global on-chip communication, consisting of a nonlinear charge-injecting (CI) 3-tap transmit filter (TX) and a sampling receiver (RX) with transimpedance pre-amplifier (TIA). Recently, pre-emphasis techniques [1-4] have demonstrated significantly better energy-efficiency than repeater interconnects. To further improve energy-efficiency over pre-emphasis techniques that require analog subtraction [3,5], our TX selects a pattern-dependent current to inject into the wire, performing feed-forward equalization (FFE) while mitigating the nonlinearity of the driver. This 3-tap charge-injecting (CI) FFE enables stronger equalization than the capacitively driven TX [1,2] or edge-detection pre-emphasis [4], achieving data-rate of 4Gb/s over a 1cm on-chip wire. The TIA at RX improves bandwidth, signal amplitude, and reduces bias power, breaking the trade-offs in conventional resistor termination [6], and mitigates equalized signal degradation due to impedance changes in dynamic current sensing [7].

Figure 3.6.1 depicts the overall link architecture with waveforms for single bit-flip pattern. Current sources at TX provide a small bias current for the TIA through signaling wires. The TX digitally computes and injects the FFE current (IT+ and IT-) into the wires. At RX, the received current (IR+ and IR-) is converted into a voltage (VS+ and VS-) by the TIA, and the slicers and DFE make a decision about the received bits.

The principle of CI FFE is shown in Fig. 3.6.2 through a conceptual comparison between the pull-down circuit of CI FFE and traditional analog FFE. For FFE coefficients (w0, w1, w2) where only w0 is negative (typical on a lossy channel) there are only 4 distinct values of IT for each direction (inward/outward): I0, I1, I2, and I0+I1+I2. Instead of having current sources with a size ratio of w0:w1:w2, the current sources in CI FFE have a I0:I1:I2 size ratio. Therefore, any value of IT can be created by addition only. This eliminates the current lost in analog FFE TX on subtraction. For example, when DD0D1D2='011', a CI FFE consumes only I0=I1=I2=I0+I1+I2 regardless of the pattern DD0D1D2. For random data, this reduces the power by half compared to analog FFE [3], with larger savings for lower activity rates.

Figure 3.6.3 shows a detailed block diagram of TX. To improve energy-efficiency, TX is designed in latch-based double-data-rate (DDR) style. TX has a weak driver design of accuracy and a strong driver designed for efficiency. Since I0 is much smaller (~30µA) and more sensitive than other current values, a differential current switch is used as the weak driver for accuracy. A strong driver injects large currents (I1, I2, and I0+I1+I2) on data transitions by driving the eight 5b PMOS or NMOS digital-to-analog converters (DACs) (P1, P2, N1, N2 for each terminal) rail-to-rail for most efficient charge delivery. Since DAC transistors are changing the region of operation as the output voltage swings from 0.5 to 0.9V (see Fig. 3.6.1), the DAC current and output impedance fluctuate. However, this nonlinearity is compensated by statically tuning each DAC segment (P1, P2, N1, N2).

Figure 3.6.4 shows a state-transition diagram of output-voltage change and driver control of TX. Since injected current IT+ depends on the transmitted data pattern, TX output voltage VT+ is determined by two consecutive data bits. For example, if DD0D1D2='011' is being transmitted, the state (‘D0’D1) changes from ‘11’ to ‘01’ (on a transition by D1) by conducting -I2 current via P2 and N2 segment. At the same time, the drain voltage of P2 segment also changes from middle level to high level. Since each state transition has unique voltage-change profile and injected current value, assigning a DAC code for each transition compensates the nonlinear behavior. Except for the transitions between ‘01’ and ‘10,’ coefficients are statically assigned since a single designated DAC segment drives each transition. With small accuracy cost, the transitions between ‘01’ and ‘10’ are done by turning on all strong-driver DACs and a weak driver, since the current errors of P1 and N1 when all segments are turned-on compared to other individual transitions cancel each other. A decoding block is implemented with small number of simple gates to control the DACs.

A TIA pre-amplifier is used in RX to combine the benefits of voltage-mode (VM) and current-mode (CM) signaling. In VM, as the termination impedance decreases, the received voltage decreases and static current increases, but the bandwidth also increases [6], while in CM, both the signal current and bandwidth increase. The TIA termination at RX provides small input impedance without large static current. The TIA has 860Ω input impedance for high bandwidth (~350MHz) and high current amplitude (~7.5µA) at 2GHz, and the received current is converted into voltage VTX (~19mV) by a 2.7kΩ TIA gain in simulation. The RX with TIA roughly doubles the received voltage at half the static current compared to VM signaling with direct 860Ω termination. After the TIA, the received voltage is fed into a 1-tap loop-unrolled DDF DFE [8]. The DFE is designed based on threshold-controllable Strong-Arm slicers and latches to minimize power and area cost.

A test link over 1cm on-chip differential M8 wires (0.6µm wide, 0.4µm spaced) is implemented in 90nm 1.2V CMOS process. By sweeping threshold voltage and clock delay of RX slicers, the BER and signal probability distributions are measured in situ [8] at room temperature. Figure 3.6.5 shows the in situ measured eye diagram at 4Gb/s with 98mV vertical and 50% UI horizontal eye. A BER test showed no errors within the test-setup-limited window of ~10^6 bits. The large eye size indicates good supply-noise immunity. Without equalization, the eye is completely closed. Only 3b out of the possible 5b DACs are used when equalized, implying potential tuning cost reduction. Although the DFE is implemented in the receiver, it is not used at 4Gb/s since the FFE provides sufficient equalization. Figure 3.6.6 shows the energy breakdown and comparison with most recent related work [1]. The energy breakdown is extracted by multiplying the measured current with energy breakdown ratio from postlayout simulation. The total transceiver energy cost is 356fJ/b. The pre-driver energy of 85fJ/b could have been smaller (~30fJ/b) since the pre-driver was oversized to handle higher data-rates. Since the DFE is not used, the DFE overhead of 30fJ/b is not included. The test-chip results show that this link design can operate about 2x faster at similar pitch for ~30% higher energy cost compared to [1]. The measured eye is larger than the eye at 1.756Gb/s reported in [1], increasing link robustness. Figure 3.6.7 is a die micrograph of the transceiver. The TX area is 1120µm^2 and RX area is 640µm^2.

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Figure 3.6.1: Overall link architecture with waveforms when ‘0001000’ pattern is transmitted.

Figure 3.6.2: Conceptual comparison between the pull-down circuits of charge injection FFE and analog subtraction FFE when D0D1D2=‘100’.

Figure 3.6.3: Block diagram of TX.

Figure 3.6.4: State transition diagram for TX control – ‘D0D1’ state with ‘D0’ transition.

Figure 3.6.5: Measured eye diagram with FFE and without DFE equalization.

Figure 3.6.6: Comparison with recent work.
Figure 3.6.7: Micrograph of 1×1mm² die.