



2.29 Numerical Fluid Mechanics

Fall 2011 – Lecture 5

REVIEW Lecture 4

- Roots of nonlinear equations: “Open” Methods

- Fixed-point Iteration (General method or Picard Iteration), with examples

- Iteration rule: $x_{n+1} = g(x_n)$ or $x_{n+1} = x_n - h(x_n)f(x_n)$

- Error estimates, Convergence Criteria: $|g'(x)| \leq k < 1, x \in I$

- Order of Convergence p : $\lim_{n \rightarrow \infty} \frac{|e_{n+1}|}{|e_n|^p} = C$ (for Fixed-Point, usually linear, $p \sim 1$)

- Newton-Raphson

- Examples and Issues

$$x_{n+1} = x_n - \frac{1}{f'(x_n)} f(x_n)$$

- Quadratic Convergence ($p=2$)

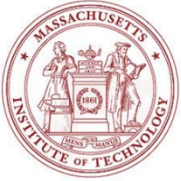
- Secant Method

$$f'(x_n) \approx \frac{f(x_n) - f(x_{n-1})}{x_n - x_{n-1}}$$

- Examples

- Convergence ($p=1.62$) and efficiency

- Extension of Newton-Raphson to systems of nonlinear eqns. (slower conver.)



Secant Method: Order of convergence

Absolute Error $\epsilon_n = x_n - x^e$

$$\epsilon_{n+1} = x_{n+1} - x^e = \frac{f(x^e + \epsilon_n)(x^e + \epsilon_{n-1}) - f(x^e + \epsilon_{n-1})(x^e + \epsilon_n)}{f(x^e + \epsilon_n) - f(x^e + \epsilon_{n-1})} - x^e$$

Using Taylor Series, up to 2nd order

Absolute Error $\epsilon_{n+1} \simeq \frac{1}{2} \epsilon_{n-1} \epsilon_n \frac{f''(x^e)}{f'(x^e)}$

Relative Error $\frac{\epsilon_{n+1}}{|x^e|} \simeq \frac{\epsilon_{n-1}}{|x^e|} \frac{\epsilon_n}{|x^e|} \frac{f''(x^e)}{2f'(x^e)} x^e$

Convergence Order/Exponent

By definition:

$$\epsilon_n = A(x^e) \epsilon_{n-1}^m \Rightarrow \epsilon_{n-1} = \left(\frac{1}{A}\right)^{1/m} \epsilon_n^{1/m} = B(x^e) \epsilon_n^{1/m}$$

Then:

$$\epsilon_{n+1} = C(x^e) \epsilon_n \epsilon_{n-1} = D(x^e) \epsilon_n \epsilon_n^{1/m} = D(x^e) \epsilon_n^{1+1/m}$$

$$\Rightarrow 1 + \frac{1}{m} = m \Leftrightarrow m = \frac{1}{2}(1 + \sqrt{5}) \simeq 1.62$$

Error improvement for each function call

Secant Method $\epsilon_{n+1}^* \simeq \epsilon_n^{1.62}$

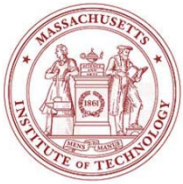
Newton-Raphson $\epsilon_{n+1}^* = \epsilon_n^2$



Fluid flow modeling: the Navier-Stokes equations and their approximations

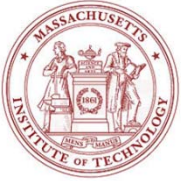
Today's Lecture

- References :
 - Chapter 1 of “J. H. Ferziger and M. Peric, Computational Methods for Fluid Dynamics. Springer, New York, third edition, 2002.”
 - Chapter 4 of “I. M. Cohen and P. K. Kundu. *Fluid Mechanics*. Academic Press, Fourth Edition, 2008”
 - Chapter 4 in “F. M. White, *Fluid Mechanics*. McGraw-Hill Companies Inc., Sixth Edition”
- For today's lecture, any of the chapters above suffice
 - Note each provide a somewhat different prospective



Conservation Laws

- Conservation laws can be derived either using a
 - Control Mass approach (CM)
 - Considers a fixed mass (useful for solids) and its extensive properties (mass, momentum and energy)
 - Control Volume approach (CV)
 - CV is a certain spatial region of the flow, possibly moving with fluid parcels/system
 - Its surfaces are control surfaces (CS)
 - Each approach leads to a class of numerical methods
- For an extensive property, the conservation law “relates the rate of change of the property in the CM to externally determined effects on this property”
- To derive local differential equations, assumption of continuum is made
 - Knudsen number (mean free path over length-scale, $\lambda/L < 0.01$)
 - => Sufficiently “well behaved” continuous functions
 - Non-continuum flows: space shuttle in reentry, low-pressure processing
 - Note CFD is also used for Newton’s law applied to each constituent molecules (simple, but computational cost often grows as N^2 or more)



Macroscopic Properties

- Continuum hypothesis allows to define macroscopic fluid properties
- Density (ρ): mass of material per unit volume [kg/m^3]
 - If the density is independent of pressure, the fluid is said incompressible
 - A measure of the flow compressibility is the Mach number:
 - $Ma = \frac{v}{a}$ where $a^2 = \left. \frac{\partial p}{\partial \rho} \right|_s$ (If $Ma < 0.3$, variations of ρ can be assumed to be negligible)
 - Typical values:
 - Water: $a = 1,400$ m/s; Air: $a = 300$ m/s
- Viscosity (μ): measure of the resistance of the fluid to deformation under stress [$Pa.s$]
 - A solid sustains external shear stresses: intermolecular forces balance the stress
 - A fluid does not: the deformation increases with time
 - If the deformation increase is linear with the stress, the fluid is said Newtonian
 - Typical values of dynamic viscosity:
 - Air: $\mu = 1.8 \times 10^{-5}$ kg/ms; Water: $\mu = 10^{-3}$ kg/ms; SAE Oil (car): $\mu = 240 \times 10^{-3}$ kg/ms
- The ratio of the inertial (nonlinear) forces to the viscous force is measured by the Reynolds number:

$$Re = \frac{\rho UL}{\mu} = \frac{UL}{\nu}$$



Observed Influence of the Reynolds Number

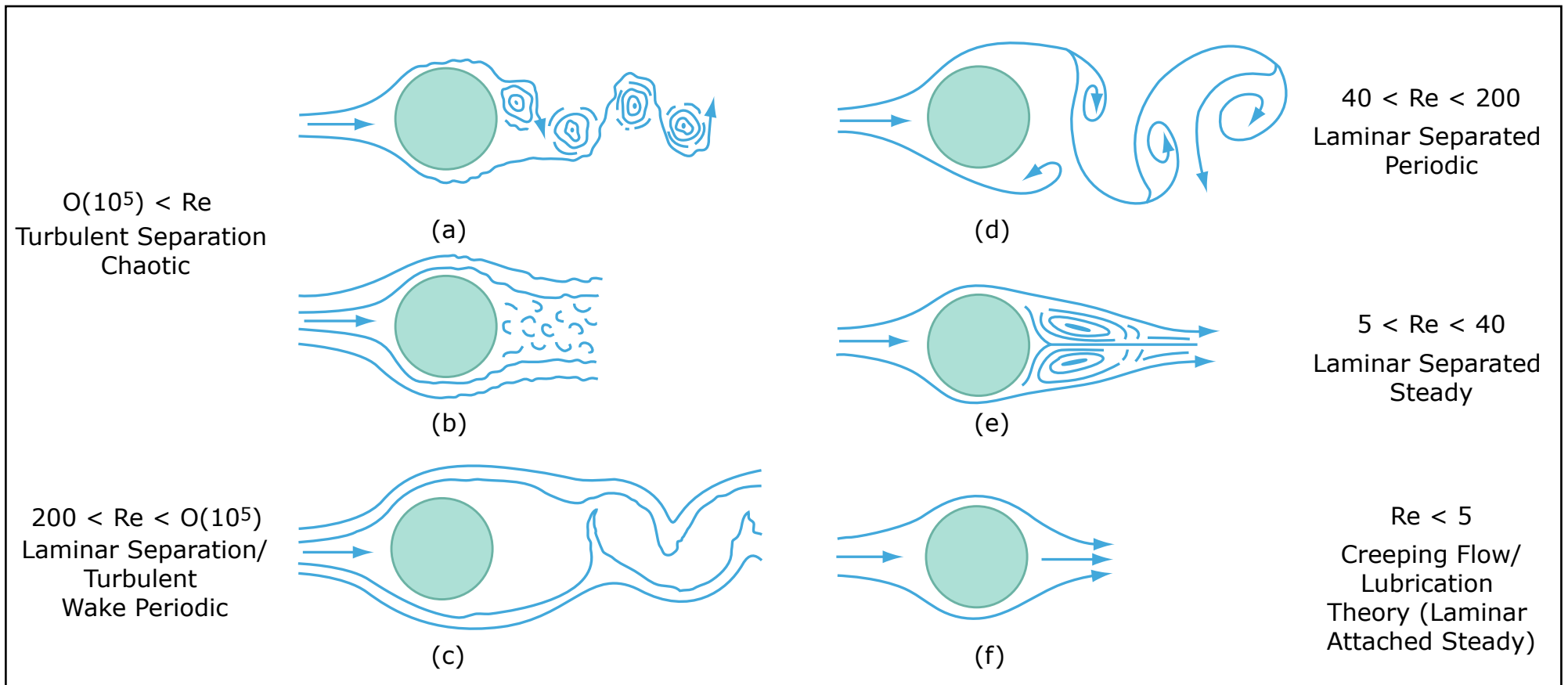


Image by MIT OpenCourseWare.



Conservation of Mass and Momentum for a CM

- Conservation of Mass
 - Mass is neither created nor destroyed in the flows of our engineering interests:

$$\frac{dM_{CM}}{dt} = 0$$

- Conservation of Momentum (Newton's second law)
 - Rate of change of momentum can be modified by the action of forces

$$\frac{d(M \mathbf{v})_{CM}}{dt} = \sum \vec{F}$$



Conservation Laws (Principles/Relations) for a CV

Mass conservation

(summation form):

$$\frac{dM_{CV}}{dt} = \sum_{in} \dot{m}_{in} - \sum_{out} \dot{m}_{out}$$

(integral form):

$$\frac{d}{dt} \int_{CV} \rho dV + \int_{CS} \rho (\vec{v}_r \cdot \vec{n}) dA = 0$$

(differential form):

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}) = 0$$

Momentum conservation

(integral form):

$$\frac{d}{dt} \int_{CV} \rho \vec{v} dV = \underbrace{\int_{CS} -P \vec{n} dA + \int_{CS} \vec{\tau} dA + \int_{CV} \rho \vec{g} dV}_{=\sum \vec{F}} - \int_{CS} \rho \vec{v} (\vec{v}_r \cdot \vec{n}) dA$$

$$\Leftrightarrow \sum \vec{F} = \int_{CS} -P \vec{n} dA + \int_{CS} \vec{\tau} dA + \int_{CV} \rho \vec{g} dV = \frac{d}{dt} \int_{CV} \rho \vec{v} dV + \int_{CS} \rho \vec{v} (\vec{v}_r \cdot \vec{n}) dA$$



Conservation Laws (Principles/Relations) for a CV

Energy conservation (First Law)

(integral form):

$$\frac{d}{dt} \int_{CV} \rho \left(u + \frac{v^2}{2} + gz \right) dV = \dot{Q} - \dot{W}_{shaft} - \int_{CS} \rho \left(h + \frac{v^2}{2} + gz \right) (\vec{v}_r \cdot \vec{n}) dA$$

(summation form):

$$\frac{dE_{CV}}{dt} = \dot{Q} - \dot{W}_{shaft} + \sum_{in} \dot{m}_{in} \left(h + \frac{v^2}{2} + gz \right)_{in} - \sum_{out} \dot{m}_{out} \left(h + \frac{v^2}{2} + gz \right)_{out}$$

Second Law of Thermodynamics

(integral form):

$$\frac{d}{dt} \int_{CV} \rho s dV = \sum_i \left(\frac{\dot{Q}}{T} \right)_i + \dot{S}_{gen} - \int_{CS} \rho s (\vec{v}_r \cdot \vec{n}) dA$$

(summation form):

$$\frac{dS_{CV}}{dt} = \sum_i \left(\frac{\dot{Q}}{T} \right)_i + \dot{S}_{gen} + \sum_{in} (\dot{m}s)_{in} - \sum_{out} (\dot{m}s)_{out}$$

Angular momentum conservation

(integral form):

$$\sum \vec{T} = \frac{d}{dt} \int_{CV} \rho (\vec{r} \times \vec{v}) dV + \int_{CS} \rho (\vec{r} \times \vec{v}) (\vec{v}_r \cdot \vec{n}) dA$$

Bernoulli Equation (unsteady)

$$\int_1^2 \frac{\partial v}{\partial t} ds + \frac{P_2 - P_1}{\rho} + \frac{v_2^2 - v_1^2}{2} + g(z_2 - z_1) = 0$$



Vector Operators

Cartesian Coordinates (x, y, z)

$$\nabla \psi = \frac{\partial \psi}{\partial x} \hat{i} + \frac{\partial \psi}{\partial y} \hat{j} + \frac{\partial \psi}{\partial z} \hat{k}$$

$$\nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

$$\nabla^2 \psi = \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{\partial^2 \psi}{\partial z^2}$$

Cylindrical Coordinates (r, φ, z)

$$\nabla \psi = \frac{\partial \psi}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial \psi}{\partial \phi} \hat{\phi} + \frac{\partial \psi}{\partial z} \hat{z}$$

$$\nabla \cdot \vec{A} = \frac{1}{r} \frac{\partial(r A_r)}{\partial r} + \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} + \frac{\partial A_z}{\partial z}$$

$$\nabla^2 \psi = \frac{1}{r} \frac{\partial}{\partial r} \left[r \frac{\partial \psi}{\partial r} \right] + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \phi^2} + \frac{\partial^2 \psi}{\partial z^2}$$

Spherical Coordinates (r, θ, φ)

$$\nabla \psi = \frac{\partial \psi}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial \psi}{\partial \theta} \hat{\theta} + \frac{1}{r \sin \theta} \frac{\partial \psi}{\partial \phi} \hat{\phi}$$

$$\nabla \cdot \vec{A} = \frac{1}{r^2} \frac{\partial(r^2 A_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial(\sin \theta A_\theta)}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial A_\phi}{\partial \phi}$$

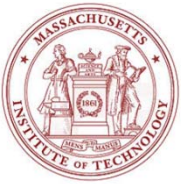
$$\nabla^2 \psi = \frac{1}{r^2} \frac{\partial}{\partial r} \left[r^2 \frac{\partial \psi}{\partial r} \right] + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial \psi}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \psi}{\partial \phi^2}$$



Material Covered in class

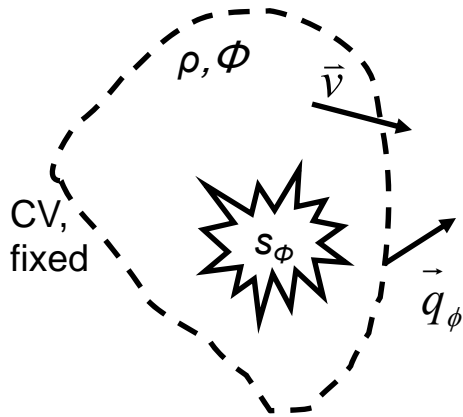
Differential forms of conservation laws (Mass, RTT, Mom. & N-S)

- Material Derivative (substantial/total derivative)
- Conservation of Mass
 - Differential Approach
 - Integral (volume) Approach
 - Use of Gauss Theorem
 - Incompressibility
- Reynolds Transport Theorem
- Conservation of Momentum (Cauchy's Momentum equations)
- The Navier-Stokes equations
 - Constitutive equations: Newtonian fluid
 - Navier-stokes, compressible and incompressible



Integral Conservation Law for a scalar ϕ

$$\left\{ \frac{d}{dt} \int_{CM} \rho \phi dV = \right\} \frac{d}{dt} \int_{CV_{\text{fixed}}} \rho \phi dV + \underbrace{\int_{CS} \rho \phi (\vec{v} \cdot \vec{n}) dA}_{\text{Advection fluxes ("convective" fluxes)}} = \underbrace{- \int_{CS} \vec{q}_\phi \cdot \vec{n} dA}_{\text{Other transports (diffusion, etc)}} + \underbrace{\sum \int_{CV_{\text{fixed}}} s_\phi dV}_{\text{Sum of sources and sinks terms (reactions, etc)}}$$



Applying the Gauss Theorem, for any arbitrary CV gives:

$$\frac{\partial \rho \phi}{\partial t} + \nabla \cdot (\rho \phi \vec{v}) = -\nabla \cdot \vec{q}_\phi + s_\phi$$

For a common diffusive flux model (Fick's law, Fourier's law):

$$\vec{q}_\phi = -k \nabla \phi$$

Conservative form of the PDE

$$\frac{\partial \rho \phi}{\partial t} + \nabla \cdot (\rho \phi \vec{v}) = \nabla \cdot (k \nabla \phi) + s_\phi$$



Additional Handouts: Derivation of Reynolds Transport Theorem

Handouts extracted from pp. 91-93 in Whitaker, S.
Elementary Heat Transfer Analysis. Pergamon Press,
1976. ISBN: 9780080189598

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