Entanglement-Enhanced Sensing in a Lossy and Noisy Environment

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Entanglement-Enhanced Sensing in a Lossy and Noisy Environment

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Nonclassical states are essential for optics-based quantum information processing, but their fragility limits their utility for practical scenarios in which loss and noise inevitably degrade, if not destroy, nonclassicality. Exploiting nonclassical states in quantum metrology yields sensitivity advantages over all classical schemes delivering the same energy per measurement interval to the sample being probed. These enhancements, almost without exception, are severely diminished by quantum decoherence. Here, we experimentally demonstrate an entanglement-enhanced sensing system that is resilient to quantum decoherence. We employ entanglement to realize a 20% signal-to-noise ratio improvement over the optimum classical scheme in an entanglement-breaking environment plagued by 14 dB of loss and a noise background 75 dB stronger than the returned probe light. Our result suggests that advantageous quantum-sensing technology could be developed for practical situations.

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Quantum information processing (QIP) exploits fundamental quantum-mechanical properties to realize capabilities beyond the reach of classical physics. Nonclassical states are essential for optics-based QIP, providing the bases for quantum teleportation [1–3], device-independent quantum key distribution [4], quantum computing [5,6], and quantum metrology [7]. Nonclassical states can increase the signal-to-noise ratios (SNRs) of quantum-metrology systems. Indeed, squeezed states have been employed to beat the classical-state limits in optical-phase tracking [8,9], biological sensing [10], and gravitational wave detection [11,12]. Squeezed states, however, are vulnerable to loss: a 10 dB SNR enhancement without loss degrades to 1 dB in a system with 6 dB of loss. Under ideal conditions, N00N states, which are superposition states of N photons in one mode and vacuum in another mode, and vice versa, yield SNR improvements comparable to those of squeezed states [13–16], but noise injection can easily render N00N states impotent in this regard [17,18]. Consequently, quantum decoherence, arising from environmental loss and noise, largely prevents any quantum-sensing performance advantage, casting doubt on the utility of QIP systems for practical situations.

Quantum illumination (QI) is a radically different paradigm that utilizes nonclassical states to achieve an appreciable performance enhancement in the presence of quantum decoherence. QI can defeat eavesdropping on a communication link [19–22], and boost the SNR of a sensing system [23–29]. QI systems are comprised of (1) a source that emits entangled signal and idler beams; (2) an interaction in which the signal beam (used as a probe) is subjected to environmental loss, modulation, and noise en route from the source to the receiver; and (3) a receiver that makes a joint measurement on the returned signal beam and the idler beam, which has been stored in a quantum memory, to extract information about the environment’s modulation of the signal. QI’s performance advantage over classical schemes of equal probe energy derives from the fact that QI’s initial entanglement—all though destroyed by the lossy, noisy environment—creates a correlation between the returned and retained light that is much stronger than what can be obtained with classical resources. The joint-measurement receiver relies on this stronger signature to achieve its better-than-classical performance. The QI-enabled performance advantage in a secure communication system was demonstrated in Ref. [21]: the measured bit-error rate (BER) for the legitimate parties in that experiment was 5 orders of magnitude lower than the BER suffered by the passive eavesdropper.

Demonstrating QI’s performance advantage in sensing is a nontrivial task. The dramatic BER disparity that has been demonstrated in QI-based secure communication results from the legitimate users having access to the initial entangled state, while the eavesdropper can only measure weak thermal states. In optimal classical sensing, however, there should be no restrictions on the transmitter other than its output energy, and there should be no restrictions on the receiver structure. Consider the QI target-detection experiment reported by Lopaeva et al. [29]. It exploited the signal-idler photon pairs produced by spontaneous parametric down-conversion (SPDC) and a coincidence-counting receiver to demonstrate an SNR improvement over probing with a weak thermal state. But a coincidence-counting receiver does not fully exploit the entanglement of SPDC’s signal and idler outputs. Moreover, neither a weak thermal-state probe nor a coincidence-counting receiver represent optimum choices for classical-illumination (CI) target detection, which are known to be a coherent-state
probe and a homodyne-detection receiver [24,26]. Hence, experimental evidence for QI’s target-detection advantage over an optimum CI system has yet to appear. In this Letter, we provide that missing evidence by showing that QI can yield an appreciable target-detection performance gain—over an optimum CI system of the same transmitted energy—in an entanglement-breaking environment plagued by 14 dB of loss and a noise background 75 dB stronger than the returned probe light.

In QI target detection using the entangled Gaussian states produced by continuous-wave (cw) SPDC [24–26], the broadband signal (S) and idler (I) beams can be taken to be a collection of $M = TW$ independent, identically distributed signal-idler mode pairs, where $T$ is the duration of the measurement interval and $W$ is the phase-matching bandwidth. Each mode pair (with annihilation operators $\hat{a}_S$ and $\hat{a}_I$) is a two-mode squeezed state (TMSS) with Fock basis representation

$$|\psi\rangle_{SI} = \sum_{n=0}^{\infty} \sqrt{\frac{N^B_n}{(N^B + 1)^{n+1}}} |n\rangle_S |n\rangle_I,$$

where $N^B_S$ is the source brightness (mean photon number per mode). Signal-idler entanglement is then quantified by the phase-sensitive cross correlation (PSCC) of the TMSS, $\langle \hat{a}_S \hat{a}_I \rangle = \sqrt{N^B_S} (N^B_S + 1)$. This PSCC equals the quantum limit for a mode-pair with $\langle \hat{a}_S^\dagger \hat{a}_S \rangle = \langle \hat{a}_I^\dagger \hat{a}_I \rangle = N^B_S$. For the usual $N^B_S \ll 1$ cw SPDC operating regime, it greatly exceeds the classical-state PSCC limit, $N^B_S$, under the same average photon-number constraints.

In our experiment, we first phase-modulate the signal modes. Then we probe a weakly reflecting target—which is embedded in a strong thermal-state background—with these phase-modulated modes, while the idler modes are stored in a quantum memory. At the input to our joint-measurement receiver, we then have available, for each SPDC mode pair, the signal-return mode, $\hat{a}_S^\dagger (\phi) = \sqrt{\kappa^S_S} e^{i\phi} \hat{a}_S + \sqrt{1 - \kappa^S} \hat{a}_B$, and the stored-idler mode, $\hat{a}_I^\dagger (\phi) = \sqrt{\kappa^I_I} \hat{a}_I + \sqrt{1 - \kappa^I} \hat{a}_e$. Here, $\phi$ is the signal-mode phase shift, $\kappa^S$ and $\kappa^I$ are the roundtrip-probe and idler-storage transmissivities, $\hat{a}_B$ (with $\langle \hat{a}_B^\dagger \hat{a}_B \rangle = N^B_B \gg 1$) is the background mode, and $\hat{a}_e$ is the vacuum-state mode associated with idler-storage loss. The joint-measurement receiver uses a low-gain $(G - 1 \ll 1)$ optical parametric amplifier (OPA) to obtain the idler-mode output $\hat{a}_I^\dagger (\phi) = \sqrt{G} \hat{a}_I^\dagger + \sqrt{G - 1} \hat{a}_e^\dagger (\phi)$ for each mode pair at its input. Direct detection of all $M$ idler-mode outputs from the OPA then yields the QI measurement $\hat{N}^I (\phi)$, whose signal-to-noise ratio,

$$\text{SNR}_{QI} = \frac{4 \langle \hat{N}^I_{\text{out}} (0) \rangle - \langle \hat{N}^I_{\text{out}} (\pi) \rangle^2}{\left( \sqrt{\text{Var}[\hat{N}^I_{\text{out}} (0)]} + \sqrt{\text{Var}[\hat{N}^I_{\text{out}} (\pi)]} \right)^2},$$

is easily shown to be

$$\text{SNR}_{QI} = \frac{4\kappa_{\text{extra}} \eta_D M \langle \hat{a}_S^\dagger (0) \hat{a}_I^\dagger \rangle - \langle \hat{a}_S^\dagger (\pi) \hat{a}_I^\dagger \rangle^2}{N^B_B + N^B_{el}},$$

$$= \frac{16\kappa \eta_{\text{extra}} \kappa_{\text{extra}} M N^S_S}{N^B_B + N^B_{el}},$$

where $\eta_D$ is the detector quantum efficiency, $N_{el}$ is due to post-detection electronics noise, $\kappa_{\text{extra}} < 1$ models all system nonidealities not otherwise accounted for, and $N^S_S \ll 1$ plus $(G - 1)N^B_B \ll 1$ have been assumed.

The preceding OPA receiver is not the optimum quantum measurement for QI target detection—its SNR is 3 dB inferior to that of the optimum receiver [26]—but no receiver structure is known that realizes that optimum quantum measurement. Even so, the nonclassical PSCC of the SPDC’s outputs makes $\text{SNR}_{QI}$ from Eq. (4) a factor of 1/$N^S_S \gg 1$ higher than what would result were the same receiver employed with a transmitter whose signal-idler mode pairs had a PSCC at the classical limit. More importantly, the ideal $(\eta_D = \kappa_I = \kappa_{\text{extra}} = 1, N_{el} = 0)$ OPA receiver’s $\text{SNR}_{QI}$ is 3 dB better than that of the optimum CI system of the same $MN^S_S$ probe energy,

$$\text{SNR}_{CI} = \frac{8\kappa \eta_D M N^S_S}{N^B_B},$$

under similar ideal conditions. Moreover, it is clear from comparing Eqs. (3) and (5) that QI’s SNR advantage under the preceding ideal conditions derives directly from the strength of its PSCC signature, $\langle \hat{a}_S^\dagger (0) \hat{a}_I^\dagger \rangle - \langle \hat{a}_S^\dagger (\pi) \hat{a}_I^\dagger \rangle^2 = 4\kappa \eta_D N^S_S (N^S_S + 1) \approx 4\kappa N^S_S$.

Figure 1 (bottom) shows our experimental setup for QI. The SPDC source is a 4-cm-long type-0 magnesium-oxide doped periodically-poled lithium niobate (MgO:PPLN) bulk crystal that is pumped by a 780 nm diode laser which is followed by a tapered amplifier. The pump is loosely focused at the PPLN crystal to guarantee a high signal-heralding efficiency [30]. The broadband entangled signal (1590 nm center wavelength) and idler (1530 nm center wavelength) beams are separated using a dichroic mirror (DM) that is highly reflective at the idler wavelength. The signal and idler beams pass through two zoom-lens systems, to adjust their confocal parameters for coupling into single-mode fiber (SMF) with maximum signal-heralding efficiency [31]. Ideally, every emitted photon would then herald an idler-photon companion, so that no probe photon is wasted. The idler is stored in a ~30-meter-long low-dispersion, negligible-loss, LEAF-fiber spool whose ends are antireflection (AR) coated. A phase modulator imposes a 500 Hz binary phase-shift keying (BPSK) modulation on the signal [32]. A ∼4-meter-long dispersion-compensating fiber (DCF) overcompensates signal-beam dispersion in the SMF [33]. The dispersion-overcompensated signal is combined with broadband amplified spontaneous emission (ASE) noise at a 50:50
A transimpedance gain, 1 kHz bandwidth, and current-noise spectrum at its input. The ampli-
fication (top) and classical illumination (bottom). DM: dichroic
mirror; PC: polarization controller; Z: zoom lens; BS: beam
splitter; SMF: single-mode fiber; SPDC: spontaneous parametric
down-conversion; OPA: optical parametric amplifier; DSF:
dispersion-shifted LEAF fiber; DCF: dispersion-compensating
fiber; POL: polarizer; PM: phase modulator; EDFA: erbium-
doped fiber amplifier; ASE: amplified spontaneous emission;
CWDM: coarse wavelength-division multiplexer; D: detector;
LO: local oscillator; Attn: attenuator. Thin lines are optical fiber;
thick lines are unguided propagation.

beam splitter. The resulting noisy signal is filtered using a
16-nm-wide coarse wavelength-division multiplexer chan-
nel centered at 1590 nm. The filtered signal is coupled into
free space and fine-tuned in time delay using a prism (not
shown). A convex-concave lens pair is employed to fine
tune the signal’s beam waist and location at the OPA. The
signal beam is then combined with the retained idler on a
DM that is highly reflective at the idler wavelength. Half-
wave- and quarter-wave plates (not shown) are used to
adjust idler’s polarization before combining. The combined
signal and idler are united with the retained pump—whose
pre-combining polarization is adjusted by half-wave and
quarter-wave plates (not shown)—on a DM that is highly
reflective above 1400 nm. Signal, idler, and pump are then
injected into a second 4-cm-long type-0 MgO:PPLN bulk
crystal that serves as the receiver’s OPA. A spatial filter,
consisting of two collimators and AR-coated single-mode
fibers, is employed at the OPA’s output to reject noncol-
linear modes. By means of a movable lens, ~90% throu-
ghput for the idler is realized. The spatially filtered
light is then guided to a pair of DMs that are highly
reflective above 1400 nm, to reject the pump, and a second
pair of DMs that are highly reflective at the idler wave-
length, to reject the signal, before the idler is focused into a
free-space AR-coated InGaAs PIN detector with 84% quan-
tum efficiency. The detected idler power is of the
order of 1 nW. The resulting weak photocurrent is
amplified using a low-noise transimpedance amplifier with
5 × 10^9 V/A transimpedance gain, 1 kHz bandwidth, and
6 fA/√Hz current-noise spectrum at its input. The ampli-
fer’s output voltage is directed to either an oscilloscope or
a low-noise 100 kHz fast Fourier transform spectrum
analyzer (FFT SA) for SNR measurements.

Figure 1 (bottom) shows our experimental setup for CI.
Light from a 1590 nm laser is guided to a 99:1 beam
splitter, whose 1% output serves as the signal while its 99%
output supplies the local oscillator for homodyne reception.
The signal strength is further reduced by a tunable digital
attenuator, after which 70 kHz BPSK modulation is applied
[34]. The modulated signal is mixed on a 50:50 beam
splitter with broadband ASE noise, as done in the QI
experiment. The noisy signal is combined with the local
oscillator on a 50:50 beam splitter, whose two output
arms are detected by a balanced receiver with ~80% quan-
tum efficiency, an internal transimpedance gain of
2 × 10^5 V/A, 120 kHz bandwidth, and negligible electrical
noise (i.e., measurement is shot-noise limited). The voltage
signal from the balanced receiver is directed to either the
oscilloscope or the FFT SA for SNR measurements.

The presence of a target yields a sharp signal peak at the
BPSK frequency on the FFT SA, whereas a flat noise
spectrum will be observed in the absence of a target, which
we accomplish by manually blocking the signal before it
mixes with the ASE noise. The spectral-peak amplitude
(SPA) fluctuates owing to thermal and mechanical insta-
bilites that cause random phase drifts between the QI
receiver’s signal and idler and between the CI receiver’s
signal and local oscillator. We are interested, however, in
the maximum SPAs for QI and CI, as functions of N_S and
κ_S. These are obtained as follows.

To measure the maximum QI SPA, we first optimize the
signal-heralding efficiency, spatial-filter collection effi-
ciency, polarizations of all beams, and signal-idler relative
delay, and then set the source brightness, channel trans-
missivity, and OPA gain to desired values. We use the FFT
SA to record the maximum SPA over 32,767 samples and
repeat the measurement five times before switching to
different experimental settings. During this ~10-minute
process, peak-to-peak signal-power fluctuations before the
phase modulator was found to be ±3%.

To measure the maximum CI SPA, we first optimize the
local oscillator’s polarization and then employ the same
measurement procedure used for QI. In the absence of a
target, we block the signal and directly measure the QI and
CI noise spectral densities at their respective BPSK
frequencies. The resolution bandwidth is 977 mHz for all
measurements.

To connect the maximum SPA and the noise spectral-
density measurements for QI and CI with Eqs. (4) and (5),
we need to convert each maximum SPA to its correspond-
ing intensity-modulation amplitude (IMA), defined by the
numerators of those two equations. To do so we use an
oscilloscope to record IMA histograms after performing the
parameter optimizations described in the preceding para-
graphs. CI’s IMA histograms are measured using strong
signal light, whereas QI’s IMA histograms are taken at the
same signal power levels used in its maximum-SPA measurements. The necessity of employing strong signal light in obtaining CI IMA histograms is due to the CI homodyne receiver’s current amplifier having a much lower gain than that of its QI-setup counterpart. Each IMA histogram consists of 10,000 samples and is captured within ~10 minutes. We repeated the histogram measurements three times each for QI and CI, and found that the recorded maximum IMA only fluctuates ±1.8%, which is consistent with the signal power fluctuations. The maximum IMA in the histogram is proportional to the maximum SPA, enabling us to convert each SPA into its corresponding IMA, calculate the SNR, and compare to theory [35].

Figure 2 shows the measured QI and CI SNRs as functions of their channel transmissivities from the outputs of the transmitters to the inputs of the receivers. Each data point represents five consecutive SNR measurements, and the error bars denote ±1 measurement standard deviation with signal-power fluctuations accounted for. A polarization controller (PC1) followed by a polarizer was used to vary the channel transmissivity in the QI experiment, whereas a tunable attenuator was used to vary the channel transmissivity in the CI experiment. The SPDC source had brightness $N_S = 3 \times 10^{-4}$ and $W = 1.89$ THz phase-matching bandwidth for all QI measurements, while all CI measurements were taken with the equivalent photon flux of $WN_S = 5.67 \times 10^8$ photons/s. In both experiments, we had $N_B = 95$ at the receivers, which is 69 dB stronger than the returned signal power when the target was present and $\kappa_S = 0.038$. The QI receiver had an estimated $\kappa_{\text{extra}} \sim 0.8$, representing the combined effects of the measured ~90% spatial-filter collection efficiency and ~10% additional nonidealities arising from imperfect signal-heralding efficiency and dispersion compensation, confirmed separately in heralding efficiency measurements using InGaAs avalanche photodiodes.

The QI SNR measurements in Fig. 2 are in excellent agreement with theory, but the CI SNR deviates somewhat from theory at the lowest and highest transmissivities we employed. At the lowest transmissivity, we attribute the deviation to slow (~minutes) drifts in polarization; at the highest transmissivity, we attribute the deviation to phase instability caused by feedback into the laser. Remarkably, QI’s SNR exceeds that of the optimum CI scheme by 20% at 3.8% channel transmissivity, where the background light is 69 dB stronger than the target return. Also, the QI system continues to offer a performance advantage even when it suffers a 19 dB transmission loss.

QI’s SNR is known to be a function of its OPA gain [26]. A sufficiently high OPA gain guarantees that the idler’s optical noise overwhelms postdetection electronics noise, but a high OPA gain violates the $(G - 1)N_B \ll 1$ assumption and thus introduces additional thermal-state noise [36]. Figure 3 plots QI’s measured SNR versus OPA gain for three different source brightnesses. All measurements were performed with 14 dB channel loss and $N_B = 95$ at the receiver. At $N_S = 7.5 \times 10^{-5}$, this background is 75 dB stronger than the target return. For all three $N_S$ values, QI provided a 20% SNR improvement over the theoretically-optimum CI performance when the QI receiver’s OPA gain satisfied $G - 1 = 7.4 \times 10^{-5}$. The solid curves are theoretical results for QI’s SNR obtained using $\kappa_{\text{extra}} = 0.8$. The departure from the theoretical predictions at low OPA gains results from slow degradations of the signal-heralding efficiency that are due to mechanical instabilities, and signal-idler delay mismatch caused by thermal drifts. These instabilities occur on time scales of minutes, and have been confirmed separately in signal-heralding efficiency measurements and fine tuning of the prism to recover the maximum QI SNR.

Our QI experiment’s SNR advantage over CI has been reaped even though the returned signal and the retained idler are in a classical state; i.e., the channel has broken the
initial signal-idler entanglement. That initial entanglement will be broken when loss and noise are such that the PSCCs at the QI receiver’s OPA input satisfy $|\langle \hat{a}_S^{\text{in}}(\phi) \hat{a}_I^{\text{in}} \rangle|^2 \leq \langle \hat{a}_S^{\text{in}}(\phi) \hat{a}_S^{\text{in}}(\phi) \rangle \langle \hat{a}_I^{\text{in}} \hat{a}_I^{\text{in}} \rangle$. In our experiment, $|\langle \hat{a}_S^{\text{in}}(\phi) \hat{a}_I^{\text{in}} \rangle|^2$ is 34–41 dB below that classical-state upper limit.

In summary, we have implemented an entanglement-based sensing protocol that achieved an SNR improvement over the optimal classical scheme in a highly lossy and noisy environment that completely breaks the initial entanglement. The realization of this quantum advantage, without making any comparison adjustment to compensate for device imperfections, is contrary to conventional thinking that the benefits of quantum entanglement would disappear when operating under high loss and high noise conditions. This surprising quantum-sensing result clearly shows that a quantum resource can still be utilized beneficially even when its initial nonclassicality is lost, suggesting that the application of QIP techniques in practical (lossy and noisy) situations warrants further investigation. This research was supported by Army Research Office Grant No. W911NF-10-1-0430 and Office of Naval Research Grant No. N00014-13-1-0774.

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[32] The 500 Hz modulation frequency was chosen to operate within the 1 kHz bandwidth of the high-gain, low-noise transimpedance amplifier.

[33] Overcompensation is done so that when the signal and idler are combined at the OPA their respective photons have both been stretched from the 0.2 ps durations they had at the SPDC source to ~3 ps, with one beam having normal dispersion and the other anomalous dispersion [21] so that the cross correlation of the signal-idler Gaussian state is recovered [37].

[34] The 70 kHz modulation frequency was chosen to minimize the effects of laser excess noise such that shot-noise limited balanced detection could be achieved.

[35] The SPA-to-IMA conversion factors that we determined experimentally were as follows: for QI, an SPA of 1 mV/√Hz corresponded to an IMA of 4.11 mV; and for CI, an SPA of 1 V/√Hz corresponded to an IMA of 4.85 V.

[36] As a practical matter, one should limit the OPA gain to avoid saturating the QI receiver’s current amplifier.