

# Zero-forcing Electrical Filters for Direct Detection Optical Systems

Peter C. Li and Pierre A. Humblet

MIT, 35-425, Cambridge, MA 02139, USA, and Eurecom, B.P. 193, 06904 Sophia Antipolis, France

**Abstract** — Intersymbol interference in direct detection optical systems can limit the channel spacing in frequency division multiplexing and prevent multi-level signaling. We investigate a zero-forcing electrical filter to cancel intersymbol interference and compare its performance with a matched filter and a rectangular response filter, for  $M$ -ary amplitude modulation.

## I. MODEL

In our model, the receiver front-end is composed of an optical filter, a photodiode and a low-pass electrical filter as shown in Figure 1. The photodiode is modelled as a square-law de-

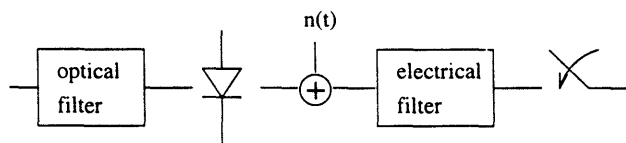


Figure 1: The receiver front-end includes an optical filter, a photodiode and a low-pass electrical filter followed by a baud rate sampler.

vice whose output is proportional to the magnitude square of the received signal envelope. The thermal noise  $n(t)$  from the electronics is assumed to be the dominant noise and is modelled as additive white Gaussian noise.

## II. ZERO-FORCING FILTERS

Without loss in generality, we design the filter for sampling time  $t = 0$ . The output of the electrical filter at this time is

$$\sum_i \sum_j a_i a_j \int p_{i,j}(\sigma) h(\sigma) d\sigma + N, \quad (1)$$

where  $h(t)$  is the *time-reversed* impulse response of the electrical filter,  $p_{i,j}(t) = \text{Re}\{p(t-iT)p^*(t-jT)\}$ ,  $p(t)$  is the complex envelope of the received optical pulse taking into account the transmit pulse and the channel response,  $p^*(t)$  is the complex conjugate of  $p(t)$ ,  $a_k$  (taken as real here) is the  $k$ th transmit amplitude, and  $N$  is the noise at the sampled output. We write the integral  $\int p_{i,j}(t)h(t)dt$  as an inner product  $\langle p_{i,j}, h \rangle$  where  $\langle x, y \rangle \equiv \int x(t)y(t)dt$ .

We define the *ISI space*,  $I$ , as the space spanned by  $p_{i,j}(t)$ 's without  $p_{0,0}(t)$ , the desired signal. The *signal space* is defined as the space spanned by  $I$  and  $p_{0,0}(t)$ . A filter  $h(t)$  is a zero-forcing filter if the sampled output has no ISI, i.e. we want the output of  $h(t)$  to depend only on  $a_0 a_0$  at sampling time  $t = 0$ . A necessary and sufficient condition for  $h(t)$  to be a zero-forcing filter is

$$\begin{aligned} \langle p_{i,j}, h \rangle &\neq 0, \text{ if } i = j = 0, \text{ and} \\ \langle p_{i,j}, h \rangle &= 0, \text{ otherwise.} \end{aligned} \quad (2)$$

For filters that satisfy (2), we are interested in the one that minimizes the noise variance when  $\langle p_{0,0}, h \rangle$  is set equal to a constant. The time-reversed impulse response of this filter, if it exists, is proportional to the component of  $p_{0,0}(t)$  orthogonal to  $I$ .

## III. FABRY-PEROT INTERFEROMETER

We consider a Fabry-Perot filter as the optical demultiplexing filter [1]. The envelope of the impulse response is well approximated by  $\frac{1}{\tau} e^{-t/\tau}$  for  $t \geq 0$ . The envelope of the transmit pulse is equal to 1 in  $[0, \frac{\log_2 M}{R}]$  and 0 otherwise, where  $M$  is the number of signaling levels and  $R$  is the bit rate. The symbol set is equal to  $\{\sqrt{\frac{i}{M-1}} \mid 0 \leq i \leq M-1\}$ . We keep the bit rate fixed and plot the normalized eye opening for different  $\tau'$ , where  $\tau' = \tau R$  is a parameter proportional to bandwidth efficiency in units of (b/s/Hz). The normalized eye opening is the vertical opening of an eye-diagram when the electrical filter has unit energy. We consider a filter matched to the post-detection electrical pulse  $p_{0,0}(t)$  (single pulse transmitted), the minimum noise variance zero-forcing filter, and a filter with rectangular impulse response on  $[0, \frac{\log_2 M}{R}]$ . For the rectangu-

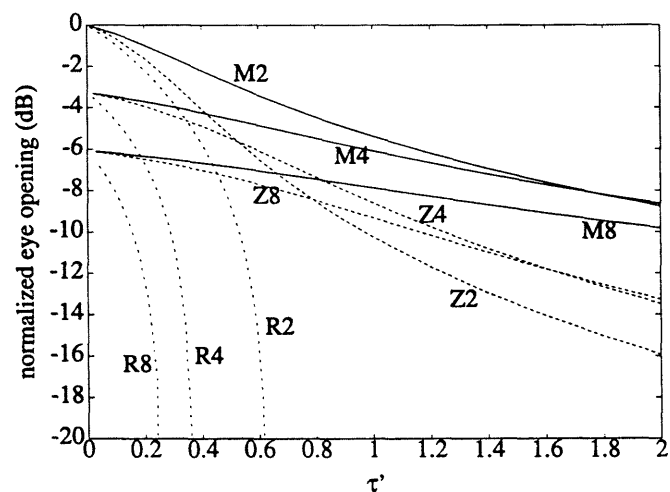


Figure 2: The optical filter is a Fabry-Perot interferometer. The curves are labelled as follows: (M) matched filter curve, (Z) zero-forcing filter, (R) rectangular filter, and (2,4,8) level signaling.

lar filter, there is no advantage to multilevel signaling, same as in [1]. On the other hand the zero-forcing filter performs much better and there is advantage to four level signaling for large values of  $\tau'$ .

## ACKNOWLEDGEMENTS

This work was supported by NSF grant 9206379-NCR.

## REFERENCES

- [1] L. Cimini and G. Foschini. Can multilevel signaling improve the spectral efficiency of ask optical fdm systems? *IEEE Transactions on Communications*, 41(7):1084-1090, July 1993.