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# Fault Detection for Uncertain LPV Systems Using Probabilistic Set-membership Parity Relation

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## Abstract

This paper considers fault detection of uncertain linear parameter varying systems that have polynomial dependence on parametric uncertainties. A conventional set-membership (SM) approach is able to ensure zero false alarm rate (FAR) by using conservative threshold sets, but usually results in a high missed detection rate (MDR) due to equally treating all uncertainty realizations without distinguishing between high and low probability of occurrence. To address this limitation, a probabilistic SM parity relation approach is proposed to exploit probabilistic information on the parametric uncertainties, which results in a reduced MDR by admitting an acceptable FAR. The parity relation is first polynomially parameterized with respect to uncertain parameters. Then, Gaussian mixtures are adopted to efficiently compute uncertainty propagation from stochastic uncertainties to the residual distribution. To achieve an acceptable FAR, a non-convex confidence set of residuals – represented by a union of ellipsoids – is determined for the consistency test. The effectiveness of the proposed approach is illustrated using a continuous stirred tank reactor example including performance comparisons with a deterministic zonotope-based method.

*Keywords:* Fault detection, linear parameter varying systems, probabilistic parametric uncertainties, parity relation, set membership approach.

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## 1. Introduction

The inherent nonlinearity of practical safety-critical systems has motivated recent research interest in nonlinear fault detection (FD) [1, 2, 3]. Linear parameter varying (LPV) models effectively represent a wide range of nonlinear systems while preserving a (quasi-)linear structure, which has motivated their use in the design of nonlinear FD methods [1, 4]. As in other FD methods, a key challenge for an LPV FD algorithm is to ensure robustness to inevitable model uncertainties to achieve a low false alarm rate (FAR), while simultaneously obtaining a low missed detection rate (MDR).

The existing robust LPV methods can be classified into two main categories. The first category relies on an LPV observer or a parity relation to generate residuals or fault estimates, and uses a norm-based threshold to indicate the occurrence of faults [5, 6, 7, 8, 9, 10, 11]. On the other hand, the second category of robust methods, known as set membership (SM), performs a more flexible set-based consistency test via a set-valued observer [12, 13, 14] or an SM parity relation [15, 16]. For tractable online computation in set-theoretic uncertainty propagation, convex outer approximations using intervals, ellipsoids, or zonotopes are often adopted, which compromises the MDR. A parity relation is a receding horizon input-output (I/O) model decoupled from the unknown initial states by using a so-called parity matrix or vector [11, 17]. To effectively address multiplicative uncertainties, the parity relation approach has been revised in the SM framework [15, 16]. The derived SM parity relation is parameterized by uncertain parameters, in contrast to a single parity relation as used in [11, 17].

The above robust approaches are developed in the deterministic setting, and aim at ensuring zero false alarms even in the worst case. The resulting MDR is high with such methods, because conservative detection thresholds or sets must be adopted to account for the worst case that rarely occurs. In order to reduce this conservatism, probabilistic robust approaches have been recently proposed that exploit the richer information represented by probability distribution of model uncertainties. One line of research formulates a probabilistic relaxation for the norm-based threshold computation [18, 19, 20, 21], while the other line employs probabilistic set approximation for the set-based consistency test [22]. The latter approach achieves better FD performance by adopting less conservative polynomial level sets, but requires solving chance-constrained optimization online via a computationally expensive randomized algorithm. To address the presence of both bounded deterministic parametric uncertainties and additive Gaussian noises, a zonotopic Kalman filter is proposed in [23, 24] by merging SM and probabilistic paradigms.

This paper investigates the FD problem for uncertain LPV systems with polynomial dependence on probabilistic parametric uncertainties. A probabilistic SM parity relation approach is proposed to reduce the MDR while ensuring an acceptable FAR. The polynomially parametrized parity relation is first derived, and then restructured as a linear time-varying (LTV) transformation of an uncertainty vector whose elements are polynomials of uncertain parameters and

stochastic noises. Considering non-Gaussian uncertainties, Gaussian mixtures (GMs) are adopted to efficiently compute stochastic uncertainty propagation from the above uncertainty vector to the residual distribution. The confidence set of the residual GM distribution is used in the consistency test to achieve an acceptable FAR. Such a confidence set is represented by a union of ellipsoids, which is a less conservative approximation of a non-convex region than the convex approximation used in [15, 16]. The proposed approach is a nontrivial extension of the authors' previous work for uncertain linear time-invariant systems in [25, 26] to LPV systems including both parametric uncertainties and imprecise scheduling parameters.

The paper is organized as follows. Sections 2 and 3 state the probabilistic FD problem and the main idea, respectively. Section 4 constructs a polynomial parity matrix. The residual uncertainty quantification for the consistency test is discussed in Section 5. The simulation results using a continuous stirred tank reactor example are presented in Section 6, and the main conclusions are drawn in Section 7.

## 2. Problem statement

Consider the fault-free uncertain discrete-time LPV system

$$\begin{aligned} x_{k+1} &= A(\tilde{\theta}, \tilde{\rho}_k)x_k + B(\tilde{\theta}, \tilde{\rho}_k)u_k + \tilde{w}_k, \\ y_k &= C(\tilde{\theta}, \tilde{\rho}_k)x_k + D(\tilde{\theta}, \tilde{\rho}_k)u_k + \tilde{v}_k, \end{aligned} \quad (1)$$

where  $u_k \in \mathbb{R}^{n_u}$ ,  $y_k \in \mathbb{R}^{n_y}$ ,  $x_k \in \mathbb{R}^{n_x}$ ,  $\tilde{w}_k$ , and  $\tilde{v}_k$  are the system input, measured output, state, process noise, and measurement noise, respectively. The system parameters  $\tilde{\theta} \in \mathbb{R}^{n_\theta}$  are unknown. The vector  $\tilde{\rho}_k \in \mathbb{R}^{n_\rho}$  contains the scheduling parameters. The measurement of  $\tilde{\rho}_k$  is denoted as

$$\rho_k = \tilde{\rho}_k + \tilde{\eta}_k, \quad (2)$$

which is corrupted by a measurement noise  $\tilde{\eta}_k$ .

**Assumption 1.** All the system matrices  $A(\tilde{\theta}, \tilde{\rho}_k)$ ,  $B(\tilde{\theta}, \tilde{\rho}_k)$ ,  $C(\tilde{\theta}, \tilde{\rho}_k)$  and  $D(\tilde{\theta}, \tilde{\rho}_k)$  in (1) have polynomial dependence on both  $\tilde{\theta}$  and  $\tilde{\rho}_k$ .

**Assumption 2.** The uncertain parameter vector  $\tilde{\theta}$  is time invariant (TI), belongs to a bounded set  $\Theta$ , and is described by TI random variables with known probability density function (PDF)  $f_\theta$ .

**Assumption 3.** Noises  $\tilde{w}_k$ ,  $\tilde{v}_k$  in (1) and  $\tilde{\eta}_k$  in (2) are of zero-mean white nature with known PDFs  $f_w$ ,  $f_v$ , and  $f_\eta$ , respectively; and  $\tilde{\theta}$ ,  $\tilde{w}$ ,  $\tilde{v}$  and  $\tilde{\eta}$  are mutually independent.

Assumption 1 is not restrictive because any nonpolynomial nonlinear dependence on  $\tilde{\theta}$  and  $\tilde{\rho}_k$  can be adequately approximated by polynomials or piecewise polynomials [27]. The approximation error can be made arbitrarily small as long

75 as the approximating polynomial has a sufficiently large degree [28]. Therefore, the approximation error is assumed negligible in this paper. Otherwise, another uncertain variable should be introduced to fully account for this approximation error, which often leads to an increased MDR.

In Assumption 2, time invariance of  $\tilde{\theta}$  can be justified because physical parameters generally have slow variations, and are usually considered as TI over 80 a finite-time horizon [16]. The PDF of  $\tilde{\theta}$  can be obtained by either offline identification from data [29, 30, 31], or *a priori* knowledge that specifies the relative importance of different points in the uncertainty region  $\Theta$ . The PDFs of  $\tilde{\theta}$ ,  $\tilde{w}$ ,  $\tilde{v}$  and  $\tilde{\eta}$  can be non-Gaussian, which is not restricted by Assumption 3.

For the sake of brevity, let  $A(\tilde{\theta}, \tilde{\rho}_k)$ ,  $B(\tilde{\theta}, \tilde{\rho}_k)$ ,  $C(\tilde{\theta}, \tilde{\rho}_k)$  and  $D(\tilde{\theta}, \tilde{\rho}_k)$  be denoted by  $A_k$ ,  $B_k$ ,  $C_k$ , and  $D_k$ , respectively. From (1) and (2), the stacked system equations over a time window  $[k-h+1, k]$  of length  $h$  can be expressed as

$$\mathbf{y}_{k,h} = \mathcal{O}(\tilde{\xi}_k)x_{k-h+1} + \mathcal{H}_u(\tilde{\xi}_k)\mathbf{u}_{k,h} + \mathcal{H}_w(\tilde{\xi}_k)\tilde{\mathbf{w}}_{k,h} + \tilde{\mathbf{v}}_{k,h}, \quad (3a)$$

$$\boldsymbol{\rho}_{k,h} = \tilde{\boldsymbol{\rho}}_{k,h} + \tilde{\boldsymbol{\eta}}_{k,h}, \quad (3b)$$

where

$$\mathbf{y}_{k,h} = \begin{bmatrix} y_{k-h+1} \\ y_{k-h+2} \\ \vdots \\ y_k \end{bmatrix}, \quad \tilde{\xi}_k = \begin{bmatrix} \tilde{\theta} \\ \tilde{\boldsymbol{\rho}}_{k,h} \end{bmatrix}, \quad \mathcal{O}(\tilde{\xi}_k) = \begin{bmatrix} C_{k-h+1} \\ C_{k-h+2}A_{k-h+1} \\ \vdots \\ C_k \prod_{i=1}^{h-1} A_{k-i} \end{bmatrix}, \quad (4)$$

$$\mathcal{H}_u(\tilde{\xi}_k) = \begin{bmatrix} D_{k-h+1} & 0 & \cdots & 0 \\ C_{k-h+2}B_{k-h+1} & D_{k-h+2} & \ddots & \vdots \\ \vdots & \vdots & \ddots & 0 \\ C_k \prod_{i=1}^{h-2} A_{k-i}B_{k-h+1} & C_k \prod_{i=1}^{h-3} A_{k-i}B_{k-h+2} & \cdots & D_k \end{bmatrix},$$

85  $\mathbf{u}_{k,h}$ ,  $\tilde{\boldsymbol{\rho}}_{k,h}$ ,  $\tilde{\mathbf{w}}_{k,h}$ ,  $\tilde{\mathbf{v}}_{k,h}$ , and  $\tilde{\boldsymbol{\eta}}_{k,h}$  are defined similarly to  $\mathbf{y}_{k,h}$ , and  $\mathcal{H}_w(\tilde{\xi}_k)$  is defined similarly to  $\mathcal{H}_u(\tilde{\xi}_k)$ .

In an SM FD method, the detection of faults relies on invalidating a fault-free model [14, 23]. Specifically, a fault alarm is reported as long as the measured output  $y_k$  cannot be generated by the fault-free model (1) and its associated 90 uncertainty descriptions, given the system input  $u_k$  and the measured scheduling parameter  $\rho_k$ . Such an invalidation approach does not require any fault model, thus is not restricted to any particular fault type [14, 23]. The conventional deterministic SM approach adopts the unknown-but-bounded uncertainty description [14, 23]. In contrast, this paper aims at exploiting the probabilistic information of uncertainties to further reduce the MDR by admitting an 95 acceptable FAR.

### 3. Overview of probabilistic SM parity relation approach

The main idea of the proposed approach is explained in this section.

According to (3), the observability matrix  $\mathcal{O}(\tilde{\xi}_k)$  polynomially depends on  $\tilde{\xi}_k$  which itself includes the unknown parameter  $\tilde{\theta}$  and the scheduling parameters  $\tilde{\rho}_{k,h}$ . Therefore,  $\mathcal{O}(\tilde{\xi}_k)$  is unknown and time-varying, which does not allow the use of a conventional time-invariant parity matrix to decouple the unknown initial state  $x_{k-h+1}$  in (3a). Alternatively, a polynomial parity matrix  $V(\tilde{\xi}_k)$  is first constructed in Section 4 to satisfy

$$V(\tilde{\xi}_k)\mathcal{O}(\tilde{\xi}_k) = 0 \text{ for any } \tilde{\xi}_k, \quad (5)$$

so that the premultiplication of (3) by  $V(\tilde{\xi}_k)$  decouples the unknown initial term  $\mathcal{O}(\tilde{\xi}_k)x_{k-h+1}$  and generates the parity relation

$$V(\tilde{\xi}_k) \left( \mathbf{y}_{k,h} - \mathcal{H}_u(\tilde{\xi}_k)\mathbf{u}_{k,h} - \mathcal{H}_w(\tilde{\xi}_k)\tilde{\mathbf{w}}_{k,h} - \tilde{\mathbf{v}}_{k,h} \right) = 0. \quad (6)$$

In the parity relation (6), the true parameter  $\tilde{\xi}_k$  and noises  $\tilde{\mathbf{w}}_{k,h}$ ,  $\tilde{\mathbf{v}}_{k,h}$ , and  $\tilde{\boldsymbol{\eta}}_{k,h}$  are unavailable. Let  $\theta$ ,  $\mathbf{w}_{k,h}$ ,  $\mathbf{v}_{k,h}$ , and  $\boldsymbol{\eta}_{k,h}$  represent random realizations of  $\tilde{\theta}$ ,  $\tilde{\mathbf{w}}_{k,h}$ ,  $\tilde{\mathbf{v}}_{k,h}$ , and  $\tilde{\boldsymbol{\eta}}_{k,h}$ , respectively. Then, by defining the parameter vector

$$\boldsymbol{\xi}_k = [\theta^\top \quad (\boldsymbol{\rho}_{k,h} - \boldsymbol{\eta}_{k,h})^\top]^\top \quad (7)$$

according to (3b), a residual can be expressed as a function of the considered uncertainties, i.e.,

$$\begin{aligned} \mathbf{r}_k(\boldsymbol{\xi}, \mathbf{w}, \mathbf{v}) &= V(\boldsymbol{\xi}_k)(\mathbf{y}_{k,h} - \mathcal{H}_u(\boldsymbol{\xi}_k)\mathbf{u}_{k,h} - \mathcal{H}_w(\boldsymbol{\xi}_k)\mathbf{w}_{k,h} - \mathbf{v}_{k,h}) \\ &= \mathcal{G}(\boldsymbol{\xi}_k)\mathbf{z}_{k,h} - \mathcal{J}(\boldsymbol{\xi}_k)\mathbf{n}_{k,h}, \end{aligned} \quad (8)$$

with

$$\begin{aligned} \mathcal{G}(\boldsymbol{\xi}_k) &= [V(\boldsymbol{\xi}_k) \quad -V(\boldsymbol{\xi}_k)\mathcal{H}_u(\boldsymbol{\xi}_k)], \quad \mathbf{z}_{k,h} = [\mathbf{y}_{k,h}^\top \quad \mathbf{u}_{k,h}^\top]^\top, \\ \mathcal{J}(\boldsymbol{\xi}_k) &= [V(\boldsymbol{\xi}_k) \quad V(\boldsymbol{\xi}_k)\mathcal{H}_w(\boldsymbol{\xi}_k)], \quad \mathbf{n}_{k,h} = [\mathbf{v}_{k,h}^\top \quad \mathbf{w}_{k,h}^\top]^\top. \end{aligned} \quad (9)$$

Note that the residual  $\mathbf{r}_k$  is random, since it is computed by using random samples of uncertain variables  $\boldsymbol{\xi}$ ,  $\mathbf{w}$ ,  $\mathbf{v}$ . Accordingly, a confidence set  $\Delta_k$  with a confidence level  $\gamma$  for  $\mathbf{r}_k$ , i.e.,

$$\Pr\{\mathbf{r}_k(\boldsymbol{\xi}, \mathbf{w}, \mathbf{v}) \in \Delta_k | \theta \sim f_\theta, w_k \sim f_w, v_k \sim f_v, \eta_k \sim f_\eta\} \geq \gamma, \quad (10)$$

is constructed in Section 5 by exploiting the distributional information of considered uncertainties, where  $\Pr\{\cdot\}$  represents the probability of the associated event.

With the above derivations, the following FD logic is adopted:

$$\begin{cases} \mathbf{0} \in \Delta_k & \Rightarrow \text{the monitored system is fault-free} \\ \mathbf{0} \notin \Delta_k & \Rightarrow \text{the monitored system is faulty.} \end{cases} \quad (11)$$

Note that  $\mathbf{0}$  in (11) is a zero vector whose dimension is the same as  $\mathbf{r}_k$ .

Although this FD logic seems similar to the deterministic SM approaches in [15, 16], there exists a significant difference: the deterministic SM approaches rely on an overbounding convex set to ensure zero FAR, while the confidence set  $\Delta_k$  used in (11) is obtained via stochastic uncertainty propagation and could be non-convex as discussed in Section 5.

#### 4. Computing a polynomial parity matrix

This section presents a method for computing the polynomial parity matrix  $V(\tilde{\xi}_k)$ , and discusses how the non-uniqueness of  $V(\tilde{\xi}_k)$  affects FD performance.

For the ease of understanding, first we consider the case with only a scalar  $\tilde{\theta}$  and no scheduling parameter  $\tilde{\rho}_k$ . In this case, the system matrices are  $A(\tilde{\theta})$  and  $C(\tilde{\theta})$ , and the corresponding observability matrix becomes  $\mathcal{O}(\tilde{\theta})$ . Let the degrees of the polynomial matrices  $A(\tilde{\theta})$  and  $C(\tilde{\theta})$  be denoted by  $d_A$  and  $d_C$ , respectively. Then the observability matrix  $\mathcal{O}(\tilde{\theta})$  can be expressed as

$$\mathcal{O}(\tilde{\theta}) = \sum_{j=0}^{d_O} O_j \tilde{\theta}^j$$

with degree

$$d_O = d_C + (h - 1)d_A. \quad (12)$$

When a polynomial parity matrix

$$V(\tilde{\theta}) = \sum_{i=0}^{d_V} V_i \tilde{\theta}^i \quad (13)$$

is selected with degree  $d_V$ , (5) becomes

$$V(\tilde{\theta})\mathcal{O}(\tilde{\theta}) = \left( \sum_{i=0}^{d_V} V_i \tilde{\theta}^i \right) \left( \sum_{j=0}^{d_O} O_j \tilde{\theta}^j \right) = 0. \quad (14)$$

The multiplication on the left-hand side of (14) is a polynomial with degree  $d_V + d_O$ , whose monomial with degree  $i$  is  $\sum_{j=0}^i V_j O_{i-j} \tilde{\theta}^i$ . All of its monomial coefficients need to be zero, i.e.,  $\sum_{j=0}^i V_j O_{i-j} = 0$ , so that (14) holds for any  $\tilde{\theta}$ .

Therefore, (14) is equivalent to

$$\mathcal{V}\mathcal{M} = 0, \text{ with} \quad (15a)$$

$$\mathcal{V} = [V_0 \quad V_1 \quad \cdots \quad V_{d_V}], \quad (15b)$$

$$\mathcal{M} = \begin{bmatrix} O_0 & O_1 & \cdots & O_{d_O} & 0 & \cdots & \cdots & 0 & \cdots & 0 \\ 0 & O_0 & \cdots & O_{d_O-1} & O_{d_O} & 0 & \cdots & 0 & \cdots & 0 \\ \vdots & \ddots & \ddots & \vdots & \vdots & \ddots & \ddots & \vdots & \ddots & \vdots \\ 0 & \cdots & 0 & O_0 & O_1 & \cdots & O_{d_O} & 0 & \cdots & 0 \\ 0 & \cdots & 0 & 0 & O_0 & \cdots & O_{d_O-1} & O_{d_O} & \cdots & 0 \\ \vdots & \ddots & \vdots & \vdots & \ddots & \ddots & \vdots & \vdots & \ddots & \vdots \\ 0 & \cdots & 0 & 0 & \cdots & 0 & O_0 & O_1 & \cdots & O_{d_O} \end{bmatrix} = 0 \text{ if } d_V \geq d_O, \quad (15c)$$

$$\mathcal{M} = \begin{bmatrix} O_0 & O_1 & \cdots & O_{d_V-1} & O_{d_V} & \cdots & O_{d_O} & 0 & \cdots & \cdots & 0 \\ 0 & O_0 & O_1 & \cdots & O_{d_V-1} & \cdots & O_{d_O-1} & O_{d_O} & 0 & \cdots & 0 \\ \vdots & \ddots & \ddots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & \cdots & 0 & O_0 & O_1 & \cdots & O_{d_O-d_V+1} & O_{d_O-d_V+2} & \cdots & O_{d_O} & 0 \\ 0 & \cdots & \cdots & 0 & O_0 & \cdots & O_{d_O-d_V} & O_{d_O-d_V+1} & \cdots & O_{d_O-1} & O_{d_O} \end{bmatrix} = 0 \text{ if } d_V < d_O. \quad (15d)$$

The multiplication between  $\mathcal{V}$  and the  $i^{\text{th}}$  block-column of  $\mathcal{M}$  corresponds to the coefficient of the monomial basis with degree  $i - 1$  in  $V(\tilde{\theta})\mathcal{O}(\tilde{\theta})$ . Hence, the size of  $\mathcal{M}$  is  $m_{\mathcal{M}} \times n_{\mathcal{M}}$ , where  $m_{\mathcal{M}} = (d_V + 1)hn_y$ , and  $n_{\mathcal{M}} = (d_V + d_O + 1)n_x$  is determined by the degree of  $V(\tilde{\theta})\mathcal{O}(\tilde{\theta})$ . The solution  $\mathcal{V}$  to (15a) can be expressed by (19) that will be explained later on. The block-columns  $\{V_i\}$  of  $\mathcal{V}$  are then used to construct the polynomial parity matrix  $V(\tilde{\theta})$  according to (13).

Next, we proceed with the general case that includes both multi-dimensional  $\tilde{\theta}$  and scheduling parameters  $\tilde{\rho}_{k,h}$ . In this case, the dimension of  $\tilde{\xi}_k$  defined in (4) is  $n_{\xi} = n_{\theta} + hn_{\rho}$ . Let  $\tilde{\xi}_{k,i}$  denote the  $i^{\text{th}}$  element of  $\tilde{\xi}_k$ , and  $\tilde{\xi}_k^{\varpi}$  a monomial  $\tilde{\xi}_{k,1}^{\varpi_1} \tilde{\xi}_{k,2}^{\varpi_2} \cdots \tilde{\xi}_{k,n_{\xi}}^{\varpi_{n_{\xi}}}$ , where  $\varpi_i$  is a nonnegative integer, and  $\varpi = [\varpi_1^{\top} \quad \varpi_2^{\top} \quad \cdots \quad \varpi_{n_{\xi}}^{\top}]^{\top}$  is the multivariate monomial exponent. Then, any polynomial matrix  $M(\tilde{\xi}_k)$  can be expressed as

$$M(\tilde{\xi}_k) = \sum_{\varpi \in \pi(M(\tilde{\xi}_k))} M_{[\varpi]} \tilde{\xi}_k^{\varpi},$$

where  $M_{[\varpi]}$  is the coefficient matrix for the monomial  $\tilde{\xi}_k^{\varpi}$ , and  $\pi(M(\tilde{\xi}_k))$  represents the set of all monomial exponents included in  $M(\tilde{\xi}_k)$ . The degree of a monomial  $\tilde{\xi}_k^{\varpi}$  is defined by  $\sum_{i=1}^{n_{\xi}} \varpi_i$ , while the degree of a polynomial matrix  $M(\tilde{\xi}_k)$  is determined by the maximal degree of the included monomials, i.e.,  $\max_{\varpi \in \pi(M(\tilde{\xi}_k))} \sum_{i=1}^{n_{\xi}} \varpi_i$ . If the degree of  $M(\tilde{\xi}_k)$  is  $d_M$ , the maximum number of monomial terms in  $M(\tilde{\xi}_k)$  is

$$g(d_M, n_{\xi}) = \frac{(d_M + n_{\xi})!}{d_M! n_{\xi}!}. \quad (16)$$



Based on these definitions, (5) can be expressed as

$$\left( \sum_{\varpi \in \pi(V(\tilde{\xi}_k))} V_{[\varpi]} \tilde{\xi}_k^{\varpi} \right) \left( \sum_{\varphi \in \pi(\mathcal{O}(\tilde{\xi}_k))} O_{[\varphi]} \tilde{\xi}_k^{\varphi} \right) = 0. \quad (17)$$

Since each monomial coefficient matrix on the left-hand side of (5) is null, (17) is equivalent to

$$\sum_{\varpi \in \pi(V(\tilde{\xi}_k))} V_{[\varpi]} \mathcal{O}_{[\sigma-\varpi]} = 0, \quad \sigma \in \pi(V(\tilde{\xi}_k)\mathcal{O}(\tilde{\xi}_k)).$$

From this equation,  $\mathcal{VM} = 0$  can be constructed similarly to (15) as follows. Each block in  $\mathcal{V}$  is  $V_{[\varpi]}$ . Each block-column of  $\mathcal{M}$  includes the coefficients

$$\left\{ \mathcal{O}_{[\sigma-\varpi]}, \varpi \in \pi(V(\tilde{\xi}_k)) \right\}$$

of monomials  $\left\{ \tilde{\xi}_k^{\sigma-\varpi} \right\}$  in  $\mathcal{O}(\tilde{\xi}_k)$ , and its multiplication with  $\mathcal{V}$  produces the monomial coefficient of  $\tilde{\xi}_k^{\sigma}$  in  $V(\tilde{\xi}_k)\mathcal{O}(\tilde{\xi}_k)$ . The size of  $\mathcal{M}$  is  $m_{\mathcal{M}} \times n_{\mathcal{M}}$ , with  $m_{\mathcal{M}} = g(d_V, n_{\xi})hn_y$  and  $n_{\mathcal{M}} = g(d_V + d_O, n_{\xi})n_x$ .

The existence of a solution to  $\mathcal{VM} = 0$  is equivalent to the existence of a left nullspace of  $\mathcal{M}$ . It can be guaranteed by a sufficient condition  $g(d_V, n_{\xi})hn_y > g(d_V + d_O, n_{\xi})n_x$ , i.e., the matrix  $\mathcal{M}$  has more rows than columns. Using (16), this sufficient condition can be rewritten as

$$\prod_{i=1}^{n_{\xi}} \left( 1 - \frac{d_O}{d_V + d_O + i} \right) > \frac{n_x}{hn_y}. \quad (18)$$

120 Since the left-hand side of (18) is smaller than 1, the inequality  $hn_y > n_x$  is a necessary condition for (18) to hold. For a fixed horizon length  $h$ , the existence of a polynomial parity matrix  $V(\tilde{\xi}_k)$  is guaranteed by selecting a sufficiently high degree  $d_V$ . Increasing either  $h$  or  $d_V$  results in higher computational cost for both offline design and online residual evaluation. Therefore, the shortest  
125 horizon length  $h$  and the lowest degree  $d_V$  are sought by iteratively increasing either  $h$  or  $d_V$  by one until a solution to  $\mathcal{VM} = 0$  is found.

Let  $r_{\mathcal{M}}$  represent the rank of  $\mathcal{M}$ . Let  $\mathcal{M}_{\perp} \in \mathbb{R}^{m_{\mathcal{M}} \times (m_{\mathcal{M}} - r_{\mathcal{M}})}$  denote the orthogonal basis of the left nullspace of  $\mathcal{M}$ , i.e.,  $\mathcal{M}_{\perp}^{\top} \mathcal{M} = 0$  and  $\mathcal{M}_{\perp}^{\top} \mathcal{M}_{\perp} = I$ , and it can be computed via singular value decomposition [32]. Then, the solution to  $\mathcal{VM} = 0$  is expressed as

$$\mathcal{V} = \Omega \mathcal{M}_{\perp}^{\top}, \quad (19)$$

where  $\Omega \in \mathbb{R}^{n_r \times (m_{\mathcal{M}} - r_{\mathcal{M}})}$  has to be determined. Without loss of generality,  $\Omega$  is assumed to be full row rank. As will be presented by the following propositions, any nonsingular matrix  $\Omega$  results in the same FAR and FDR, and gives a better  
130 FD performance than using a column-rank deficient matrix  $\Omega$ .

Define  $\mathcal{V}^* = \mathcal{M}_\perp^\top$ , then the corresponding polynomial parity matrix and generated residual are denoted as  $V^*(\boldsymbol{\xi})$  and  $\mathbf{r}_k^*$ , respectively, where  $\mathbf{r}_k^*$  is defined as in (8) by replacing  $V(\boldsymbol{\xi}_k)$  with  $V^*(\boldsymbol{\xi}_k)$ . Define a closed confidence set  $\Delta_k^*$  for  $\mathbf{r}_k^*$  by following (10). Assume that this closed set  $\Delta_k^*$  is described by  $\Delta_k^* = \{\mathbf{r}_k^* | \mu(\mathbf{r}_k^*) \leq 0\}$ , where  $\mu : \mathbb{R}^{n_r} \mapsto \mathbb{R}^q$  is a continuous vector-valued function.

**Proposition 1.** *If  $\Omega$  is nonsingular, the achieved FAR and MDR do not depend on the selection of  $\Omega$ .*

*Proof.* With the chosen  $\Omega$ , we have  $\mathcal{V} = \Omega\mathcal{V}^*$ ,  $V(\boldsymbol{\xi}_k) = \Omega V^*(\boldsymbol{\xi}_k)$ , and  $\mathbf{r}_k = \Omega\mathbf{r}_k^*$  according to (8) and (19). Therefore, the confidence sets  $\Delta_k^* = \{\mathbf{r}_k^* | \mu(\mathbf{r}_k^*) \leq 0\}$  and  $\Delta_k = \{\mathbf{r}_k | \mu(\Omega^{-1}\mathbf{r}_k) \leq 0\}$  give the same FAR and MDR, because  $\mu(\mathbf{r}_k^*) = \mu(\Omega^{-1}\mathbf{r}_k)$  holds in any case.  $\square$

**Proposition 2.** *If  $\Omega$  is column-rank deficient, the resulting parity relation achieves a lower FAR but a higher MDR, compared to the selection  $\mathcal{V}^* = \mathcal{M}_\perp^\top$ .*

*Proof.* According to (8), the residual  $\mathbf{r}_k^*(\boldsymbol{\xi}, \mathbf{w}, \mathbf{v})$  generated by using  $\mathcal{V}^*$  can be rewritten as

$$\mathbf{r}_k^*(\boldsymbol{\xi}, \mathbf{w}, \mathbf{v}) = \bar{\mathbf{r}}_k^*(\boldsymbol{\xi}, \mathbf{w}, \mathbf{v}) + V^*(\boldsymbol{\xi}_k)\mathbf{f}_k, \quad (20)$$

where  $\bar{\mathbf{r}}_k^*$  is the fault-free part, and  $\mathbf{f}_k$  describes the contribution of latent faults. When using  $\mathcal{V} = \Omega\mathcal{V}^*$  to generate a residual  $\mathbf{r}_k(\boldsymbol{\xi}, \mathbf{w}, \mathbf{v})$ ,  $\mathbf{r}_k = \Omega\mathbf{r}_k^*$  holds. Then it follows from (20) that  $\mathbf{r}_k$  can be similarly decomposed as  $\mathbf{r}_k = \Omega\bar{\mathbf{r}}_k^* + \Omega V^*(\boldsymbol{\xi}_k)\mathbf{f}_k$ . Since  $\Omega$  is column-rank deficient, there might exist  $\boldsymbol{\xi}_k$  such that the set of undetectable faults  $\{\mathbf{f}_k | \Omega V^*(\boldsymbol{\xi}_k)\mathbf{f}_k = 0\}$  is not null, thus increasing the MDR achieved by using  $\mathcal{V} = \Omega\mathcal{V}^*$ . For the same reason, it is possible in the fault-free case that a residual  $\bar{\mathbf{r}}_k^*$  giving a false alarm lies in the null space of  $\Omega$ , which reduces the FAR achieved by  $\mathbf{r}_k$ .  $\square$

**Remark 1.** *The Cayley-Hamilton theorem was exploited in [33] to construct a polynomial parity vector for linear time-invariant systems with parametric uncertainties, which is not applicable for the uncertain LPV systems considered in this paper.*

**Remark 2.** *How the FD performance of the proposed approach depends on the horizon length  $h$  and the degree  $d_V$  is illustrated in Section 6.3 via Monte Carlo simulations. It can be observed that (i) the MDR becomes higher when  $d_V$  is larger than its minimal value, and (ii) the MDR decreases as  $h$  increases. A rigorous proof for these observations is left to future work.*

**Remark 3.** *For the iteration from  $h$  to  $h+1$  or from  $d_V$  to  $d_V+1$ , there exist methods to incrementally update  $\mathcal{M}_\perp$ , without computing it from scratch. As  $h$  or  $d_V$  increases by one, additional rows and columns are inserted into  $\mathcal{M}$ , according to (15c), (15d), and (17). This feature allows incrementally updating the SVD of  $\mathcal{M}$ , see [34] as an example.*

## 5. Computing the residual distribution and its confidence set

Since the FD logic (11) requires the confidence set  $\Delta_k$  defined in (10), the residual distribution has to be quantified. In this section, the residual (8) is first structured as an LTV transformation of an uncertainty vector. Then, the residual distribution and its confidence set  $\Delta_k$  defined in (10) are computed using a GM approach.

### 5.1. Residual in an LTV structure

According to Assumption 1,  $\mathcal{G}(\boldsymbol{\xi}_k)$  and  $\mathcal{J}(\boldsymbol{\xi}_k)$  defined in (9) are polynomial matrices depending on  $\theta$ ,  $\boldsymbol{\eta}_{k,h}$ , and  $\boldsymbol{\rho}_{k,h}$ . Hence  $\mathcal{G}(\boldsymbol{\xi}_k)$  and  $\mathcal{J}(\boldsymbol{\xi}_k)$  can be expressed as

$$\begin{aligned}\mathcal{G}(\boldsymbol{\xi}_k) &= \sum_{i=0}^N G_i(\theta, \boldsymbol{\eta}_{k,h}) \psi_i(\boldsymbol{\rho}_{k,h}), \\ \mathcal{J}(\boldsymbol{\xi}_k) &= \sum_{i=0}^N J_i(\theta, \boldsymbol{\eta}_{k,h}) \psi_i(\boldsymbol{\rho}_{k,h}),\end{aligned}\tag{21}$$

which are regarded as polynomials in terms of  $\boldsymbol{\rho}_{k,h}$ :  $\{\psi_i(\boldsymbol{\rho}_{k,h})\}$  are the monomial bases, and  $\{G_i(\theta, \boldsymbol{\eta}_{k,h})\}$  and  $\{J_i(\theta, \boldsymbol{\eta}_{k,h})\}$  are the corresponding coefficients. The number  $N$  of the monomial bases  $\{\psi_i(\boldsymbol{\rho}_{k,h})\}$  is determined by the dimension of  $\boldsymbol{\rho}_{k,h}$  as well as the highest degree of  $\boldsymbol{\rho}_{k,h}$  in  $\{G_i(\theta, \boldsymbol{\eta}_{k,h})\}$  and  $\{J_i(\theta, \boldsymbol{\eta}_{k,h})\}$ . As long as the polynomial matrices  $\mathcal{G}(\boldsymbol{\xi}_k)$  and  $\mathcal{J}(\boldsymbol{\xi}_k)$  are obtained,  $\{G_i(\theta, \boldsymbol{\eta}_{k,h})\}$  and  $\{J_i(\theta, \boldsymbol{\eta}_{k,h})\}$  can be determined according to their polynomial structure. For instance,

$$\begin{bmatrix} \theta + \eta\rho^2 \\ 2 + \eta^2\rho \end{bmatrix} = \begin{bmatrix} \theta \\ 2 \end{bmatrix} + \begin{bmatrix} 0 \\ \eta^2 \end{bmatrix} \rho + \begin{bmatrix} \eta \\ 0 \end{bmatrix} \rho^2.$$

Let  $n_r$  be the dimension of the residual vector,  $\otimes$  represent the Kronecker product, and  $\text{vec}(\cdot)$  denote the vectorization of a matrix by stacking its columns into a single column vector. Then, using (21), the residual in (8) can be rewritten into an LTV form

$$\begin{aligned}\mathbf{r}_k(\boldsymbol{\xi}, \mathbf{w}, \mathbf{v}) &= \sum_{i=0}^N \{G_i(\theta, \boldsymbol{\eta}_{k,h}) \mathbf{z}_{k,h} \psi_i(\boldsymbol{\rho}_{k,h}) - J_i(\theta, \boldsymbol{\eta}_{k,h}) \mathbf{n}_{k,h} \psi_i(\boldsymbol{\rho}_{k,h})\} \\ &= \sum_{i=0}^N \{L_{i,k} \text{vec}(G_i(\theta, \boldsymbol{\eta}_{k,h})) - S_{i,k} J_i(\theta, \boldsymbol{\eta}_{k,h}) \mathbf{n}_{k,h}\} \\ &= \underbrace{\begin{bmatrix} \mathcal{L}_k & -\mathcal{S}_k \end{bmatrix}}_{\boldsymbol{\Gamma}_k} \underbrace{\begin{bmatrix} \boldsymbol{\lambda}_L(\theta, \boldsymbol{\eta}_{k,h}) \\ \boldsymbol{\lambda}_S(\theta, \boldsymbol{\eta}_{k,h}, \mathbf{n}_{k,h}) \end{bmatrix}}_{\boldsymbol{\lambda}(\theta, \boldsymbol{\eta}_{k,h}, \mathbf{n}_{k,h})},\end{aligned}\tag{22}$$

with

$$L_{i,k} = (\mathbf{z}_{k,h}^\top \psi_i(\boldsymbol{\rho}_{k,h})) \otimes I_{n_r}, \quad S_{i,k} = \psi_i(\boldsymbol{\rho}_{k,h}) \otimes I_{n_r}, \quad (23)$$

$$\mathcal{L}_k = [L_{0,k} \quad L_{1,k} \quad \cdots \quad L_{N,k}], \quad \mathcal{S}_k = [S_{0,k} \quad S_{1,k} \quad \cdots \quad S_{N,k}], \quad (24)$$

$$\boldsymbol{\lambda}_L(\theta, \boldsymbol{\eta}_{k,h}) = \begin{bmatrix} \text{vec}(G_0(\theta, \boldsymbol{\eta}_{k,h})) \\ \text{vec}(G_1(\theta, \boldsymbol{\eta}_{k,h})) \\ \vdots \\ \text{vec}(G_N(\theta, \boldsymbol{\eta}_{k,h})) \end{bmatrix}, \quad \boldsymbol{\lambda}_S(\theta, \boldsymbol{\eta}_{k,h}, \mathbf{n}_{k,h}) = \begin{bmatrix} J_0(\theta, \boldsymbol{\eta}_{k,h}) \mathbf{n}_{k,h} \\ J_1(\theta, \boldsymbol{\eta}_{k,h}) \mathbf{n}_{k,h} \\ \vdots \\ J_N(\theta, \boldsymbol{\eta}_{k,h}) \mathbf{n}_{k,h} \end{bmatrix}. \quad (25)$$

The second equation in (22) is derived from the property that

$$\text{vec}(X_1 X_2 X_3) = (X_3^\top \otimes X_1) \text{vec}(X_2)$$

holds for matrices  $X_1$ ,  $X_2$ , and  $X_3$ .

With the above derivations, the residual in (22) is expressed as a multiplication between the coefficient matrix  $\boldsymbol{\Gamma}_k$  and the uncertainty vector  $\boldsymbol{\lambda}$ . The coefficient matrix  $\boldsymbol{\Gamma}_k$  in (22) is time-varying, and can be computed with the online data  $\mathbf{z}_{k,h}$  and  $\boldsymbol{\rho}_{k,h}$  according to (23) and (24). The uncertainty vector  $\boldsymbol{\lambda}$  is random, and Section 5.2 will present how to compute its PDF by exploiting the PDFs of the unknown parameter  $\theta$ , the measurement noise  $\boldsymbol{\eta}_{k,h}$  of scheduling parameters, and  $\mathbf{n}_{k,h}$  representing the process noise and output measurement noise.

### 5.2. Residual distribution and its confidence set

To construct the FD logic (11), this subsection presents the computation of the residual distribution and its confidence set. Due to its polynomial dependence on uncertain variables, the uncertainty vector  $\boldsymbol{\lambda}$  is non-Gaussian distributed. Hence the residual generated by (22) is also non-Gaussian. To enable efficient online computation of the residual distribution, a GM approach is proposed by exploiting GM approximations to the distributions of the uncertainty vector  $\boldsymbol{\lambda}$  and the residual  $\mathbf{r}_k$ . The details are as follows.

Since  $\boldsymbol{\lambda}(\theta, \boldsymbol{\eta}_{k,h}, \mathbf{n}_{k,h})$  in (22) has TI polynomial dependence on stochastic uncertainties  $\theta$ ,  $\boldsymbol{\eta}_{k,h}$ , and  $\mathbf{n}_{k,h}$ , it is a stochastic vector whose PDF is also TI and can be approximated offline by a mixture of Gaussians, i.e.,

$$p(\boldsymbol{\lambda}) = \sum_{j=1}^K \pi_j \mathcal{N}(\boldsymbol{\lambda}; \mu_\lambda^{(j)}, \Sigma_\lambda^{(j)}), \quad (26)$$

where  $K$  is the number of Gaussian components, the mixing coefficients  $\{\pi_j\}$  satisfy  $0 \leq \pi_j \leq 1$  and  $\sum_{j=1}^K \pi_j = 1$ , and  $\mu_\lambda^{(j)}$  and  $\Sigma_\lambda^{(j)}$  represent the mean and covariance matrix of each Gaussian component, respectively. The offline procedure for constructing the GM distribution (26) is: (i) generate a sufficient

number of samples  $\{\theta^{(i)}, \boldsymbol{\eta}_{k,h}^{(i)}, \mathbf{n}_{k,h}^{(i)}\}$ , and compute  $\boldsymbol{\lambda}^{(i)} = \boldsymbol{\lambda}(\theta^{(i)}, \boldsymbol{\eta}_{k,h}^{(i)}, \mathbf{n}_{k,h}^{(i)})$  according to (22) and (25); and (ii) determine the GM parameters  $\{\pi_j, \mu_\lambda^{(j)}, \Sigma_\lambda^{(j)}\}$  in (26) by solving the maximum likelihood estimation problem

$$\max_{\{\pi_j, \mu_\lambda^{(j)}, \Sigma_\lambda^{(j)}\}} \sum_{i=1}^{N_\lambda} \ln \left\{ \sum_{j=1}^K \pi_j \mathcal{N}(\boldsymbol{\lambda}^{(i)}; \mu_\lambda^{(j)}, \Sigma_\lambda^{(j)}) \right\}$$

190 with the expectation-maximization (EM) algorithm [35], where  $N_\lambda$  represents the number of samples. The  $K$  can be determined by comparing multiple models with different  $K$ 's using the Akaike information criterion [35].

As in the EM algorithm, the subsequent analysis relies on formulating GMs in (26) in terms of a discrete latent variable  $\boldsymbol{\omega}$  [35]. Let  $\boldsymbol{\omega}$  denote a  $K$ -dimensional binary random vector with each element  $\omega_j$  satisfying  $\omega_j \in \{0, 1\}$  and  $\sum_{j=1}^K \omega_j = 1$ , i.e., a particular element  $\omega_j$  is equal to 1 and all the other elements are null. In order to express the GM distribution  $p(\boldsymbol{\lambda})$  as a marginal distribution obtained from the joint distribution  $p(\boldsymbol{\lambda}, \boldsymbol{\omega})$ , define the marginal distribution  $p(\boldsymbol{\omega})$  and the conditional distribution  $p(\boldsymbol{\lambda}|\boldsymbol{\omega})$  as  $p(\omega_j = 1) = \pi_j$  and  $p(\boldsymbol{\lambda}|\omega_j = 1) = \mathcal{N}(\boldsymbol{\lambda}; \mu_\lambda^{(j)}, \Sigma_\lambda^{(j)})$ , respectively. Therefore, the joint distribution is given by  $p(\boldsymbol{\lambda}, \boldsymbol{\omega}) = p(\boldsymbol{\omega})p(\boldsymbol{\lambda}|\boldsymbol{\omega})$ , and the GM distribution  $p(\boldsymbol{\lambda})$  in (26) is then equivalently expressed as

$$p(\boldsymbol{\lambda}) = \sum_{\boldsymbol{\omega}} p(\boldsymbol{\omega})p(\boldsymbol{\lambda}|\boldsymbol{\omega}) = \sum_{j=1}^K p(\omega_j = 1)p(\boldsymbol{\lambda}|\omega_j = 1).$$

This expression explicitly associates every realization of  $\boldsymbol{\lambda}$  with a discrete value of  $\boldsymbol{\omega}$ , i.e., a realization of  $\boldsymbol{\lambda}$  is generated from a conditional Gaussian distribution  $p(\boldsymbol{\lambda}|\omega_j = 1)$ . This point of view is useful for constructing the residual distribution online.

For the EM algorithm to produce a reliable GM approximation, the number of data samples should be sufficiently large compared to the number of free GM parameters, i.e.,

$$(K - 1) + Kn_\lambda + \frac{1}{2}Kn_\lambda(n_\lambda - 1),$$

where  $n_\lambda$  denotes the dimension of  $\boldsymbol{\lambda}$ ,  $K - 1$ ,  $Kn_\lambda$ , and  $\frac{1}{2}Kn_\lambda(n_\lambda - 1)$  are respectively the number of free parameters in the mixing coefficients  $\{\pi^{(j)}\}$ , the means  $\{\mu_\lambda^{(j)}\}$ , and the covariance matrices  $\{\Sigma_\lambda^{(j)}\}$ . This requirement can be demanding from the computation perspective if  $n_\lambda$  is large. Actually,  $\boldsymbol{\lambda}$  would have a rather high dimension as the window length  $h$  grows or the degree  $d_V$  of the polynomial parity matrix increases, according to the definition of  $\boldsymbol{\lambda}$  in (22) and (25). In addition, in such a high dimensional case, the EM algorithm is prone to numerical ill-conditioning [36]. On one hand, the estimated covariance matrix  $\Sigma_\lambda^{(j)}$  is more likely to be singular, since the number of samples involved in computing  $\Sigma_\lambda^{(j)}$  is small compared to the dimension of  $\Sigma_\lambda^{(j)}$  [36]. On the other hand, since the elements of  $\boldsymbol{\lambda}$  have polynomial dependence of rather different

degrees on uncertain variables, their numerical values could differ by orders of magnitude, which might also results in an ill-conditioned covariance estimate.

210 Two remedies are adopted in this paper to address the above issue. Firstly, zero elements may be present in  $\boldsymbol{\lambda}$  due to the zero elements of  $G_i(\boldsymbol{\theta}, \boldsymbol{\eta}_{k,h})$  and  $J_i(\boldsymbol{\theta}, \boldsymbol{\eta}_{k,h})$ , thus they are removed without any information loss. Secondly, the GM modeling step is performed on the intrinsic low-dimensional subspace of  $\boldsymbol{\Lambda}$  by first conducting dimensional reduction as a preprocessing step. As a popular  
 215 method for dimension reduction, principal component analysis (PCA) is used here. Let  $\mathbf{\Lambda}$  denote the data matrix consisting of the sampled uncertainty vector  $\boldsymbol{\lambda}^{(i)}$ , i.e.,  $\mathbf{\Lambda} = \begin{bmatrix} \boldsymbol{\lambda}^{(1)} & \boldsymbol{\lambda}^{(2)} & \dots & \boldsymbol{\lambda}^{(N_\lambda)} \end{bmatrix}$ . Its singular value decomposition is  $\mathbf{\Lambda} = \mathcal{U}\mathcal{S}\mathcal{V}^\top$ . By selecting the largest  $n_c$  singular values that capture a significant portion (e.g., 95%) of total variance of  $\mathbf{\Lambda}$ , the approximated data matrix is  $\hat{\mathbf{\Lambda}} =$   
 220  $\mathcal{U}_1\mathcal{S}_1\mathcal{V}_1^\top$ , where  $\mathcal{U}_1$  and  $\mathcal{V}_1$  consist of the corresponding singular vectors within  $\mathcal{U}$  and  $\mathcal{V}$ , respectively, and  $\mathcal{S}_1$  represents a diagonal matrix with its diagonal entries being the largest  $n_c$  singular values. After dimensional reduction, the GM modeling step is carried out for  $\mathcal{V}_1^\top$ , which is in a reduced subspace of dimension  $n_c$ , and its estimated GM parameters are denoted by  $\{\hat{\pi}_j, \hat{\mu}^{(j)}, \hat{\Sigma}^{(j)}\}$ .  
 225 Accordingly, the GM parameters  $\{\pi_j, \mu_\lambda^{(j)}, \Sigma_\lambda^{(j)}\}$  for  $\boldsymbol{\lambda}$  are obtained as  $\pi_j = \hat{\pi}_j$ ,  $\mu_\lambda^{(j)} = \mathcal{U}_1\mathcal{S}_1\hat{\mu}^{(j)}$ ,  $\Sigma_\lambda^{(j)} = \mathcal{U}_1\mathcal{S}_1\hat{\Sigma}^{(j)}\mathcal{S}_1^\top\mathcal{U}_1^\top$ .

**Remark 4.** *With the introduced dimensional reduction, the GM model is constructed for  $\hat{\mathbf{\Lambda}}$  instead of the original sampled data matrix  $\mathbf{\Lambda}$ . Since a small  
 230 portion of total variance in  $\mathbf{\Lambda}$  is lost in the dimension reduction,  $\hat{\mathbf{\Lambda}}$  in the reduced space, hence its corresponding GM model, cannot capture some uncertain variations under the fault-free condition. This implies that some fault-free variations are not represented by the GM approximation of the residual distribution, which could lead to false alarms in FD, as will be illustrated by the simulation study in Section 6.3.*

235 **Remark 5.** *Other approaches reviewed in [36] can be also utilized for the high-dimensional GM modeling, but they are not the focus of this paper.*

**Remark 6.** *To validate the GM approximation, the well-known Kolmogorov-Smirnov distance*

$$\sup_{\boldsymbol{\lambda} \in \mathbb{R}^{n_\lambda}} |F_n(\boldsymbol{\lambda}) - \hat{F}(\boldsymbol{\lambda})|$$

240 *can be used to evaluate the goodness-of-fit between the empirical cumulative distribution function (CDF)  $F_n(\boldsymbol{\lambda})$  of the samples  $\{\boldsymbol{\lambda}^{(i)}\}$  and the CDF of the GM approximation  $\hat{F}(\boldsymbol{\lambda})$  [37], with  $n_\lambda$  denoting the dimension of  $\boldsymbol{\lambda}$ . Computing the above distance for multivariate distributions is non-trivial, and interested readers are referred to [37] for more details.*

From the online measurements  $\{\mathbf{u}_{k,h}, \mathbf{y}_{k,h}, \boldsymbol{\rho}_{k,h}\}$ ,  $L_{i,k}$ ,  $S_{i,k}$ ,  $\mathcal{L}_k$ ,  $\mathcal{S}_k$ , and  $\Gamma_k$  can be computed according to their definitions in (22)–(24). With  $\omega_j = 1$ , the

conditional distribution of the residual  $\mathbf{r}_k$  is then derived as

$$\begin{aligned} p(\mathbf{r}_k|\omega_j = 1) &= \mathcal{N}(\mathbf{r}_k; \mu_{r,k}^{(j)}, \Sigma_{r,k}^{(j)}), \\ \mu_{r,k}^{(j)} &= \mathbf{\Gamma}_k \mu_\lambda^{(j)}, \quad \Sigma_{r,k}^{(j)} = \mathbf{\Gamma}_k \Sigma_\lambda^{(j)} \mathbf{\Gamma}_k^\top, \end{aligned} \quad (27)$$

by performing a linear transformation (22) on the conditional Gaussian component  $p(\boldsymbol{\lambda}|\omega_j = 1)$ . Hence, the distribution of the residual can be also approximated by a Gaussian mixture

$$p(\mathbf{r}_k) = \sum_{j=1}^K \pi_j \mathcal{N}(\mathbf{r}_k; \mu_{r,k}^{(j)}, \Sigma_{r,k}^{(j)}). \quad (28)$$

Next, the confidence set  $\Delta_k$  for the random residual  $\mathbf{r}_k(\boldsymbol{\xi}, \mathbf{w}, \mathbf{v})$  is determined such that (10) holds.

**Theorem 3.** *Given the GM distribution (28) of the random residual  $\mathbf{r}_k$ ,  $\Pr\{\mathbf{r}_k \in \Delta_k\} \geq \gamma$  holds if the confidence set  $\Delta_k$  is constructed as*

$$\Delta_k = \bigcup_{j=1}^K \Delta_k^{(j)}, \quad (29)$$

where

$$\Delta_k^{(j)} = \left\{ \mathbf{r}_k \mid (\mathbf{r}_k - \mu_{r,k}^{(j)})^\top (\Sigma_{r,k}^{(j)})^{-1} (\mathbf{r}_k - \mu_{r,k}^{(j)}) \leq \chi_{n_r}^2(\gamma) \right\}, \quad (30)$$

is an ellipsoidal confidence set defined for the  $j^{\text{th}}$  Gaussian component  $p(\mathbf{r}_k|\omega_j = 1)$ , and  $\chi_{n_r}^2(\gamma) \in \mathbb{R}$  represents the value whose cumulative probability under the  $\chi^2$  distribution with  $n_r$  degrees of freedom is specified by  $\gamma$ .

*Proof.* With  $\omega_j = 1$ ,  $\mathbf{r}_k$  follows the conditional Gaussian distribution  $p(\mathbf{r}_k|\omega_j = 1)$ , and  $\Pr\{\mathbf{r}_k \in \Delta_k|\omega_j = 1\} \geq \Pr\{\mathbf{r}_k \in \Delta_k^{(j)}|\omega_j = 1\} \geq \gamma$  holds for  $\Delta_k$  and  $\Delta_k^{(j)}$  defined in (29) and (30). Then it follows that

$$\begin{aligned} \Pr\{\mathbf{r}_k \in \Delta_k\} &= \sum_{j=1}^K \Pr\{\mathbf{r}_k \in \Delta_k|\omega_j = 1\} \Pr\{\omega_j = 1\} \\ &\geq \sum_{j=1}^K \Pr\{\mathbf{r}_k \in \Delta_k^{(j)}|\omega_j = 1\} \Pr\{\omega_j = 1\} \\ &\geq \gamma \sum_{j=1}^K \Pr\{\omega_j = 1\} = \gamma. \end{aligned}$$

□

**Remark 7.** *Due to the possible overlaps among the confidence sets  $\{\Delta_k^{(j)}\}$ , the actually achieved probability  $\Pr\{\mathbf{r}_k \in \Delta_k\}$  can be larger than the predefined confidence level  $\gamma$ .*

With the confidence set  $\Delta_k$  defined in (29) and (30), the FD logic (11) amounts to checking whether there exists at least one confidence ellipsoid  $\Delta_k^{(j)}$  such that  $\mathbf{0} \in \Delta_k^{(j)}$ , or equivalently,  $(\mu_{r,k}^{(j)})^\top (\Sigma_{r,k}^{(j)})^{-1} (\mu_{r,k}^{(j)}) \leq \chi_{n_r}^2(\gamma)$ , holds. This FD logic can be further compactly expressed as

$$\begin{cases} \nu_k \leq 1 & \Rightarrow \text{the monitored system is fault-free} \\ \nu_k > 1 & \Rightarrow \text{the monitored system is faulty} \end{cases} \quad (31)$$

with

$$\nu_k = \min_{1 \leq j \leq K} \frac{(\mu_{r,k}^{(j)})^\top (\Sigma_{r,k}^{(j)})^{-1} (\mu_{r,k}^{(j)})}{\chi_{n_r}^2(\gamma)}. \quad (32)$$

The proposed FD approach is summarized in Algorithm 1.

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**Algorithm 1** Probability-guaranteed parity relation

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*Offline procedures:*

1. Select a horizon length  $h$  and a degree  $d_V$ . Compute the polynomial parity matrix  $V(\xi_k)$  by following Section 4.
2. Determine the monomial bases  $\{\psi_i(\boldsymbol{\rho}_{k,h}), i = 0, \dots, N\}$  and the polynomial matrices  $\{G_i(\theta, \boldsymbol{\eta}_{k,h}), J_i(\theta, \boldsymbol{\eta}_{k,h})\}$  in (21). Note that specific values of  $\theta$ ,  $\boldsymbol{\rho}_{k,h}$ , and  $\boldsymbol{\eta}_{k,h}$  are not required in this step.
3. Generate a sufficient number of samples  $\{\theta^{(i)}, \boldsymbol{\eta}_{k,h}^{(i)}, \mathbf{n}_{k,h}^{(i)}\}$ , compute  $\boldsymbol{\lambda}^{(i)} = \boldsymbol{\lambda}(\theta^{(i)}, \boldsymbol{\eta}_{k,h}^{(i)}, \mathbf{n}_{k,h}^{(i)})$  according to (22) and (25); determine the GM approximation (26) to the sample distribution of  $\{\boldsymbol{\lambda}^{(i)}\}$  using the EM algorithm.
4. Select the confidence level  $\gamma$  in (10).

*Online procedures:*

Initialization with  $k = h$ .

5. Construct  $\mathbf{u}_{k,h}, \mathbf{y}_{k,h}, \boldsymbol{\rho}_{k,h}$  over the horizon  $[k - h + 1, k]$ .
  6. Compute  $L_{i,k}$  and  $S_{i,k}$  in (23),  $\mathcal{L}_k$  and  $\mathcal{S}_k$  in (24),  $\Gamma_k$  in (22).
  7. Compute  $\{\mu_{r,k}^{(j)}, \Sigma_{r,k}^{(j)}\}$  in (27) for each Gaussian component of the residual distribution.
  8. Compute  $\nu_k$  in (32), and determine the fault presence according to (31).
  9.  $k \leftarrow k + 1$ , go to Step 5.
- 

## 6. Case study

### 6.1. Simulation setting and model description

In the case study, a well-mixed non-isothermal continuous stirred tank reactor is considered. It includes three parallel irreversible elementary exothermic reactions  $A \rightarrow B$ ,  $A \rightarrow U$ , and  $A \rightarrow R$ , where  $A$  is the reactant species,  $B$  is the desired product, and  $U$  and  $R$  are undesired byproducts. The reactant  $A$  is fed



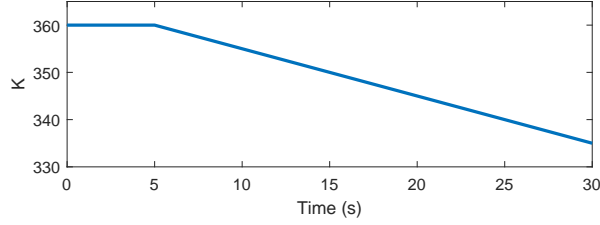


Figure 1: Profile of coolant temperature  $T_{cf}$ .

to the reactor at a flow rate  $F$ , concentration  $C_{Af}$ , and temperature  $T_{Af}$ . To remove heat from the reactor, a cooling stream at a flow rate  $F_c$  and temperature  $T_{cf}$  goes into the equipped cooling jacket. The process dynamics takes the form [38]:

$$\begin{aligned}
\dot{C}_A(t) &= \frac{F}{V}(C_{Af} - C_A(t)) - \sum_{i=1}^3 \kappa_i(t)C_A(t), \\
\dot{C}_B(t) &= -\frac{F}{V}C_B(t) + \kappa_1(t)C_A(t), \\
\dot{T}(t) &= \frac{F}{V}(T_{Af} - T(t)) + \sum_{i=1}^3 \frac{(-\Delta H_i + \delta_{H_i})}{\rho c_p} \kappa_i(t)C_A(t) \\
&\quad - \frac{UA + \delta_{UA}}{\rho c_p V}(T(t) - T_c(t)), \\
\dot{T}_c(t) &= \frac{F_c}{V_c}(T_{cf}(t) - T_c(t)) + \frac{UA + \delta_{UA}}{\rho_c c_{pc} V_c}(T(t) - T_c(t)),
\end{aligned} \tag{33}$$

where  $\kappa_i(t)$  is defined as

$$\kappa_i(t) = k_i \exp\left(\frac{-E_i}{RT(t)}\right), \tag{34}$$

$C_A$  and  $C_B$  denote concentrations of the species A and B in the reactor,  $T$  and  $T_c$  denotes temperatures of the reactor and the cooling jacket. The feed concentration and temperature are fixed at  $C_{Af} = 4$  mol/L and  $T_{Af} = 360$  K, respectively. The initial condition is  $C_A(0) = 3.5$  mol/L,  $C_B(0) = 0$  mol/L,  $T(0) = T_c(0) = 360$  K, which is unknown regarding the FD problem. The cooling stream temperature  $T_{cf}$  varies as depicted in Figure 1. With a sampling interval  $t_s = 0.1$  s, the sensor outputs  $C_B^m$ ,  $T^m$ , and  $T_c^m$  are the measurements of the reactor concentration  $C_B$ , the reactor temperatures  $T$  and the cooling jacket temperature  $T_c$ , with zero-mean Gaussian white noises  $v_{C_B}$ ,  $v_T$ , and  $v_{T_c}$ , whose standard deviations are 0.01 mol/L, 0.1 K, and 0.1 K, respectively.

The system parameters are described in Table 1. As shown in (33), the enthalpies  $\{\Delta H_i\}$  and the heat transfer coefficient UA are subject to probabilistic time-invariant uncertainties represented by  $\{\delta_{H_i}\}$  and  $\delta_{UA}$ , respectively. In this simulation,  $\{\delta_{H_i}\}$  are uniformly distributed over the interval  $[-100, 100]$  J/mol,

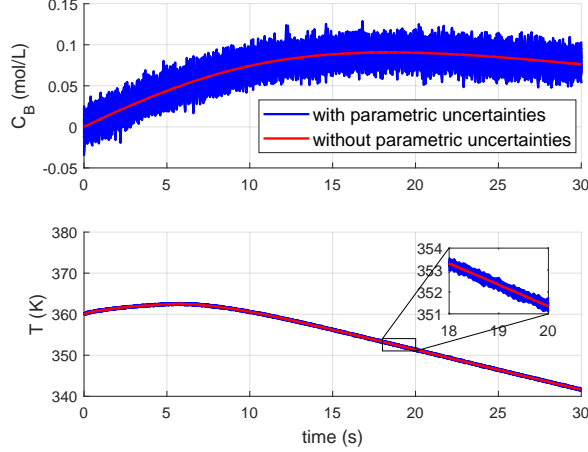


Figure 2: System outputs from 100 fault-free Monte Carlo simulations with and without parametric uncertainties.

while  $\delta_{\text{UA}}$  follows a truncated Gaussian distribution which is truncated over  $[-1 \times 10^5, 1 \times 10^5] \text{ J}/(\text{min}\cdot\text{K})$  from a conventional Gaussian distribution with zero mean and standard deviation  $1 \times 10^5 \text{ J}/(\text{min}\cdot\text{K})$ . Figure 2 depicts the sensor outputs  $C_B^m(t)$  and  $T^m(t)$  from 100 fault-free Monte Carlo simulations with and without the above uncertain parameters. The clear difference between fault-free output behaviors in the above two cases implies that neglecting parametric uncertainties would result in severe false alarms.

The following two fault scenarios are considered:

- Sensor bias: the reactor temperature sensor output  $T^m(t)$  becomes biased by 1.7 K, i.e.,  $T^m(t) = T(t) + 1.7 + v_T(t)$  for  $t \geq 15$  s.
- Valve stuck: the flow valve of the cooling stream gets stuck at  $T_{\text{cf}} = 22 \text{ L}/\text{min}$  for  $t \geq 15$  s.

To account for the nonlinear dependence of  $\{\kappa_i(t)\}$  in (34) on  $T$ ,  $\{\kappa_i(t)\}$  over the operation range  $T \in [345, 365] \text{ K}$  are approximated by polynomials  $g_1(T_k)$ ,  $g_2(T_k)$ , and  $g_3(T_k)$  with degrees 5, 4, and 4, whose maximum absolute approximation errors are  $1.05 \times 10^{-10}$ ,  $3.06 \times 10^{-12}$ , and  $3.06 \times 10^{-12}$ , respectively. By applying the Euler method and replacing  $\{\kappa_i\}$  in (34) with polynomials  $\{g_i(T)\}$ , the continuous-time system (33) with parameters in Table 1 is transformed into the following discrete-time LPV form whose scheduling parameter is the reactor temperature  $T_k$ , i.e.,

$$\begin{aligned} x_{k+1} &= A(T_k)x_k + Bu_k + B_w w_{0k}, \\ y_k &= Cx_k + D_v v_{0k}, \end{aligned} \quad (35)$$

Table 1: System parameters

Parameter	Description	Value	Unit
$F$	Inlet flow rate	83.3	L/min
$F_c$	Flow rate of cooling stream	50	L/min
$V$	Tank volume	1000	L
$V_c$	Volume of cooling jacket	100	L
$\Delta H_1$	Enthalpy of A→B	$-5 \times 10^4$	J/mol
$\Delta H_2$	Enthalpy of A→U	$-5.2 \times 10^4$	J/mol
$\Delta H_3$	Enthalpy of A→R	$-5.4 \times 10^4$	J/mol
UA	Heat transfer coefficient	$9.01 \times 10^5$	J/(min·K)
$k_1$	Pre-exponential constant of A→B	$5 \times 10^4$	min <sup>-1</sup>
$k_2$	Pre-exponential constant of A→U	$5 \times 10^3$	min <sup>-1</sup>
$k_3$	Pre-exponential constant of A→R	$5 \times 10^3$	min <sup>-1</sup>
$E_1$	Activation energy of A→B	$5 \times 10^4$	J/mol
$E_2$	Activation energy of A→U	$7.53 \times 10^4$	J/mol
$E_3$	Activation energy of A→R	$7.53 \times 10^4$	J/mol
$R$	Gas constant	8.314	J/(mol·K)
$\rho$	Fluid density in reactor	1000	g/L
$c_p$	Fluid heat capacity in reactor	0.231	J/(g·K)
$\rho_c$	Fluid density in cooling jacket	1000	g/L
$c_{pc}$	Fluid heat capacity in cooling jacket	4.2	J/(g·K)

where

$$x_k = [C_{A,k} \quad C_{B,k} \quad T_k \quad T_{c,k}]^\top, \quad u_k = [C_{Af} \quad T_{Af} \quad T_{cf,k}]^\top,$$

$$y_k = [C_{B,k}^m \quad T_k^m \quad T_{c,k}^m]^\top,$$

$$A(T_k) = \begin{bmatrix} 0.9917 - 0.1 \sum_{i=1}^3 g_i(T_k) & 0 & 0 & 0 \\ 0.1g_1(T_k) & 0.9917 & 0 & 0 \\ \sum_{i=1}^3 (\alpha_i + \beta_1 \delta_{H_i}^0) g_i(T_k) & 0 & 0.6017 - \beta_2 \delta_{UA}^0 & 0.3900 + \beta_2 \delta_{UA}^0 \\ 0 & 0 & 0.2145 + \beta_3 \delta_{UA}^0 & 0.7355 - \beta_3 \delta_{UA}^0 \end{bmatrix},$$

$$\alpha_1 = 21.6450, \quad \alpha_2 = 22.5108, \quad \alpha_3 = 23.3766,$$

$$\beta_1 = 0.0433, \quad \beta_2 = 0.0390, \quad \beta_3 = 0.0214,$$

$$B = \begin{bmatrix} 0.0083 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0.0083 & 0 \\ 0 & 0 & 0.0500 \end{bmatrix}, \quad B_w = \begin{bmatrix} 10^{-6} & 0 & 0 & 0 \\ 0 & 10^{-6} & 0 & 0 \\ 0 & 0 & 10^{-5} & 0 \\ 0 & 0 & 0 & 10^{-5} \end{bmatrix},$$

$$D_v = \begin{bmatrix} 0.01 & 0 & 0 \\ 0 & 0.1 & 0 \\ 0 & 0 & 0.1 \end{bmatrix},$$

<sup>280</sup>  $\delta_{H_i}^0$  and  $\delta_{UA}^0$  are scaled from  $\delta_{H_i}$  and  $\delta_{UA}$  to lie within  $[-1, 1]$ , and  $w_{0k}$  and  $v_{0k}$  follow standard normal distribution to account for discretization errors and

measurement noises, respectively.

### 6.2. Implemented algorithms

Both the proposed Algorithm 1 and the zonotope-based parity relation in [15] are implemented for comparisons. In the offline procedures of Algorithm 1, the horizon length  $h$  is set to 3, and the obtained polynomial parity matrix  $V(T_k, \delta^0)$  is  $2 \times 9$  with degree 1, where  $\delta^0$  represents  $[\delta_{H_1}^0 \ \delta_{H_2}^0 \ \delta_{H_3}^0 \ \delta_{UA}^0]$ . To account for the additive noise  $0.1v_{0k,T}$  of the measured temperature  $T_k^m$ ,  $T_k^m - 0.1v_{0k,T}$  is used to replace  $T_k$  in the parity matrix  $V(T_k, \delta^0)$ , hence  $V(T_k^m - 0.1v_{0k,T}, \delta^0)$  is used instead. Then, the uncertainty vector  $\boldsymbol{\lambda}$  defined in (22) includes 98 nonzero entries, each of which is a polynomial in terms of  $\delta^0$ ,  $w_{0k}$ , and  $v_{0k}$ . For the offline GM modeling, 5000 samples  $\{\boldsymbol{\lambda}^{(i)}\}$  of  $\boldsymbol{\lambda}$  are generated to construct a sampled data matrix  $\mathbf{\Lambda}$ . To avoid ill-conditioning, dimension reduction via PCA is applied to the sampled data matrix  $\mathbf{\Lambda}$  such that the data variance in a reduced subspace of dimension 7 can captures 99% of the total variance. The corresponding PDF of the sampled data in this reduced subspace is approximated by a GM with 2 components. As illustrated in Figure 3, the non-Gaussian distribution of samples in the reduced subspace is well approximated by the obtained GM. The selected confidence level  $\gamma$  is 99%. In the online procedures of Algorithm 1, steps 5-7 are followed to compute the GM parameters of the residual distribution, and the FD decision is made by following step 8.

As for the zonotope-based method in [15], a zonotope

$$\mathcal{Z} = \{\mathbf{p} + \mathbf{E}\epsilon : \epsilon \in \mathbb{B}^{n_\epsilon}\} \quad (36)$$

is constructed offline such that it contains 99% of the sampled uncertainty vectors  $\{\boldsymbol{\lambda}^{(i)}\}$ , where  $n_\epsilon$  is equal to the rank of the sampled data matrix  $\mathbf{\Lambda}$ , and  $\mathbb{B}^{n_\epsilon} \in \mathbb{R}^{n_\epsilon \times 1}$  is a unitary box composed of  $n_\epsilon$  unitary intervals  $\mathbb{B} = [-1, 1]$ . In this particular example, the dimensions of  $\mathbf{p}$ ,  $\mathbf{E}$ , and  $\epsilon$  are  $\mathbf{p} \in \mathbb{R}^{98}$ ,  $\mathbf{E} \in \mathbb{R}^{98 \times 8}$ , and  $\epsilon \in \mathbb{R}^{8 \times 1}$ , respectively. Please refer to [15] for more details of computing the center  $\mathbf{p}$  and the shape matrix  $\mathbf{E}$  of the zonotope  $\mathcal{Z}$ . The associated FD decision depends on checking whether the origin lies in the residual confidence zonotope  $\{\Gamma_k \mathbf{p} + \Gamma_k \mathbf{E}\epsilon : \epsilon \in \mathbb{B}^{n_\epsilon}\}$  computed from (22) and (36). This corresponds to the FD logic [15]

$$\begin{cases} \nu_{\text{zono},k} \leq 1 & \Rightarrow \text{the monitored system is fault-free} \\ \nu_{\text{zono},k} > 1 & \Rightarrow \text{the monitored system is faulty} \end{cases} \quad (37)$$

where  $\nu_{\text{zono},k}$  is the solution to the linear program

$$\begin{aligned} \min_{\epsilon, \nu_{\text{zono},k}} \quad & \nu_{\text{zono},k} \\ \text{s.t.} \quad & \Gamma_k \mathbf{p} + \Gamma_k \mathbf{E}\epsilon = 0, \\ & -\nu_{\text{zono},k} \leq \epsilon_i \leq \nu_{\text{zono},k}, \quad 1 \leq i \leq n_\epsilon, \\ & \nu_{\text{zono},k} \geq 0 \end{aligned} \quad (38)$$

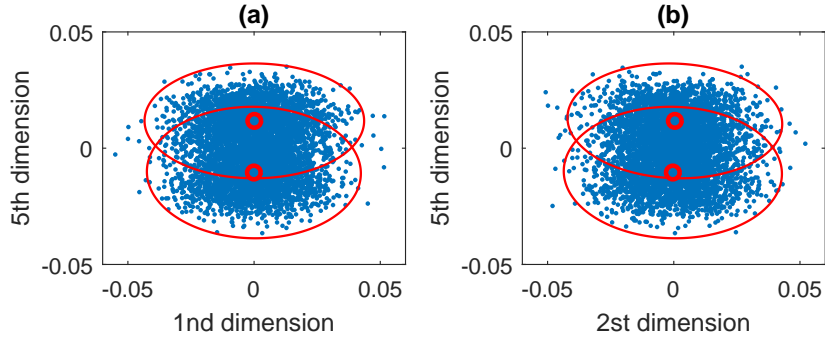


Figure 3: 2-dimensional projections of the sampled  $\lambda$  and its GM approximation within the reduced subspace. The blue dots represent the 5000 random samples. Each red circle and ellipse indicate the mean and 99% confidence set of the corresponding Gaussian component, respectively.

with  $\epsilon_i$  denoting the  $i$ th element of  $\epsilon$ . Two cases of the solution to (37) imply the detection of faults: (i) a feasible solution with  $\nu_{\text{zono},k} > 1$ ; and (ii) no feasible solution exists. In the latter case,  $\nu_{\text{zono},k}$  can be set to any value larger than 1 for the FD purpose. Note that the zonotope-based method in [15] relies on an LPV residual generator similar to the form of (22), but does not derive the polynomial parity matrix used in this paper.

### 6.3. Performance evaluations and comparisons

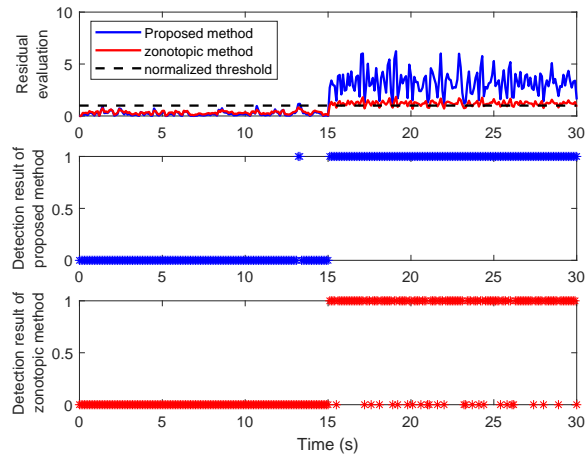
The FD results of one simulation run in the considered two fault scenarios are shown in Figure 6.3. The “residual evaluation” in Figure 6.3 refers to  $\nu_k$  in (32) and  $\nu_{\text{zono},k}$  in (38). Compared to the zonotope-based method, in both two fault scenarios, our proposed approach is more sensitive to faults, and achieves much fewer number of missed detections after fault injection at 15 s, while giving only one false alarm before fault injection.

In order to evaluate the statistical FD performance, Monte Carlo simulations are performed for  $N_{mc}$  times, and the performance metrics are defined by

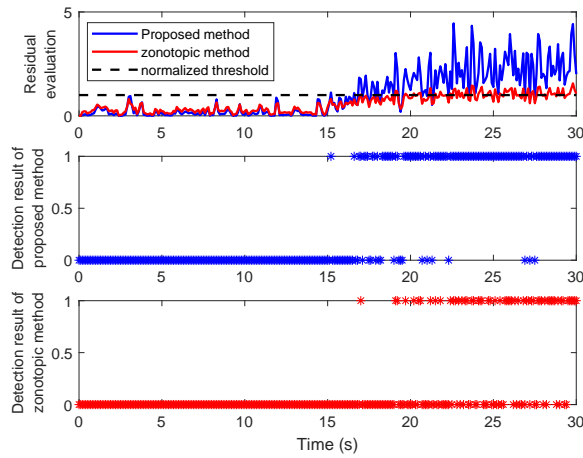
$$\text{FAR} = \frac{\text{total number of false alarms for } t \in [0, 15]}{(\text{number of samples for } t \in [0, 15]) \times N_{mc}} \times 100\%,$$

$$\text{MDR} = \frac{\text{total number of miss detections for } t \in (15, 30]}{(\text{number of samples for } t \in (15, 30]) \times N_{mc}} \times 100\%.$$

The effect of parametric uncertainty bounds on the FD performance is evaluated by the minimal fault magnitude that is detected with an MDR less than 5% in 100 Monte Carlo runs. As shown in Table 2, when using the tuning parameters described in Section 6.2, as the bound of  $\delta_{\text{UA}}$  grows, there is always an increase in the minimal sensor fault magnitude detected with an MDR less than 5%.



(a) Reactor temperature sensor bias 1.7 K after 15 s..



(b) Cooling flow valve stuck at 22 L/min after 15 s.

Figure 4: Residual evaluation and detection results of one simulation run in the considered two fault scenarios. In the lower two plots of each subfigure, at each time instant, “1” indicates an alarm from the detector, while “0” represents no reported alarm.

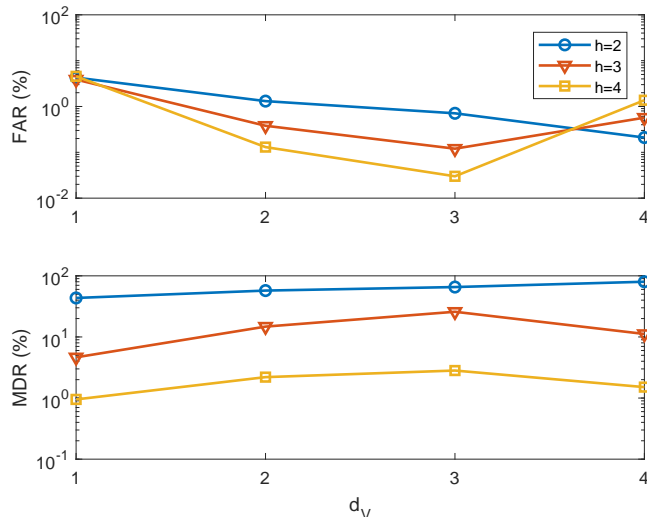


Figure 5: FAR and MDR for different choices of the horizon length  $h$  and the degree  $d_V$ . The number of Gaussian components is fixed to 2. The simulated fault is a constant bias 1.4 K on the reactor temperature sensor.

How the statistical FD performance depends on tuning parameters is analyzed by performing Monte Carlo runs, and illustrated in Table 3 and Figure 5. It can be seen from Table 3 that

- 325 • increasing the reduced dimension  $n_c$  results in a lower FAR and a higher MDR, due to less information loss in the dimensional reduction step as explained in Remark 4;
- by setting a larger confidence level  $\gamma$ , the achieved FAR decreases while the MDR increases, which is consistent with our expectation.

330 Figure 5 illustrates how the FAR and MDR vary with the horizon length  $h$  and the degree  $d_V$ . For each choice of  $(h, d_V)$ , the dimension reduction step captures 99% of the total variance of the sampled data matrix of  $\lambda$ . In Figure 5, the FAR remains below 5% in all cases. It is also observed that (i) the MDR becomes higher when  $d_V$  is larger than its minimal value 1; and (ii) for each fixed degree

335 from 1 to 4, the MDR decreases as  $h$  increases.

To show the benefit of exploiting distributional information of uncertain parameters, the PDF of  $\delta_{UA}$  is changed from the truncated Gaussian distribution to the uniform distribution over the same uncertainty range. Compared to case 5 of Table 3, the same tuning parameters are applied under the uniformly distributed  $\delta_{UA}$ , then the obtained FAR 4.17% almost remains unchanged, and the achieved MDR increases to 5.01%. This is due to not distinguishing high and low probability of occurrence in the uniformly distributed  $\delta_{UA}$ , compared to the truncated Gaussian distributed  $\delta_{UA}$ .

340

Table 2: For different uncertainty ranges of  $\delta_{UA}$ , minimal magnitudes of reactor temperature sensor bias that are detected with an MDR less than 5% in 100 Monte Carlo runs. The tuning parameters of our proposed algorithm are fixed as described in Section 6.2.

Range of $\delta_{UA}$ (J/min·K)	$[-1, 1]$ $\times 10^4$	$[-5, 5]$ $\times 10^4$	$[-9, 9]$ $\times 10^4$	$[-13, 13]$ $\times 10^4$
Minimal fault magnitude (K)	1.42	1.44	1.50	1.62

Table 3: FAR and MDR when tuning the reduced dimension  $n_c$  and the confidence level  $\gamma$ . The number of Gaussian components is fixed to 2. The simulated fault is a constant bias 1.4K on the reactor temperature sensor.

Tuning case	Horizon length $h$	Degree $d_V$	Reduced dimension $n_c$ for $\lambda$	Confidence level $\gamma$ (%)	FAR (%)	MDR (%)
1	3	1	6	95	5.56	2.41
2	3	1	7	95	4.15	3.03
3	3	1	7	99	0.97	9.19
4	3	1	8	99	0.86	11.67

## 7. Conclusions

345 This paper presents a probabilistic SM parity relation approach for LPV systems with polynomial dependence on probabilistic parametric uncertainties. A polynomially parameterized parity relation is constructed, and GMs are used to efficiently compute uncertain propagation from stochastic uncertainties to the residual distribution. To achieve an acceptable FAR, the consistency test  
350 uses the residual confidence set in the form of a union of ellipsoids. Guidelines for tuning parameters are discussed. The proposed approach is effective for a simulation example, which includes performance comparisons with a zonotope-based method. A comprehensive solution to fault isolation for the considered uncertain LPV system will be a focus of future research.

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