### **Engineering at the Limits of the Nanoscale**

**by**

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B.A.Sc. Nanotechnology Engineering, University of Waterloo (2011) **S.M.** Massachusetts Institute of Technology **(2013)**

Submitted to the Department of Electrical Engineering and Computer Science

in partial fulfillment of the requirements for the degree of

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#### **Abstract**

At the nanoscale, unique properties and phenomena emerge that can lead to scientific and technological paradigms beyond those classically envisioned. Exploring these opportunities at the few-nanometer regime requires unprecedented precision, resolution, control and uniformity, not readily feasible through conventional fabrication and metrology techniques. In particular, the dynamic, reliable and reversible structural tuning of such small dimensions remains a great challenge, yet a promising platform to enable devices of new and improved functionalities. To overcome these challenges, alternative techniques are necessary to push the frontiers of nanoscale processing.

In this thesis, the challenges and prospects of engineering active devices at the limits of the nanoscale are evaluated using a case study that focuses on developing a new platform for nanoelectromechanical **(NEM)** switches. The proposed **NEM** switches that rely on electromechanical modulation of the tunneling current in **<5** nm switching gaps possess the potential to overcome the limitations of the conventional counterparts **-** minimizing stiction and lowering the actuation voltage.

Combined top-down and bottom-up fabrication methodologies are introduced for achieving active structures of the desired complexity with nanometer precision, resolution and control. Integration of device engineering and physics with chemistry and materials science leverages an understanding of material synthesis, surfaces and interfaces to achieve manipulation of matter in the nanometer regime with a precision and control otherwise not feasible. Accordingly, two example hybrid fabrication techniques are introduced allowing precise fabrication of electrically-active nanogaps.

Molecules are proposed as nanoscale structural components which can also control surface interactions and forces utilizing their chemical and mechanical properties. When used as interconnects between neighboring surfaces, they can precisely define nanoscale spacings. Uniquely, the mechanics of the molecular layer can be used to allow controlled and reversible tuning of the spacing where the elastic restoring force of the molecules balances the dominating surface adhesive forces to allow for stable yet mechanically active structures. Feasibility of molecules as nanoscale scaffolds and springs are demonstrated in this work in an electromechanically tunable molecular tunneling junction.

In such a junction, changes in the tunneling gap leads to an exponential modulation of the tunneling current. If sufficiently large, this modulation can serve as a **NEM** switching mechanism. The molecules provide precision in defining small switching gaps necessary to reduce the actuation voltage while the force control provided through the molecular layer's mechanics helps control the surface adhesion. These proposed tunneling-based switches, referred to as "squitches", form a promising platform towards a more energy-efficient operation. Two- and multi-terminal designs of squitches are proposed and experimentally demonstrated with example devices showing actuation voltages  $\langle 2 \text{ V} \rangle$  and current modulations  $>10^4$ .

The design of squitches pushes the limits of nanoscale processing and broadly helps reveal the challenges and prospects of engineering at dimensions few nanometers in size. **By** implementing a multidisciplinary approach, one can gain access to the limits of the nanoscale to investigate the emerging physical phenomena and develop next generation nanodevices beyond squitches. The key is continuous development of versatile processing techniques allowing nanoscale manipulation and characterization with high precision and control.

Thesis Supervisor: Vladimir Bulovid Title: Professor of Electrical Engineering and Computer Science

Thesis Supervisor: Jeffrey H. Lang Title: Professor of Electrical Engineering and Computer Science

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**My** journey, over the past few years, has been filled with invaluable learning experiences and friendships that **I** will always cherish and reflect upon as **I** move towards future adventures with great motivation and excitement.

> *Farnaz Niroui August 2017 Cambridge, MA*

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### **Chapter 1**

### **Introduction**

*"There's plenty of room at the bottom." -Richard Feynman*

### **1.1 Engineering at the Limits of the Nanoscale**

Consider the period at the end of this sentence – it is  $\sim 5 \times 10^5$  nm in diameter, or  $\sim 3 \times 10^6$  carbon atoms arranged next to each other. Two carbon atoms form a covalent bond approximately **0.15** nm in size. Eight of these carbon atoms can build up a small alkane molecule  $\sim$ 1 nm in length. Consider engineering devices at such small scale **-** unprecedented precision, resolution and uniformity would be essential. This thesis explores engineering at such small dimensions **-** at the limits of the nanoscale **-** where structures *single-digit nanometers* in size are needed towards development of active devices of unique functionalities.

At the nanoscale, properties and phenomena emerge that are classically unattainable. In past decades, these principles offered tremendous opportunities for interdisciplinary scientific and technological advancements, driving the field of nanotechnology. Exploiting these opportunities became feasible through innovations in nanoscale fabrication, visualization and characterization. However, despite vast improvements, these techniques become limiting in precision, control, resolution and uniformity as dimensions are further reduced towards the few-nanometer regime. In particular, the dynamic, controlled and reversible tuning of such small dimensions is a great challenge, often facing structural collapse due to the lack of control over surface adhesive forces. However, control over such dimensions, if implemented successfully, can lead to unexplored phenomena and device principles benefiting diverse areas of electronics, optics, spintronics, nanoelectromechanical systems and excitonics to name a few examples. To reach these potentials, alternative approaches are necessary to push the frontiers of nanoscale processing and control.

These alternative approaches should focus beyond incremental improvements in conventional fabrication tools, re-envisioning processing methodologies **by** bridging the boundaries between different disciplines. Integration of device engineering and physics with chemistry and materials science leverages an understanding of material synthesis, surfaces and interfaces to achieve manipulation of matter in the nanometer regime with a precision and control otherwise not feasible, down to **<1** nm. When addressing the nanoscale from the bottom up through such an interdisciplinary approach, an extensive toolset emerges to develop new processing techniques and also redefine the limits of the conventional approaches **by** realizing new strategies of using them. However, given the small dimensions, processing is further challenged **by** the lack of resolution in visualization and characterization. In many cases, the needs are pushed well beyond the capabilities in reach of the state-of-the-art metrology techniques. Yet, detailed characterization of structures at the few nanometer dimensions and their performance are much needed to provide continuous feedback to guide engineering and scientific studies at this size scale. Thus, development of new metrology techniques and unique ways of utilizing conventional tools are as essential as new developments in processing.

As the processing and metrology methodologies advance to gain access to the fewnanometer regime and address the desired complexity of functional nanostructures, an important consideration is for these techniques to possess flexibility: the ability to readily reconfigure in operation and integrate with one another in such a way to accommodate a wide variety of material systems and functionalities that emerge at the nanoscale. Unlike conventional approaches which are often restricted in operation mode and capabilities, such versatile techniques are desired at the nanoscale to keep up with the demands of the continuously evolving field of nanotechnology and its multidisciplinary nature.

In this thesis, the challenges and prospects of engineering active devices at the limits of the nanoscale are evaluated. In doing so, a case study is considered through which a new platform for nanoelectromechanical (NEM) switches is introduced with the potential to overcome the limitations of their conventional counterparts. In demonstrating these devices, various processing techniques are developed to allow: **1)** nanoscale fabrication with nanometer precision, control and uniformity, and 2) nanoscale force control for dynamic tuning of dimensions in a controlled and reversible manner. Engineering approaches are consequently realized which can extend in application beyond **NEM** switches to broadly enable active devices with critical features nanometer in size.

## **1.2 Towards Low-Voltage and Stiction-Free NEM Switches - A Case Study**

**A** nanoelectromechanical **(NEM)** switch in the simplest form is composed of a movable electrode, such as a cantilever, faced opposing stationary electrodes to form a capacitor structure as shown in Figure 1-la. An applied voltage across the capacitor provides an electrostatic force to attract the top electrode towards the bottom. Once reaching the pull-in, the point at which the combined electrostatic and surface adhesive forces overwhelm the elastic restoring force, the deflected electrode collapses to come into physical contact with the opposing electrode to turn the device **ON.** As the applied voltage is removed, the elastic restoring force in the deflected electrode overcomes the surface adhesive forces causing it to return to its original position, turning the device OFF. This switching mechanism allows **NEM** switches to exhibit a near-zero off-state leakage current and abrupt switching behavior with an effectively infinite sub-threshold slope **[1,** 2], schematically shown in Figure **1-1b.** Consequently, **NEM** switches have the potential to achieve more energy-efficient performance than



Figure **1-1:** Schematic representation of the design and performance of a cantilever-based NEM switch. (a) An electrostatic force (F<sub>electrostatic</sub>) induced through an applied voltage combined with the van der Waals forces  $(F_{vdW})$  cause collapse of the cantilever onto the opposing electrode to turn **ON** the device as they come into contact. Once the voltage is removed, the elastic restoring force **(Felastic)** overcomes the surface adhesive forces to turn OFF the device. **(b)** The switching mechanism leads to a near zero OFF-state leakage current and an abrupt switching behavior with a large **ON-OFF** current ratio.

their complementary metal-oxide-semiconductor **(CMOS)** counterparts that are limited to a **60** mV/decade sub-threshold swing **[1,** 2].

Approaching an energy-efficient reliable performance for ultra-low power applications though requires overcoming two of the main challenges faced **by** the current **NEM** switches: large actuation voltage and stiction which refers to the adhesion between the contacting electrodes **[1,** 2]. To examine these challenges, one should focus on the switching gap of such a device, shown in Figure 1-la.

Assuming a near zero off-state leakage, the dynamic energy consumption *(E)* in a switching cycle is approximated by  $E \sim CV_{actuation}^2$  where *C* is the capacitance. A lowering of the actuation voltage ( $V_{actualion}$ ) is necessary to reduce the switching energy [2]. With switching gaps typically **>10** rm, current electrostatic **NEM** switches commonly exhibit operating voltages **>1** V **[1,** 2]. Assuming a simplified design based on a parallel plate capacitor,  $F_{electrostatic} \propto V^2/(g_0 - z)^2$  where *V* is the applied voltage,  $g_0$  is the initial switching gap and  $z$  is the displacement. Accordingly, to move

towards millivolt actuation, the switching gaps need to be reduced in width **-** in a relay  $V_{activation} \propto (g_0)^{3/2}$  where the actuation voltage is considered to be equal to the pull-in voltage [2]. Miniaturization of such a mechanically-active structure to a fewnanometer regime is not trivial as the surface adhesive forces, including the van der Waals forces, increase drastically with a reduction in the separation distance between the approaching electrodes  $(F_{vdW} \propto 1/(g_0 - z)^3)$ . These dominating surface adhesive forces can cause collapse of the structure and adhesion between the contacting surfaces, referred to as stiction, during fabrication and operation **[3-7].** Reducing the switching gap size is further challenged **by** the roughness of the contacts, inherent to the processing techniques conventionally employed, as schematically shown in Figure 1-la **,** limiting the extent of miniaturization.

Over the past years, extensive research has focused on developing new designs and fabrication schemes enabling low-voltage **NEM** switches with an operating voltage of  $\sim$ 400 mV, the lowest reported to date without any pre-biasing and with a switching gap of  $\sim$ 4 nm [8]. An overview of some representative NEM switches are outlined in Table **A.1** (Appendix **A) [8-26].** Despite various developments, overcoming these challenges is yet to be fully realized beyond proof of principle. The surface adhesive forces remain a challenge, causing unstable electrostatic modulation of the gap, leading to unreliable performance and often premature failure due to permanent stiction. Beyond unreliable performance, contact stiction also leads to hysteresis in switching (Figure **1-1b).** The hysteresis limits the lowest operating voltage and active power consumption achievable **[11].** To acquire a more energy-efficient operation, the hysteresis voltage should also be minimized **by** reducing the surface adhesion.

While developing techniques to scale down device dimensions, methodologies should also be devised to provide nanoscale force control to minimize stiction and allow controlled electrostatic modulation of nanogap electrodes to enable energy-efficient yet reliable performance. In designing such a switch, engineering a stable electromechanically active nanogap becomes the main challenge. As this thesis works towards addressing this objective, three considerations are made: **1)** miniaturization of the switching gap, 2) reduction in surface roughness, and **3)** force control to reduce hysteresis and allow controlled mechanical tuning. The end result is a switching gap **<10** nm wide, formed with nanometer precision and uniformity, capable of controlled and reversible electromechanical modulation.

### **1.3 Thesis Organization**

As discussed, this thesis studies the challenges of engineering at the limits of the nanoscale and introduces approaches to address them **by** focusing on the design of electromechanically active nanogaps. **By** developing new fabrication techniques and methodologies for force control, this work then introduces and experimentally demonstrates a switching mechanism for low-voltage and stiction-free **NEM** switches as an example device concept enabled **by** the ability to manipulate features single-digit nanometers in size. In doing so, three interdependent areas are investigated as outlined below.

#### **Part I - Fabrication with Nanorneter Precision, Control and Uniformity**

To allow engineering of active nanostructures with features few nanometers in size, Chapter 2 introduces fabrication techniques which combine top-down and bottom-up approaches. These techniques can be versatile, capable of integrating with novel and existing platforms, while allowing structures of desired complexity to be designed with nanometer resolution, control, and uniformity as building blocks of active nanoscale devices. Two example fabrication methodologies developed for formation of **<10** nm electrically active gaps are reported in Chapters **3** and 4. The technique in Chapter **3** complements top-down fabrication with bottom-up engineering of surfaces and forces to achieve unprecedented resolution while the method in Chapter 4 utilizes top-down fabrication to assist bottom-up assembly of nanogaps.

#### **Part II - Nanoscale Force Control - A Molecular Approach**

Molecules are introduced in Chapter **5** as building blocks that contribute precision in fabrication while also providing nanoscale force control through their chemical and mechanical properties. It is proposed that when used as nanoscale springs between neighboring surfaces, the molecule's mechanical compression provides an elastic restoring force to overcome surface adhesive forces to allow dynamic tunability in a controlled and reversible manner. This is shown in an electromechanically tunable molecular tunneling junction in Chapter **6.**

**Part III - Device Design - Tunneling Nanoelectromechanical Switches towards Low-Voltage and Stiction-Free Performance**

Electromechanical modulation of the tunneling current in a molecular nanogap is used to propose a tunneling-based **NEM** switch. The molecular layer helps define switching gaps much smaller than that feasible through conventional fabrication techniques while helping avoid stiction, enabling a more energy-efficient alternative to common electromechanical switches. An example two-terminal design of such a **NEM** switch is demonstrated in Chapter **7,** while Chapter **8** discusses a proposed multi-terminal architecture.

Lastly, Chapter **9** summarizes the thesis while reflecting on the **NEM** switch case study to provide a general perspective on the challenges of engineering at the limits of the nanoscale. The extension of the toolset developed in this thesis and the lessons learned in designing the switch to other device applications at the few-nanometer regime is discussed. **A** pictorial summary of this thesis is shown in 1-2.



Figure 1-2: Pictorial thesis overview: To enable engineering at the limits of the nanoscale, an interdisciplinary approach is necessary to develop alternative techniques for nanoscale fabrication and force control, leading to new paradigms of active devices.

# **Part I**

# **Fabrication with Nanometer Precision, Control and Uniformity**

## **Chapter 2**

# **Combining Top-Down and Bottom-Up Fabrication: Hybrid Nanotechnologies**

Fabrication technologies have continuously evolved over the past decades driven **by** the progress in the semiconductor electronics industry to keep up with the need for continuous device miniaturization. These predominantly top-down methodologies are often optimized for particular applications and material systems. In addition to the lack of versatility in processing, these techniques become limiting in resolution, precision and uniformity as dimensions continue to scale down. Therefore, they are not broadly suited for manufacturing of the various unconventional structures of unique functionalities that emerge at the nanoscale. Alternative methodologies are necessary to promote engineering of active devices in the few-nanometer regime.

### **2.1 Top-Down Fabrication**

Conventionally, nanoscale features are fabricated through top-down approaches in which bulk components are patterned into miniaturized entities (Figure 2-1). Lithography is the most commonly used top-down approach with the resolution mainly limited **by** the exposure wavelength. The schematic overview of the process is shown

in Figure 2-2. In this process, a polymeric resist responsive to the wavelength of the exposure source is deposited onto the substrate. Once exposed through a photomask or **by** direct-write, the desired pattern is transferred onto the resist. In this process the chemical properties of the resist alter where exposed. Once rinsed through the development process, a resist-based mask forms on the substrate. Following a deposition or etching step and after removing the resist, the desired features form on the underlying surface. Exposure wavelengths transitioning from visible to extreme ultraviolet and soft x-ray have allowed improvements in resolution from micron-scale features, when using conventional photo-lithography, to sub-100 nm **[27-30].** Reduction in wavelength combined with improvements in optical and processing techniques can further improve resolution to **<10** nm. Ion and electron-beam lithography techniques have been implemented that allow features as small as a few nanometers **[31-33].** However, widespread use of the next generation lithography processes is a technological challenge, having a low throughput while being costly and time-consuming.



Figure 2-1: Hybrid top-down and bottom-up fabrication techniques enable complex active structures with nanometer precision, resolution and control. Top-down fabrication involves use of processes including lithography to machine down bulk materials into nanostructures. Alternatively, bottom-up techniques involve nanoscale building blocks that assemble into larger functional entities. Example nanoscale building blocks are depicted here including chemically-synthesized molecules, nanoparticles and nanomaterials, and nanostructures formed through top-down fabrication.

Alternative techniques have also been developed to be used in conjunction with these lithographic approaches to allow for high-throughput and low-cost processing
of a wide variety of materials beyond conventional semiconductors, and on versatile surfaces including those nonplanar and pliant. **A** widely studied category of these techniques are soft lithography methodologies. Broadly, these techniques rely on using an elastomeric mold or stamp, commonly made out of polydimethylsiloxane (PDMS), to transfer desired patterns of a particular ink onto a receiving substrate. The patterns are defined **by** the topography of the stamp. Soft lithography processes typically involve printing, molding and embossing [34-36]. Figure 2-2 summarizes example techniques in the simplest forms, but it should be noted that variations of each have been developed for optimized performance and to accommodate different needs.

Amongst these techniques, microcontact printing is a versatile soft lithography approach through which an elastomeric stamp formed using a lithographically patterned master is used to transfer an ink onto a substrate. Example inks include molecules such as alkane thiolates, silanes, or biomolecules. The patterned molecular layer can then be used as an etching mask, or as a seed layer to promote spatially-selective growth or deposition of a material such as a metallic or semiconducting thin-film **[35, 37, 38].** Similarly, nanotransfer printing utilizes an elastomeric stamp to transfer patterns of a solid ink, such as thin-films of metals, onto a substrate with shapes defined **by** the surface topography of the stamp while layer-by-layer stacking enables three-dimensional arrangements [39-41].

In addition to printing, molding is also a common soft lithography technique. In the simplest form, replica molding allows fabrication of a replica of the original master **by** solidifying a liquid precursor (prepolymer) against the elastomeric mold **[35].** In a variation of this technique, known as microtransfer molding, the patterned features on the stamp are filled with a liquid precursor and are transferred onto a substrate in contact with the mold upon curing of the prepolymer **[35].** It is possible to use capillary forces to **fill** the channels formed in the mold with the prepolymer, leading to a technique referred to as micromolding in capillaries **[35].** In another emerging technique, referred to as nanoimprint lithography, the topographic patterns in a rigid mold are transferred to a thermoplastic polymer film placed on the substrate heated above its glass-transition temperature under an applied pressure **[35,** 42, 43]. Such high-throughput techniques have shown to allow sub-100 nm features applicable to a wide range of materials. However, fabrication of structures with high spatial complexity that requires multiple processing steps with precision in alignment and relative placement while maintaining high spatial density remains an ongoing challenge.

Focused ion beam milling which develops the desired features **by** direct sputtering of the material using a focused ion beam, such as gallium or helium ions, has also been shown effective in high resolution fabrication with features **<10** nm reported [44-47]. This maskless and resistless process can be implemented in a single step with precise positioning of arbitrary-shaped high resolution features. Despite its efficacy for planar fabrication, complex three-dimensional features are challenging to form. With the need for direct manipulation of the beam to individually pattern each component, large area processing is time consuming and not effective. The process is also not compatible to all material types as high energy ion beam can cause damage, in particular, to organic components.

Top-down techniques and their variations provide sufficient control over deterministic positioning of the features with the desired spatial variation and complexity. The fabricated nanostructures can also be easily accessed externally such that they can be electrically, optically or mechanically activated for the desired function. However, for further miniaturization, these techniques become limiting in resolution, precision and uniformity. Most notably, surface and edge imperfections are inevitable. At the few-nanometer regime, such irregularities, though small, can be on the order of the device critical dimensions and will hinder the desired function. To highlight these challenges, an example structure fabricated through top-down lithography and lift-off is shown in Figure 2-3 capturing the resulting edge defects and  $\sim$ 3 nm surface roughness. When building complex nanoscale devices with features only few nanometers in size and requiring multiple processing steps, such topographical non-uniformities will accumulate to challenge fabrication and impede successful device functionality.



Figure 2-2: An overview of various lithographic techniques. Conventional lithography involves use of an illumination source to expose through a photomask or direct-write a polymeric resist layer sensitive to the exposure wavelength. Once developed, the resistbased mask is used with a deposition or etching step to transfer the patterns onto the substrate. Nanoimprint lithography transfers the topographical patterns on a solid master onto a heated thermal polymer under an induced pressure. Focused ion-beam milling utilizes high energy ion-beam to directly write the patterns **by** sputtering. Soft lithography involves techniques through which elastomeric molds or stamps are used to transfer onto the substrate an ink in form of the patterns defined **by** the topography of the master.



Figure **2-3:** Nanostructures formed through top-down lithography, thermal evaporation of Au and lift-off. The scanning electron micrograph (left) shows the nonuniform edges of the structure while the atomic force microscope topography scan (right) shows  $\sim$ 4 nm roughness associated with the thermally-evaporated Au film.

### **2.2 Bottom-Up Fabrication**

Bottom-up fabrication, schematically shown in Figure 2-1, is an additive multidisciplinary technique where nanostructured building blocks are assembled to form larger functional entities with atomic precision [48-50]. These nanoscale building blocks include atoms, molecules, nanoparticles and other nanomaterials that are commonly chemically synthesized with sub-nanometer control over dimensions, surface topography and geometry. The chemical nature of the bottom-up methodologies also accommodates broad material systems much larger than that tolerated **by** the top-down approaches, making them suitable for engineering of emerging nanoscale devices. The building blocks can also be formed from nanostructures patterned through conventional top-down lithography techniques as will be discussed in the following chapter. In bottom-up assembly, controlled local interactions defined **by** surface properties are induced to rearrange the building blocks until the desired structure which corresponds to the lowest energy state of the system is assumed. Such thermodynamically-driven assembly leads to well-defined planar structures with nanometer resolution and uniformity but is insufficient to form complex, asymmetric and three-dimensional features.

Structures of higher complexity however, can also be realized **by** utilizing directedassembly methodologies in which asymmetric and directional interactions are used to promote directionality and specificity in assembly. **A** widely studied technique allowing controlled fabrication of complex three-dimensional nanostructures utilizes deoxyribonucleic acid **(DNA)** to induce programmable assembly **[51-53].** The **DNA** strands can be designed with desired nucleotide sequence ensuring pre-determined complementary base pairing in such a way that desired three-dimensional structures can be spontaneously formed. Nanostructures decorated with such **DNA** strands can also be selectively assembled into desired custom shapes as complementary base pairing occurs.

When developing nanoscale devices, precise positioning of the components is also important but not readily feasible through a self-assembly process. The deterministic positioning of the building blocks can be enhanced utilizing external stimuli including physical and chemical guides, electric and magnetic fields, and light **[54-57].** Collectively, a versatile approach emerges to assemble structures with nanoscale precision and resolution in a controlled and predictive manner. Figure 2-4 compares planar selfassembly of Au nanocubes with their directed-assembly where top-down fabricated physical templates direct the nanocubes' precise positioning.

### **2.3 Hybrid Top-Down and Bottom-Up Fabrication**

Bottom-up programmable assembly provides nanometer precision, resolution and uniformity desired for engineering at the limits of the nanoscale. However, these techniques alone can be insufficient to develop structures for functional devices and their integration into existing platforms. This typically requires higher order complexity and connectivity between individual components and external accessibility to provide driving input and extract output signals, particularly important for electrically-active devices. On the other hand, top-down techniques provide control over large-area processing of features of arbitrary shapes and complexity with the necessary interconnections. However, they lack the much needed nanometer precision, resolution



Figure 2-4: Comparison between self-assembly and directed-assembly of Au nanocubes. (a) Self-assembly promoted through surface interactions allows formation of an ordered layer of chemically-synthesized Au nanocubes. **(b)** The precise positioning of the cubes can be directed utilizing physical templates formed lithographically in a poly(methyl-methacrylate) (PMMA) layer.

and uniformity. The two methodologies can be cohesively combined to allow parallel integration of heterogeneous nanocomponents into higher order structures to yield complex active devices bearing features and uniformity in the nanometer scale **[58, 59].**

In one scheme, the bottom-up techniques can be complemented with the conventional top-down approaches to enable assembly of more complex structures. Concurrently, this integrative technique can add to the design components including interconnects needed for transforming the structures into active devices and systems **-** linking the nanoscale to the micro- and macroscale. Alternatively, top-down fabricated structures can undergo bottom-up engineering of surfaces and forces to evolve into desired architectures possessing critical dimensions of few nanometers. In combining these techniques complementary assistive fabrication techniques are needed. The objective of these techniques is to: **1)** maintain the nanometer precision and uniformity throughout the processing, 2) ensure successful integration of top-down and bottom-up schemes, and **3)** provide versatility such that the fabricated structures can be incorporated into novel and existing platforms regardless of the infrastructure.

Building on this premise, two techniques for controlled fabrication of electrically-

active nanogaps are introduced in Chapters **3** and 4. Extensions of these multidisciplinary techniques are then used in the following chapters in the design of low-voltage and stiction-free nanoelectromechanical switches.

### **2.4 Summary**

With continuous need for miniaturization, top-down fabrication techniques become limiting in resolution and uniformity. To overcome these limitations, chemistry has been used to formulate alternative bottom-up techniques through which nanometer control over manipulation of matter is feasible. Despite providing nanometer precision and uniformity, these processes lack the ability to achieve the complexity needed for functional nanodevices. To engineer active devices at the limits of the nanoscale hybrid top-down and bottom-up techniques appear promising as they can leverage the advantages of each methodology to enable complex active devices with nanometer precision, control and uniformity. Such integrative fabrication techniques should also provide sufficient flexibility to accommodate the diverse material systems, beyond conventional semiconductors, that are relevant to device engineering at the nanoscale. This in turn opens up a wide range of material properties and functionalities that would not have been available if only relying on top-down fabrication.

## **Chapter 3**

# **Controlled Fabrication of Nanoscale Gaps using Stiction**

Electrodes separated **by** nanometer-thin gaps are important building blocks of functional nanoscale devices and a platform for studying fundamental properties of materials with applications in molecular electronics, plasmonics and nanoelectromechancal systems, to name a few. Current methods of fabricating such nanogaps include electrochemical plating, focused ion-beam milling, electromigration, mechanical break junctions, nanosphere lithography, molecular junctions, adhesion lithography, atomic layer lithography, oblique-angle shadow evaporation and selective etching of welldefined sacrificial layers *[47,* **60-69].** Even though successful in forming individual sub-10 nm gaps, these approaches which involve multiple processing steps do not allow high throughput fabrication. The resulting devices typically lack robustness and exhibit unstable operation due to the inherent nonuniformities. These techniques also commonly used for two-terminal devices lack the versatility to be effectively incorporated into more complex, multi-terminal designs necessary for practical applications in integrated systems.

Here, we propose the use of stiction, an otherwise irreversible failure mode, to

Chapter **3** is adapted with permission from [F. Niroui, **E.** M. Sletten, P. B. Deotare, **A. I.** Wang, T. M. Swager, J. H. Lang and V. Bulović, Controlled fabrication of nanoscale gaps using stiction, *Micro Electro Mechanical Systems (MEMS), 28th IEEE International Conference,* **85-88, 2015].** Copyright **2015** IEEE.

promote controlled fabrication of nanogap electrodes **[70].** In this integrative approach, top-down fabricated metallic nanostructures will undergo structural changes induced **by** bottom-up modulation of surface interactions such that nanogaps smaller than originally patterned are achieved. The feasibility of this approach and example applications are discussed in this chapter.

### **3.1 Design Principles**

Stiction is a common mode of failure in electromechanical systems. It arises when the surface adhesive forces, including capillary, van der Waals, and electrostatic, overwhelm the elastic restoring force of the mechanically-active component, leading to its collapse and permanent adhesion. The drastic increase in adhesive forces with the decrease in the separation distance between approaching surfaces makes stiction increasingly more prominent as dimensions are scaled down. This failure mode however if induced in a controlled manner can be leveraged to assist formation of nanogap electrodes with a separation much smaller than that possible through conventional fabrication, as will be discussed in the following sections **[70, 71].**

In the scheme proposed here, laterally-actuated cantilevers and other device components are first formed using a one-step top-down lithography process. The design involves cantilevers facing opposing stationary structures such that a gap is formed between them. Capillary forces exerted on these mechanically-active cantilevers during a liquid phase processing step can induce deflection and eventual collapse. As the cantilever deflects due to the induced surface adhesive forces, the separation gaps can be modulated. The eventual stiction between the cantilever and a support structure stabilizes the system and enables formation of gaps smaller than originally patterned between the cantilever and additional electrodes located relative to the point of stiction. Through changes to the structures and liquid phase processing, surface adhesive forces caused **by** the capillary action, as well as van der Waals forces, can be adjusted to allow for precise tuning of the gap size.

### **3.2 Fabrication Flow**

The fabrication scheme for the stiction-induced formation of nanogap electrodes is shown in Figure **3-1.** Five layers of poly(methyl-methacrylate) (PMMA), a positive electron-beam resist, are spun over a silicon (Si) substrate with 2  $\mu$ m-thick thermal oxide (SiO<sub>2</sub>). Each layer is spun at 2000 rpm for 45 s and baked at  $180^{\circ}$ C for 90 s. The initial three layers of PMMA have molecular weight of 495 kg/mol (PMMA 495 **A6)** followed **by** two layers of molecular weight **950** kg/mol (PMMA **950** A4). Next, the cantilever and other electrodes are patterned onto the PMMA film using electronbeam (e-beam) lithography. The resist is developed in **1:3** dilution of methyl isobutyl ketone (MIBK) in isopropanol for **3** min, thoroughly rinsed in clean isopropanol and dried under a gentle stream of nitrogen. Finally, about **10** nm of chromium (Cr) and **100** nm of gold (Au) are deposited over the substrate using thermal evaporation to form the electrodes.

The five layers of PMMA of two different molecular weights with a total thickness of about 1.5  $\mu$ m allow fabrication of large aspect ratio features with an undercut profile, a thinner base and a thicker top as shown in Figure **3-2.** The undercut is achieved due to the differential dissolution rate of PMMA of varying molecular weights in MIBK **-** lower molecular weight PMMA has a faster dissolution rate than the higher molecular weight PMMA. The undercut prevents sidewall coverage during metal deposition and ensures electrical isolation between the electrodes such that functional devices can be achieved.

During the wet-developing process, a capillary force is exerted onto the cantilever, labelled as Electrode 1 in Figure **3-1.** This force can cause deflection of the cantilever. **If** sufficiently large to overcome the spring restoring force, the cantilever collapses on to an opposing PMMA support structure (Electrode 2) and undergoes stiction. The deflection and stiction reduce the gap between the cantilever and opposing electrodes, leading to the formation of nanogaps smaller than originally patterned. The spring constant of the cantilever can be adjusted **by** altering its geometry and constituent material. At the same time, the surface adhesive forces experienced **by** the cantilever

can be changed **by** the material selection, solvent and temperature used in the processing, and the placement and geometry of the stationary structures. **By** adjusting the surface adhesive forces, one can control the extent of deflection and its profile such that desired gap dimensions are achieved. The nanogaps further reduce in size when evaporating a thin-film of metal onto the PMMA to define the conductive electrodes with the reduction in the size depending on the thickness of the deposited film.



Figure **3-1:** Controlled fabrication of nanoscale gaps using stiction: (a) multilayer PMMA e-beam resist is spun onto  $Si/SiO<sub>2</sub>$  substrate and baked after each spin at 180°C, (b) resist is patterned using e-beam to define cantilever and opposing electrodes separated **by** a defined gap **"g13",** (c) resist is developed in **1:3** solution of MIBK in isopropanol, rinsed in isopropanol bath and dried under a stream of nitrogen, **(d)**  $\sim$ 10 nm of Cr and  $\sim$ 100 nm of Au is evaporated onto the patterned structures defining the electrodes. The gap formed after stiction  $(g'_{13})$  is smaller than that originally patterned  $(g_{13})$ . Upon evaporation of the metallic layers, the gap becomes even smaller  $(g_{13}^* \lt g_{13}' \lt g_{13})$ .



Figure **3-2:** An undercut structure formed in PMMA to enable electrical isolation between different device components upon evaporation of the Au film.

### **3.3 Controlled Formation of Nanogap Electrodes**

Figure **3-3** shows the feasibility of the proposed stiction-assisted fabrication scheme to form nanoscale gaps through a single lithography step. As mentioned previously, the surface adhesive forces induced can be modulated **by** controlling the design and processing conditions including the dimensions of the cantilever, gap size, and the solvent and temperature involved in the liquid-phase fabrication step. **If** the surface adhesive forces are sufficient to overcome the elastic restoring force, the cantilever collapses onto the support structure where stiction makes this deformation irreversible. The cantilevers of Figure **3-3** are formed based on the scheme shown in Figure **3-1.** To promote stiction in this design, the gap size between Electrode 1 and the opposing electrodes is decreased **by** approximately **30** nm in the cantilever of Figure **3-3b** compared to that in Figure 3-3a. Once collapsed, an effective gap of  $\sim 50$  nm is achieved between Electrodes 1 and **3** at the point closest to the stiction region compared to the 200 nm gap in a similar cantilever that has not undergone collapse and stiction. The proposed fabrication technique is also applicable to material sets beyond those investigated here for the proof of principle demonstration. Changes in the constituent materials and surface engineering using additional coatings can also help modify the adhesive forces to further tune the nanogaps.

Through engineering of the spring constant of the cantilever, and the geometry

and relative placement of the electrodes, the size of the nanogaps can be controlled. An example **~35** nm gap is shown in Figure 3-4a. **By** positioning Electrode **3** closer to the point of stiction, a smaller gap  $\sim 10$  nm is achieved as shown in Figure 3-4b. The tunability of the gap dimension is further demonstrated in Figure **3-5** where gaps ranging from about **10** nm to **170** nm are formed on a single substrate and through a single lithography step providing a platform for more complex device designs and concepts. With versatility to use a broad set of materials to achieve complex nanostructures over large areas, the stiction-induced fabrication is a promising method for developing functional nanoscale devices that require controlled formation of nanogap electrodes.



Figure **3-3:** Stiction promotes formation of nanogaps smaller than patterned: (a) Scanning electron micrograph  $(SEM)$  of a cantilever with a gap of  $\sim 200$  nm, (b) SEM of the same cantilever positioned closer to Electrodes 2 and **3.** Larger capillary force in **(b)** causes collapse of the cantilever, leading to stiction and reducing the gap between Electrodes **<sup>1</sup>** and **3.**



Figure 3-4: **SEM** of nanogaps fabricated using the scheme in Figure **3-1.** Capillary forces during wet developing of the pattern cause stiction between Electrodes 1 and 2, while forming a gap of  $\sim$ 35 nm (a) and  $\sim$ 10 nm (b) between Electrodes 1 and 3. The smaller gap in **(b)** is achieved **by** positioning Electrode **3** closer to 2.

### **3.4 Example Applications**

### **3.4.1 Electrostatically Tunable Nanogaps**

**A** potential application of the proposed nanogap fabrication is in the development of **NEM** switches where stiction, a common mode of **NEM** switch failure, is used to promote device miniaturization. To design a **NEM** switch, the nanogap needs to be electrostatically tunable. In forming the nanogap, depending on the design, the collapsed electrode can be made to remain stationary or undergo mechanical motion in response to electrostatic actuation. As shown in Figure 3-6a, a smaller gap and a more flexible cantilever allow electromechanical modulation of the gap. In this twoterminal example, a current modulation  $>10^{11}$  is achieved within 3 V applied bias. The switching performance can be optimized **by** modifying the device design achieved through changes in the fabrication process. This approach can also be extended to multi-terminal **NEM** switches that more closely resemble the operation of conventional



Figure **3-5:** Optimizing device architecture and electrode placement relative to the point of stiction allow achieving nanogaps with controlled width, useful for fabrication of multiterminal devices.

transistors. **A** prototype design is shown in Figure **3-6b.**

#### **3.4.2 Molecular Tunneling Junctions**

Nanogap electrodes have also been widely desired for applications in molecular electronics that rely on metal-molecule-metal building blocks. These molecular junctions are conventionally formed using techniques such as direct deposition of metallic contacts, nanotransfer printing of top electrodes and break junctions **[63].** The resulting devices commonly lack stability, uniformity and robustness. Additionally, high-throughput fabrication and integration into more complex designs and systems to extend practical applications are limited.

The proposed stiction-induced nanogap fabrication introduces an alternative approach to forming molecular junctions. In this approach, damage to the molecular layer can be avoided and device stability improved as the molecules are introduced into the gap after formation of the electrodes through techniques such as vapor de-



Figure 3-6: Electromechanically modulated nanogap formed using the stiction-based fabrication technique. (a) Through altering device geometry to achieve smaller gaps and more flexible cantilevers, nanogaps can be fabricated to undergo electromechanical modulation (blue compared to red), useful for applications in NEM switches. Insets show corresponding devices with the bottom cantilever (blue)  $\sim 20$  nm thinner than the top (red). The voltage is applied across Electrodes 1 and 2 and the current between them is monitored. (b) Prototype design of a three-terminal NEM switch with a source-drain gap of  $\sim 50$  nm. The electrodes are labeled as per a comparable field-effect transistor.

position or liquid-phase self-assembly. In self-assembly, molecules are functionalized with **terminal** groups that enable selective attachment onto the electrode surfaces, as will be discussed further in Chapter 5. For example, thiolated molecules readily self-assemble on gold.

Figure 3-7 shows the current-voltage characteristics of nanogaps of different sizes with thin-films of fluorinated decanethiol self-assembled on the Au surface using vapor-phase deposition. As expected, a general increase in current is observed with the decrease in gap size. Further analysis of the data to understand the specifics of the molecular gap requires more detailed experimentation. It is speculated that as molecular layers are formed, further decrease in the gap size can be achieved through changes in the surface adhesive forces imposed by changes in the surface properties. Integration of molecular layers in the nanogaps can also be useful for applications

in **NEM** devices where anti-stiction coatings can be introduced to enhance operation reliability. With the versatility to accommodate various metallic electrodes, this fabrication technique can be compatible to a wide set of molecular layers, allowing fundamental analysis of their properties while extending functionalities.



Figure **3-7:** (a) Nanogap electrodes formed using the stiction-based fabrication technique involving self-assembled molecular layers. The molecules can serve as coatings on the electrodes to modify surface interactions or can bridge the gap between the two electrodes forming a metal-molecule-metal structure. **(b)** Chemical structure of fluorinated decanethiol molecule. (c) Current-voltage characteristics of three gaps of different sizes with molecular layers of fluorinated decanethiols self-assembled on the Au electrodes. Representative **SEM** image of the devices is shown. Nanogaps of different sizes are achieved **by** changing the original size of the gap patterned through electron-beam lithography.

### **3.5 Challenges and Outlook**

Despite providing a promising platform for controlled fabrication of nanogap electrodes, the proposed technique faces some challenges. As seen in the **SEM** images, the metal electrodes have a large surface roughness, which introduces inhomogeneity in the gap size, making the device performance less stable and susceptible to electrical shorting. These topographical nonuniformities can also accumulate through potential subsequent processing steps, making this a less ideal basis for fabrication of more complex nanoscale devices and systems. To overcome this challenge, materials alternative to Au and PMMA or techniques such as atomic layer deposition which leads to atomically smooth surfaces should be implemented. In addition, some functional devices can be envisioned that require nanogaps with asymmetric metal electrodes of different materials. Enabling such structures requires modifications to the fabrication scheme that may increase the process complexity. It should be noted that in these electrically-active nanogaps, the induced electrostatic force through an applied voltage can provide yet another mechanism to tune the nanogap post-fabrication to achieve the desired size.

### **3.6 Summary**

**A** stiction-assisted fabrication is proposed and demonstrated as a promising technique for controlled formation of precisely defined nanogap electrodes. In this approach, top-down lithography is facilitated **by** the bottom-up engineering of forces to gain nanometer control and precision in fabrication. Capillary forces induced during liquid phase processing of the lithographically patterned sample cause deflection of the mechanically movable electrodes and subsequent stiction to the opposing stationary support structures. The deflection caused **by** modulation of surface adhesive forces leads to a reduction in the gap size to achieve a width less than originally patterned. The experimental results support the feasibility of the proposed method to fabricate nanogaps, with controlled widths smaller than **15** nm being demonstrated. Further optimization of this versatile fabrication platform allows development of nanogap electrodes for applications including plasmonic, electromechanical and molecular devices.

**56**

 $\sim 10^4$ 

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## **Chapter 4**

# **Fabrication of Nanoscale Gaps with Nanometer Resolution and Surface Uniformity**

When engineering at the limits of the nanoscale, in addition to nanometer control and resolution in fabrication, nanometer surface uniformity is essential. In developing nanogap electrodes, a fundamental component of active nanoscale devices such as nanoelectromechanical switches, many of the techniques developed to date including that introduced in Chapter **3** lack the desired surface uniformity. The resulting irregularities which can be on the order of the device critical dimensions can hinder the expected function. Furthermore, some of these techniques suffer from inefficient scalability to larger areas and lack versatility in the choice of compatible materials and substrates.

As discussed in Chapter 2, bottom-up techniques promise to achieve nanometer precision, resolution and uniformity beyond the limits feasible through top-down approaches. Importantly, they are well suited for large-area processing with minimal limitations on the choice of substrate or the materials employed. However, the re-

Chapter 4 is adapted with permission from [F. Niroui, M. Saravanapavanantham, T. M. Swager, **J. H. Lang and V. Bulović, Fabrication of nanoscale structures with nanometer resolution and surface** uniformity, *Micro Electro Mechanical Systems (MEMS), 30th IEEE International Conference,* **659- 662, 2017].** Copyright **2017** IEEE.

sulting structures often lack the infrastructure needed to function as independent electrically-controlled entities, a feature required for many device applications. To overcome the limitations of bottom-up assembly while leveraging their benefits, here we propose a hybrid approach in which bottom-up assembly is assisted **by** the topdown lithographic techniques **[72].**

### **4.1 Design Principles**

The integrative fabrication methodology proposed here consists of three main steps. First, bottom-up assembly is used to promote controlled formation of well-defined nanogaps using chemically-synthesized single-crystalline Au nanoplates shown in Figure 4-1. These Au nanoplates have surface uniformity significantly better than Au thin-films formed through thermal evaporation. While an evaporated Au film exhibits roughness  $\sim$ 4 nm, single-crystalline Au nanoplates posses roughness  $\lt 1$  nm (Figure 4-2). Second, top-down lithography is used to integrate interconnects with the nanogaps such that they can be electrically-activated. Third, a technique is implemented to planarize the step height that is introduced across the nanogap **by** the nonuniform thicknesses of the chemically-synthesized nanoplates. The planarization also helps eliminate the edge imperfections and reduce surface roughness of the lithographically patterned electrical connections. The latter will be discussed in more detail in Chapter **8** where a variation of this method is implemented in another device design.

### **4.2 Fabrication Flow**

The fabrication scheme used for formation of nanogap electrodes using the singlecrystalline nanoplates is shown in Figure 4-3. Au nanoplates are synthesized **by** reducing gold(III) chloride hydrate  $(HAuCl<sub>4</sub>)$  with ethylene glycol in presence of aniline and using polyvinylpyrrolidone (PVP) as the capping agent **[73].** The synthesis protocol is outlined in Appendix B. The self-assembly of the nanoplates is driven **by**



Figure 4-1: **SEM** images of chemically-synthesized Au nanoplates with well-defined shapes, edges and thicknesses (a and **b).** The single-crystalline nature of the nanoplates is confirmed in the transmission electron microscopy diffraction pattern of (c) showing Au(111) plane.

engineering the surface interactions between the plates such that they come together to form the nanogaps (Figure 4-3a). The as-synthesized Au nanoplates are functionalized with octadecanethiol to assume a hydrophobic surface, and then are phase transferred into chloroform. A  $\sim$ 20  $\mu$ L droplet of the functionalized Au nanoplates is then dispensed on a thin layer of deionized water coating a  $SiO<sub>2</sub>$  substrate of about 1 **cm<sup>2</sup> .** Chloroform is immiscible in water. The hydrophobic surfaces of the Au plates allow them to disperse in chloroform but prevent them from entering the hydrophilic phase, enabling them to be suspended at the water-chloroform interface. Chloroform, having a higher density than water, exerts a downward force on the plates to stabilize them at the interface. As the solvents evaporate, a force is exerted laterally to bring the Au plates together to form nanogaps that adhere onto the substrate once the solvents are completely evaporated.

Upon assembly, the substrate containing the nanogaps is briefly sonicated in ethanol to remove the undesired aggregated Au nanoplates and spherical Au particles that are formed as byproducts of the synthesis. To remove the residual PVP and octadecanethiol molecules, the substrate is then rinsed in a piranha solution. Once cleaned, interconnects and contact pads are added to the nanogaps using electronbeam lithography and a lift-off process based on thermally evaporated Au. It should be noted that the commonly used Cr adhesion layer is not used here. This ensures that the Au electrodes have a weak adhesion to  $SiO<sub>2</sub>$  to enable future processing steps, as will be discussed.



Figure 4-2: Atomic force microscope surface topography scan of the single-crystalline Au nanoplate shows roughness of  $\leq 1$  nm (a), much smaller than  $\sim$ 4 nm roughness expected for a thermally evaporated layer of Au **(b).**

At this point, electrically accessible well-defined nanogaps are achieved. However, due to nonuniformities in the thicknesses of the Au nanoplates, a step height across the nanogap may be present. **If** a planarized profile is required, the height variation must be eliminated. This is achieved through peeling the Au nanoplates and the electrical contacts using a receiving surface covered with an adhesive layer. The peeling reveals the coplanar side of the plates originally in contact with the substrate. To do so, first, the substrate is functionalized with a layer of low surface-energy trichloro(1H,1H,2H,2H-perfluorooctyl)silane through vapor or liquid-phase growth. The molecular structure is depicted in Figure 4-3b. The functional silane end-groups of the molecules allow assembly on the  $SiO<sub>2</sub>$  such that surfaces not covered by the Au acquire an anti-stiction property promoted **by** the fluorinated chains of the molecular coating. Then, a  $\sim 30 \mu L$  drop of an ultraviolet light (UV) curable epoxy (Norland Optical Adhesive **61)** is dispensed onto the substrate, following which, a receiving



Figure 4-3: Combined bottom-up self-assembly and top-down lithography formation of electrodes separated **by** nanogaps and with nanometer uniformity. (a) To self-assemble the nanogaps, nanoplates are surface functionalized with octadecanethiol to assume **hy**drophobic surface properties and then are assembled at the water-chloroform interface using hydrophobic-hydrophilic interactions and capillary forces as the solvents evaporate. **(b)** Nanogaps are formed using self-assembly of Au nanoplates **(1)** upon which wires and contacts are added using electron-beam lithography and lift-off (2). After anti-stiction treatment of the substrate surface **(3)** with trichloro(perfluorooctyl)silane, a UV-curable epoxy is used to peel off the nanogap and the interconnects onto a glass substrate to planarize the surface (4). (c) Chemical structure of trichloro(perfluorooctyl)silane used as anti-stiction coating in the planarization process.

glass substrate is placed on top of the adhesive layer. Capillary forces cause the epoxy to spread, forming a uniform layer in between the original substrate and the receiving surface. The uniformity of the epoxy layer is further improved **by** placing the sample inside a vacuum desiccator. Pulling vacuum also assists in eliminating the small air bubbles that might be introduced in the epoxy. If not removed, these bubbles can add to the undesired surface roughness. After removing the substrate from the desiccator, the epoxy is cured under **UV** light. Once cured, the glass is detached from the  $SiO<sub>2</sub>$ , peeling off the Au nanoplates and electrical connections as a uniform layer.

The surface uniformity of the fluorinated coating is influenced **by** the deposition technique and its roughness translates into the roughness of the peeled epoxy layer. It is desired to minimize the roughness of the peeled surface such that it is suited to serve as a platform for fabrication of nanoscale devices and systems upon further processing steps. For vapor-phase deposition of the molecules, the substrate is placed inside a vacuum desiccator in close proximity to a small droplet of the molecules. Under vacuum, the molecules vaporize and assemble onto the substrate. This process can lead to polymerization and formation of thicker and nonuniform molecular films. The roughness of these films can then replicate into a rougher epoxy surface upon peeling as shown in Figure 4-4a. This roughness can be minimized if the substrate is rinsed in fresh ethanol under brief sonication upon the vapor-phase assembly process. Alternatively, liquid-phase assembly of the fluorinated coating leads to a uniform surface, shown in Figure 4-4b. To promote liquid-phase assembly, the substrate is placed inside a **5** mM solution of fluorinated molecules in anhydrous ethanol in a nitrogen glovebox environment. After 4 hours, the substrate is removed from the solution of molecules, rinsed in fresh ethanol and dried under a stream of nitrogen.

## **4.3 Electrically-Active Nanogaps with Nanometer Resolution and Uniformity**

The self-assembly of Au nanoplates leads to formation of well-defined nanogaps with nanometer resolution and precision. Figure 4-5 shows nanogaps of various widths as small as  $\sim$ 10 nm formed through this bottom-up approach with a resolution, and edge and surface uniformity not feasible through conventional top-down fabrication.



Figure 4-4: The deposition technique used to fluorinate the substrate influences the molecular layer's uniformity which defines the roughness of the peeled epoxy surface. AFM topography scan of a surface containing a Au nanoplate peeled off a substrate fluorinated **by** vapor-phase assembly shows a rough surface (a). The surface roughness is minimized when trichloro(perfluorooctyl)silane is assembled in a liquid-phase instead **(b).**

The gap width is influenced **by** factors including the substrate surface properties, types of immiscible solvents used, molecular coating on the nanoplates, density of Au nanoplates, and temperature used for the assembly process. The smallest nanogap possible is limited **by** the thickness of the molecular layer that functionalizes the nanoplates. However, to reach this limit other experimental conditions, mentioned above, need to be controlled as they influence the assembly process.

As mentioned previously, due to variations in thicknesses of the nanoplates chemically synthesized, there typically exists a step height and nonuniform profile across the nanogap. An example is shown in Figure 4-6 where **~5** nm height variation is observed across the gap. Depending on the application, it might be desired to planarize this profile. Figure 4-7 illustrates an electrically accessible,  $\sim 30$  nm gap with  $\lt 1$  nm surface roughness and a planarized surface fabricated using the scheme of Figure 4-3. In this example, peeling is used to ensure the step height across the nanogap is removed. The peeling also eliminates the edge defects on the lithographically patterned electrical wires and pads, associated with the lift-off process, **by** exposing the side originally in contact with the  $SiO<sub>2</sub>$  substrate. The bottom surfaces of the patterned structures



Figure 4-5: Precisely defined nanogaps with nanometer resolution and surface uniformity formed through self-assembly of Au nanoplates based on the method shown in Figure 4-3a.

assume the surface roughness of the underlying substrate. **By** revealing this surface after peeling, the electrical connections acquire a roughness much smaller than that associated with the top surface of the evaporated Au thin-film.

### **4.4 Example Application**

The fabricated electrically-driven nanogaps can be used as building blocks of nanoscale devices with applications in nanoelectromechanical systems, molecular electronics and active plasmonics. They serve as a platform where further processing can be used to form more complex nanoscale structures with tailored functionalities.

An example application is shown in Figure 4-8. Here, Au nanoparticles coated with a layer of cetylpyridinium chloride **(CPC)** are dielectrophoretically trapped across the gap to form a vertically-defined molecular junction **[74-77].** The current-voltage characteristics of Figure 4-8 show an increase in conduction through the molecular junction formed based on the nanoparticle, compared to the current conduction through the



Figure 4-6: AFM surface topography shows a height variation of  $\sim$ 5 nm across the nanogap formed between the Au nanoplates due to the variations in thicknesses of the chemicallysynthesized nanoplates.

laterally aligned nanogap prior to nanoparticle trapping. **By** tailoring the thickness and the type of molecular coating employed in functionalizing the nanoparticle or the Au nanoplate surfaces, molecular junctions of varying electronic performance emerge. Subsequently, a range of applications in molecular devices can be realized.

### **4.5 Challenges and Outlook**

The proposed fabrication technique is demonstrated with Au nanoplates and interconnects. However, this process can be extended to other materials and their combinations to accommodate various applications. Currently, due to the relatively large size distribution that is present in the synthesized nanoplates, the assembly is of-



Figure 4-7: (a) Optical image of a planarized electrically contacted nanogap formed in between Au nanoplates. (b) SEM of the corresponding nanogap with a width of  $\sim 30$ nm. (c) The AFM surface topography of the structure shows uniform surfaces on the Au nanoplates and lithographically patterned Au wires achieved through the peeling technique. **(d) A** uniform AFM profile is observed across the nanogap.

ten localized. Further optimization is necessary to enable uniform self-assembly over larger areas with precise control over spatial positioning. This can be achieved **by** improving the synthetic approach to yield nanoplates with a smaller size distribution, and **by** optimizing the assembly conditions. To allow for deterministic positioning of the nanogaps, directed assembly methodologies can also be implemented, for example, through use of physical guides formed using conventional lithography.

### **4.6 Summary**

The unprecedented precision and resolution of bottom-up assembly is combined with the versatility of top-down lithography to develop a technique for fabrication of



Figure 4-8: Through dielectrophoretic positioning of Au nanoparticles coated with a molecular layer across the nanogap, vertical molecular tunnel junctions can be formed. The **SEM** image shows Au nanoparticles coated with cetylpyridinium chloride bridging  $a \sim 30$  nm Au nanoplate electrodes. The current-voltage characteristic compares the current conduction before (blue curve) and after trapping (two consecutive measurements are shown in red).

electrically-active well-defined nanogaps **<10** nm. **By** engineering surfaces and interfaces, chemically-synthesized gold nanoplates, with **<1** nm surface roughness, are assembled to form nanogaps. Interconnects and electrical contact pads are added using top-down lithography to introduce electrical functionality to the assembled nanogaps. **A** planarization technique is employed to eliminate nanometer-scale height variations across the gap due to the thickness inhomogeneity inherent to synthesized nanoplates. This is achieved **by** peeling the nanoplate electrodes as a uniform layer off the original substrate using an adhesive receiving surface, revealing the coplanar side originally in contact with the substrate. The peeling also eliminates edge defects and minimizes the surface roughness inherent to features formed through lithography. Overall, a platform to enable nanoscale devices of various functionalities including those relevant to molecular electronics, plasmonics, and nanoelectromechanical systems is achieved.

## **Part II**

# **Nanoscale Force Control - AMolecular Approach**

## **Chapter 5**

# **Molecules and their Applications in Nanoscale Processing**

The field of molecular electronics, dating back to nearly **50** decades ago, has been dominantly focused on the study of molecules as the building blocks of electronic devices and corresponding transport phenomena. Progress in the field has been continuously challenged **by** the limitations in fabrication and measurement capabilities. Given the nanometer scale dimensions of the molecular devices, the performance reliability is notably sensitive to any nonidealities, even though small, in the fabricated structures and the measurement methodologies. With rapid progress in fabrication and characterization over the past years, the field of molecular electronics has expanded beyond electronic transport to explore other intrinsic features and their utility in functional devices **[78-84].** Examples of emerging applications include molecular spintronics, plasmonics, thermoelectrics, optoelectronics, and quantum optics. Despite rapid progress in the field, an in-depth understanding of the underlying physical phenomena and full exploration of the technological opportunities are in their infancy and a topic of active research. In particular, integration of emerging device concepts into more complex functional systems remains a challenging prospect.

The atomic control over molecular design achieved through chemical synthesis provides a versatile approach to engineer molecule's inherent properties. The result is a large library of molecular units that can chemically or physically interact with

one another or other nanostructures to build active devices and systems. In addition to the possibility of possessing unique properties such as electrical, optical or thermal, importantly, molecules can serve as structural units to facilitate engineering of nanoscale structures in the few-nanometer regime with atomic resolution. Their mechanical properties and induced surface interactions defined **by** their chemical composition further assist in controlling nanoscale forces towards structural robustness and tunability. With the ability to serve as chemically-engineered nonlinear springs, molecules can offer a new dimension to the properties of restoring springs that are needed in mechanically-active structures. Thus, when designing emerging molecular devices, the molecules' structure, chemical composition and mechanical properties are important in nanoscale processing (Figure **5-1).**



Figure **5-1:** Molecules which can be precisely engineered through chemical synthesis serve as nanoscale building blocks **by** helping define device design and surface interactions using their inherent structural, mechanical and chemical properties.

### **5.1 Molecules as Structural Components**

As discussed in Part I, fabrication of structures few nanometers in size is often limited **by** the resolution of the processing techniques. In particular, defining nanometerthin spacing between neighboring structures is a challenge as the dominating surface adhesive forces at such small spacing can cause collapse of the structures. Molecules which can be precisely defined in conformation using chemical synthesis can serve as interconnects between neighboring surfaces. The atomic precision in defining the size of the molecule leads to an unprecedented precision in defining the spacing. Additionally, the molecules provide a restoring force to help balance out the surface adhesive forces to provide structural stability. In simplest form, this can help develop stable nanogaps, a topic of interest in this thesis, but more complex structures can also be facilitated.

Molecules can form into a thin-film using a self-assembly process. Through chemical synthesis, molecules can be designed with functional end groups that allow specific and spontaneous assembly onto the desired surface (Figure **5-2).** Such self-assembly of molecular layers have been widely studied through which functional groups suitable for assembly **by** covalent or noncovalent interactions onto a wide range of materials have been identified. Thiol-chemistry for example, through which sulfhydryl (thiol) functional group **(-SH)** adsorbs to surfaces including Au, **Ag,** Pt, Ru and Ni, has been extensively studied and employed in molecular electronics **[85].**

Through engineering of the spacer group, the length of the molecules can be tuned to precisely control the molecular layer thickness and consequently the spacing between neighboring surfaces. Figure **5-2b** shows an example where poly(ethylene glycol)dithiol (PEG-dithiol) is self-assembled using thiol-chemistry on the surface of Au nanocubes. **By** changing the polymer chain length, reflected in its molecular weight, the effective thickness of the self-assembled layer can be modified.

Beyond self-assembly, other techniques including thermal evaporation, spin-coating, molecular layer deposition, and layer-by-layer deposition can also be used in the formation of nanometer-thin molecular layers. Among these techniques, layer-by-layer deposition which relies on cyclic deposition of alternatively charged molecules through electrostatic interactions provide nanometer precision in defining thicknesses, over large areas and applicable to a wide range of materials. The control over thickness is shown in Figure **5-3** for the case of layer-by-layer deposited films of poly(sodium styrenesulfonate) **(PSS)** and poly(allylamine hydrochloride) (PAH) on Au substrates and measured with a spectroscopic ellipsometer. Here, **PSS** serves as the polyanion and PAH forms the polycation needed in the assembly process.



Figure **5-2:** (a) Molecules can be engineered through chemical synthesis with the desired head, terminal and spacer groups where the functional end groups can be selected to allow spontaneous and selective assembly onto a desired surface, while the spacer group can help define the size, structure, chemical and mechanical properties. As an example, thiol functional groups in poly(ethylene glycol)dithiol allow self-assembly on Au. The transmission electron micrographs (TEM) in **(b)** show the surface of a Au nanocube without any molecular coating compared to that with  $\sim$ 3 nm-thick self-assembled layer of PEG-dithiol. The thickness of the molecular film is dependent on the polymer chain length.

### **5.2 Engineering Surface Interactions with Molecules**

The spacer and functional end groups of a molecule can also help define its chemical properties, determining its interactions with the surrounding. **By** coating surfaces with the molecules, consequently, the surface properties can be modified. This has made molecular layers a versatile approach for surface and interface engineering to either enhance or reduce the surface interactions with the surrounding components. **By** controlling the surface interactions, the molecules help provide control over nanoscale processes from bottom up and hence yield higher precision. For example, **by** enhancing compatibility between typically incompatible surfaces, their uniform integration into multi-component structures can be improved using molecular coatings. On the other hand, molecular layers can be used as anti-stiction coatings to avoid adhesion between neighboring or approaching surfaces. Beyond providing structural stability, this technique can assist with the controlled and reversible dynamic tunability. An important application of the latter will be in nanoelectromechanical systems that involve electromechanically tunable nanogaps.

**By** modifying the contacts in an electromechanically active nanogap with a low surface energy molecular layer, the interactions between the approaching electrodes


Figure **5-3:** (a) Layer-by-layer deposition of polyelectrolytes allows cyclic assembly of oppositely charged entities for example poly(allylamine hydrochloride) (PAH) and poly(sodium styrenesulfonate) **(PSS)** with precise thicknesses. The precision in forming nanoscale molecular layers is shown in **(b)** for the case of layer-by-layer deposition with PAH and **PSS** on a Au substrate and characterized with a scanning ellipsometer.

can be minimized **[11, 86, 87].** This will not only help improve the device reliability and robustness but can help lower the hysteresis. The area within the hysteresis curve in a **NEM** switch corresponds to the lost switching energy. Reducing the hysteresis is therefore necessary to reduce the switching energy to move towards a more energyefficient operation. The importance of molecular coatings in reducing surface adhesive forces is evident in Figure 5-4 where the hysteresis voltage of the **NEM** relay is reduced by  $\sim$ 40% to  $\lt$ 50 mV when contacts are treated with fluorinated alkane molecules (1H,1H,2H,2H-perfluorodecyltriethoxysilane) **[11].** The fluorocarbon backbone lowers the surface energy and the surface adhesive forces while the silane functional group is used to promote the self-assembly onto the W contacts. The x-ray photoemission spectrum (XPS) in Figure **5-5** confirms successful self-assembly of the molecules which is performed in vapor phase.

#### **5.3 Molecules as Nanoscale Scaffolds and Springs**

As discussed, molecules can serve as scaffolds to define the spacing between neighboring nanostructures with nanometer precision and control. The mechanical properties of the molecules can further be leveraged to promote controlled and reversible tuning



Figure 5-4: Modifying contacts of a **NEM** relay with low surface energy fluorinated molecules reduces stiction demonstrated through lowering of the hysteresis voltage, in this example design achieving ~40% reduction on average. The **NEM** relay design is shown in the **SEM** image of (a) with the schematic cross-section of the device and the chemical structure of the molecular coating shown in **(b)** and **(d)** respectively. An example switching performance with and without molecular coating is included in (c), a hystereis **<50** mV is achieved **[11].**

of the defined dimensions. In this scheme, shown in Figure **5-6,** an applied external force can compress the molecules as the two surfaces approach each other. The elastic restoring force in the deformed molecules can help balance the surface adhesive forces during this process. Once the applied force is removed, the surface adhesive forces are overcome **by** the elastic restoring force of the deformed molecules to avoid stiction, transition back to the original dimensions, promoting controlled and reversible operation. This nanoscale force control in particular is important at the few-nanometer regime where controlling large surface adhesive forces is a great challenge.

The key is precise engineering of the mechanical response to achieve continuous balancing of the surface attractive forces throughout the tuning process. The mechan-



Figure **5-5:** The XPS spectrum of a tungsten (W) film with and without surface treatment **by** perfluorodecyltriethoxysilane confirms self-assembly of the molecular layer through use of silane end groups in a vapor-phase process. This is confirmed as a fluorine (F) peak is detected when characterizing the sample with the self-assembled fluorinated molecules while no F peak is observed for the sample without exposure to the molecules.

ical properties and their deformation-dependent dynamics can be engineered through chemical composition and physical form. This can be achieved at two levels: the design of individual molecules through chemical synthesis or collective engineering of the molecular layer **by** modifying its morphology and incorporating molecular entities of different properties. Such engineering of molecular mechanics is feasible but lacks the comprehensive knowledge-base needed for the design due to the limited studies executed to date concerning mechanics at molecular level. Tunability of dimensions can also be achieved **by** utilizing electrically-active molecules that change conformation in response to introducing a charge imbalance **[88, 89].** The different approaches to



Figure **5-6:** Nanoscale force control using molecular layers as springs. An applied force (Fapplied) compresses molecules connecting two neighboring surfaces. The elastic force  $(F_{elastic})$  stored in compressed molecules overcomes the van der Waals forces  $(F_{vdW})$  to make the process controlled and reversible.

engineering mechanically conformal spacers are outlined in Figure **5-7.** Few research efforts have fundamentally studied mechanical performance of molecules, effects of molecular deformation on the electronic transport, and conformational changes in molecules due to optical or electrical stimuli **[90-93].** However, utility of mechanical properties in developing active yet autonomously functioning molecular devices has not been well explored. The field remains to be an ongoing area of research while many opportunities for devices of unique functionalities can be envisioned given the added degree of freedom provided **by** nanomechanics to promote engineering at the limits of the nanoscale.



Figure **5-7: A** molecular layer that can define the spacing between two neighboring surfaces to allow dynamic tunability can be composed of (a) a single type of molecule, **(b)** engineered molecules with different components, (c) engineered thin-film composed of different molecular species, **(d)** active molecules that change conformation in response to an external stimulus. For example, dibenzocyclooctatetraene which has a tub conformation in the ground state flattens when reduced.

Force control using molecules as nanoscale springs provides a promising platform to develop precisely defined sub-10 nm nanogaps that can be dynamically tuned electromechanically. The structure is composed of an insulating molecular layer sandwiched between metallic contacts. In this metal-molecule-metal junction, an applied voltage across the electrodes provides an electrostatic force which can attract the top electrode towards the bottom, compressing the molecules in the process. The compressed molecules provide elastic restoring force that balances the surface adhesive forces. The feasibility of this mechanism to produce stiction-free controlled and reversible electromechanically tunable nanogaps is explored in the following chapter.

#### **5.4 Summary**

Molecules can serve as structural building blocks to facilitate nanoscale processing. Atomic resolution feasible through chemical synthesis provides precise control over the structure and chemical composition. Consequently, molecules can precisely define the spacing between neighboring surfaces with resolution superior to that feasible through conventional fabrication techniques. **By** engineering surfaces, molecular coatings can adjust surface interactions to assist with structural robustness and controlled tunability. The mechanical properties of the molecules are proposed to further provide means of controlled and reversible tuning of the spacing between the structures. This is achieved **by** predictive conformational changes in molecules defined **by** their customizable mechanical response.

**78**

 $\mathcal{L}^{\text{max}}_{\text{max}}$ 

 $\label{eq:2} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$ 

 $\label{eq:2} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$ 

### **Chapter 6**

## **Controlled and Reversible Tuning of Nanogap Electrodes**

Previous chapter discussed the utility of molecules as building blocks of nanoscale structures providing nanometer precision, control and resolution in processing. We proposed use of molecules as nanoscale springs to precisely tune the distances between the neighboring surfaces. Here, using an electromechanically tunable molecular junction, the feasibility of molecules in precisely defining nanoscale gaps and providing force control is investigated [94].

#### **6.1 Design Principle**

The desired design will be composed of a molecular layer sandwiched between two conducting electrodes where one can be mechanically mobile, as shown in Figure **6-1.** The width of the gap is defined **by** the thickness of the molecular film. An applied voltage across the contacts induces an electrostatic force to cause the top electrode to approach the bottom **by** compressing the molecules. As the voltage is removed, the elastic force of the deformed molecules provides the restoring force necessary to

Chapter **6** is adapted with permission from [F. Niroui, P. B. Deotare, **E.** M. Sletten, **A.** I. Wang, E. Yablonovitch, T. M. Swager, J. H. Lang and V. Bulović, Nanoelectromechanical tunneling switches based on self-assembled molecular layers, *Micro Electro Mechanical Systems (MEMS), 27th IEEE International Conference,* **1103-1106,** 2014.]. Copyright 2014 IEEE.

overcome the surface adhesive forces such that the gap recovers to its original width. Given the small dimensions involved and the fragility of the organic materials, direct and reliable probing of the nanogap's mechanical tunability is not trivial using the conventional imaging and characterization techniques.



Figure **6-1:** Molecules can help precisely define a nanogap electrode and allow its controlled and reversible electromechanical modulation **by** providing force control. **If** sufficiently small, conduction through quantum tunneling is observed where the tunneling current changes exponentially as a function of the tunneling gap. Here,  $\alpha$  is an adjustable parameter that accounts for the effects of barrier shape and electron effective mass. In this example,  $\alpha$  is selected to be **0.57,** within the range reasonable for organic molecular layers.

**If** the molecular gap is sufficiently small, it allows conduction through the junction due to quantum tunneling in response to the applied voltage. The conduction mechanism through self-assembled monolayers of organic molecules has been extensively studied and can be explained based on the Simmons model for  $V < \phi/q$  [95-100]:

$$
I = \left(\frac{qA}{4\pi^2\hbar G^2}\right) \quad \{(\phi - \frac{qV}{2})exp[-\frac{2(2m)^{1/2}}{\hbar}\alpha(\phi - \frac{qV}{2})^{1/2}G] \tag{6.1}\n- (\phi + \frac{qV}{2})exp[-\frac{2(2m)^{1/2}}{\hbar}\alpha(\phi + \frac{qV}{2})^{1/2}G]\}
$$

where  $m$  is the electron mass,  $q$  is the electron charge,  $G$  is the tunneling distance,  $A$  is

the overlapping area between the electrodes,  $\phi$  is the molecular layer tunneling barrier height, and  $\alpha$  is an adjustable parameter that accounts for the effects of barrier shape and electron effective mass. The exponential dependence of the tunneling current on the tunneling distance, as depicted in Figure **6-1,** can serve as a suitable approach to probe electromechanical changes in the gap size with sub-nanometer precision. As will be discussed in Part III, this current modulation which can be tuned **by** the mechanical properties of the molecular layer can develop a new platform for lowvoltage and stiction-free **NEM** switches.

#### **6.2 Fabrication Flow**

To acquire an electromechanically active metal-molecule-metal structure, a fabrication scheme similar to that presented in Chapter **3** is implemented using a laterallyactuated cantilever design. The process flow is outlined in Figure **6-2.** In brief, a cantilever and opposing electrodes are formed using electron-beam lithography in  $\sim$ 1.5  $\mu$ m thick layer of poly(methyl-methacrylate) (PMMA) spun over a silicon (Si) substrate with 2  $\mu$ m-thick thermal oxide (SiO<sub>2</sub>). Once the structures are formed, **100** nm of Au is deposited over the substrate using thermal evaporation to define the electrodes. Upon deposition of the Au film, the nanogap width is reduced in size with the reduction determined **by** the thickness of the film. The device fabrication is completed **by** self-assembly of fluorinated decanethiol molecules in vapor phase onto the Au surfaces through the use of thiol chemistry. The molecular film forms uniformly over the entire substrate including inside the nanogap. Results indicate that through the assembly process Electrodes 2 collapses onto Electrode 1 with the molecules sandwiched between the electrodes, forming a gap narrower than originally patterned and leading to a metal-molecule-metal junction **~1** nm wide with a movable electrode. **A** scanning electron micrograph of a fabricated cantilever and the chemical structure of the fluorinated decanethiol molecule are shown in Figure 6-3a and **b,** respectively.



Figure **6-2:** Fabrication process of the tunneling **NEM** switch: (a) multilayer PMMA electron-beam resist is spun on a  $Si/SiO<sub>2</sub>$  substrate and baked after each spin, resist is then electron-beam-patterned to define the switch components, **(b)** resist is developed in **1:3** solution of MIBK in isopropanol, (c) **100** nm of Au is evaporated over the substrate, **(d)** fluorinated decanethiol is self-assembled in vapor phase over Au, bridging the gap between Electrodes 1 and 2.

#### **6.3 Results and Discussions**

The fabricated cantilever has a gap of  $\sim$ 15 nm after the deposition of the Au film and prior to the self-assembly of fluorinated alkane molecules. When electrically actuated, this structure which resembles a conventional relay relies on the elastic restoring force of the cantilever to overcome the surface adhesive forces to ensure repeatable operation. The current-voltage (I-V) characteristic of such a device in the absence of a molecular layer is shown in Figure 6-4a. **A** successful initial actuation is followed **by** subsequent electrical shorting of the device due to stiction. This irreversible operation arises since the surface adhesive forces in this design have overcome the elastic



Figure **6-3:** (a) Scanning electron micrograph of a laterally actuated cantilever formed based on the fabrication scheme in Figure **6-2. (b)** Chemical structure of fluorinated decanethiol used in forming the molecular gap. The assembly process is executed in vapor-phase using thiol-chemistry.

restoring force of the cantilever, causing cantilever collapse and permanent adhesion between the contacting electrodes.

On the other hand, a similar device characterized after the self-assembly of fluorinated decanethiol molecules exhibits repeatable operation as shown in Figure 6-4b. The presence of the molecular layer helps reduce the possibility of stiction. This reversible operation can be attributed to the reduction in surface energy and the introduction of an elastic restoring force **by** the molecules while also avoiding direct contact between the electrodes. Figure 6-4b shows a distribution in the measured results over multiple runs. The nonuniformity in operation may be caused **by** the irregular topography of the electrodes as seen on the **SEM** image of Figure 6-3a. The surface uniformity and consequently the performance stability can be improved **by** using alternative materials and deposition techniques. For example changing the PMMA support structure to  $SiO<sub>2</sub>$  or utilizing atomic layer deposition are expected to improve surface uniformity.



Figure 6-4: (a) Current-voltage characteristics of a tunneling **NEM** switch in the absence of fluorinated decanethiol molecular layer showing device failure due to stiction after the first run; **(b)** Current-voltage characteristics of the switch after self-assembly of fluorinated decanethiol showing repeatable operation. Note that the highest value of current is set **by** the compliance of the measurement setup and is not a property of the device.

Notably, the current-voltage characteristics before and after molecular layer deposition are distinct, with the behavior obtained after incorporation of the molecules resembling that of quantum tunneling. The Simmons model is used to compare the experimental results with the theoretically expected behavior. Here, to acquire a close fit to the experimental data,  $\phi$  of 1.4 eV and  $\alpha$  of 0.6 are selected, within the range of values reported in the literature for similar molecular layers **[96, 97].** Even though the selected values of  $\phi$  and  $\alpha$  are reasonable approximates, note that the exact values can vary depending on the specifics of the tunneling junction. Based on the experimental data, the initial thickness of the tunneling gap is estimated to be  $\sim$ 1.0 nm, which is consistent with the expected thickness of a monolayer of decanethiol **[92].** Accordingly, it is deduced that Electrode **1** and Electrode 2 collapse onto each other through the self-assembly of the molecules to form a metal-molecule-metal structure with a gap smaller than  $\sim$ 15 nm that was originally patterned. This is an example hybrid fabrication technique where top-down fabrication of nanostructures is combined with bottom-up self-assembly of molecules, and engineering of surfaces and forces to allow controlled formation of electromechanically-active molecular gaps.

When compared to the theoretical expected behavior assuming a constant tun-

neling distance (nanogap width) throughout the actuation process, a close fit with the experimental data is obtained at lower voltage values but a larger discrepancy is observed as the voltage increases. The comparison is shown in Figure **6-5.** The faster increase in current than expected at larger voltage values may be accounted for **by** a reduction in the tunneling width throughout the actuation process. Applying a voltage across the metal-molecule-metal structure induces an electrostatic force. If sufficient to overcome the elastic restoring force of the molecular layer, it can compress the molecular layer and reduce the gap between Electrodes 1 and 2. The decrease in the electrode-electrode tunneling distance results in a faster increase in the tunneling current than that expected for a constant gap. To evaluate this possibility, the theoretical model is modified **by** taking into account the electromechanical modulation of the molecular junction.

To do so, the balance of electrostatic, van der Waals and spring restoring forces at equilibrium are used to determine the electrode-electrode distance at each applied voltage. Subsequently, the extracted gap size is used within the Simmons model to evaluate the tunneling current. The force balance equation is given **by**

$$
M\frac{d^2z}{dt^2} = \frac{\epsilon_r \epsilon_0 A V^2}{2(G_0 - z)^2} + \frac{A_H A}{6\pi (G_0 - z)^3} - k(L - G_0 + z)
$$
(6.2)

where  $M$  is the mass of Electrode 2,  $G_0$  is the initial distance between the electrodes, z is the displacement of Electrode 2, *L* is the initial thickness of the molecular layer, *A* is the overlapping area between the electrodes,  $A_H$  is the Hamaker constant,  $\epsilon_0$  is the permittivity of free space,  $\epsilon_r$  is the dielectric constant of the molecular layer, and *k* is the spring constant of the layer related to the Young's modulus Y by  $k = YA/L$ . The relative permittivity of the molecular layer is assumed to be 2.0, within the range of values reported for alkanethiols **[100].** The Hamaker constant is considered to be  $3 \times 10^{-19}$  J based on the values reported for capacitive structures with Au electrodes **[101].** Considering the structural profile of Electrode 2, its spring constant is estimated to be orders of magnitude smaller than that expected for the molecular layer; thus, its contribution to the force balance equation is neglected.

The green curve in Figure **6-5** shows the simulated current-voltage characteristic using the modified model. **By** taking into account electromechanical compression of the molecular layer a closer fit to the experimental result is obtained compared to the case of a constant switching gap. In this case, electromechanical modulation of the fluorinated molecular layer leads to about 10-fold increase in current within the voltage range considered. To achieve the best-fit curve it is deduced that the molecular gap underwent  $\sim 26\%$  or  $\sim 3$  Å decrease in the tunneling distance. The theoretical model suggests a Young's modulus of approximately **0.23** GPa for fluorinated decanethiol, in agreement with the measurements reported in the literature for alkanethiols of similar molecular structure **[92].** It is worth noting that this device platform provides a suitable approach for studying mechanical properties of molecular layers which would be difficult to study using conventional metrology tools due to the small dimensions involved.



Figure **6-5:** Experimental current-voltage characteristic of the tunneling **NEM** switch (blue) compared to the theoretical characteristics based on the Simmons model of tunneling with a constant gap (red) and a variable gap (green).

The results imply that in addition to providing precision in defining dimensions between surfaces, molecular layers can provide control of surface adhesive forces necessary to achieve dynamic and reliable tuning of these dimensions. This feature which relies on the mechanical properties of the molecular layer is in particular helpful for

the design of active devices only few nanometers in scale which would commonly face premature failure due to stiction. To emphasize the prospects, the following section introduces a new platform for low-voltage and stiction-free **NEM** switches using the proposed electromechanically tunable molecular junctions.

#### **6.4 Summary**

Molecules can serve as structural components to allow precise formation and dynamic tuning of nanogap electrodes with unprecedented nanometer precision and control. The feasibility of this concept is investigated based on a metal-molecule-metal junction formed using a laterally actuated cantilever and fluorinated alkanethiol molecules. In this design,  $\sim$ 1 nm molecular gap undergoes controlled electromechanical compression, modulating the electrode-electrode distance and consequently the tunneling conduction. With versatility in design of the structure and mechanical properties of the molecular films, an engineering approach emerges to support the development of active nanoscale devices in the sub-10 nm regime that would otherwise not be easily feasible due to stiction-induced failures. More fundamentally, this platform can also serve as a metrology tool for studying the combined electrical and mechanical properties of molecular thin-films.

## **Part III**

# **Device Design - Tunneling Nanoelectromechanical Switches towards Low-Voltage and Stiction-Free Performance**

### **Chapter 7**

## **Two-Terminal Tunneling Nanoelectromechanical Switches**

Reversible conformational changes in engineered nanostructures due to external stimuli can lead to modulation of characteristics including light-matter interaction, electrical conduction and optical properties. This controlled alteration of properties creates a foundation for a broad range of active nanoscale devices. Electromechanical devices, which involve movable structures with electrostatically tunable spacing, are an extensively studied example with applications such as switches, memory units, tunable optical filters, light modulators and sensors to name a few. Most commonly studied structures have tunable dimensions larger than tens of nanometers. Miniaturization to smaller dimensions can lead to improved device performance including energy-efficiency while also introduce unique functionalities that are not feasible at larger scale. As discussed previously however, miniaturization to the few-nanometer regime is challenged **by** limited resolution of the fabrication techniques and the large surface adhesive forces causing stiction.

In previous sections, various processes were discussed to enable nanometer precision, control and uniformity in fabrication and mechanical tuning of dimensions to

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promote engineering at the limits of the nanoscale. **A** scheme was proposed in Part II where molecules help define electromechanically tunable nanogap electrodes with nanometer resolution and with alleviated stiction despite the small dimensions. This mechanism can form a platform for electromechanical systems with critical dimensions  $\langle 10 \rangle$  nm and without stiction. With the ability to create nanogaps only few nanometers in size and with controlled and reversible electromechanical modulation such tunable metal-molecule-metal structures are proposed here as a platform for low-voltage and stiction-free **NEM** switches [102]. The **NEM** switch to be discussed is only one of many devices that could benefit from hybrid fabrication techniques and molecular engineering, and so serves as an illustrative example.

#### **7.1 Operating Principles of Tunneling NEM Switches**

#### **7.1.1 Tunneling Switching Mechanism**

Unlike conventional **NEM** switches which rely on direct contact between electrodes **[1,** 2], the proposed switching mechanism relies on electromechanical modulation of tunneling current in a metal-molecule-metal switching gap. This tunneling-based **NEM** switch, named a squeezable switch or a "squitch", has the potential to overcome two of the main challenges of current **NEM** switches: large actuation voltage and stiction-induced premature device failure, while maintain the benefits that **NEM** switches offer: near-zero off-state leakage and abrupt switching behavior. Through the use of molecules to form the switching gap, nanogaps can be defined with dimensions much smaller than conventionally feasible, leading to a lowering of the actuation voltage. Furthermore, through the reversible electromechanical compression of these molecules, an approach for controlling surface adhesive forces is introduced to prevent stiction during fabrication and operation.

The exponential dependence of tunneling current on tunneling distance can ensure large **ON-OFF** current ratio if sufficient modulation of the switching gap is facilitated. In the example in Chapter **5,** a 10-fold increase in current is observed for

 $\sim$ 3 Å compression of a nanogap composed of a fluorinated decanethiol layer with a large Young's modulus of  $\sim 0.23$  GPa. To ensure current modulation  $> 10^6$ , a larger modulation of the tunneling gap is necessary. For example, in reference to Figure **6-1,** a 50% modulation of a 3 nm gap with  $\phi$  of 3.5 eV and  $\alpha$  of 0.57 leads to  $>10^6$  ON-OFF current ratio. The OFF-state switching gap should be selected to ensure low leakage current while the gap should be sufficiently small such that the actuation voltage can be kept at the lowest possible. To further allow for a low actuation voltage, the Young's modulus of the molecular layers should be kept at the lowest tolerable **by** the design. The Young's modulus should be sufficiently low to allow low-voltage actuation while be large enough to provide adequate restoring force to ensure reversible stiction-free performance. This means that the elastic restoring force provided **by** the compressed molecular layer should exceed the van der Waals forces while being less than the combined van der Waals and applied electrostatic forces  $(F_{vdW} < F_{elastic}$ *<[Fvdw +* Felectrostatic]). Figure **7-1** shows the dependence of the actuation voltage on the Young's modulus for an example switch. In this particular architecture, a modulus of **<11** MPa provides an actuation in the sub-1 V regime.

#### **7.1.2 Squitch Design**

The main component of the design is the metal-molecule-metal switching gap composed of an electrically insulating compressible molecular layer sandwiched between conductive electrodes. For the proof-of-concept design investigated here, an offstate switching gap of  $\sim$ 3 nm is deemed suitable. To ensure a large modulation of the switching gap, a low Young's modulus self-assembled layer of poly(ethylene glycol)dithiol (PEG-dithiol) is incorporated in the design. The self-assembled layer of the polymeric material is expected to form a thin-film composed of void space which can yield a lower effective Young's modulus compared to a well-packed film of shorter alkane molecules. Such nanometer-thin polymeric layer is susceptible to the damage imposed **by** the fabrication technique in particular that of the top electrode. For example, the most widely used deposition techniques are not adequate for this design as direct deposition onto the molecular layer can cause penetration of metallic



Figure **7-1:** (a) Actuation voltage of an example two-terminal metal-molecule-metal squitch as a function of Young's modulus of the compressible molecular film showing an increase in the actuation voltage with an increase in the Young's modulus. **(b)** To achieve sub-i V actuation in this example, a material with a Young's modulus **<11** MPa is desired.

filaments into the layer causing nonuniform switching gap and electrical shorting. The resulting nonuniformities even though small are significant given the **<3** nm width of the switching gap. Hence, these can correlate to large perturbations in the device reliable and stable operation.

In Chapter **5,** a fabrication technique is introduced to form electromechanically tunable molecular tunneling junction using a laterally-actuated cantilever. This approach is not suitable for the formation of molecular junctions made of **PEG** selfassembled layer. The cantilever design requires vapor-phase growth of the molecules and in the current form cannot accommodate solution-based assembly. The solutionbased assembly can cause collapse of the cantilever structure due to capillary action and induce structural degradation depending on the solvents involved in the growth process. Therefore, an alternative design based on a vertically-actuated junction with Au bottom electrode, PEG-dithiol spacer and graphene top electrode is utilized. The fabrication process is selected such that damage to the molecules can be avoided to form well-defined compressible tunneling junctions.

To avoid the need for making electrical connections to the top electrode to ease fabrication, and to avoid damage to the graphene and the nanometer-thin molecular layer, the design is selected such that two bottom electrodes are bridged **by** a mechanically and electrically floating top electrode. In this case, an applied voltage across the two bottom electrodes induces an electrostatic force in this capacitive structure such that the top electrode is attracted towards the bottom, compressing the molecules to modulate the tunneling gap. A variation of this design can also incorporate interdigitated bottom electrodes.

#### **7.2 Two-Terminal Squitch Fabrication Flow**

The fabrication scheme is shown in Figure **7-2.** The bottom electrode is formed through top-down lithography and lift-off using thermally evaporated Cr and Au **(5** nm and **50-100** nm, respectively). The molecular layer is formed through thiol-based self-assembly of PEG-dithiol. The molecular weight is selected to acquire a selfassembled layer of the desired thickness. Molecular weight of 2000 g/mol with 22 repeat units in the polymer chain yields a self-assembled layer of  $\sim$ 3 nm as shown in the transmission electron micrograph of Figure **5-2.** To promote self-assembly, the patterned bottom-electrodes are immersed in a **5** mM solution of PEG-dithiol in ethanol inside a nitrogen-filled glovebox at room temperature. After 24 hours, the substrates are removed from the PEG-dithiol solution, thoroughly rinsed in ethanol and gently dried under a stream of nitrogen.

To avoid damage to the molecular layer due to the top electrode deposition and in an attempt to achieve a well-defined switching gap, a graphene layer is used as the top electrode and transferred onto the molecular layer through an additive process. The atomically smooth surface of graphene with sub-nm localized roughness, as shown in Figure **7-2b,** provides the desired uniformity to form a well-defined switching gap. The graphene is first synthesized through a chemical vapor deposition **(CVD)** technique **[103].** To transfer the graphene onto the molecular layer, first the CVD-grown graphene on copper (Cu) foil is spun with poly(methyl-methacrylate) (PMMA) on one side and baked at **80'C** for **10** min. The graphene on the back side of the Cu foil is then removed with an  $O_2$  plasma etch. The Cu/graphene/PMMA stack is then placed in Cu etchant for **15** min, allowing the Cu to dissolve. The remaining graphene/PMMA film which floats at the water-air interface is rinsed in deionized water thoroughly and finally removed from the water using the receiving substrate which contains the bottom electrodes and the assembled molecules [104].

As seen in Figure **7-2b,** despite graphene's local smooth topography, it exhibits surface nonuniformities over larger areas due to roughness of the underlying Cu foil used in the growth process and the wrinkles produced through the large-area transfer. This roughness can influence the device reproducibility and stability and can contribute to device-to-device variation in performance. Thus, to realize the squitch's optimal performance and enhance the fabrication yield, further improvements in the graphene transfer process are necessary.

In a variation of the transfer process outlined in scheme II of Figure **7-2d,** to help define smaller devices which would enhance uniformity of the tunneling junction and performance, the graphene layer is lithographically patterned prior to the transfer onto the molecular layer. In this approach, graphene layer is first transferred onto a  $SiO<sub>2</sub>$  substrate using the process outlined above. Then, using lithography and lift**off,** thermally-evaporated Au features with the desired form and dimensions of the graphene top electrode are patterned on the graphene surface. The Au then serves as a mask to etch the exposed graphene using **02** plasma, leaving behind patterned graphene covered with Au to be used as the top electrode. To form the switching gap, the patterned top electrodes need to be aligned to the bottom electrodes prior to the transfer. In addition to serving as the etch mask, the Au covering the patterned graphene helps with the alignment process as it enhances graphene monolayer's visibility under an optical microscope. The Au also enhances the robustness and conductivity of monolayer graphene while the interface uniformity of the top electrode is still dominated **by** the sub-nm smoothness of the graphene layer. An example device is shown in Figure **7-3.**



Figure **7-2:** (a) Fabrication scheme for a two-terminal squitch with Au-(PEG-dithiol) graphene switching gaps. **(b)** AFM topography of CVD-grown graphene transferred on a substrate showing sub-1 nm local roughness. (c) Chemical structure of PEG-dithiol used for the spacer layer. **(d)** The technique used to transfer the top graphene electrode onto the molecular layer. The transfer can either be done without an alignment over the entire substrate as a single sheet (Scheme **I),** or, the graphene can be first lithographically patterned into smaller features and transferred onto the bottom electrodes locally using an aligned transfer technique under an optical microscope (Scheme **II).**



Figure **7-3:** (a) Optical image of an example two-terminal squitch. **(b)** Schematic crosssection of a two-terminal squitch with graphene top electrode, PEG-dithiol spacer layer and Au bottom electrodes. An applied voltage across the bottom electrodes induces an electrostatic force to compress the molecular layer and tune the tunneling gap through which the tunneling current is modulated.

#### **7.3 Results and Discussions**

The measured current-voltage characteristics of three example squitches fabricated based on Au-PEG-graphene tunneling junctions are shown in Figure 7-4a. Two operating regimes are observed. An increase in the applied voltage results in an initial exponential increase in the tunneling current followed **by** an abrupt jump. The point of abrupt increase corresponds to the pull-in. Prior to pull-in, current increases exponentially as the tunneling gap is reduced **by** electrostatically induced compression of the molecular layer. Once the pull-in distance is reached, where the combined electrostatic and van der Waals forces overwhelm the elastic restoring force of the molecular layer, the top graphene electrode accelerates rapidly towards the bottom electrodes causing an abrupt decrease in the electrode-electrode distance and an increase in the tunneling current. The current saturation is due to the compliance set to the measurement instrument. The performance variations between devices may be attributed to differences in the molecular layer thickness and packing density, roughness of the electrodes which may result in variations in the effective width of the gap, and the properties of the Au-molecule or graphene-molecule junctions.



Figure 7-4: Current-voltage characteristics of two-terminal squitches. (a) I-V characteristics for three example squitches fitted to the theoretically simulated behavior. The following parameters were used to achieve the simulated best-fit curves: Device 1:  $\phi = 1.6$  eV,  $\alpha =$ 0.46,  $L = 3.1$  nm,  $G_{pull-in} = 2.2$  nm,  $\epsilon_r = 2.2$ ,  $Y = 11$  MPa; Device 2:  $\phi = 1.2$  eV,  $\alpha =$ 0.43,  $L = 2.2$  nm,  $G_{pull-in} = 1.6$  nm,  $\epsilon_r = 1.4$ ,  $Y = 17$  MPa; and Device 3:  $\phi = 4.4$  eV,  $\alpha = 0.41, L = 2.6 \text{ nm}, G_{pull-in} = 1.9 \text{ nm}, \epsilon_r = 2.9, Y = 16 \text{ MPa}.$  (b) Three consecutive measurement sweeps show hysteresis associated with the operation. (c) Three consecutive measurement sweeps for another device with the first 2 runs executed in the pre-pull-in regime and the third showing device pull-in. **(d)** The first two sweeps show no significant hysteresis when the device is operating in the pre-pull-in regime.

To further study the current conduction mechanism, the experimental results are fitted against the simulated performance. Taking the point of sudden increase in the current as the pull-in, the pull-in voltage in each device is used to extract the expected tunneling gap change with each applied voltage through solving the equation of motion (Equation **6.2).** The evaluated tunneling gaps are then used with the Simmons tunneling model (Equation **6.1)** to simulate the expected current modulation. In fitting the experimental data, a Monte Carlo approach is implemented where the tunneling barrier height  $(\phi)$ , tunneling barrier shape  $(\alpha)$ , initial thickness of the molecular film *(L)* and the pull-in point are the unknown parameters selected randomly within a predefined range to simulate the device performance and extract the expected dielectric constant and Young's modulus. In this analysis, the Hamaker constant is set to be  $3 \times 10^{-19}$  J. A detailed overview of the simulation approach and analysis is provided in Appendix **C.**

It should be noted that due to the large number of unknown parameters present in the model, many combinations of values for  $\alpha$ ,  $\phi$  and *L* can yield a close fit to the experiment. Nevertheless, within the possible results, combinations of unknown parameters exist that are within physically reasonable bounds while strongly agreeing with experimentally extracted values of  $\epsilon_r$  and Y. With  $\alpha$  constrained to 0.7  $\pm$  0.3,  $\phi$  $= 3 \pm 2$  eV and  $\epsilon_r = 3 \pm 2$ , the Young's modulus extracted for a self-assembled layer of PEG-dithiol (2000 g/mol) based on the three devices is within the **5** MPa to 40 MPa range (Appendix **C).** The pull-in gap for these devices is determined to be in the range of **0.71L** to 0.74L where L is the initial thickness of the PEG self-assembled layer. **A** more precise determination of the parameters requires further information regarding the specifics of the tunneling junction, mechanical properties of the molecular layer, and dynamics of molecular layer electromechanical deformation which necessitates further experimentation. Acquiring the added information though is challenged **by** the inadequate characterization tools and experimental approaches currently available to independently extract each unknown component, in particular influenced **by** the extremely small dimensions being investigated. As a result, alternative metrology tools are also needed. The squitch concept augmented **by** a plasmonic ruler can be a suitable characterization platform as will be briefly discussed in Chapter **9.**

The best-fit curves simulated for each device along with the corresponding parameters and extracted material properties are shown in Figure 7-4a. The close fit between the simulated and experimental results supports the proposed tunneling switching mechanism of squitches where electromechanical modulation of the tunneling current arises due to the controlled compression of the molecular film. This is compared to the theoretically simulated performance with no compression of the molecular layer in Figure 7-4a. Comparing the two scenarios, the experimental results show  $> 10^4$  current modulation with actuation voltage  $< 2$  V. With relatively low actuation voltage and an abrupt switching, the tunneling switching mechanism provides a promising platform for low-voltage and low-sticiton **NEM** switches. To achieve such optimal performance however, the device design and mechanics of the molecular layer and its dynamics need to be optimized.

**A** limitation of the prototype squitch design investigated here is that the operation in the pull-in regime is accompanied **by** a hysteresis. Figure **7-4b** which depicts three consecutive current-voltage measurements of a squitch shows electromechanical modulation of the tunneling current and the associated hysteresis. Such hysteresis is undesirable as it causes unreliable performance over repeatable actuation and limits the energy efficiency of the device **by** adding to the active power consumption. In an ideal design, precise balancing of the surface adhesive forces through use of the elastic properties of the molecular layer is expected to help minimize hysteresis. The hysteresis observed in this example may be attributed to the non-ideal balance of forces due to the non-optimal morphology and mechanics of the molecular layer, intermolecular interactions, adhesion between the electrodes or the molecules and the electrodes, and presence of capillary forces. This hysteresis is not observed in the prepull-in regime. Figure 7-4c shows three consecutive current-voltage measurements of another squitch with the first two measurements performed prior to the pull-in while the third shows the pull-in at  $\sim$ 1 V.

It should be noted that the concept squitches introduced here serve as preliminary efforts towards the demonstration of tunneling current modulation as the main switching mechanism in an electromechanical switch. In particular, PEG-dithiol is selected as a model material with a low Young's modulus, and a wide variety of other material systems and engineered thin-films can be designed for an improved performance. As well, alternative fabrication approaches and device architectures can be implemented. In the current design, despite the sub-nm smoothness of the top graphene electrode, the bottom electrode still has a roughness inherent to the lithography and deposition techniques utilized. The roughness of the underlying electrode can contribute to device instability. Development of an optimal squitch with sub-1 V actuation and reliable switching performance requires engineering of molecular layers with tailored mechanical properties, characterization of molecular layer's electromechanical performance, and practical integration of the molecular layer into optimized device geometries. Furthermore, extension of two-terminal squitches to more complex multi-terminal designs with gate-control is desired to render them more practical for applications in integrated systems, a topic of discussion in Chapter **8.**

#### **7.4 Summary**

This chapter proposes **NEM** switches that operate through electromechanical modulation of tunneling current across a switching gap composed of a compressible molecular layer sandwiched between conductive contacts. In this design, electrostatic actuation of the switching gap results in the mechanical compression of the molecules as the two contacts approach each other. The decrease in the tunneling distance leads to an exponential increase in the tunneling current which defines the switching performance. Presence of the molecules provides a means of controlling surface adhesive forces while avoiding direct contact between the electrodes helping alleviate stiction. Concurrently, molecular films which can be precisely controlled in thickness help define switching gaps much smaller than allowed **by** conventional fabrication techniques to lower the actuation voltage. An example device in a two-terminal form is shown here using a Au-PEG-graphene tunneling junction with actuation voltage <2 V and current conduction modulation  $>10^4$ . Further optimization of the molecular layer and device architecture are needed to realize the optimal performance feasible through this tunneling switching mechanism.

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### **Chapter 8**

## **Multi-Terminal Tunneling Nanoelectromechanical Switches**

Incorporating the tunneling-based switching mechanism within multi-terminal device architectures allows gated modulation of current. Such device resembles a conventional transistor in operation, extending squitch application as components of integrated systems. With increase in design complexity in multi-terminal devices to accommodate the desired performance parameters, however, fabrication becomes more demanding. An example design of a multi-terminal squitch and the corresponding fabrication procedure is presented here to demonstrate the possibility of the gated switching performance.

#### **8.1 Multi-Terminal Squitch Design**

Figure **8-1** shows a proposed design of a multi-terminal squitch. In this example, an applied voltage between gate electrodes 1 and 2 provides an electrostatic force to attract the top electrode towards the bottom to reduce the switching gap size and modulate the source-to-drain tunneling current. Similar to the two-terminal architecture, the sub-5 nm switching gap is composed of a compressible molecular layer. In the multi-terminal design though, to avoid an on-state tunneling leakage current, the gate electrodes should be recessed relative to the source and the drain **by** a few nanometers. With a goal of minimizing switching energy, in an optimal design, the recess should be sufficiently large to avoid leakage without inducing unnecessary increase in the actuation voltage. Such precisely defined surface topography with nanometer height variations between neighboring structures while maintaining **<1** nm surface and edge uniformity is challenging to achieve through conventional techniques. Consistent with previously discussed examples, a hybrid top-down and bottom-up process would accommodate the design needs **-** developing electromechanically active switching gaps with nanometer precision, control and uniformity.



Figure **8-1:** An example design of a multi-terminal squitch. An applied voltage across gate electrodes **1** and 2 provides an electrostatic force to compress the molecular layer to tune the tunneling gap between the top electrode and the source/drain electrodes and consequently modulate the drain current  $(I_D)$ .

#### **8.2 Multi-Terminal Squitch Fabrication Flow**

Multi-terminal squitches consists of three components: bottom electrodes, molecular layer and the top electrode. In forming the bottom electrodes controlling the surface topography is necessary to achieve nanometer uniformity of surfaces and edges while acquiring the precise spatial profile needed between the electrodes. In this approach which is summarized in Figure 8-2a, two-dimensional materials, such as graphene, are lithographically patterned to be used as the sacrificial layer defining the recessed region. Two-dimensional materials are in particular suitable as their layered structure provides nanometer precision in thickness while also possessing atomically smooth surfaces. Once the sacrificial layer is formed, electrodes and interconnects are patterned using electron-beam lithography followed **by** thermal evaporation of Au and lift-off. Then, a technique similar to that discussed in Chapter 4 is implemented to

peel the structures off the original substrate exposing the side originally in contact to the  $SiO<sub>2</sub>$  for further processing. The exposed sacrificial layer is then etched, revealing a recessed profile corresponding to the thickness of the two-dimensional material template. Figure 8-3 shows neighboring electrodes fabricated with  $\sim$ 4 nm height difference, illustrating the versatility of the peeling technique to achieve nanometer vertical resolution.

As shown through the atomic force micrographs of Figure 8-4, significant reduction is also observed in the edge and surface roughness that is otherwise inherent to the top-down fabrication techniques. The surface exposed through peeling assumes the roughness of the underlying flat  $SiO<sub>2</sub>$  substrate. Therefore, the edge defects are eliminated to achieve coplanar structures (Figure 8-4a and **b).** Additionally, the surface roughness is reduced from  $\sim$ 4 nm common to a thermally evaporated Au film to less than 1 nm on the peeled surface (Figure 8-4c and **d).** With sub-nm surface uniformity and resolution in defining the surface profile, a desired platform emerges to fabricate squitch bottom electrodes but is also broadly applicable to engineering other structures at the few-nanometer regime.

Once the bottom electrodes are fabricated, the molecular layer is formed through self-assembly in liquid phase using thiol-chemistry. Similar to the two-terminal devices, poly(ethylene glycol)thiol (PEG-thiol) is used as the compressible molecular layer. To promote the self-assembly, the bottom electrodes are placed in a **5** mM solution of PEG-thiol in deionized (DI) water for  $\sim$ 12 hours in a nitrogen-filled glovebox. Upon completion of the growth process, the substrate is then rinsed thoroughly in DI water and dried under a stream of N<sub>2</sub>. Alternatively, the molecular layer can be self-assembled on the top electrode prior to the placement on the bottom contacts. **A** combination of molecular layer growth on both the bottom and top electrodes can also be implemented to achieve the desired thickness **(8-2b).**

Lastly, the top electrode needs to be added to the design without inducing damage to the molecular film. Direct deposition of the top contact in particular would be inadequate as it would lead to electrical shorting and nonuniform molecular junctions. To ensure achieving a well-defined switching gap with the desired surface uniformity,



Figure **8-2:** Fabrication scheme for multi-terminal squitches. (a) Bottom electrode fabrication: **A** sacrificial layer made out of two-dimensional materials such as graphene is lithographically patterned to define the surface topography. Electrodes and interconnects are formed using electron-beam lithography. The substrate surface is fluorinated. Using an epoxy adhesive layer and a glass receiving substrate the structures are peeled off the surface. Sacrificial layer is etched, using  $O_2$  plasma in the case of graphene, revealing the bottom electrode with the desired topography. **(b)** Molecular layers are self-assembled either on the bottom electrodes (Scheme I), top electrode (Scheme II) or a combination of the two (Scheme III). (c) Chemical structure of PEG-thiol used as the molecular spacer layer. **(d)** Top electrode is formed using chemically synthesized Au nanorods. The nanorod is precisely positioned on the bottom electrodes using a dielectrophoretic trapping approach. (e) **SEM** image of chemically-synthesized Au nanorods.



Figure **8-3:** An example three-terminal bottom electrode formed using the fabrication technique of Figure 8-2a with Electrode 2 being recessed by  $\sim$ 4 nm relative to Electrodes 1 and **3** using graphene as the sacrificial material, and evaporated Au as electrodes.

chemically synthesized Au nanorods are utilized as the top contact. The scanning electron micrograph of the nanorods is shown in Figure 8-2e. These nanorods can be made with the desired length and diameter through an approach summarized in Appendix B **[105].** The Au nanorods lack order as-synthesized. To allow device fabrication, individual nanorods need to be precisely positioned over the source-drain electrodes. To accommodate such precise manipulation of the nanoparticle, a dielectrophoretic approach is implemented (Figure 8-2d)  $[74-77]$ . A 10  $\mu$ L droplet of the Au nanorod solution in water is placed on the electrodes. An **AC** voltage is applied between the source and drain electrodes **(2-5** V peak to peak depending on the electrode design at **100** KHz **-** 1 MHz frequency). The applied voltage induces an electric field attracting the nanorod to the region of highest field intensity. As the rod aligns with the field it bridges the source to drain gap creating the desired squitch design. To limit the trapping to a single nanorod, a voltage dividing resistor is placed in series with the electrodes with a resistance intermediate to that of the nanogap with and without the bridged rod.

The transmission electron micrograph of Figure **8-5** shows the cross-section of a



Figure 8-4: The peeling technique helps eliminate the edge defects imposed **by** the liftoff process. Here, an edge roughness  $\sim 50$  nm caused by the lift-off process (a) is eliminated through the peeling technique **(b).** The peeling also minimizes the surface roughness, achieving  $\langle 1 \rangle$  nm average surface roughness on the peeled surface (d) compared to  $\sim$ 4 nm roughness expected for the surface of an evaporated thin-film of Au (c).
representative molecular junction formed through the aforementioned process. The cross-section shows  $\sim$ 6 nm molecular gap formed between the atomically smooth facet of the top nanorod electrode and the peeled bottom electrode which has a sub-1 nm surface roughness. This cross-section clearly illustrates the benefit of the peeling technique in enhancing surface uniformity. The bottom edge of the evaporated electrode (Surface 1) shows a roughness  $\sim$ 4 nm consistent with the roughness expected for an evaporated Au film. However, the top peeled surface (Surface 2) shows a drastic decrease in roughness to **<1** nm which promotes formation of a well-defined molecular gap. In addition to allowing formation of precisely defined molecular junctions, the proposed hybrid bottom-up and top-down technique can also lead to large-area device fabrication.



Figure **8-5:** (a) TEM image of the cross-section of a molecular gap with Au nanorod top electrode and peeled evaporated Au film as the bottom electrode. **(b)** The magnified image shows the well-defined uniform molecular layer formed between the Au nanorod facet and the peeled electrode, both surfaces exhibiting roughness **<1** nm.

#### **8.3** Results and Discussions

The electrical characterization of the multi-terminal squitches suggests the gatedmodulation of the tunneling current as shown in Figure **8-6.** Similar to the case of two-terminal devices, two main sections are observed in the device operation. First, an exponential increase in the drain current  $(I_D)$  with an applied gate voltage corresponds to the decrease in the tunneling gap between the bottom electrodes and the top contact due to the induced electrostatic force. This is followed **by** an abrupt increase in *ID* corresponding to pull-in at which point the combined electrostatic and van der Waals forces overwhelm the restoring force of the molecular layer such that the top electrode rapidly approaches the bottom leading to an abrupt decrease in the tunneling gap and consequently an abrupt increase in the current. The saturation region is due to the compliance set to the measurement tool.



Figure **8-6:** Current-voltage characteristics of an example multi-terminal squitch showing gated modulation of drain current. The experimental measurement is compared against the theoretically simulated performance showing a good fit when considering compression of the switching gap. To achieve the best-fit curve it is deduced that PEG-thiol layer has a Young's modulus of ~20 MPa. **(b)** Consecutive measurements of another device shows **<50** mV hysteresis.

Assuming a pull-in voltage of 2.4 V, using the modified Simmons model in an approach similar to that discussed in Chapter **7,** the experimental results are fitted against the theoretical simulation. Compared to the theoretical case where no compression of the molecular layer would be expected, electrostatically-induced compression of PEG-thiol molecular layer in this device results in **>10'** modulation of the current. Repeatable measurements also show **<50** mV hysteresis associated with the devices, much smaller than that common in conventional contact-based **NEM** switches.

The results presented here are based on preliminary designs and more in-depth understanding of the device operation requires further experimentation. With the potential for low-voltage and abrupt switching with low hysteresis, squitches appear as a promising platform for energy-efficient **NEM** switches. To achieve ideal performance, optimization of device design and molecular layer chemical and mechanical properties are necessary. Beyond switches, the proposed tunable molecular gaps can also be applied to other mechanically-active nanoscale devices where control of surface adhesive forces is required for reliable and reversible operation.

#### **8.4 Summary**

An example design of a multi-terminal squitch is proposed where gated modulation of the tunneling current **-** resembling the operation of a conventional transistor **-** is achieved. To experimentally demonstrate this concept, a hybrid bottom-up and topdown fabrication is developed where nanometer precision, control and uniformity is achieved in forming well-defined molecular switching gaps. This technique leads to **<1** nm uniformity of edges and surface roughness while providing nanometer resolution in defining surface topography with height variations between neighboring electrodes **<5** nm. With the potential for low-voltage and abrupt switching with low hysteresis, tunable molecular gaps can serve as a promising platform towards more energy-efficient **NEM** switches. However, ideal operation requires further optimization of the device design and molecular layer chemical and mechanical properties. The fabrication and tunability techniques discussed here for multi-terminal squitches can also serve to form other building units of nanoscale devices and systems that require nanometer precision and uniformity.

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### **Chapter 9**

### **Summary and Outlook**

#### **9.1 Summary**

Engineering at the limits of the nanoscale, dimensions in the few-nanometers regime, necessitates nanoscale precision, control and uniformity beyond those commonly possible through conventional techniques. In addition to precise fabrication, controlled placement of nanostructures relative to one another is challenging, in particular if mechanically active. The large surface adhesive forces hinder structural stability often causing adhesion between components or permanent collapse of structures. Therefore, when engineering at the limits of the nanoscale, beyond developing alternative fabrication techniques, devising approaches for nanoscale force control are essential. These challenges are investigated in this thesis while focusing on developing a new platform for energy-efficient **NEM** switches. With the goal of reducing actuation voltage and stiction, **NEM** switches require miniaturization of the electromechanically tunable switching gaps to **<10** nm while controlling surface adhesion. Engineering such tunable nanogaps pushes the limits of nanoscale processing.

To achieve active nanoscale devices, such as electromechanically tunable nanogaps, with nanometer precision, control and uniformity, this thesis emphasizes hybrid topdown and bottom-up fabrication methodologies. This leads to techniques where chemistry, and surface and force engineering are integrated with conventional fabrication processes to enhance the resolution attainable while maintaining versatility. Utilizing this principle, two approaches are developed for controlled fabrication of electrically active nanogaps. In one, top-down fabricated nanostructures reconfigure through bottom-up engineering of surfaces and forces to achieve dimensions **<10** nm much smaller than that readily feasible through the top-down approach. In an alternative technique, bottom-up assembly of nanogaps **<10** nm is complemented **by** the lithographic patterning of electrical contacts and interconnects. These approaches facilitate nanoscale engineering **by** developing new fabrication processes and re-envisioning conventional ones while bridging the boundaries between different disciplines. The key is achieving integrative methodologies that provide the versatility needed to readily accommodate the more diverse material systems and unique capabilities that emerge as dimensions approach a few nanometers.

As is discussed in this thesis, controlling surface adhesive forces is another challenge of engineering at the limits of the nanoscale. Such control is in particular necessary for mechanically-active devices such as **NEM** switches. Dominating surface adhesive forces complicate device fabrication as dimensions are miniaturized, and impede reversible and reliable operation. In the case of a **NEM** switch, the surface adhesion also induces a hysteresis in performance setting a limit on the energy efficiency of the device. In this thesis, molecules are proposed as suitable building blocks to help minimize surface adhesion effects through use of their tailored chemical and mechanical properties. It is shown that molecules can serve as anti-stiction coatings lowering the surface energy of structures coming into contact with each other in a **NEM** switch, thus, minimizing the surface adhesive forces experienced. This scheme is schematically shown in Figure **9-1b.** Furthermore, the molecules can serve as interconnects between the electrodes forming the switching gap. In this scheme, the molecules not only assist precise formation of nanometer-thin gaps **by** controlling molecular lengths through chemical synthesis but serve as nanoscale springs to tune the relative spacing in a controlled and reversible manner. The molecular layer can undergo controlled mechanical compression in response to an applied external force, for example an electrostatic force due to an applied voltage. As the molecules compress, the surfaces sandwiching the molecular film approach one another. The elastic restoring force of the molecules help balance the increasing surface adhesive forces. Once the applied force is removed, this elastic restoring force overcomes the surface adhesive forces to ensure that the movable surface transitions to its original position for a reversible operation, overcoming stiction. This principle is used to develop an electromechanically tunable metal-molecule-metal tunneling junction, where presence of the molecules helps formation of nanometer thin gaps with controlled and reversible tunability.



Figure **9-1:** Schematic representation of strategies toward low-energy stiction-free **NEM** switches utilizing molecular layers. (a) In a conventional contact-based **NEM** switch, the elastic restoring force should exceed the surface adhesive forces to overcome the energy barrier  $(\Delta E)$  to break the contact. (b) Low surface energy molecular layers reduce the surface adhesive forces at contact, decreasing the potential for stiction. (c) Additional minimization of stiction can be achieved using a metal-molecule-metal switching gap which further lowers the surface adhesive forces and allows nanoscale force control through compression of the molecular layer, while enabling formation of a few nanometer-thick gap for sub-1 V operation [102].

**A** decrease in the tunneling gap leads to an increase in the tunneling current. The tunneling current modulation in an electromechanically tunable molecular nanogap is proposed as a switching mechanism for **NEM** switches, devices referred to as squitches. Implementing hybrid fabrication techniques, example squitches are demonstrated in this thesis in two-terminal form with  $\langle 2 \rangle$  v actuation voltage and  $> 10^4$  current modulation. Extension to multi-terminal designs utilizing newly developed hybrid fab-

rication techniques suggests gated modulation of the tunneling current resembling operation of conventional transistors necessary for use in integrated systems. These devices also show **<50** mV hysteresis, among lowest reported for **NEM** switches. With the potential to miniaturize the switching gap to much smaller than conventionally feasible while providing nanoscale force control, a platform for low-voltage and lowstiction energy-efficient switches emerges (Figure 9-1c). However, realizing optimal performance and full understanding of the switching mechanism require further improvements in device architecture, and chemical and mechanical properties of the molecular layer beyond the proof-of-concept designs explored here. Even though applied to tunneling-based **NEM** switches, the nanoscale processing toolsets developed here can also be broadly applicable to other active devices with critical features a few nanometers in size.

#### **9.2 Outlook**

#### **9.2.1 Tunneling NEM Switches - Squitches**

The squitch designs presented in this thesis demonstrate the feasibility of the proposed tunneling-based switching mechanism towards low-voltage and stiction-free **NEM** switches. The switching mechanism however, is not limited to the example designs and model material systems used. As mentioned previously, to realize an optimal switching performance in accordance to the desired application, optimizing the device architecture and molecular layer structural, mechanical and chemical properties are necessary. Further experimentation is also needed to investigate the device stability and lifetime. Stability of molecular layer under continuous high frequency mechanical deformation with electrical actuation is necessary to ensure long term device integrity and is a topic of future studies. Furthermore, future work will emphasize experimental characterization of the switching parameters including the switching speed and energy in various designs of squitches and corresponding circuits to identify performance limits and ideal designs.

Maintaining uniformity and precision is important in defining the sub-5 nm molecular switching gaps to maintain device stable operation. However, the need for uniformity extends beyond individual devices. Integration into circuits for practical applications requires large-area and high-density fabrication of such nanoscale devices which can be challenged **by** presence of device-to-device variations. Given the small dimensions and exponential dependence of the tunneling current on changes in the switching gap, minute conformational variations may lead to drastic discrepancies in performance. The sensitivity of squitch performance at a systems level to such structural variations should be evaluated and appropriate measures put in place to provide the necessary compensations to maintain consistency. When designing squitches, as considered in this thesis, new fabrication techniques are required to allow for the desired precision and uniformity. The fabrication techniques and device designs though are not limited to those introduced here. The concept can be implemented in a versatile set of device designs accommodated **by** various integrative fabrication methodologies. In some cases even conventional contact-based **NEM** switches can be modified to accommodate the tunneling-based switching mechanism through post-fabrication processing utilizing engineering of surfaces and forces.

The molecular layer's mechanical properties and time-dependent mechanical response defines the switching performance. Numerically simulated switching parameters of a simplified two-terminal design represent this dependence in Figure **9-2.** As discussed in Chapter **5,** the mechanical properties of the molecular layers can be engineered at two levels: **1)** inherent properties of the molecules tuned through chemical synthesis, and 2) effective properties of the layer **by** using a combination of different molecular species. Furthermore, the mechanical tunability of the switching gap can be imposed **by** the use of responsive molecules that can undergo conformational changes in response to an external stimulus. Engineering of the molecular layer with the desired mechanics and dynamics though requires an in-depth understanding of these properties which have only been subject of minor studies in the past with limited reports in the literature. These properties are challenging to probe using conventional metrology tools, which are mainly based on scanning probe techniques, as they face

limitations in resolution and accuracy given the small dimensions under consideration. These techniques are also largely inadequate in dynamic device characterization during active operation which would otherwise be useful in elucidating performance principles. Thus, alternative metrology techniques are necessary to study dynamic device operation, nanoscale motion and mechanical properties of the molecular layers to acquire the much needed knowledge-base to engineer molecular films with designer nanomechanics.



Figure **9-2:** Switching parameters including actuation voltage, switching energy and switching time change as a function of the mechanical properties of the molecular spacer.

To concurrently allow performance control, it is desired for the characterization technique to be integrated within the active device design **-** a feature beneficial in particular for devices only few nanometers in size where any structural variations could lead to drastic performance inconsistencies. The methodology should also provide the much needed sensitivity where sub-nm conformation changes can be detected. To

this end, a scheme that we propose involves use of plasmonic properties of metallic nanostructures. **A** metallic nanostructure in close proximity of an underlying metal film can plasmonically couple with a distance-dependent resonance red shift in its peak plasmon wavelength as it approaches the film **[106-108].** The shift in plasmon resonance due to changes in the gap width has high spectral sensitivity. Thus, minute structural changes, even in the  $\tilde{A}$  regime, can be detected through the output optical response **by** monitoring the far-field scattering spectrum. In the molecular nanogaps, changes in the gap size are imposed **by** electrostatically-induced compression of the molecules. As the two electrodes approach each other, a shift in resonance can be detected. Figure **9-3** shows this in two structures composed of a plasmon resonant Au nanoparticle coupled to Au film at two different molecular spacings. Collectively, the foundation for a metrology tool is provided where nanoscale motion and mechanical properties of molecules are characterized. The need for such alternative characterization means emphasizes the importance of developing metrology tools concurrent to processing techniques to push the boundaries of engineering at the limits of the nanoscale.



Figure **9-3:** In a Au-molecule-Au nanogap, the plasmon resonance shifts as the metal-metal gap decreases. Dark-field microscope images of Au nanocubes spaced from an underlying Au film at different distances using molecular layers show the gap-dependent resonance.

### **9.2.2 Engineering at the Limits of the Nanoscale - Beyond Squitches**

Squitches are just an example device platform made feasible **by** the ability to precisely manipulate dimensions, surfaces and forces at the few-nanometer regime. With the need for sub-5 nm and mechanically tunable molecular gaps, the challenges faced in the design of a squitch exemplify limitations broadly expected when engineering at such small dimensions. These are dominated **by** the lack of resolution and precision in defining nanoscale features, and the lack of control over surface interactions and adhesive forces. As discussed in this thesis, conventional fabrication techniques alone are insufficient to provide the unprecedented resolution, control and uniformity essential. When engineering devices with critical dimensions in the few-nanometer regime, such as the sub-5 nm width of the switching gap in a squitch, surface irregularities on the nanometer scale even though conventionally considered small can be detrimental for the device performance. To overcome the challenges, alternative approaches to fabrication are necessary **-** approaches that can be fundamentally new in functionality but also those that complement the conventional techniques to redefine their limits. Multidisciplinary methodologies leveraging the opportunities offered through chemistry and materials science, such as those introduced in this work, provide the much desired sub-nm control in manipulation. In designing these techniques, care should be taken to ensure that sufficient versatility is incorporated to readily accommodate the broad range of unconventional materials and functionalities involved in the evolving field of nanotechnology.

Beyond developing alternative nanoscale processing, this thesis also emphasizes the need for controlling surface adhesive forces to achieve not only fabrication **by** controlled and reversible tunability essential for mechanically-active structures. **By** achieving nanoscale force control, dynamic alteration of nanostructure's physical conformation allows modulation of the structural form and inherent properties beyond the electronic transport. The tunability in operation is dependent on the mechanical performance of the structures involved. Through use of nanomechanics, and **by** controlled and reversible modulation of the related properties, mechanically-active nanoscale devices with applications beyond conventional **NEMS** can emerge, with dimensions **<10** nm being feasible. Such devices are not readily feasible conventionally. However, through use of alternative fabrication and implementing appropriate force control methodologies, the emerging nanoscale mechanically-active architectures can lead not only to the conventional devices of improved performance but those with fundamentally unique operating principles otherwise not attainable at larger dimensions.

The importance of molecules as nanoscale building blocks is also demonstrated in this thesis. Molecules which can precisely be defined in structure, chemical composition and mechanical properties do not only accommodate the fabrication of nanoscale features but help control surface interactions and forces. The versatility provided through chemical synthesis then leads to an extensive library of molecular components that can be integrated into nanoscale devices formed through the alternative fabrication methodologies introduced here. This allows a wide range of molecular device platforms. These devices can help advancements in the field of molecular electronics but also serve to expand device functionalities beyond those dependent on electronic transport.

"There's plenty of room at the bottom", an idea introduced **by** Richard Feynman in **1959.** Decades later, even after tremendous improvements in nanotechnology engineering, we have yet to exploit the full potential of the field and there still remains plenty of room for scientific and technological advancements at the bottom. Currently, a limitation is in the ability to readily gain access to, control and tune such small dimensions. **By** implementing a multidisciplinary approach, techniques necessary to allow precise nanoscale manipulation and control are developed. This results in a wide range of active nanoscale structures with critical dimensions **<10** nm in size and with the potential to uniquely manipulate excitonic, optical, mechanical, electronic, magnetic and/or spintronic properties (Figure 9-4). An example in reference to this thesis is shown in Figure **9-5.** Precise manipulation of these properties leads to unique physical phenomena based on which a platform for the development of next generation nanodevices emerge, forming an ongoing interdisciplinary area of research.



Figure 9-4: Engineering at the limits of the nanoscale, enabled through development of alternative fabrication techniques and **by** achieving control over surfaces and forces, makes feasible unique manipulation of properties including electronic transport, light-matter interactions, mechanics, magnetics, exciton and spin dynamics that can lead to new paradigms of active devices.



Figure **9-5:** Alternative fabrication methodologies are needed to achieve resolution, control and uniformity required to promote engineering of active devices at the limits of the nanoscale. For the example of electromechanically tunable molecular junctions, conventional top-down lithography and thermal evaporation commonly lead to nonuniform molecular junctions with metal penetration through the molecular layer inducing damage (a) while hybrid top-down and bottom-up techniques help formation of well-defined molecular nanogaps with sub-nm precision, control and uniformity **(b).** The molecular junctions are outlined in dotted red lines.

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### **Appendix A**

### **An Overview of NEM Switches**



Table **A. 1:** Representative electrostatic **NEM** switches **-** design and performance.

Litho.: Lithography; EBL: Electron-beam lithography; a-C: Amorphous carbon; **CNT:** Carbon nanotube; Dep.: Deposition; **PFDTES:** Perfluorodecyltriethoxysilane; Actuation: Actuation gap; Contact: Contact gap.

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## **Appendix B**

# **Synthesis of Au Nanoplates and Nanorods**

#### **B.1 Au Nanoplate Synthesis**

The Au nanoplates are sythesized following a modified procedure reported **by** Gu *et* al. [73]. A solution of 0.054 mmol of  $HAuCl_4.4H_2O$  is heated to 65<sup>o</sup>C in a water bath for 20 min. Then, **0.1** M aniline solution in ethylene glycol is added to the heated  $HAuCl<sub>4</sub>$  solution under mild stirring to acquire a 2:1 molar ratio of aniline to Au. This reaction is allowed to proceed for **3** hours without stirring, leading to formation of triangular and hexagonal Au nanoplates with spherical nanoparticles as byproducts. The nanoplates precipitate at the bottom of the vial while the red supernatant mainly contains the spherical particles. The supernatant is gently removed without disturbing the precipitant and replaced with fresh ethanol. The vial is sonicated for about **10** s in pulses to disperse the Au nanoplates in ethanol. Note that a long sonication step will induce damage to the plates. The particles are allowed to settle and the supernatant is replaced with fresh ethanol. This is repeated **3** times to ensure the spherical particles are mainly removed. The cleaning can also be done through several centrifugation cycles instead of precipitation. In an alternative approach, upon addition of aniline,  $900 \mu L$  of 1 mol/L polyvinylpyrrolidone (PVP) in ethylene glycol is added dropwise to the solution under gentle stirring before allowing the growth reaction to

proceed for **3** hours. Addition of PVP leads to formation of smaller nanoplates with a tighter size distribution. Example scanning electron micrographs of the nanoplates are shown in Figure B-1.



Figure B-1: **SEM** images of Au nanoplates synthesized in presence of PVP capping agent.

#### **B.2 Au Nanorod Synthesis**

Au nanorods are synthesized using a seeded growth method reported **by** Wang *et al.* **[105].** In this process seed and growth solutions are prepared as follows.

Au seed solution preparation. A 10 mL solution of 0.25 mM HAuCl<sub>4</sub> and 0.1 M CTAB is prepared in deionized water. Then,  $450 \mu L$  of 0.02 M ice-cold sodium borohydride (NaBH<sub>4</sub>) solution is injected into the CTAB-HAuCl<sub>4</sub> solution while stirring vigorously. Once stirred for **5** min, the solution is then left undisturbed at **270C** for 2 hours resulting in gold nanopartices a few nanometers in size.

Au growth solution preparation. Depending on the length of the nanorods desired, the growth solution will be slightly different. First, **180** mL aqueous solution of 0.1 M CTAB and 0.175 mM HAuCl<sub>4</sub> is prepared, and aliquoted into 3 flasks: flasks **A** and B contain **2.5** mL of solution and **C** holds **25** mL. Then, different amounts of **0.5** M nitric acid as per the amounts outlined in Table B.1 are added to flask **C.** Lastly, 10  $\mu$ L, 10  $\mu$ L, and 100  $\mu$ L of 0.1 M ascorbic acid are added to flasks A, B, and **C** respectively and shaken gently until they become colorless.

**Au nanorod synthesis.** To form the Au nanorods, first 200  $\mu$ L of seed solution

is added to Flask **A** and shaken for **10** seconds. This is followed **by** immediately adding  $200 \mu L$  of this solution to flask B and gently shaking the solution for 10 seconds. Then, a volume of this solution is added to flask **C** as per the amounts summarized in Table B.1 with reference to the desired particle size, and gently shaken for **5** seconds. The solution in flask **C** is then left undisturbed for 12 hours at **270 C.** After incubation, the purple-pink colored supernatant is carefully removed, leaving nanorods precipitated at the bottom of the vial. The rods are re-dispersed in **10** mL of deionized water. To remove excess reagents and nanoparticles of undesired shapes, the solution is cleaned twice **by** centrifuging it at 2000 rpm, removing the supernatant, and re-dispersing the particles in fresh deionized water. Scanning electron micrographs of example nanorods with two different lengths are shown in Figure B-2. It should be noted that the nanorod synthesis contains Au nanoplates and spherical nanoparticles as byproducts. The number of Au nanoparticles of undesired shapes and the rod's size distribution increase for the longer nanorods.



Figure B-2: **SEM** images of Au nanorods of two different lengths with the length modified **by** the reaction conditions according to the procedure outlined in this section.



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### **Appendix C**

# **Theoretical Simulation and Fitting of Experimental Results**

The experimental results were fitted using the Simmons tunneling model while taking into account the switching gap compression **by** the applied voltage. In the analysis performed, several fitting parameters including the tunneling barrier shape  $(\alpha)$ , tunneling barrier height  $(\phi)$ , Hamaker constant  $(A_H)$ , Young's modulus  $(Y)$  and dielectric constant  $(\epsilon_r)$  of the molecular layer are unknown. Thus, to achieve a more cohesive overview of the fit to the experiment, we implemented a Monte Carlo approach. In this technique, values of  $\alpha$ ,  $\phi$ , the initial thickness of molecular layer (L) and the normalized pull-in gap  $(\Delta)$  are randomly selected within a pre-defined range to execute the model and extract  $\epsilon_r$  and Y while optimizing the fit to the experiment. The process is outlined below.

For this analysis, the applied voltage corresponding to an abrupt increase in the measured current is considered to be the pull-in voltage of the device. Utilizing this voltage value, the normalized equation of motion is solved to simulate the expected tunneling gap modulation and the current conduction behavior. The equation of motion (Equation **6.2)** at equilibrium can be written in the normalized form,

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$$
\delta^4 - \delta^3 + \frac{\epsilon_r \epsilon_0 V^2}{2Y L^2} \delta + \frac{A_H}{6\pi Y L^3} = 0
$$
 (C.1)

where L is the thickness of the uncompressed molecular film,  $\delta = g/L$  is the normalized tunneling gap,  $\epsilon_0$  is the permittivity of free space,  $\epsilon_r$  is the dielectric constant of the molecular layer, Y is the material's Young's modulus, and *AH* is the Hamaker constant set to be  $3 \times 10^{-19}$  J in this analysis. Equation C.1 can be rearranged in the form of Equation C.2 with lumped parameters  $K_0$  and  $K_1$ ,

$$
\delta^4 - \delta^3 + K_1 V^2 \delta + K_0 = 0 \tag{C.2}
$$

$$
K_0 = \frac{A_H}{6\pi Y L^3} = 3\Delta^4 - 2\Delta^3, \text{ and } K_1 = \frac{\epsilon_0 \epsilon_r}{2Y L^2} = \frac{2\Delta^3 - \Delta^2 - \frac{2}{\Delta} K_0}{V^2_{Pull-in}}
$$
(C.3)

where  $\Delta$  is the normalized pull-in gap which can range between 2/3, if pull-in is purely electrostatically driven, to 3/4, when pull-in is induced purely **by** van der Waals forces.

Setting  $\Delta$  values within the range 2/3 to 3/4, *L* in the range of 2 to 4 nm and pull-in voltage  $(V_{pull-in})$  extracted from experimental data, Equation C.2 is solved to determine the tunneling gap at each applied voltage. The calculated gap thicknesses are then utilized with  $\alpha$  constrained in the range of 0.4 to 1, and  $\phi$  between 1 eV to **5** eV in the Simmons tunneling model to simulate expected current-voltage characteristics. The corresponding values of  $\epsilon_r$  and *Y* are then calculated based on Equations **C.3.** The model is executed for a large number of randomly selected points and the case leading to the smallest discrepancy between the experiment and theory is determined.

Due to the large number of unknown parameters, determining a unique fit to the experimental data is not feasible. Other sets of numerical parameters can also lead to a good agreement with the measured results. However, amongst these value sets exist parameter combinations that are within physically viable bounds. Constraining the dielectric constants of the molecular layer to within 1 to **5,** a reasonable range for organic materials, the Young's modulus of the material extracted from the three devices presented in Figure 7-4a are deduced to be approximately **5** MPa to 40 MPa with higher density of points in the **5** MPa to **15** MPa regime (Figure **C-1).** The mechanical properties of PEG self-assembled thin-films have not been previously studied, however, reports of bulk **PEG** material properties suggest that the Young's modulus range we deduce here satisfies that of the experimentally measured values for similar material sets. For example, the Young's modulus of **PEG 600** g/mol is reported to be about **5** MPa **[109].** More conclusive analysis of the experimental results require further knowledge of the mechanical properties of the molecular layer, the specifics of the tunneling junctions and the dynamics of the tunneling gap electromechanical modulations.



Figure C-i: The distribution of Young's moduli extracted from modeling the three squitches of Figure 7-4a over 1 million simulation runs with the possible dielectric constant values being constrained to the range 1 to 5. The values of  $\alpha$  and  $\phi$  leading to this distribution are in the range of 0.4 to 1, and 1 to 5 eV, respectively.

134

 $\hat{\mathcal{A}}$  and  $\hat{\mathcal{A}}$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$  ,  $\mathcal{L}^{\text{max}}_{\text{max}}$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$ 

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