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CNT-BASED GAS IONIZERS WITH INTEGRATED MEMS GATE FOR PORTABLE MASS SPECTROMETRY APPLICATIONS

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ABSTRACT

We report the fabrication and experimental characterization of a novel low-cost carbon nanotube (CNT)-based electron impact ionizer (EII) with integrated gate for portable mass spectrometry applications. The device achieves low-voltage ionization using sparse forests of plasma-enhanced chemical vapor deposited (PECVD) CNTs field emitter tips, and a proximal gate with open apertures to facilitate electron transmission. The gate is integrated using a deep reactive ion etched (DRIE) spring-based high-voltage MEMS packaging technology. The device also includes a high aspect-ratio silicon structure (µfoam) that facilitates sparse CNT growth and limits the electron current per emitter. The devices were tested as field emitters in high vacuum (10⁻⁸ Torr). Electron emission starts at a gate voltage of 110 V, and reaches a current of 9 uA at 250 V (2.25 mW) with more than 55% of the electrons transmitted through the gate apertures. The devices were also tested as electron impact ionizers using Argon. The experimental data demonstrates that the CNT-EIIs can operate at mtorr-level pressures while delivering 60 nA of ion current at 250 V with about 1% ionization efficiency.

KEYWORDS

Carbon nanotubes (CNTs), DRIE, gas ionizer, electron impact ionization, field emission, portable mass spectrometry, 3D MEMS packaging.

INTRODUCTION

MEMS-based analytical instrumentation has been an active area of research for more than a decade. In particular, some research efforts have focused on the development of rugged gas chromatography and mass spectrometry (GC/MS) systems that are smaller, lighter, cheaper, faster, and more power efficient [1], [2]. The power consumption, size, and weight of these systems are driven by the pumping requirements. Therefore, the relaxation of the pressure level at which the system components can operate would enable its portability. Portable GC/MS systems, either as individual units or as part of massive networks, can be used in a wide range of applications including in-situ geological survey, law enforcement, environmental monitoring, and space exploration [3]–[5].

One of the core components of an MS system is the ionizer. In electron impact ionization, a stream of electrons is used to ionize neutral gas molecules by collision. The ratio between the ion current $I_i(E)$ to the electron current $I_E(E)$ is

$$\frac{I_i(E)}{I_E(E)} = \frac{P}{K_b \cdot T} \cdot \sigma_{total}(E)$$

where $E$ is the energy of the electrons, $P$ is the gas pressure, $K_b$ is Boltzmann’s constant, $T$ is the gas temperature, $L$ is the collision path length (i.e., the distance between the electron source and the ion collector), and $\sigma_{total}(E)$ is the total ionization cross section. State-of-the-art EIIs for MS systems accomplish ionization using a thermionic electron source. Thermionic-based EIIs are power hungry (>1W), can only operate at low pressure (<10⁻⁵ torr) due to back-ion bombardment reliability, and have low ionization efficiency [6], [7]. Therefore, thermionic-based EIIs are not suitable for portable mass spectrometry.

A low-power approach to implement EIIs for portable MS systems involves the use a cold cathode. Electrons are field emitted from the surface of metals and semiconductors when the potential barrier that holds electrons within the material (workfunction) is deformed by the application of a high electrostatic field [8]. High surface electrostatic fields are typically obtained by the application of a voltage to a high aspect-ratio structure with nanometer-scaled tip radius. Field emission is described by the Fowler-Nordheim (FN) model, which predicts that the electron current $I_E(V_G)$ from a tip biased at a voltage $V_G$ has an exponential dependence with respect to the field factor $\beta$ [8]:

$$I_E(V_G) \approx V_G^2 \cdot \exp \left( \frac{-0.95 \cdot B \cdot \phi^{1.5}}{\beta \cdot V_G} \right)$$

where $B = 6.87 \times 10^7$ and $\phi$ is the workfunction of the emitter tip. The inverse of the field factor has dimensions of length. The field factor relates the electric field at the tip surface to the applied gate voltage and it is to first order equal to the inverse of the emitter tip radius $r$. 
DEVICE STRUCTURE AND DESIGN

Our NEMS/MEMS CNT-EII (Fig. 1) is composed of two parts which are 1) a main body and 2) a gate. The main body (Fig. 2) is a two-wafer stack that includes sparse arrays of plasma enhanced chemical vapor deposited (PECVD) CNTs, a high aspect-ratio silicon structure (μfoam), and a system of DRIE patterned springs to assemble the gate to the main body. The gate is a 1-cm wide disk-shaped component with a perforated grid that includes a set of notches that are used to lock-in the gate (Fig. 3, left). The μfoam structure and the gate grid do not line up (Fig. 3, right) because the gate is used as a shadow mask during the deposition of the CNT catalyst.

Figure 1: An assembled CNT-based gated electron impact ionizer (left), and cross-section of the device (right).

Figure 2: SEMs of the CNT-EII main body: spring assembly system (top left), μfoam (top right), sparsely grown CNTs (bottom left), and detail of the PECVD CNTs (bottom right).

Figure 3: A DRIE-patterned assembly spring locked into a gate notch (left), and top view of the μfoam through an assembled gate using backside light (right).

DEVICE FABRICATION

Two silicon wafers are required to fabricate the ionizer. The two wafers are used to fabricate the main body, while portions of one of the wafers are used to fabricate the MEMS gate. The main fabrication technologies used in the process flow are contact photolithography, fusion bonding, and DRIE. The PECVD CNTs are sparsely grown using a combination of selective growth [9] and shadow masking, using the PECVD CNT growth process described by Teo et al [15].
The ionizer gate is integrated using a high-voltage MEMS packaging technology based on DRME-patterned mesoscaled deflection springs [10]. The gate is reversibly assembled with micron-level precision and micron repeatability, and it can also withstand large inertial forces without detaching [11]. This assembly technology makes it possible to define the CNT catalyst and grow the CNTs without affecting the electrical insulation of the device. Further details are given elsewhere [16].

EXPERIMENTAL CHARACTERIZATION

The CNT-EIIIs were tested as field emitters and as electron impact ionizers. In both cases the gate was biased positive with respect to the main body, and there was an external ball collector biased at 1100V with respect to the main body of the CNT-EII.

The CNT-EIIIs were tested as field emitters in high vacuum ($10^{-8}$ Torr). The data shows that electron emission above the noise floor ($10^{-11}$ A) starts at a gate voltage of 110 V, with an emitted electron current of 9 uA at 250 V (Fig. 4). More than 55% current transmission through the gate was measured. The percentage of current transmitted through the gate is more than an order of magnitude larger than the percentage of current transmitted we previously reported using a µfoam structure with a non-aligned grid [9]. We speculate that a larger current transmission could be obtained if the gate were able to apply a more symmetric electric field around the CNT tips. This is currently not possible due to fabrication constraints (the aperture of the gate grid would need to be of the order of the CNT-to-gate separation) and alignment limitations of the spring assembly. The emitted current is visibly smaller than the mA-level electron current we previously reported from the µfoam structure [9]. However, unlike in our previous report, the electron current coming out of the µfoam is clearly limited, as evidenced by the FN plot (Fig. 5). The current limitation effect seems to be related to the high aspect-ratio of the µfoam structure, and the high resistivity (> 50 Ω.cm) of the silicon substrate used to create it. The µfoam acts as an ungated field-effect transistor (FET) that limits the current due to velocity saturation of electrons in silicon [12], [13]. The linear part of the FN plot predicts a field factor $\beta = 3.3 \times 10^7$/cm. Using $\phi = 4.8$ eV, and assuming $\beta \sim r^{-1}$, it is estimated a CNT tip diameter equal to 61 nm, in good agreement with the 67 nm value from SEMs.

The devices were also tested as EIIs using Argon (Fig. 6). The device produces ion currents larger than the noise floor ($\sim 5 \times 10^{-12}$ A) at a gate voltage of 125 V and an acceleration voltage of 300 V. At a gate voltage of 250 V, and ion current of 60 nA was measured while operating at 1 mtorr. As shown in Fig. 7, the ion current scales linearly with the background pressure, as expected from Eq. (1). In addition, using the values $\sigma_\text{total} \sim 3 \times 10^{-16}$ cm$^2$, $K_0 = 1.38 \times 10^{-23}$ J/K, $T = 300$ K, and $L \sim 3$ cm, an intercept equal to -1.52 is obtained vs. -1.31 from the linear fit of the data. Based on the field emission and electron impact ionization data, about 1% ionization efficiency is estimated when de ionizer operates at 1 mtorr. The ionization efficiency is defined as the number of ions per electron, i.e., the ratio between the ion current and electron current.
Figure 7: Ratio of ion current to electron current vs. pressure.

Our ionizer compares favorably with respect to the work reported by other researchers. For example, the electron current level and operational voltage is substantially larger than the performance of nanostructured boron nitride cathodes reported by Liu et al [17]. Also, the ionization efficiency is comparable to the ionization efficiency reported by Chen et al at a slightly higher pressure [18]. However, our ionizer should have higher ionization efficiency if operated at higher pressures. In addition, our ionizer has an estimated field factor in the linear part of the FN plot that is 50% larger than the corresponding values reported by Manohara et al [19], which should be related to the shadowing effect that their CNTs suffer due to their proximity within the same fiber.

REFERENCES

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