**Cavity-enhanced multispectral photodetector using phase-tuned propagation: theory and design**

The MIT Faculty has made this article openly available. **Please share** how this access benefits you. Your story matters.

<table>
<thead>
<tr>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>As Published</td>
<td><a href="http://dx.doi.org/10.1364/OL.35.000742">http://dx.doi.org/10.1364/OL.35.000742</a></td>
</tr>
<tr>
<td>Publisher</td>
<td>Optical Society of America</td>
</tr>
<tr>
<td>Version</td>
<td>Final published version</td>
</tr>
<tr>
<td>Accessed</td>
<td>Fri Dec 28 14:37:46 EST 2018</td>
</tr>
<tr>
<td>Citable Link</td>
<td><a href="http://hdl.handle.net/1721.1/79688">http://hdl.handle.net/1721.1/79688</a></td>
</tr>
<tr>
<td>Terms of Use</td>
<td>Article is made available in accordance with the publisher's policy and may be subject to US copyright law. Please refer to the publisher's site for terms of use.</td>
</tr>
<tr>
<td>Detailed Terms</td>
<td></td>
</tr>
</tbody>
</table>
Cavity-enhanced multispectral photodetector using phase-tuned propagation: theory and design

Jianfei Wang, Juejun Hu,* Xiaochen Sun, Anu Agarwal, and Lionel C. Kimerling

Microphotonics Center, Massachusetts Institute of Technology, Cambridge, Massachusetts 02139, USA

Received October 5, 2009; revised November 14, 2009; accepted January 7, 2010; posted January 26, 2010 (Doc. ID 118216); published February 26, 2010

We propose and theoretically analyze what we believe to be a novel design of cavity-enhanced photodetectors capable of sensing multiple wavelengths simultaneously in a single pixel. The design is based on phase-tuned propagation of resonant modes in cascaded planar resonant cavities. We show that this concept can be generalized to detect multiple wavelength combinations covering the entire near to far infrared spectrum. Besides its multispectral detection capability, the design also features minimal spectral cross talk and significantly suppressed noise. The intrinsic design versatility and scalability, as well as process compatibility with planar microfabrication, suggest the design’s wide application potential for telecommunications, infrared imaging, and biochemical sensing. © 2010 Optical Society of America

OCIS codes: 310.6805, 040.5160, 110.4234, 040.3060

Multispectral infrared (IR) detection has been widely employed for applications including hyperspectral imaging, IR spectroscopy, and target identification. Traditional multispectral technology is based on the combination of single spectral focal plane arrays (FPAs) and spectral filters or spectrometers, which require bulky high-cost mechanical scanning instruments and have a slow response. Single pixels capable of detecting multiple wavebands simultaneously thus have become the focus of the third generation FPA development [1]. Recently, three-color HgCdTe photodiodes have been demonstrated, although their spectral cross talk is large (>10%) [2]. A competing multicolor detector technology is quantum-well IR photodetectors (QWIPs) [1]. However, the QWIP device optimization is limited by its low quantum efficiency (QE) (<10%) [3]. Other alternative solution tandem detectors have limited band selection options and large cross talk issues due to material compatibility issues and radiative coupling. A solution, which combines a high QE and a low spectral cross talk, is yet to be explored.

Our approach involves a multilayer cascaded cavity structure shown schematically in Fig. 1. Each wavelength to be detected leads to a unique resonant mode locally confined within one cavity, where an absorbing active layer is placed for spectral selective detection of this wavelength. The major challenge is the spatial localization of the resonant modes without compromising the QE. Our solution employs a novel phase-tuned propagation design. We insert phase-tuning layers between the cascaded cavities to control the optical phase and hence the coupling strength between the incident light and the resonant modes. Thereby, we show that near unity QEs can be achieved for all cavities. Comparing to previous work on multispectral detection using a single cavity [4], spectral cross talk is significantly suppressed given the wavelength-selective spatial localization of resonant modes in different cavities. The electrical signal originating from each wavelength may be separately read out by contacting the corresponding active layer, either in a photoconductive [4] or in a photovoltaic mode. Further, since resonant cavity enhancement effect leads to field buildup in the cavity and dramatically increases absorption, IR active layers with reduced thicknesses can be used while maintaining near-unity QEs. Consequently, detector noise can be suppressed without compromising responsivity. In this Letter, we theoretically analyze the design principles of the multispectral pixel design using the transfer matrix method (TMM).

To start with, we consider an IR active layer sandwiched within a generic multilayer resonant cavity stack, where near-unity IR absorption (internal QE) can be attained when the critical coupling condition is met at the resonant wavelength,

\[ R_t = (1 - A_L)R_b, \quad R_b < 1, \]

where \( R_t \) and \( R_b \) are the reflectivities of top and bottom mirrors and \( A_L \) denotes the optical resonant mode loss. When the cavity quality factor \( Q \gg 1 \), \( A_L \) can be calculated using cavity perturbation theory as

\[ A_L = \epsilon d \int \frac{|E_0|^2 dV}{\text{active}} - \int \frac{|E_0|^2 dV}{\text{stack}}, \]

Fig. 1. (Color online) Cross sectional schematic of a multispectral pixel consisting of cascaded planar resonant cavities (not drawn to scale).

© 2010 Optical Society of America
where $\varepsilon$ and $\alpha$ are the dielectric constant and the absorption coefficient of the IR active material, $d$ is the cavity length, $E_0$ denotes the electric field distribution of the resonant mode, and $e_c$ gives the dielectric constant profile of the stack. Notably, when the active material completely fills the cavity between the two mirrors, $A_L$ can be given as $(1-e^{-2\alpha d})$ and Eq. (1) reduces to the critical coupling formulation by Unlu and Strite [5]. Equation (1) states that given a bottom mirror with near unity reflectivity ($R_1 \sim 1$), the maximum QE at the resonant wavelength may be obtained by choosing a top mirror reflectivity ($R_t$) to satisfy Eq. (1).

Now we apply the above analysis to the $i$th ($i=1, 2, 3, \ldots$) cavity in Fig. 1. As shown in Fig. 2, the “top mirror” of the $i$th cavity includes cavities 1 to $i-1$. To satisfy Eq. (1), we insert a coupling-matching layer $m$ in the top mirror stack to allow effective tuning of the top mirror reflectivity $R_{t,i}$ (the second subscript $i$ denotes the sequential number of cavity in the stack).

Here we use TMM to derive the top mirror reflectivity $R_{t,i}$ of the $i$th cavity as shown in Fig. 2. Following the convention of Sun [6], we label the layers sequentially starting from the incident medium. The transfer matrix $T_i$ of the entire stack may be written as

$$T_i = T_M^{-1}M_1L_mT_{(2)}, \quad (3)$$

where $T_{(2)}$ corresponds to the transfer matrix of layers from the first to the ($i-1$)th cavity including the $m$th coupling-matching layer and $T_{(3)}$ is the transfer matrix of the quarter-wavelength stack (QWS) designed for the $i$th cavity's resonant wavelength $\lambda_i$. It can be proven that the matrix $T_{(2)}$ may be generically represented as

$$T_{(2)} = M_{m-2p}^{-1}(M_{m-1}L_{m-1}M_{m-1}^{-1}) \cdots (M_{m+1}L_{m+1}M_{m+1}^{-1})M_{1} = (i)^{2p-1}
\begin{pmatrix}
A + B & -A + B \\
-A - B & -A - B
\end{pmatrix}, \quad (5)$$

where

$$A = \frac{n_1}{2n_1+1} \left( \frac{n_{m+2}}{n_{m+1}} \right)^{p-1}, \quad B = \frac{n_{m+2}}{2n_1+2p} \left( \frac{n_{m+1}}{n_{m+2}} \right)^{p-1}. \quad (6)$$

Substituting Eqs. (7) and (8) into Eq. (6), we have

$$R_{t,i} = |r|^2 = \frac{T_{21}}{|T_{22}|} = \frac{\left| A_{m}(T_{222})e^{i(\theta_{21}+\theta_{22})} - T_{222}e^{2i\delta_m} + B_{1}(T_{222})e^{i(\theta_{21}+\theta_{22})} + T_{222}e^{2i\delta_m} \right|^2}{\left| T_{222} \right|^2}, \quad (7)$$

where $\delta_m = (2\pi/\lambda_i)n_mt_m$, and $n_m$ and $t_m$ are the refractive index and the thickness of the $m$th layer, i.e., the coupling-matching layer at $\lambda_i$. Such a functional dependence provides a lever to tune $R_{t,i}$ simply by adjusting $t_m$ to satisfy Eq. (1) and thereby reach a near unity QE. In the example we give later, we illustrate how this condition can be solved graphically.

There are two special cases though where the $R_{t,i}$ tuning mechanism fails. When the resonant wavelength of the $i$th cavity $\lambda_i$ falls in one of the stop bands of cavities 1 to $i-1$, $R_{(2)} \sim 1$ and $|T_{(22)}|$

Fig. 2. Structures used in deriving the coupling-matching condition for cavity $i$. Stack (1) is the entire structure which can be decomposed into stacks (2) and (3). The layers corresponding to stack (1) are also shown in Fig. 1. The matrix of the quarter-wavelength stack (QWS) designed for the $i$th cavity’s resonant wavelength $\lambda_i$. It can be proven that the matrix $T_{(2)}$ may be generically represented as

$$T_{(2)} = M_{m-2p}^{-1}(M_{m-1}L_{m-1}M_{m-1}^{-1}) \cdots (M_{m+1}L_{m+1}M_{m+1}^{-1})M_{1} = (i)^{2p-1}
\begin{pmatrix}
A + B & -A + B \\
-A - B & -A - B
\end{pmatrix}, \quad (5)$$

where $T_{(2)}, T_{(222)}, \theta_{22}$, and $\theta_{22}$ are functions of $\phi_j$, $n_j$, $\mu_j$, $t_j$ ($j=1$ to $m$), and $\lambda$. In high-index-contrast Bragg cavities, the angular dependence of spectral response is minimal. Practically we only need to consider normal incidence. $T_{(3)}$ then follows ($\lambda = \lambda_i$, $p$ pairs)

$$T_{(3)} = M_{m-2p}^{-1}(M_{m-2p-1}L_{m-2p-1}M_{m-2p-1}^{-1}) \cdots (M_{m+1}L_{m+1}M_{m+1}^{-1})M_{1} = (i)^{2p-1}
\begin{pmatrix}
A + B & -A + B \\
-A - B & -A - B
\end{pmatrix}, \quad (5)$$

where $\delta_m = (2\pi/\lambda_i)n_\lambda t_m$, and $n_\lambda$ and $t_\lambda$ are the refractive index and the thickness of the $m$th layer, i.e., the coupling-matching layer at $\lambda_i$. Such a functional dependence provides a lever to tune $R_{t,i}$ simply by adjusting $t_\lambda$ to satisfy Eq. (1) and thereby reach a near unity QE. In the example we give later, we illustrate how this condition can be solved graphically.

There are two special cases though where the $R_{t,i}$ tuning mechanism fails. When the resonant wavelength of the $i$th cavity $\lambda_i$ falls in one of the stop bands of cavities 1 to $i-1$, $R_{(2)} \sim 1$ and $|T_{(22)}|$
(1) Select mirror materials for the N wavelengths to avoid overlapping \( \lambda_i \) and the photonic stop bands of cavities 1 to \( i-1 \), and to minimize parasitic loss due to mirror absorption.

(2) Start from the first cavity on top of the stack and choose appropriate numbers of top/bottom mirror QWS pairs to satisfy Eq. (1).

(3) Move on to the next cavity \( i \) and adjust the coupling-matching layer thickness sandwiched between cavity \( i-1 \) and cavity \( i \) so that the critical coupling condition is met.

(4) Repeat steps (2) and (3) until the entire stack design is complete.

As an example to validate the principles, \( \lambda_1 = 1550 \text{ nm} \) and \( \lambda_2 = 3600 \text{ nm} \) are chosen as the two wavelengths to be detected. \( \text{As}_2\text{S}_3 \) and \( \alpha\text{-Ge} \) are used as the mirror materials given their IR transparency. PbTe layers are used as IR absorbers in both cavities. The wavelength-dependent refractive indices are measured using IR ellipsometry [7].

Figure 3(a) shows a schematic cross section of the pixel designed following the above procedures, and Fig. 3(b) illustrates graphic solutions to the critical coupling condition (1). Here we use a 340-nm-thick Ge layer between the two cavities as the coupling-matching layer (pair No. = 2). Figure 3(c) shows the QE spectra for the two PbTe absorbers. The peak QE over 80% is realized in both wavebands with only 50 and 100 nm thick PbTe absorbers given the strong resonant cavity enhancement. In comparison, a conventional free-space PbTe detector operating at 3600 nm wavelength requires an absorber as thick as 10 \( \mu \text{m} \). Consequently, the \( G-R \) and Johnson noise in our design will be ten times lower, since both types of noise scale with the square root of the active material volume. The ripples between peaks (side lobes) can be suppressed by integrating a planar band-stop filter or employing an apodized cavity design.

Besides the high QE, the high degree of spatial localization of modes effectively minimizes the spectral cross talk. Figure 3(d) plots the light intensity distributions in the stack at the two resonant wavelengths. The spectral cross talk in a dual wavelength detector can be measured using [8]

\[
\text{Cross talk} = \frac{\eta_{\text{active}2}(\lambda_1)}{\eta_{\text{active}2}(\lambda_2)}, \quad \lambda_1 < \lambda_2, \tag{8}
\]

where \( \eta_{\text{active}2}(\lambda_1) \) is the QE of the second active layer at \( \lambda_1 \), and \( \eta_{\text{active}2}(\lambda_2) \) is the peak QE of the second active layer at \( \lambda_2 \). Our design gives a spectral cross talk as low as 0.1%, more than 2 orders of magnitude lower compared to a tandem design [8] or a single cavity design [4].

To summarize, we propose and analyze a versatile and scalable design for cavity-enhanced photodetectors capable of sensing multiple wavebands simultaneously in a single pixel. The design is based on phase-tuned propagation in cascaded planar resonant cavities and this concept can be generalized to detect virtually any arbitrary number of wavelengths. This proposed pixel structure combines a high QE, reduced detector noise, as well as a low cross talk, and thus may find wide applications in security surveillance, imaging, and spectroscopy.

This work is supported by the Singapore DSO National Laboratories.

References