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1 Ground Motion in Kuwait from Regional and Local Earthquakes:

2 **Potential Effects on Tall Buildings**

3 Chen Gu¹, Germán A Prieto⁴, Abdullah Al-Enezi³, Farah Al-Jeri³, Jamal Al-

4 Qazweeni³, Hasan Kamal³, Sadi Kuleli¹, Aurélien Mordret¹, Oral Büyüköztürk²,

5 M. Nafi Toksöz¹

⁶ ¹Earth Resources Laboratory, Department of Earth, Atmospheric, and Planetary

- 7 Sciences, Massachusetts Institute of Technology, Cambridge, MA, USA.
- ⁸ ²Laboratory for Infrastructure Science and Sustainability, Department of Civil
- 9 and Environmental Engineering, Massachusetts Institute of Technology,
- 10 Cambridge, MA, USA.
- ³Kuwait Institute for Scientific Research, Kuwait City, Kuwait.
- ⁴Departamento de Geociencias, Facultad de Ciencias, Universidad Nacional de
- 13 Colombia, Bogotá, Colombia

Abstract In recent years, the construction of tall buildings has been increasing in 14 many countries, including Kuwait and other Gulf states. These tall buildings are 15 especially sensitive to ground shaking due to long period seismic surface waves. 16 Although Kuwait is relatively aseismic, it has been affected by large (Mw > 6)17 regional earthquakes in the Zagros Fold-Thrust Belt (ZFTB). Accurate ground 18 motion prediction for large earthquakes is important to assess the seismic hazard to 19 tall buildings. In this study, we first analyze the observed ground motions due to 20 two earthquakes widely felt in Kuwait: the 08/18/2014 Mw 6.2 earthquake, 360 km 21 NNE of Kuwait City, and the 11/12/2017 Mw 7.3 earthquake, 642 km NNE of 22 Kuwait City. The peak spectral displacement periods of the ground motion from 23 the 08/18/2014 Mw 6.2 earthquake matched well with the ambient vibration 24 25 spectra of the tallest building - the Al-Hamra Tower. We calculate the ground motions from potential regional and local earthquakes. We use a velocity model 26 obtained by matching the observed seismograms of the 2014 and 2017 27 earthquakes. We calculate ground motions in Kuwait due to a regional Mw = 7.528 29 earthquake, and a local Mw = 5.0 earthquakes. Our study shows that a significant source of seismic hazard to tall buildings in Kuwait comes from the regional 30 tectonic earthquakes. However, local earthquakes have the potential to generate 31 high peak ground accelerations (~ 98 cm/sec^2) close to their epicenters. 32

35	There has been a rapid increase in the total number and construction of tall
36	buildings worldwide, including in Kuwait. Tall buildings are greatly affected by
37	long trains of low-frequency seismic surface waves from regional earthquakes.
38	Ground motions from regional large earthquakes have frequency contents that may
39	be in the same range as the natural frequencies of some of these tall buildings; and
40	this may have damaging consequences (Shakal et al., 1996; Çelebi and Liu, 1998;
41	Çelebi et al., 2014). The building response to seismic shaking may be obtained by
42	seismic interferometry using ambient vibrations or recorded earthquakes from the
43	building monitoring system (Kohler et al., 2005; Snieder and Şafak, 2006; Prieto et
44	al., 2010; Sun et al., 2017).
45	Previous studies used different methods to calculate the ground motion in a
46	region (Abrahamson and Shedlock, 1997; Olsen et al., 1995; Pitarka et al., 1998;
47	Olsen, 2000; Olsen et al., 2006, 2009; Prieto and Beroza, 2008; Denolle et al.,
48	2013, 2014). The ground motion prediction equation (GMPE) is one method to
49	estimate ground motion intensity based on the observed seismic data and
50	attenuation laws (Abrahamson and Shedlock, 1997; Cauzzi et al., 2014; Danciu et
51	al., 2017, 2018; Şeşetyan et al., 2018). However, in many areas with limited
52	information this approach is primarily directed to acceleration and does not include
53	long period surface waves and the earthquake source rupture process, especially

54 important for large earthquakes; it also ignores the effects of regional variations in crustal structures along the wave propagation path. To make the prediction more 55 physical and realistic, many studies use numerical methods to predict ground 56 motions from a simulated large earthquake (Olsen et al., 1995; Pitarka et al., 1998; 57 Olsen, 2000; Olsen et al., 2006, 2009). The reliability of these ground motion 58 simulations depends heavily on the accuracy of the earthquake source rupture 59 model and the velocity and attenuation models used to propagate seismic waves. In 60 the last decade, studies have started using the ambient seismic field to predict the 61 ground motions from sources around seismic stations (Prieto and Beroza, 2008; 62 Denolle et al., 2013, 2014). This method, although appealing, is limited because it 63 only predicts the ground motions near available seismic stations and thus requires a 64 high-density network. In this report, we use numerically simulated ground motions 65 for both regional and local earthquakes in and near Kuwait. 66 67 Ground motion predictions in Kuwait are possible thanks to well-documented studies on regional tectonics, earthquake source mechanisms and seismic velocity 68 structures in and around Kuwait. These data provide the starting models for the 69 ground motion calculations (Jackson and McKenzie, 1984; Ni and Barazangi, 70 1986; Bou-Rabee, 2000; Gök et al., 2000; Talebian and Jackson, 2004; Pasyanos et 71 al., 2007; Sadek, 2008; Abbas and Al-Sabri, 2015; Kottmeier et al., 2016; Caktı et 72 73 al., 2016). In addition, some previous research has been conducted on long-period

74 ground motions in the Arabian Gulf (Pitarka et al., 2012, 2015). El-Hussain et al. (2012, 2013, 2015) carried out extensive studies of earthquake catalogs for the 75 Zagros Fold-Thrust Belt (ZFTB) and Gulf region as part of their study of seismic 76 hazard in Oman. In the State of Kuwait, hazard studies have been confined mostly 77 to local regions and earthquakes (Bou-Rabee, 2000). 78 In this paper, we calculate ground motions from large regional earthquakes 79 around Kuwait, mostly in the ZFTB and from the largest local earthquakes in 80 Kuwait. To minimize uncertainties associated with crustal and sedimentary basin 81 82 structures, we determine a regional velocity model using data from two regional earthquakes, 08/18/2014 Mw 6.2 and 11/12/2017 Mw 7.3, recorded by seismic 83 stations in Kuwait. To deterministically address seismic hazard from regional 84 85 earthquakes in Kuwait City, we simulate ground motions from a Mw = 7.5 regional earthquake, located 300 km east of Kuwait City. The response spectra (spectral 86 displacement/pseudo-acceleration spectra) are also calculated and compared with 87 the mode vibrations obtained from ambient vibrations spectra of the Al-Hamra 88 89 Tower to assess the seismic hazard to tall buildings in Kuwait City. In addition, the ground motions due to recent local earthquakes are calculated. 90

92	The Kuwait National Seismic Network (KNSN), started in 1997, has been
93	monitoring earthquakes since then (Figure 2b). The KNSN initially consisted of
94	seven three-component short-period stations (AB, MI, QR, RD, RS, SA, UM) and
95	one three-component broadband station (KB). In 2013, the KNSN upgraded their
96	seismic monitoring network by replacing five short-period stations (MI, QR, RD,
97	RS, UM) with broadband stations (RefTek's 151-120 broadband seismometers with
98	a natural period of 120 sec). In this study, we use only the broadband seismic data,
99	since the instrument response files for short-period stations AB and SA are not
100	available. We deconvolve the instrument response from the raw digital data to
101	convert them to ground velocity seismograms. A quarter-cycle cosine taper, with
102	unit response between 0.0125 Hz and 8.0 Hz and zero below 0.01 Hz and above
103	10.0 Hz, was applied during the deconvolution to dampen the response at very low
104	and high frequencies. The displacement and acceleration seismograms are obtained
105	by integrating and differentiating the velocity seismograms, respectively. The
106	spectral displacement, pseudo-velocity spectra and pseudo-acceleration spectra are
107	calculated to estimate the potential effects of earthquakes on civil structures (Gupta,
108	1992).

109 To calculate the ground motion, we used the discrete-wavenumber method110 (Bouchon, 1981; 2003). This method, which converts the continuous wavenumber

111	integration to a summation of discrete wavenumbers, is an accurate and
112	computationally efficient method for generating synthetic seismograms for a 1-D
113	layered velocity model. We could have used a finite difference method for 2-D or
114	3-D velocity models if such models were available (Olsen, 2000; Olsen et al.,
115	2006; Maeda and Furumura, 2013; Almuhaidib and Toksöz, 2014).
116	The 1-D layered velocity model we used is based on the KUW1 model of
117	Pasyanos et al. (2007). The KUW1 model was modified to include the
118	sedimentary layers and fit the observed seismograms from the two large
119	earthquakes in 2014 and 2017. The new model, designated KUW-P or preferred
120	model, is listed in Table 1 and shown in Figure 3. More detailed velocity model
121	improvement procedure is included in the supplemental materials. The large
122	regional earthquakes occur mostly in the Zagros Fold-Thrust Belt (ZFTB) and
123	surrounding areas (Pasyanos et al., 2007; Sadek, 2008). Figure 1 shows significant
124	regional earthquakes around Kuwait in the period 1997-2017. On average, about
125	one earthquake of magnitude 6 or greater occurs in the region per year. In Figure 1,
126	we also show sample seismograms (vertical components) recorded at station MI.
127	Unfortunately, the length of the recordings is limited to 200 seconds and
128	seismograms are truncated. For closer events (e.g. at about 300 km distance), we
129	note the long duration of surface waves.

The observed long-period, long-duration ground motion in Kuwait shows that regional earthquakes are one source of hazards to tall buildings in Kuwait. To demonstrate the impact of regional earthquakes on tall buildings in Kuwait, we analyze seismograms from two large Zagros belt earthquakes that occurred in 2014 and 2017.

The 08/18/2014 Mw 6.2 earthquake, which happened at the Iran-Iraq border, 135 360 km NNE of Kuwait City, was widely felt in Kuwait. We show the three-136 component seismograms of this earthquake from four stations in Kuwait and 137 RAYN in Saudi Arabia in Figure 2. Since this earthquake occurred to the north of 138 Kuwait and from station RYAN in Saudi Arabia, the Z and N component 139 140 seismograms are alike and are with a 90-degree phase shift, mostly Rayleigh waves. The seismograms at the station RD and QR in Kuwait are truncated 141 because the recordings were limited to 200 secs. The E component is primarily 142 Love waves. 143 To calculate synthetic seismograms, we use a 1-D layered velocity model 144

145 (KUW-P). The comparison between the observed and calculated seismograms for

the Mw 6.2 are shown in Figure 4. The figure also includes the spectral

147 displacements. The peak displacement response peaks at periods 3.4 s, 6.9 s, and

148 16.0 s are due to shear, Rayleigh and Love waves, respectively.

We do the similar comparison of synthetic and observed seismograms for the 149 recent 11/12/2017 Mw 7.3 earthquake, 642 km NNE of Kuwait City, at the Iran-150 151 Iraq border. The comparison of the observed and modeled ground displacements and spectral displacements of the Mw 7.3 earthquake at stations KB, QR and RS is 152 shown in Figure 5. The horizontal components of broad band recordings were 153 slightly clipped due to the large magnitude. In spite of this, the match between the 154 observed displacement seismograms and spectral displacements is good, especially 155 for the vertical components least impacted by the clipping. The peak spectral 156 displacements are above 10 s period. The peak ground displacement is about 4 cm 157 and the duration of the ground motions is longer than 300 sec. 158

159 *3. Ground Motions in Kuwait Due to Regional and local Earthquakes*

160 The determination of ground motion requires the maximum credible magnitude, source properties and the most likely locations. For Kuwait, the primary site for a 161 regional earthquake is the segment of the ZFTB, 300 km east of the Kuwait City. 162 163 The maximum credible magnitude is Mw = 7.5, based on the regional earthquake catalog from the KNSN and the work of El-Hussain et al. (2012, 2013), who have 164 165 conducted extensive studies of regional earthquakes in the ZFTB for seismic hazard zonation in the Sultanate of Oman. A Mw = 7.5 earthquake corresponds to 166 a moment of $M_0 = 2.24 \times 10^{27}$ dyne \Box cm. In our calculation, source (fault rupture 167

area) was assumed to be 20 km \times 40 km with the top of the rupture 5 km below the surface. The modeled earthquake is a thrust event with fault plane: strike = 300°, dip = 20°, and rake = 90°. Using the KUW-P velocity model (Table 1), we calculate synthetic seismograms with the epicenter located 300 km east of Kuwait City.

The calculated ground accelerations and displacements in Kuwait are shown in Figure 6. Our calculations show that in Kuwait City, the maximum acceleration is 46 cm/sec² and maximum displacement is 23 cm. The peaks of the displacement response spectra are above 10 s period. The duration of the ground motion is longer than 300 seconds.

178 To demonstrate the effects of ground motions in Kuwait due to regional 179 earthquakes on tall buildings in Kuwait City, we look at the Al-Hamra Tower. The Al-Hamra Tower is a 414 m tall sculpted concrete steel structure. The resonant 180 frequencies of the tower were obtained by finite element modeling and by ambient 181 vibrations measurements. For the ambient vibrations monitoring, Kuwait Institute 182 183 for Scientific Research (KISR) deployed two accelerometers at the top terrace of the Al-Hamra Tower in Kuwait City (two Kinemetrics systems, with 3-component 184 Episensor and Q330 dataloggers). We used ambient vibrations to obtain vibration 185 spectra of the Al-Hamra Tower on day 329 of 2013, shown in Figure 7. 186

187 The peak periods obtained from the two instruments are quite consistent. The periods of the first and second strongest building spectral peaks (7.1 sec and 5.7 188 sec) are close to the calculated peak spectral displacement shown in Figure 4. This 189 overlap between the dominant frequency of ground motions from regional 190 earthquakes, similar to the Mw 6.2 earthquake, and the natural frequencies of the 191 192 Al-Hamra Tower suggests that regional earthquakes will cause strong resonance vibrations in the Al-Hamra Tower and other tall buildings of similar height. The 193 observed ground motions due to the Mw 7.3 earthquake, 642 km from Kuwait City, 194 195 have large (about 4 cm) amplitudes at periods less the 10 sec, but the peak displacement response periods are larger than 10 sec; however, the large peak 196 ground displacements, ~4 cm due to the Mw 7.3 earthquake could still cause large 197 motions at the higher floors of the building. The observed building motions due to 198 the Mw 7.3 earthquake from the first GPS measurements of the Al-Hamra tower 199 (Herring et al., 2018, submitted) indicate a building displacement of ~20 cm at the 200 top of the 414 m tall building. This amount of motion did not cause any damage to 201 202 the Al-Hamra tower.

It is important to mention that the calculated ground motions shown in the figures are for a competent rock layer with shear velocity of 1.4 km/sec. "Soft" sediments with lower shear velocity would further amplify the ground motions. More detailed geotechnical information about the soil properties and sedimentary

structures at the site are needed to better quantify and predict the ground motions
(Bowden and Tsai, 2017). However, this is beyond the scope of this paper.
Local earthquakes in Kuwait occur frequently but tend to have small
magnitudes (Pasyanos, 2007). Since 1997, the KNSN has recorded more than 1000
earthquakes (Mw $<$ 5). Most of the local earthquakes are distributed close to the
oil/gas fields in the northeast and southwest of Kuwait (Figure 8) and are probably
induced by oil production activities (Gu et al., 2017). Two of the largest local
earthquakes - Mw 4.5 on 03/21/2015 and Mw 4.1 on 08/18/2015 - are located near
the southern oil fields and near the northern oil fields, respectively. Such seismicity
related to oil/gas fields has also been observed in North America, Europe and the
Middle East (Sarkar, 2008; Li et al., 2011a, b; Zoback and Gorelick, 2012;
Ellsworth, 2013; Shapiro, 2015; Rubinstein, 2015; Bommer et al., 2017).
The seismograms of the Mw 4.5 earthquake from three selected stations and the
corresponding pseudo acceleration response spectra are shown in Figure 9. The
peak acceleration response periods are in the range from 0.1 s to 1 s (10 Hz to 1
Hz).
So far, no earthquakes of magnitude greater than Mw 4.5 have been recorded in
Kuwait. To determine the ground motions due to the largest local earthquake in
Kuwait, we assumed a maximum credible magnitude Mw 5.0. We generated 3-
compoment synthetics for a local Mw 5.0 earthquake at depth of 3 km (see Figure

10), with a reverse fault and source mechanism (strike = 85° , dip = 20° , and rake = 227 10°) that are consistent with regional stress (Carman, 1996; El-Hussain et al., 2012, 228 229 2015; Abbes and Al-Sabri, 2015; Gu et al., 2017). Figure 10 shows the peak 230 ground acceleration (PGA), representing the root mean square (RMS) of the east and north components. Unlike the large regional earthquakes, the local 231 earthquakes, which excite short period ground motions, would not affect the tall 232 buildings. These earthquakes could generate accelerations (~ 98 cm/sec^2) high 233 enough to affect small structures, built without seismic design codes. Because of 234 the shallow depths, the maximum shaking generates high ground motions but is 235 confined to a small area around these local earthquakes with a steep fall-off. Note 236 237 that the maximum frequencies for the synthetics are 2Hz, this frequency limitation 238 may under-estimate the PGA.

239

4. Conclusions

For tall buildings and large structures in Kuwait, the primary hazard is due to regional earthquakes (e.g., from Zagros Fold-Thrust Belt), especially from surface waves. Our ground motion calculation shows a maximum acceleration of 46 cm/sec² and a maximum displacement of 23 cm in Kuwait City from a virtual Mw 7.5 earthquake in the Zagros region. The presence of near surface "soft" layers increases duration and amplitudes of the surface waves (site amplification) and,

246	hence, increases the hazard. Knowing the detailed shallow structure at the building
247	site would help to better estimate the seismic site specific ground motions.
248	The local earthquakes, most likely induced by oil/gas field activities, can also
249	represent seismic hazard (Gu et al., 2017). They can generate high peak ground
250	accelerations (~ $0.1g$) at periods less than 1 second, close to their epicenters. These
251	local earthquakes may potentially affect local structures.
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Layer	Thickness	V _P	Vs	Density	Q _P	Qs
number	(km)	(km/s)	(km/s)	(g/cm^2)	(s^{-1})	(s^{-1})
1	2.0	2.25	1.40	2.50	40	20
2	2.0	4.76	2.75	2.60	100	50
3	17.0	5.89	3.40	2.70	300	150
4	9.0	6.41	3.70	2.70	300	150
5	11.0	6.95	3.90	2.70	300	150
6	∞	7.80	4.40	2.70	300	150

409 Table 1. Preferred 1-D elastic model (KUW-P) for ground motion calculation^a

⁴¹¹ ^aTo better fit the observed seismograms, we varied the thickness, P-wave velocity 412 (V_P) , and S-wave velocity (V_S) of the first layer of the KUW1 model of Pasyanos 413 et al. (2007).



Figure 1. Significant regional earthquakes since 1997. Seismograms are recorded by the broadband station MI in
Kuwait. Duration of recording is limited to 200 seconds for each event. For events farther than 300 km, surface
waves are not recorded because the recordings are limited to 200 seconds and seismograms are truncated.



419	Figure 2. (a) The 2014/08/18 Mw 6.2 and 2017/11/12 Mw 7.3 earthquakes and
420	seismic stations in a geographic map. The yellow and blue stars show the
421	hypocenters of the Mw 6.2 and Mw 7.3 earthquakes, the yellow circle shows
422	Kuwait City, the red rectangle shows the region covered by Kuwait National
423	Seismic Network (KNSN), the white triangles show station RAYN in Saudi Arabia
424	and station UOSS in UAE and the red and blue beach balls show the source
425	mechanism of the Mw 6.2 and Mw 7.3 earthquake. This earthquake was widely
426	felt in Kuwait. (b) The eight stations of KNSN throughout Kuwait. The five
427	broadband Stations MI, QR, RD, RS and UM were operational when the Mw 6.2
428	earthquake occurred. (c) The observed seismograms of Mw 6.2 earthquake at MI
429	in Kuwait. Since the epicenter is north of the station, the Z and N component
430	seismograms are alike, mostly Rayleigh waves. The E component is primarily
431	Love waves. (d)-(f) The three-component seismograms of Mw 6.2 earthquake at
432	station RS, RD and QR. Because all the stations of KNSN are to the south of the
433	hypocenter of Mw 6.2 earthquake, all the waveforms are very similar showing very
434	consistent Love and Rayleigh waves. The Rayleigh waves of RD and QR are
435	truncated because of the 200 sec recording limits (g) The three-component
436	seismograms of stations RAYN. Because RAYN is almost to the south of the
437	hypocenter of Mw 6.2 earthquake, the seismograms show similar Love and
438	Rayleigh waves as stations of KNSN.



Figure 3. The comparison of the KUW1 and the preferred velocity (KUW-P) models. The red and blue lines show
the P and S velocities of the KUW-P model. The black dashed line denotes the KUW1 P (right) and S (left)
velocity models.



444 **Figure 4.** The observed and modeled ground displacement and spectral displacement of the 08/18/2014 Mw 6.2

- 445 earthquake at MI. (a) The blue lines show the observed seismograms and the red lines show the synthetic
- seismograms using the KUW-P velocity model, (b) The blue lines show the observed seismograms and the dashed
- 447 black lines show the synthetic seismograms using the KUW1 velocity model. (c) The blue lines show the observed

- 448 spectral displacement, the red lines show synthetic spectral displacement using the preferred velocity model, and
- the dashed black lines show the synthetic seismograms using the KUW1 velocity model.



- 451 **Figure 5.** The comparison of the observed (blue) and modeled (red) ground displacement and spectral
- 452 displacement of the 11/12/2017 Mw 7.3 earthquake at stations KB, QR and RS using the KUW-P. (a)-(c) 3-
- 453 Component displacement seismograms. (d)-(f) 3-Component spectral displacements.



- 455 **Figure 6.** Modeled ground motions in Kuwait City (yellow circle) due to magnitude Mw=7.5 thrust earthquake in
- 456 Zagros with strike = 300° , Dip= 20° , and Rake= 90° . (a) The contour of peak ground displacement (PGD; cm) in
- 457 the north-south direction around the epicenter (green star); (b) the 3-component displacement (cm) at Kuwait City;
- 458 (c) the spectral displacement (cm); (d) the contour of peak ground accelerations (PGA; cm/s^2) in the north-south
- 459 direction around the epicenter (green star); (e) the 3-component acceleration (cm/s^2) at Kuwait City; (f) the
- 460 pseudo-acceleration response spectra (cm/s^2).



Figure 7. Amplitude spectra, calculated using ambient vibrations data recorded by two Kinemetrics EpiSensor
instruments, at the top of the Al-Hamra Tower. Average spectra for the day 329 were computed with a 600 s
moving window. The vertical component of station 1017 was not working.



466 **Figure 8.** Local earthquakes (left) during 1997 to 2015 in Kuwait. We show earthquakes with $M \ge 4$ as yellow

stars, $4 > M \ge 3$ as large red circles, and M < 3 in small red circles. The 03/21/2015 Mw 4.5 and 08/18/2015 Mw 4.68 4.1 earthquakes are marked as blue stars.



- 470 **Figure 9.** (a)-(c) 3-Component acceleration seismograms for the Mw 4.5 local event (from Kuwait National
- 471 Seismic Network stations. (d)-(f) Pseudo-acceleration response spectra of 3-Component seismograms for the Mw
- 472 4.5 local event (from Kuwait National Seismic Network stations).



Figure 10. (a) The location of the modeled Mw 5.0 local earthquake (blue star). (b) The contour of peak ground acceleration (PGA; cm/sec²) around the epicenter (blue star). We generate the synthetic acceleration seismograms in the map region for this Mw 5.0 earthquake, a thrust event with fault plane: strike = 85° , dip = 20° , and rake = 10° . The PGAs are calculated from the acceleration seismograms.