Macroscopic Phase-Field Model of Partial Wetting: Bubbles in a Capillary Tube

The MIT Faculty has made this article openly available. Please share how this access benefits you. Your story matters.

Citation

As Published
http://dx.doi.org/10.1103/PhysRevLett.108.144502

Publisher
American Physical Society

Version
Final published version

Accessed
Fri Feb 15 08:56:19 EST 2019

Citable Link
http://hdl.handle.net/1721.1/71625

Terms of Use
Article is made available in accordance with the publisher's policy and may be subject to US copyright law. Please refer to the publisher's site for terms of use.

Detailed Terms
Macroscopic Phase-Field Model of Partial Wetting: Bubbles in a Capillary Tube

Luis Cueto-Felgueroso and Ruben Juanes

Massachusetts Institute of Technology, 77 Massachusetts Avenue, Building 48, Cambridge, Massachusetts 02139, USA

(Received 28 July 2011; published 5 April 2012)

Multiphase flow systems are often described by using upscaled mathematical models, aimed at capturing the relevant flow mechanisms while keeping the problem tractable in a computational or analytical sense. Upscaling procedures invoke approximations that reduce the dimensionality of the models, write equations at a scale that is much larger than the typical capillary length, or both. Examples are ubiquitous in fluid mechanics, from Lucas-Washburn laws during imbibition in nanopores [1,2] to basin-scale models of CO$_2$ migration in geologic carbon sequestration [3]. Assumptions of vertical flow equilibrium, or the lubrication approximation, permit reducing the dimensionality of thin film flows [4,5] and gravity currents [6], usually described by evolution equations for the height of the interface. By averaging the pore-scale processes over a representative elementary volume, multiphase flow through porous media is modeled by balance laws written in terms of fluid volume fractions, or saturations [7]. Necessarily, all these upscaled descriptions lead to loss of information about complex small-scale flow features. What is surprising, and disturbing, is that current theories fail to describe simple capillary phenomena, like a droplet on a flat surface or an air bubble at rest in a capillary tube [Fig. 1(a)]. The origin of the problem seems to lie in the macroscopic description of nonspreading systems associated to partial wetting.

The equilibrium shape of a water droplet deposited on a flat solid surface illustrates two regimes in wetting phenomena [8,9]. In the complete wetting regime, the droplet spreads over the solid surface, ultimately leaving a microscopic film attached to the solid. In the partial wetting regime, the droplet relaxes towards an equilibrium configuration, characterized by a static contact angle $\theta$. The transition from complete to partial wetting, or from spreading to nonspreading systems, is controlled by the interfacial energies through the spreading coefficient, $\Sigma = \gamma_{ss} - (\gamma_{sv} + \gamma)$, where $\gamma$ is the surface tension between the two fluids and $\gamma_{ss}$ and $\gamma_{sv}$ are the surface tensions associated with solid-fluid interfaces. Spreading systems ($\Sigma > 0$) are relatively well understood, and diffusive scaling laws for the evolution of relevant quantities have been derived and confirmed experimentally [1,5,8,9]. Nonspersing systems ($\Sigma < 0$), however, continue to challenge our mathematical descriptions. In some cases, such as thin film flows, the difficulty arises from the description of the dynamics of the contact line [5]. In volume-fraction-based models, the problem can be stated in mathematical

---

FIG. 1 (color online). Statics and dynamics of fluid slugs in a capillary tube. (a) Static configuration of an air bubble (transparent) between two slugs of water (dyed blue) in a glass capillary tube. The liquid-gas interface exhibits a well-defined contact angle, characteristic of a system with partial wetting. (b) Snapshot of an advancing liquid slug, blown by air from left to right. The leading interface advances with a contact angle that is larger than the static contact angle. At the back end of the slug, air penetrates through the center of the tube and leaves a macroscopic film of viscous fluid attached to the walls. The advancing contact angle and the film thickness are rate-dependent.
terms: how to obtain local, nonspreading, and compactly supported features—bubbles in a capillary tube—as steady-state solutions of a scalar, parabolic conservation law. Here, we address this latter challenge. We build a model of two-phase flow (e.g., air displacing water) in a capillary tube, which describes the flow dynamics through the evolution of gas and water saturations, $S_g$ and $S_w$, respectively, along the tube. The saturation of a fluid is the fraction of the cross-sectional area of the tube occupied by that fluid. Our simple 1D model captures hitherto unexplored capillary phenomena by accurately reproducing the thermodynamic equilibrium of the system. One of the fundamental advances in our model is that the steady-state solutions are bubbles or fluid slugs—local, nonspreading, compactly supported features.

The transition from the capillary-dominated to the viscous-dominated regimes is another fascinating aspect of our model. Physically, multiphase systems often exhibit “dynamic” behavior, that is, flow features that are rate-dependent, like contact angles [8–11], displacement efficiencies [12–14], capillary pressures [15–17], fractional flow [18], or displacement pattern morphologies [19–21]. For instance, when air is injected at a constant rate in a tube initially filled with a viscous fluid, the invading air forms an advancing finger that leaves a macroscopic film of the viscous fluid attached to the tube walls [Fig. 1(b)] [12, 13]. The thickness of the film increases monotonically with the capillary number $C_a = U \eta_w/\gamma$, where $U$ is the velocity of the finger tip, $\eta_w$ is the viscosity of the invading fluid, and $\gamma$ is the surface tension between the fluids [14, 22–24]. Here, we show that rate dependency of the global displacement patterns, such as the amount of fluid left behind in the classical Bretherton experiment, can be explained and modeled as the competition between capillary and viscous forces, without resorting to rate-dependent constitutive relations.

We consider incompressible, isothermal two-phase flow in a tube, driven by imposed pressure gradients and capillary forces. The evolution of fluid saturations can be expressed as conservation of mass of the fluids, $\partial_t S_\alpha + \nabla \cdot u_\alpha = 0$ with $\alpha = g, w$, subject to the constraint $S_g + S_w = 1$. We assume gradient-type volumetric fluxes $u_\alpha = -\lambda_\alpha \partial_s \Pi_\alpha$, where $\lambda_\alpha$ denotes the mobility of phase $\alpha$. In the classical models, the flow potentials $\Pi_\alpha$ are identified as averaged fluid pressures [7, 17]. In contrast, we follow the framework of E and Palffy-Muhoray for incompressible polymer mixtures [25, 26] and split the potentials as $\Pi_\alpha = \mu_\alpha + p + \rho_\alpha g z$, where $\mu_\alpha$ is the chemical potential derived from a phenomenological free energy functional of the two-component system, $p$ is the pressure, which enforces the incompressibility constraint, $\rho_\alpha$ is the fluid density, and $g$ is the gravitational acceleration. After algebraic manipulation, assuming for now a horizontal tube, and using gas saturations as primary variables, the model reads

$$\partial_t S_g + \partial_x (f_g u_T + \lambda_g (1 - f_g) \partial_x (\mu_w - \mu_g)) = 0, \quad (1)$$

$$\partial_t u_T = 0, \quad (2)$$

$$u_T = -[(\lambda_g + \lambda_w) \partial_x \Pi_g + \lambda_w \partial_x (\mu_w - \mu_g)]. \quad (3)$$

The fractional flow function $f_g = \lambda_g / (\lambda_g + \lambda_w)$ is a nonconvex, $S$-shaped function of the gas saturation that controls the viscous-dominated flow regime. Closure of the model (1)–(3) requires specifying constitutive relations for the fluid mobilities $\lambda_\alpha$ and the thermodynamic potentials $\mu_\alpha$. We set the gas and water mobilities as $\lambda_g = R^2 S_g/8 \eta$ and $\lambda_w = R^2 S_w/8 \eta$, respectively, where $R$ is the radius of the tube and $\gamma(S_g)$ is an averaged viscosity of the mixture. For simplicity, we assume that $\eta^{-1}$ is linear with the fluid saturations: $\eta^{-1} = \eta_w^{-1} + (\eta_w^{-1} - \eta_g^{-1}) S_g$.

The chemical potential difference $\mu_w - \mu_g$ plays a central role in the structure of saturation profiles at equilibrium ($u_T = 0$). In traditional models, this difference in chemical potential is understood as a monotonic function of the phase saturation—the so-called capillary pressure function [7]. While a term of such nature can describe diffusive, spreading behavior [1, 7], nonspreading static fundamental advances in our model is that the steady-state solutions are compactly supported features.

To construct the $F$ functional, we follow the classical theory of phase separation of Cahn and Hilliard [27], and de Gennes’s model for incompressible polymer mixtures [25]. We approximate the specific free energy as the sum of bulk, $F_0$, and interfacial, $F_i$, free energies. The former is solely a function of fluid saturations, while the latter includes gradient terms: $F = F_0(S_g, S_w) + F_i(S_g, S_w, \nabla S_g, \nabla S_w)$. Our basic requirements are that two stable states of the free energy correspond to the bulk fluids, $S_g = 1$ and $S_w = 1$, and that differences in chemical potential between bulk fluids are consistent with the Young-Laplace equation $[[\mu_g]] = 2 \gamma \cos \theta / R$, where $[[\mu_g]] = \mu_g|_{S_g=1} - \mu_g|_{S_g=0}$. The simplest specific free energy satisfying these conditions is

$$F = -\frac{\gamma_{sg} - \gamma_{sw} - \gamma}{R} (1 - S_g)^2 (1 - S_w)^2$$

$$+ \frac{\gamma_{sw} - \gamma_{sg}}{R} [(1 - S_g)^2 - (1 - S_w)^2]$$

$$+ \frac{\Gamma}{4} \kappa(S_g, S_w)((\partial_x S_g)^2 + (\partial_x S_w)^2). \quad (4)$$

In the following, we consider strictly nonspreading systems, $\gamma_{sw} - \gamma_{sg} - \gamma < 0$, for which the three surface energies are linked through the static contact angle, $\gamma_{sw} - \gamma_{sg} = \gamma \cos \theta$. Note that we define the contact angle $\theta$ with respect to the “gas” phase, regardless of which phase is more dense. Based on the above free energy, the
The position of the interface is determined as 
\[ \theta = \theta_c \] for \( \theta < 90^\circ \) and \( \theta > 90^\circ \). The equilibrium saturation transitions (menisci) for a given static contact angle. By construction, the free energy functional [Eq. (4)] leads to pressure jumps across interfaces that are consistent with the Young-Laplace equation.

FIG. 2 (color online). (a),(b) Steady-state configurations, obtained by numerically solving the model equations (1)–(3) with \( u_T = 0 \), and their axisymmetric interpretation of the fluid distribution along the tube: a gas bubble surrounded by a wetting fluid such as water (a) or by a nonwetting fluid such as mercury (b). The position of the interface is determined as \( h_\delta = \sqrt{S_g} \) for \( \theta > 90^\circ \) and \( h_\delta = \sqrt{1 - S_g} \) for \( \theta < 90^\circ \). The equilibrium saturation and pressure profiles change with the static contact angle.
To test the ability of our model to capture the dynamic features of air-water displacements, we simulate constant-rate air injection into a water-filled circular tube (Fig. 3). We explain the classical experimental observations [12–14], in which a film of the defending fluid is left attached to the tube walls, as a result of the competition between capillary and viscous forces. In our model, capillary terms induce phase separation and therefore a complete displacement of the resident fluid, while viscous forces, represented by the hyperbolic term in Eq. (1), tend to create a fast displacement along the center of the tube that leaves a film of the more viscous fluid behind. Our simulations honor this behavior: At small capillary numbers, the meniscus advances through contact-line motion. Mathematically, the parabolic term dominates, and therefore the behavior of the solutions resembles phase separation. For large capillary numbers, viscous forces dominate, and thick water films are left behind attached to the walls [Fig. 3(b)]. In mathematical terms, the hyperbolic term dominates, and the saturation profile resembles the classical Lax shock solution [Fig. 3(a)]. For intermediate capillary numbers, the gas saturation profiles exhibit undercompressive shocks with a plateau, induced by the structure of the bulk free energy and the presence of the fourth-order term [31].

Under dynamic conditions, which drive the system out of capillary equilibrium, the symmetry of displaced bubbles or slugs is broken as the capillary number increases. We simulate the displacement of a capillary bridge by air at a constant rate (Fig. 4). In quasistatic conditions \( Ca \to 0 \), the water slug is displaced almost completely, and therefore the symmetry is essentially retained: The advancing and receding contact angles are similar. Higher capillary numbers lead to steeper fronts, inducing a transition. As \( Ca \to \infty \), the symmetry is lost, and films are left behind. In accordance with the classical experiments of Hoffman [8,10], the advancing contact angle increases with the flow rate. This effective dynamic behavior of the contact...
angle is a fascinating feature of our model, which emanates from the competing effects of the various terms in the governing equations. Other interesting features of capillary phenomena in confined geometries could be analyzed with extensions of the proposed model. These may include instabilities in core-annular flow [32] or the effect of spatial variations in pore geometry and surface properties [11,33,34], limited to cases where the 1D upscaling is appropriate.

As a further quantitative assessment of the model predictions, we consider the rise of a meniscus in a vertical capillary, as predicted by our model and the Lucas-Washburn theory (Fig. 5). The dimensionless parameter comparing gravitational and capillary forces is the Bond number $Bo = \Delta \rho g R^2 / \gamma \cos \theta$, where $\Delta \rho = \rho_w - \rho_g$ is the density difference between fluids.

It is well understood that upscaled capillary phenomena often require higher-order mathematical models. Surprisingly, it has been commonly accepted that upscaled descriptions of important multiphase flows, in particular, flow through porous media, can be cast as second-order, nonlinear advection-diffusion equations. Here we show that a phase-field formulation captures static and dynamic features of such flows that are precluded within the classical theories. Local, nonspreading structures, which are characteristic of partially wetting systems, can be obtained as steady-state solutions in the absence of external forces. Pseudodynamic effects emerge naturally as the transition from the capillary-dominated regime to the viscous-dominated regime. The present study suggests that a paradigm shift towards higher-order models in the macroscopic description of multiphase flow through porous media may henceforth be warranted [35].

Funding for this research was provided by Eni S.p.A. under the Multiscale Reservoir Science project and by the ARCO Chair in Energy Studies.