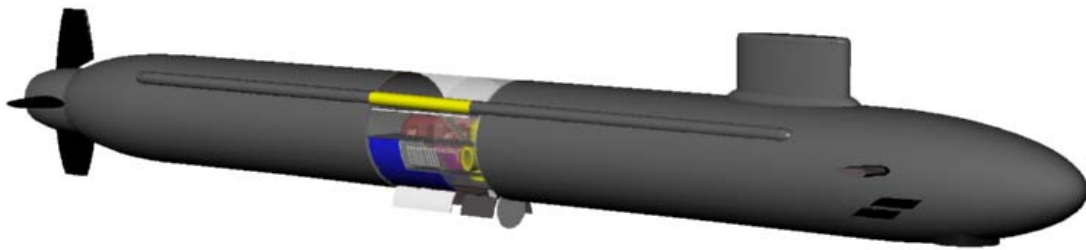


Deep Sea Research Submarine



LCDR Jeff Woertz

LT Erik Oller

LT Ereik Withee

February 1, 2002

Massachusetts Institute of Technology

Cambridge, MA

Executive Summary

The Deep Sea Research Submarine (Figure 1) is a modified VIRGINIA Class Submarine that incorporates a permanently installed Deep Sea Operations Compartment (Figure 2). Table 1 summarizes the characteristics of the Deep Sea Research Submarine and the Deep Sea Operations Compartment. The compartment, inserted as a 46-ft parallel midbody section, carries a heavy lift system capable of retrieving a 15-ton object (submerged weight) from depths greater than 2400 ft. A 26-ft L x 22-ft H x 12-ft W payload bay external to the pressure hull is used to house the object for transport. This payload bay also serves as a fully functioning mid-ship Main Ballast Tank. The compartment is supported by a combination of ship service and compartment-specific auxiliary systems.

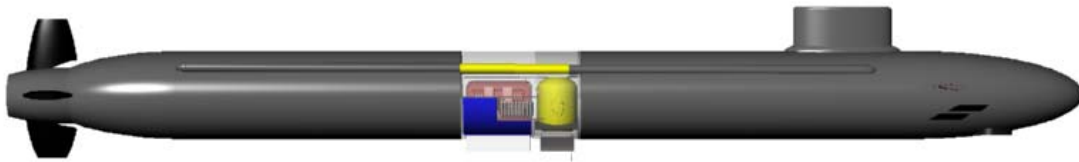


Figure 1. Deep Sea Research Submarine

The compartment also contains a 16 ft diameter x 17 ft high Remotely Operated Vehicle (ROV) Chamber outfitted with a Triton ZX ROV capable of excursions to depths of 9800 ft. The ROV Chamber permits dry access to the ROV for maintenance and mission-related tasks. The control center for the lift system and the ROV and a "mission flexible" space are located on the compartment's upper deck

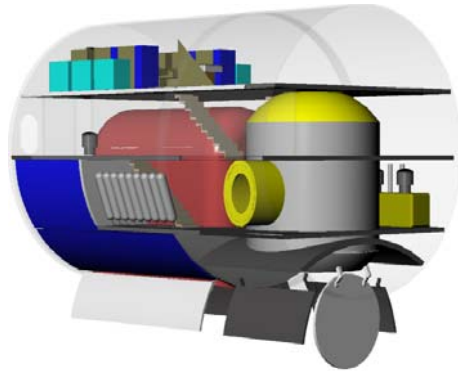


Figure 2. Deep Sea Operations Compartment

**Table 1. Deep Sea Research Submarine and Deep Sea Operations Compartment
Principle Characteristics**

Deep Sea Research Submarine	
Length	423 ft
Diameter	34 ft
Draft	28 ft 5 in
Speed Reduction	11%
Surfaced Displacement	7861 lton
Submerged Displacement	8870 lton
LCG	192.06 ft
GM _T	1.05 ft
Reserve Buoyancy	12.8%
Deep Sea Operations Compartment	
Length	46 ft
NSC Weight	999.1 lton
Submerged Lifting Capacity	14.7 lton
Maximum ROV Depth	9800 ft
Maximum Retrieval Depth	> 2400 ft
Conversion Cost as Percentage of Baseline Virginia Cost	20 %
Estimated Conversion Cost	\$650 million

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1.0 Mission Need

1.1 Defense Guidance and Policy.

This Mission Need Statement (MNS) provides requirements for a multi-mission submarine with deep-sea research capability for the 21st Century battle force vision. Through technology investment and insertion, the Deep Sea Research Submarine (DSRS) will be able to perform deep-sea research missions in addition to all the missions of a fast attack submarine. This submarine must operate wherever required to enable joint maritime expeditionary force operations, project precise strike power ashore, and conduct scientific and military research missions. The mission capabilities must be fully interoperable with other naval, interagency, joint and allied forces.

This unclassified MNS in part addresses Joint Vision 2020, published in June 2000. This document outlines the vision for creation of a force that “is dominant across the full spectrum of military operations – persuasive in peace, decisive in war, preeminent in any form of conflict.” Additionally, the document addresses “the need to prepare now for an uncertain future”.¹

The deep-sea research functions described in this MNS address the requirements set forth in Joint Vision 2020 to have “access to and freedom to operate in all domains”² as well as to support the information superiority which has been regarded as a key enabler of victory.³

This MNS should guide 21st century DSRS design, research, development and acquisition program decisions, service and joint doctrine, and cooperative efforts with U.S. allies.

1.2 Adversary Capabilities Analysis

As a result of the 2001 Quadrennial Defense Review, the basis of defense planning has been shifted from a threat-based model to a capabilities-based model. The

¹. Chairman of the Joint Chiefs of Staff, Joint Vision 2020 (Washington, D.C.: US Government Printing Office, 2000). 1

². Ibid., 8

³. Ibid., 10

capabilities-based model focuses on how an adversary might fight instead of who that adversary might be. This model recognizes that planning for large wars in distant theaters is not sufficient. The United States must also plan for adversaries who will rely on surprise, deception and asymmetric warfare to meet their objectives.⁴ Adversary capabilities will include asymmetric approaches to warfare that include terrorism and weapons of mass destruction.

In the past, the large distances between adversaries and the United States have provided a significant level of protection. As the events of September 11, 2001 illustrate, the U.S. can no longer rely upon this geographic protection. The rise of international travel and trade has made even the United States homeland vulnerable to hostile attack.⁵

Makers of national strategy will need to consider the rise and decline of regional powers. Some of these states are vulnerable to overthrow by radical or extremist internal forces. Many of these states have large armies and the capability to possess weapons of mass destruction.⁶ In some states, the governments are unable to prevent their territories from serving as sanctuaries for terrorists and criminals which may pose threats to the safety of the United States. In these cases, “threats can grow out of weakness of governments as much as out of their strength.”⁷

Asymmetric warfare, reduced protection from geographical distances, and vulnerabilities of foreign governments result in the need for the United States to maintain the ability to gather intelligence in all forms and in all areas of the globe. A key element in intelligence gathering is the ability to recover objects from the sea floor.

1.3 Current United States Capability Assessment

The purpose of the deep-sea research submarine is to augment the fleet by providing an autonomous deep-sea research platform with long-term station-keeping ability. The principal deep-sea research submarine of today’s Navy is the NR-1. This vessel was launched in 1969 and is among the oldest submarines in the Navy. NR-1’s missions have

⁴. Department of Defense, Quadrennial Defense Review Report (Washington, D.C.: US Government Printing Office, 2001). iv

⁵. Ibid., 4

⁶. Ibid.

⁷. Ibid., 5

included search, object recovery, geological survey, oceanographic research, and installation and maintenance of underwater equipment.⁸ NR-1 continues to provide a valuable service to the Navy and many research and educational institutions, but a replacement must be obtained in order to perform these missions after the end of NR-1's design life.

1.4 Mission Need

The roles of a future DSRS will include the following principal areas of naval warfare and research:

A. Intelligence, Surveillance, and Reconnaissance (ISR). A submarine's stealth makes it an ideal platform because the submarine can slip undetected into areas that are denied to surface and air platforms. To enhance its ability to accomplish this mission, the submarine must have the appropriate sensors, possibly including unmanned underwater vehicles (UUV's) and unmanned air vehicles (UAV's).⁹

B. Sea Control. A submarine's stealth again makes it a good platform for being the first to enter hostile areas. The future submarine should have the ability to locate and possibly neutralize diesel electric or air-independent propulsion submarines and mines.¹⁰

C. Land Attack. Submarines have already proven their ability to carry out strike operations. The importance of this mission will continue to increase because the submarine allows much more flexibility in the selection of the launch point. Launching missiles close to the enemy coastline, perhaps inside the defensive air umbrella, results in shorter flight times, greater surprise, and increased accuracy.¹¹

D. Special Operations Forces (SOF) Support. SOF mission support includes transit to and from the launch site, launch and recovery of SOF, and shore and surface fire support.

⁸. *United States Navy Fact File: NR-1 Deep Submergence Craft*. 1999.
www.chinfo.navy.mil/navpalib/factfile/ships/ship-nr1.html

⁹. Edward C. Whitman "Submarines in Network Centric Warfare." *Seapower* (July, 1999): 33-36.

¹⁰. *Ibid.*

¹¹. Whitman.

E. Oceanographic Sciences. The submarine will provide support for research in a variety of fields including Physical Oceanography, Ice Science, Geology/Geophysics, Marine Biology, Atmospheric Science, Ocean Engineering, Chemical Oceanography, Maritime Archeology, and Environmental Science.

F. Object Manipulation and Recovery. The submarine will be able to locate, manipulate, and recover objects of military or scientific interest from the ocean floor. The submarine may utilize remotely operated vehicles (ROV's) to perform these missions.

Appendix A contains more detailed information regarding the mission need.

1.5 Recommended Alternatives

Potential alternatives for meeting the need described above include:

- A. Design of an entirely new class of submarine.
- B. Modification of an Improved Los Angeles Class Design to meet the mission requirements.
- C. Modification of an Ohio Class Design to meet the mission requirements.
- D. Modification of a Seawolf Class Design to meet the mission requirements.
- E. Modification of a VIRGINIA Class Design to meet the mission requirements.

The VIRGINIA Class Design Modification is selected for further investigation.

2.0 Design Requirements and Plan

2.1 Required Operational Capability

The DSRS must be capable of supporting all VIRGINIA Class Submarine combat missions and a variety of military and scientific research missions. These missions require the launch and recovery of an ROV, the ability to perform heavy lifts, and possibly the ability to launch expendable UUV's. These missions also require analysis and berthing facilities for embarked research mission personnel.

2.2 Concept of Operations/Operational Scenarios/Performance Assessment Models

The concept of operations for the DSRS includes combat missions and a variety of military and scientific research missions. Combat missions will not be affected by this study and will not be discussed here. The research missions of the DSRS are related to those currently performed by other research submarines such as NR-1 and principally include object recovery and data acquisition. Two potential scenarios for these missions follow.

2.2.1 Scenario 1: Locate, Identify and Recover an Object of Interest

The first scenario includes the location, identification, and recovery of an object of interest from the ocean floor. The DSRS will stealthily proceed to the search area and commence searching for the object. The search will use a variety of sensors including side scan sonar and visual. These sensors will be located on the DSRS, UUV's, and/or an ROV. Once the object has been located the identity of the object will be confirmed and the recovery process will begin.

The ROV will be used to inspect the object for connection points, physical integrity and potential risk to the DSRS. The ROV may need to manipulate the object to render it safe for transport or to disable any threat to the DSRS. The ROV may need to reposition the object to enable attachment to the lifting frame. The ROV will install four lift points on the object. The ROV may use a specialized lifting harness for the object or existing features on the object. Once the object is ready for lift the ROV will return to the submarine.

The DSRS will lower the lift frame to the object. The lift frame will be remotely controlled from the submarine. The lift frame will have thrusters, cameras and lights for proper positioning. The lift frame arms will attach the lift points on the object to the lift points on the lift frame. The lift mechanism will lift the object into the DSRS for transportation to its ultimate destination.

2.2.2 Scenario 2: Conduct Scientific Research

The variety of possible scenarios for scientific research is infinite. This discussion is a simplified approach to meeting the needs presented in those scenarios. The DSRS will stealthily proceed to the region of interest. The ROV will be deployed to obtain samples or make observations at deep depths and on the sea bottom. Scientific sensors attached to the lifting frame will be lowered into the water to make other measurements and observations.

2.3 Goals, Constraints and Standards

Table 2 shows the goals for the DSRS.

Table 2. DSRS Goals

	Goals
Science and Research Mission Depth	2400 ft
Maximum Lift Capability	33,000 lb
VIRGINIA Class Speed Reduction	15%

The MNS provides the following constraints.

A. Architecture - The ship design must employ a total ship architectural/engineering approach that optimizes life cycle cost and performance, minimizes operating conflicts, permits rapid upgrade and change in response to evolving operational requirements, and allows computational and communication resources to keep technological pace with commercial capabilities. More specifically, this implies physical element modularity; functional sharing of hardware; open systems information architecture; ship wide resource management; automation of Command, Control, Communications, and Computers (C4I), and navigation functions; integrated ship wide data management; automation and minimization of maintenance and administrative functions; and embedded training.

B. Design - Consideration should be given to the maximum use of modular designs in the research vessel's infrastructure. Emerging technologies must be accounted for during the developmental phase. Since communication and data systems hold the greatest potential for growth, and therefore obsolescence, their installations must be

modularized as much as possible to allow for future upgrades. Systems onboard must use standard man-to-machine interfaces. The man-to-machine interfaces should be consistent with existing user-friendly systems.

C. Personnel - The ship must be automated to a sufficient degree to realize significant manpower reductions in engineering, ship support and watchstanding requirements. Preventive maintenance manpower requirements must be reduced by incorporating self-analysis features in equipment designs and by selecting materials and preservatives that minimize corrosion.

A. Operational Constraints.

1. The DSRS must remain fully functional and operational in all environments, whether conducting independent or force operations; in heavy weather; or in the presence of electromagnetic, nuclear, biological and chemical contamination.
2. The DSRS must provide ROV launching and recovery facilities.
3. The DSRS must be able to operate in U.S., foreign, and international waters in full compliance with existing U.S. and international pollution control laws and regulations.
4. All ship system elements must use standard subsystems and meet required development practices.
5. The DSRS must be able to embark Special Operations Forces (SOF) when required for selected missions.
6. The DSRS must be able to transit through the Panama Canal.

The ship must also meet the design requirements listed in

Table 3.

Table 3. Design Requirements

Requirement	Description
Schedule	Initial Operational Capability 2015.
Reserve Buoyancy	12% Minimum.
Margin Lead	No less than current amount.
BG	No less than 1.0 ft.
Propulsion	Maintain Current Configuration.
Speed	No more than 15% reduction in speed.
Stealth	Maintain current level of stealth during transit.

2.4 Design Philosophy and Decision Process

The purpose of this study is to examine the ability of a submarine to operate with ROV's and conduct heavy lifts up to 33,000 lb. The design philosophy consists of several principles:

- A. In order to minimize unnecessary rework, use the results of previous studies as baseline information for this one.
- B. Focus on accomplishing the mission before attempting modularity.
- C. Maintain the combat capabilities of the VIRGINIA Class Submarine.
- D. Minimize the amount of modification necessary to the systems on the VIRGINIA Class Submarine.
- E. Look at cost only after obtaining a baseline design.
- F. Once the basic structure is determined, carefully explore how the ROV will be used.

The decision process involves the comparison of possible variants to determine which variant or combination of variants best meets the mission requirements. The combat

systems and research payload for all acceptable variants will be identical. Each variant will have different effects on ship characteristics including speed, stability and access to ports. The variants were compared qualitatively to determine the one most suitable for our study.

3.0 Concept Exploration

3.1 Baseline Concept Design

The current design of the VIRGINIA Class Submarine provides the baseline concept design for this study. This design is summarized in Table 4.

Table 4. VIRGINIA Class Submarine Characteristics

Length	377 ft
Beam	34 ft
Displacement (Normal Surface)	6965 ltons
Crew	134
Armament	12 VLS tubes 4 Torpedo Tubes Advanced Mobile Mines
Propulsion	One nuclear reactor, one shaft
Reserve Buoyancy	12.55%
BG	1.03 ft

3.2 Concept Ship Variants

The DSRS is required to perform scientific and research missions as well as all of the combat missions of the VIRGINIA Class Submarine. Any modification of existing arrangements would detract from the combat abilities. Therefore, additional volume must be added to contain the equipment related to the scientific and research missions. The volume must be added to the ship in such a way as to minimize the modifications necessary to the existing design, provide personnel access to control and analysis

equipment, and maintain stability of the DSRS. Additionally, the requirement to transport the recovered object provides difficulties of arrangement exterior to the hull.

3.2.1 Addition of a Parallel Mid-Body (PMB)

Addition of a PMB would provide significant room near the center of gravity of the ship. This space could be used to meet all mission needs including ROV launch and recovery, heavy lift, and control and analysis. The PMB could be sized to transport the recovered object either internally or externally. The streamlined nature of the submarine would be preserved, stealth would be preserved, and all combat capabilities of the submarine would be preserved.¹²

A PMB adds considerable buoyancy to the ship that must be compensated for using variable ballast and additional main ballast tank capacity. This capacity can be obtained by altering the VIRGINIA Class Submarine design or by including those capacities in the plug.

3.2.2 Addition of Module Forward of the Sail

Addition of a module forward of the sail would have advantages similar to those of the PMB addition, but would also provide significant complications. The torpedo tube and shutter doors would have to be considered in the arrangement to prevent possible interference with weapon launch. The trim system of the ship would have to be modified to compensate for the heavy weight added forward of the ship's center of gravity. Additionally, this section of the ship has a tapering cross-section and would be less simple to construct than a PMB section.

3.2.3 Bow Reconfiguration

Reconfiguration of the bow to accommodate the ROV and the lifting mechanism would require the removal of the VLS tubes and the replacement of the sonar sphere and access trunk with a bow conformal array. The speed and maneuvering characteristics of the submarine would be preserved, the cost of modification would be minimal, and the

¹². Mark Galvin, Chris Hanson, Joe Harbour and David Hunt. VIRGINIA Class Payload Improvement Concept: Mission Flexibility by Modularity MIT Conversion Design Project (Cambridge, MA: Massachusetts Institute of Technology, 2000).

pressure hull would require minimal modification. However, the removal of the VLS tubes would seriously degrade the ship's combat capabilities. The reconfigured bow would require modification of the torpedo tube shutter doors. The added weight from the additional equipment at the front of the submarine would result in stability problems. Additionally, the necessary analysis and control equipment would not fit in the reconfigured space so the interior of the pressure hull would have to be modified.

3.2.4 Use of Appendages

Appendages could be added to the exterior of the hull to transport the ROV and the carry the lifting mechanism. A pod similar to the dry deck shelter used for special operations forces could be used to transport and launch the ROV. This would also provide additional flexibility for special operations deployment from the vessel.

Heavy lift capability could be installed using appendages at the sides or bottom of the ship. These appendages would not require modification of the pressure hull other than small penetrations for hydraulic and electrical services.

Appendages cause significant additional drag on the submarine and result in reduced speed capability. Also, appendages that alter the draft would restrict maneuverability in coastal waters. Just as in the case of bow reconfiguration, the interior of the pressure hull would need to be altered to make room for control equipment.

3.3 Variant Assessment and Trade-off Studies

The first step in the variant assessment process was to eliminate those variants that would reduce the combat capabilities of the submarine. The reconfiguration of the bow is eliminated. Next, we eliminated those variants that require scientific and research mission equipment to be stored within the pressure hull without adding additional space within the pressure hull. The use of appendages is eliminated. Finally, the relative merits of adding to the pressure hull forward of the sail and at the mid-body were examined. The addition of a PMB was selected because it required the least modification of the existing ship while meeting all mission needs.

3.4 Final Baseline Concept Design

The Baseline Concept Design, summarized in Table 5 and shown in Figure 3, is the VIRGINIA Class Submarine hull with a 46 ft long PMB added aft of the Operations Compartment. The forward section of the PMB contains a lockout chamber that will launch and recover ROV's (Figure 4). The lockout chamber also allows access to the ROV for recovery of samples and maintenance. The aft section of the PMB contains a cargo bay and heavy lift mechanism for recovery of objects from the ocean bottom. The upper deck of the PMB contains mission control and analysis equipment.

Table 5. DSRS Design Summary

DSRS Length	
DSOC Length	
Speed Reduction	
Displacement	
Submerged BG	
GM _T	
Conversion Cost	
Reserve Buoyancy	
Max. Retrieval Depth	
ROV Operating Depth	9800 ft

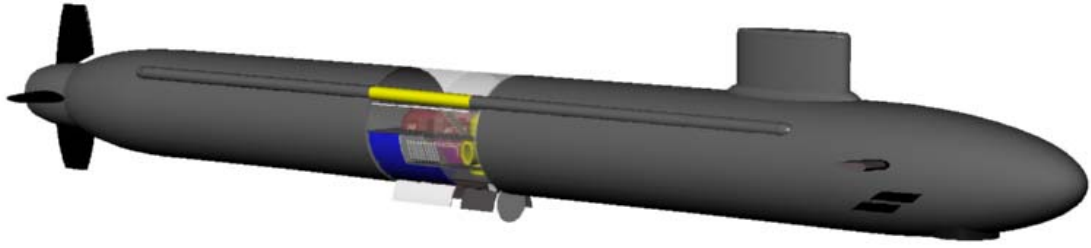


Figure 3. Final Baseline Concept Design

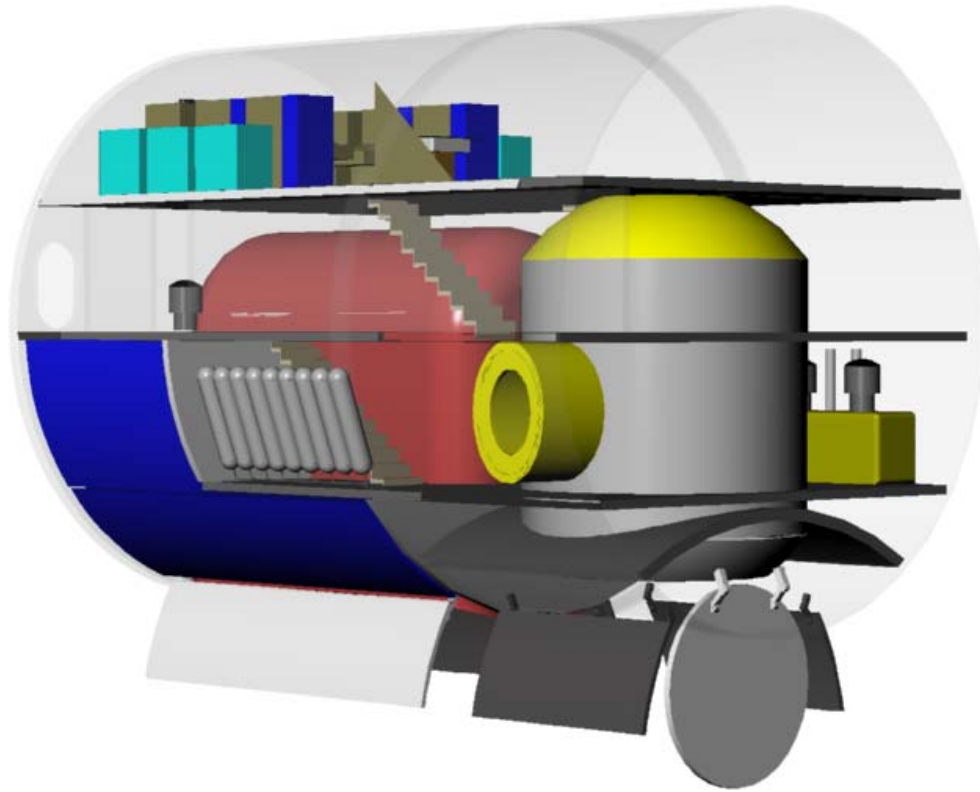


Figure 4. Parallel Mid-Body Addition Showing Internal Arrangements and Doors.

4.0 Feasibility Study and Assessment

The Final Baseline Concept Design was analyzed to evaluate its feasibility. The principle tool for analysis was the Massachusetts Institute of Technology XIII-A Submarine Math Model.¹³ This model is included as Appendix B.

4.1 Design Definition

4.1.1 Ship Geometry

The VIRGINIA Class Submarine design has been modified by adding a 46-ft PMB, labeled the Deep Sea Operations Compartment (DSOC), aft of the Operations

¹³ Jeffrey Reed and Mark Welsh. "Massachusetts Institute of Technology XIII-A Submarine Math Model", July 2001.

Compartment. Table 6 summarizes the geometry and characteristics of the DSOC and its principle components. The length and the location of the DSOC are based upon the results of VIRGINIA Class Payload Improvement Concept: Mission Flexibility by Modularity, by Mark Galvin, Chris Hanson, Joe Harbour and David Hunt.¹⁴ The PMB selected is six feet longer than that of the study to allow volume for the payload bay.

Table 6. Deep Sea Operations Compartment Characteristics

DSOC Length	46 ft
DSOC Diameter	34 ft
DSOC Displacement	1193.3 lton Subm 1033.7 lton Surf
ROV Chamber Dimensions	15.2 ft High x 15.0 ft Diameter
ROV Chamber Volume	3897 ft ³
Payload Bay Dimensions	21.3 ft High x 25.7 ft Long x 12 ft Wide
Payload Bay Volume	76010 ft ³

4.1.2 ROV and Equipment

The DSOC was designed to utilize the TRITON ZX Heavy Duty Work Class ROV manufactured by Perry Slingsby Systems. The MNS specified the TRITON ROV. Model ZX was selected because it is the most capable of TRITON ROV's. Table 7 summarizes the ROV's characteristics. More detailed information is included as Appendix 0.

¹⁴ Galvin, et al.

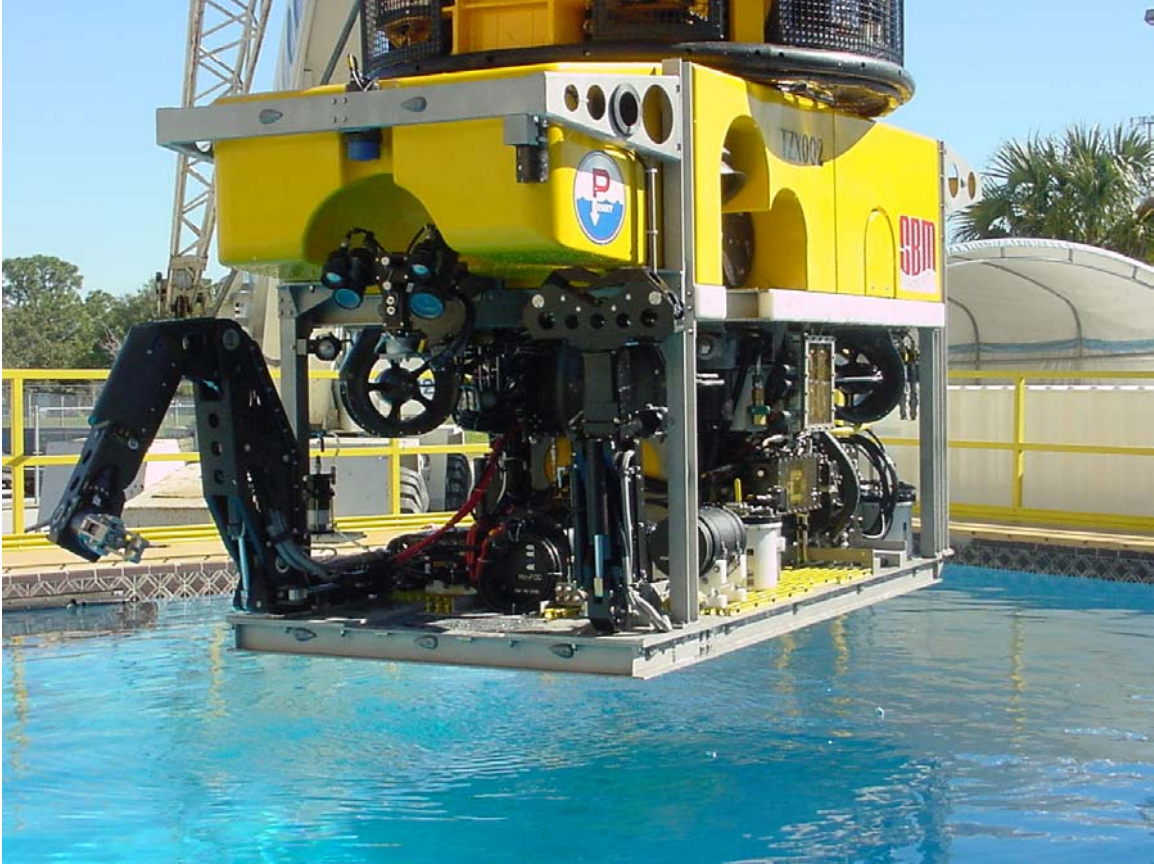


Figure 5. TRITON ZX ROV

Table 7. TRITON ZX Characteristics

ROV Dimensions	8.1 ft Long x 5.0 ft Wide x 6.2 ft High
Depth Rating	9800 ft
Payload Capacity	441 lb

The ROV and its auxiliary equipment are controlled by a set of three consoles in the DSOC. Figure 6 shows a typical arrangement. One console is required for control of the ROV itself and two others are required for control of the auxiliary equipment. Power is provided to the ROV through a high voltage transformer unit (HVTU), a high voltage junction box (HVJB), and a power distribution unit (PDU) (Figure 7 and Figure 8). Table 8 contains equipment characteristics. All of this equipment is installed on the upper level of the DSOC.



Figure 6. ROV Control Consoles in a Typical Arrangement



Figure 7. High Voltage Transformer Unit and High Voltage Junction Box



Figure 8. Power Distribution Unit

Table 8. ROV Control Equipment Data

	Consoles (Combined)	HVTU	HVJB	PDU
Weight	1300 lb	2300 lb	500 lb	800 lb
Height	73.63 in	36.5 in	28.75 in	72 in
Depth	26.31 in	21.38 in	24 in	17 in
Width	67.68 in	43 in	36 in	36 in

4.1.3 Lift Mechanism and Equipment

The lift mechanism consists of a maneuverable lift frame, a lift cable, a cable handling system, and associated controls. Figure 9 shows a drawing of the lift frame. For the purposes of this study, the lift mechanism controls and associated equipment are assumed to be identical to those of the ROV.

The cable handling system lowers the lift frame to the object. Once the lift frame is directly above the object, the operator uses manipulator/camera pairs on each corner of the lift frame to attach the frame to the object. The cable handling system lifts the lift

frame and the object into the payload bay. During descent and ascent, the operator controls the horizontal position of the lift frame using thrusters.

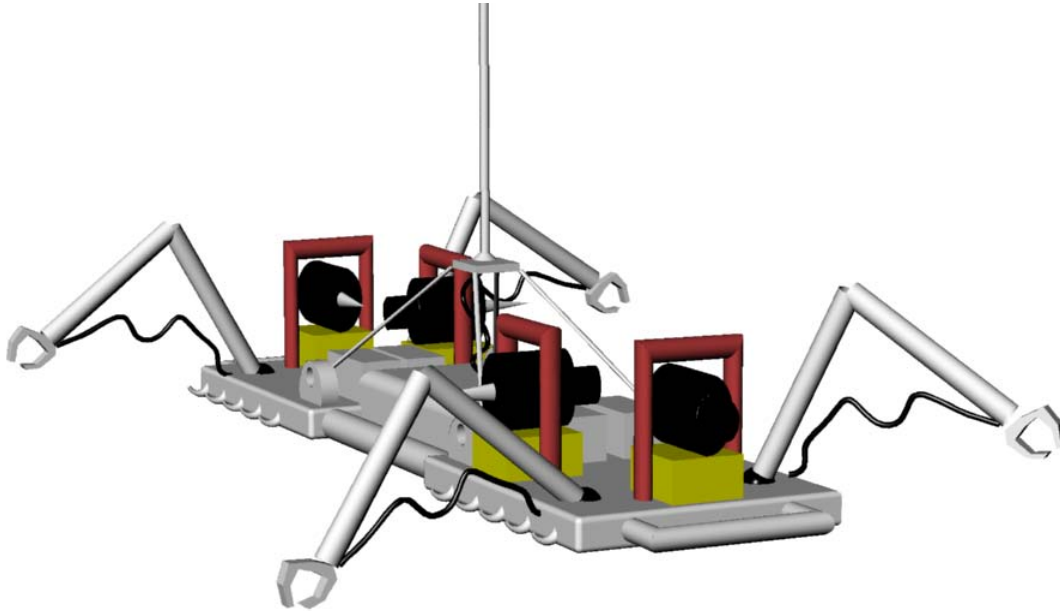


Figure 9. Lift Frame

Power and control signals are passed to the lift frame via the lift cable. Table 9 shows the characteristics of a representative heavy lift cable.

Table 9. Characteristics of a Representative Heavy Lift Cable

Theoretical Breaking Load	114,000 lb
Diameter	1.5 in
Weight in Water	2.0 lb/ft
Weight out of Water	2.8 lb/ft

4.1.4 Combat Systems/C4ISR

The DSRS contains all combat systems and C4ISR systems of the VIRGINIA Class Submarine.

4.1.5 Propulsion, Electrical and Auxiliary Systems

The VIRGINIA Class Submarine propulsion and electrical generation plants remain unchanged. The ship's auxiliary systems are modified to:

- A. Provide heating, ventilation, and air conditioning to the DSOC.
- B. Cross-connect to the DSOC hydraulic plant in the event of casualties.
- C. Cross-connect to the DSOC variable ballast system in the event of casualties.
- D. Connect Ventilation, High Pressure Air and Emergency Main Ballast Tank Systems to the Cargo Bay for Main Ballast Tank functions.

The ship's electrical distribution system has been modified to provide power to the ROV and lift mechanism controls as well as research and analysis equipment. Table 10 provides a list of the estimated electrical loads on the ships systems. These systems are compatible with 450 V, 60 Hz, 3 phase AC.

Table 10. Estimated DSOC Power Requirements

ROV and Control Equipment	200 kVA
Lifting Frame and Control Equipment	200 kVA
DSOC Trim Pumps	50 kVA
Total	450 kVA

4.1.6 Survivability and Signatures

The DSOC utilizes the same hull structure as the VIRGINIA Class Submarine with the exceptions of the apertures for the payload bay and the ROV chamber. The DSRS is expected to have the same level of survivability as the VIRGINIA Class Submarine. More detailed analysis is necessary to verify survivability.

The addition of the DSOC and the scientific and military research missions will affect the stealth of the DSRS in transit and on station. The doors for the payload bay and ROV chamber will affect the stealth of the DSRS in transit by generating additional flow-related noise. The operation of the doors, the ROV, and the lifting mechanism will cause sound transients when on station conducting missions. Further analysis and study is

required to determine the severity of these generated noises and their effects on the ship's mission.

4.1.7 Manning

The scientific and research functions require four personnel in addition to the ship's regular complement. Two will be scientists or mission specialists. The other two will be required for ROV and lift mechanism control. The DSOC does not have berthing space, so berthing will be provided in the submarine's berthing spaces.

Berthing can be obtained by leaving some non-essential personnel ashore for the mission, increased hot racking, or using alternatives such as the Submarine Torpedo Room Berthing Pod (Figure 10), developed by the Dutch company Polymarin. The berthing pod is the size of a MK-48 torpedo and has three berths with individual lighting, forced air ventilation, and storage space. They are loaded onto the submarine and handled just like a torpedo is handled. The berthing pod is scheduled to be evaluated for use on United States submarines as part of the Office of the Secretary of Defense Foreign Comparative Testing Program.



Figure 10. A Submarine Torpedo Room Berthing Pod being loaded into a Dutch submarine.

4.1.8 Arrangement

4.1.8.1 Stack Length

A previous feasibility study found that the best longitudinal location at which to make a plug insertion is aft of frame 39. The same study used 40-ft plug length, which is insufficient for this modification.¹⁵

Equipment stack length drove the compartments 46-ft overall length. The design payload is 23 ft long, 10.5 ft wide, and 6 ft tall. The payload bay requires: 1 ft of object clearance on all sides, 9 in. of space at the fore and aft ends for bay door hydraulic motors and gearing, and 1 ft additional side space for the rotating door hinges. This brought the payload bay's overall outer dimensions to 26 ft long and 12 ft wide. Similarly, the bay's 22-ft height was driven by the stacked dimensions of the payload item, lift frame, 3000-ft cable reel, hydraulic motors, and overhead supports (Figure 11).

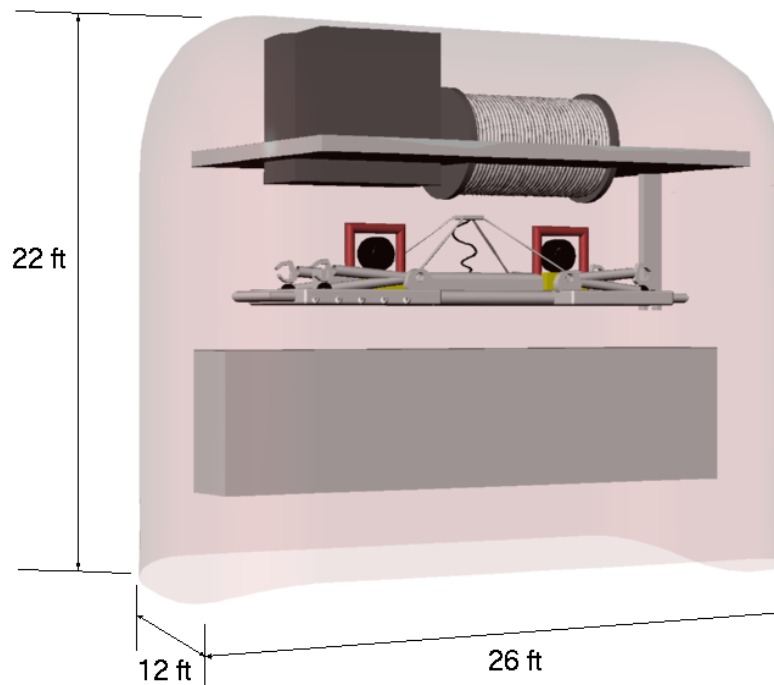


Figure 11. Payload Bay Internals

¹⁵. Galvin et al.

The ROV Chamber requires an 11-ft hatch for vehicle egress, as well as 36-in. internal clearances on all sides of the ROV to permit maintenance. As Figure 12 shows, stacked equipment dimensions drove the required height of the chamber.

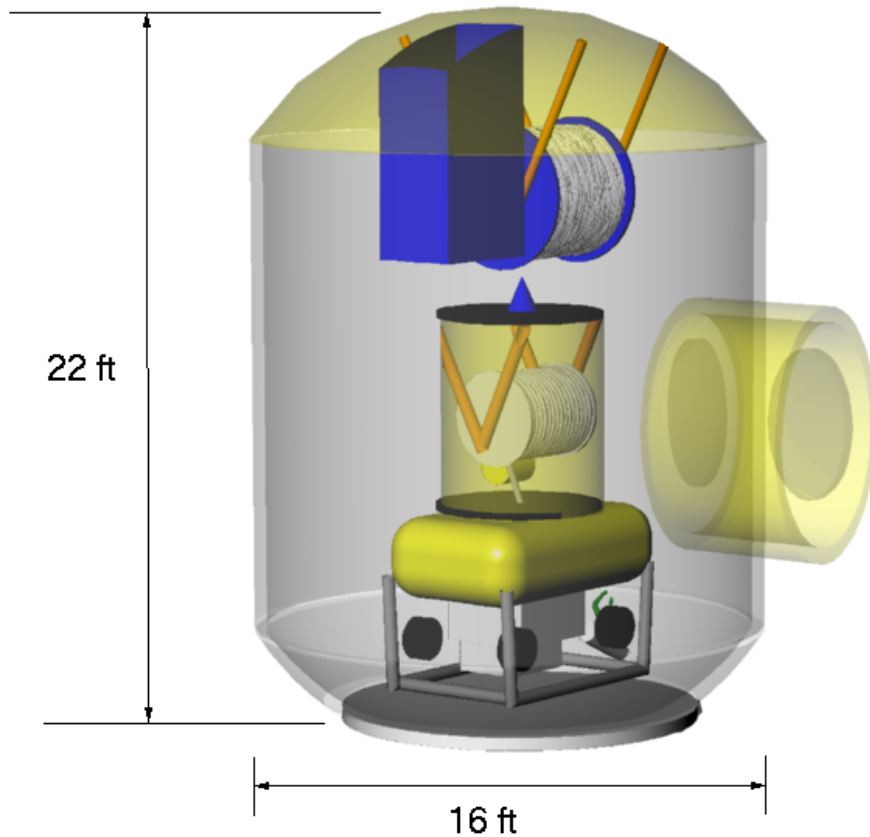


Figure 12. ROV Chamber Internals

The remaining 4 ft of DSOC length (46 ft, less the 26 ft and 16 ft already allocated) allows sufficient room for personnel to move between the structures on the two lower levels.

4.1.8.2 Reserve Buoyancy

The ship's safety requires that the Reserve Buoyancy (ROB) be greater than 12.5%. In order to maintain this level of ROB several modifications to the ship's hull were necessary. The most significant reason for this is the heavy weight of the DSOC. In fact, the DSOC weighs 40% more per foot than the VIRGINIA Class Submarine.

Figure 13 shows the design considerations and the final design space allowed. The weight line shows the weight of the DSOC for each length. The ROB line shows the

ROB that the ship would have for each plug length with no other modification. The length of the plug was selected as 46 ft to allow for both the ROV Chamber and the Payload Bay. This resulted in a ROB of 11.1%.

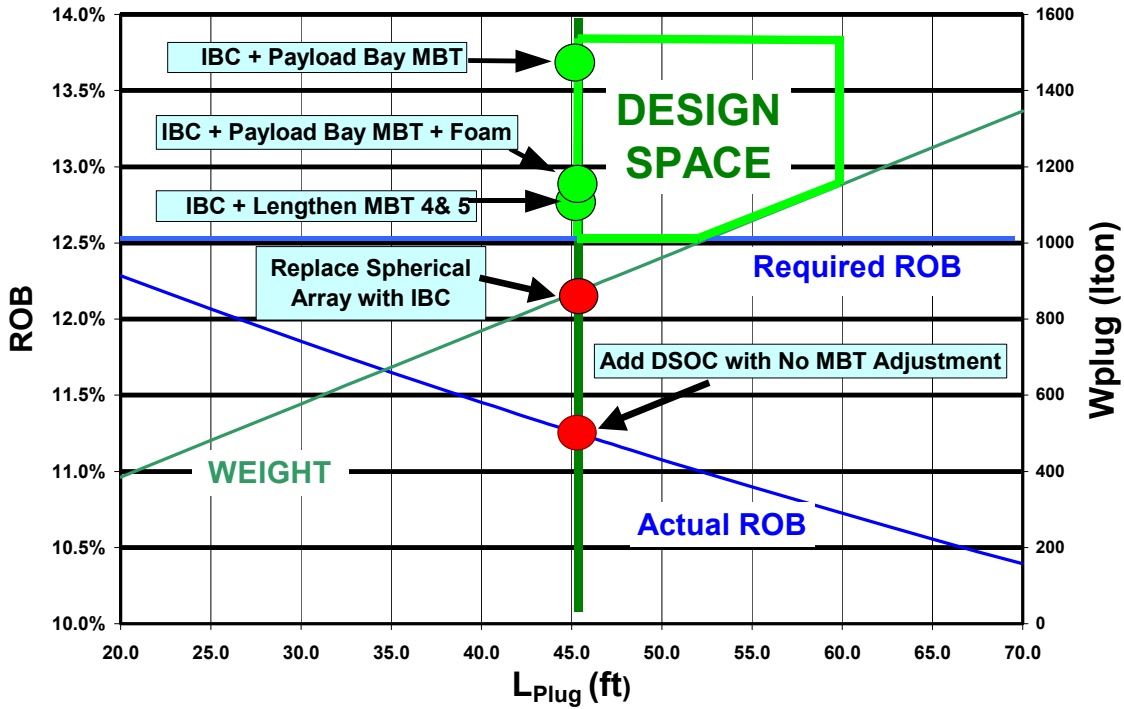


Figure 13. Plug Length Tradeoff Space

Several options were explored to maintain the required 12.5 % ROB. First, the existing spherical array was replaced with a conformal array (IBC) to expand the forward ballast tank capacity by 48 lton. This modification raised ROB to 12.1%. Figure 14 shows the variant dimensions after the plug insertion and installation of a bow conformal array.

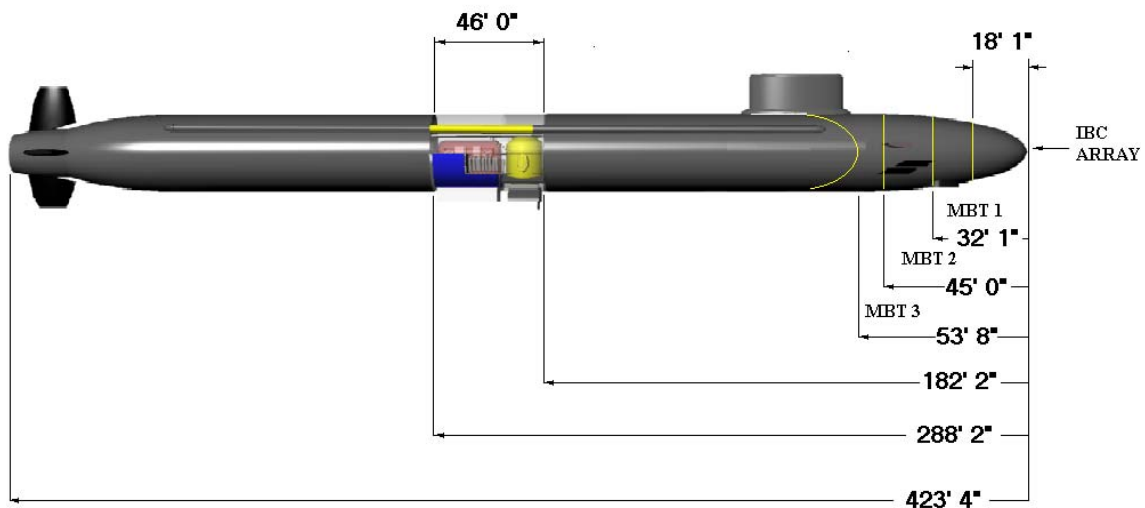


Figure 14. DSRs Profile

To achieve the required level of ROB, the aft MBT's would require enlargement, or the plug itself would have to incorporate an additional MBT. Calculations showed that lengthening the stern an additional four feet would increase the capacity of MBT 4 and 5 by 92 tons, providing 12.6% ROB. Lengthening the stern would involve significant structural modification to the original VIRGINIA Class design and is contrary to the group's design philosophy for this project.

Additional calculations showed that the Payload Bay contains 159 lton of seawater. Using the Payload Bay as an MBT and replacing the spherical array with an IBC Array results in a ROB of 13.8%. The longitudinal balance of the ship required reducing the volume of MBT 5. Syntactic foam was added to MBT 5 to achieve the proper longitudinal balance. The Weights and Stability section provides a more detailed discussion of the longitudinal balance. After all modifications, the final ROB was 12.8%.

4.1.8.3 Plug Internal Arrangements

In order to minimize impact on the Virginia class, no major alterations were made to the baseline ship arrangement other than the mid-body insertion. DSOC passageway locations correspond to the existing watertight door locations. Some minor changes in

pipng, ventilation, and electric cabling runs are required for the modification, but the overall effect on the ship's existing layout is small.

The DSOC is arranged in four levels. Figure 15 shows the upper level. The aft area of the upper level (24 ft ABL) is the Operations Center where ROV and Crane evolutions are monitored and controlled. The forward section of the space is designated as a "mission flexibility" space. This space is 21 ft long and could be used as a mission stowage space, general stores location, or portable temporary berthing area (though the DSOC contains no sanitary facilities). Figure 15 shows a plan view of the upper level.

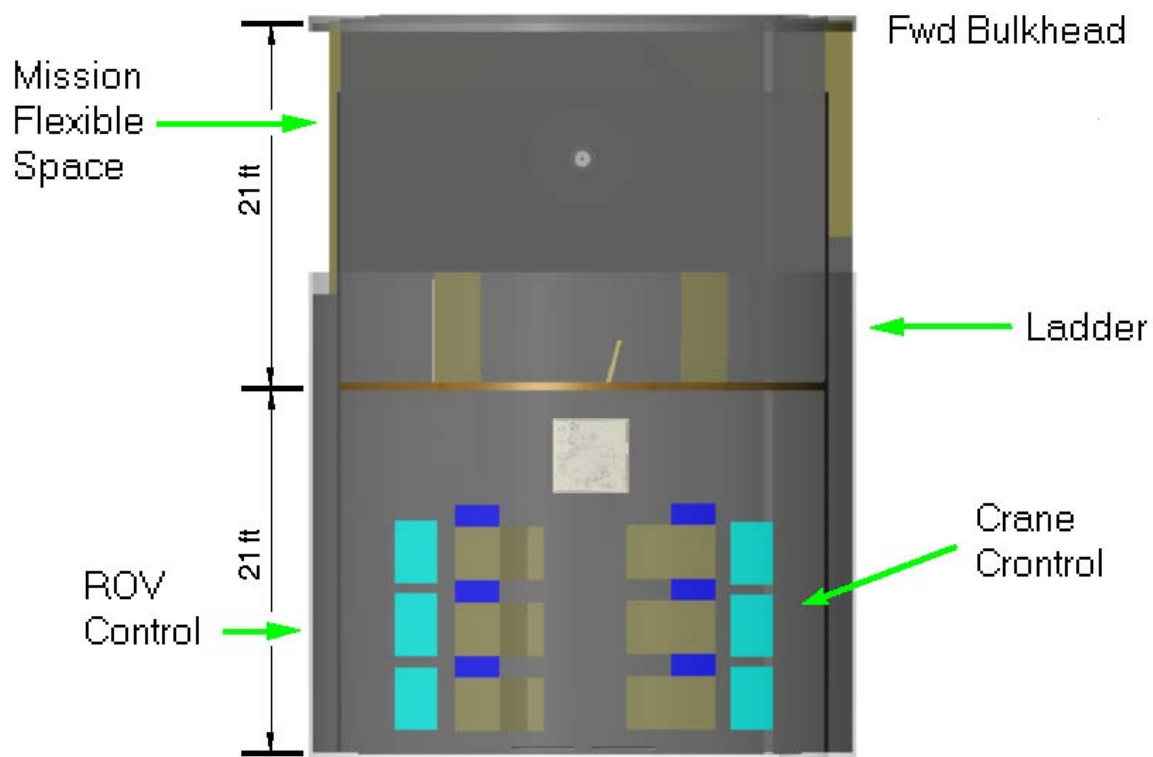


Figure 15. DSOC Upper Level

The middle level at 16.5 ft ABL (Figure 16) provides access to the fore/aft tunnel passageway. This level is connected by ladders to the decks above and below. A majority of the space on this level is consumed by the crane bay and ROV Chamber shells, however there remains a significant amount of area for mission related or general stores. This level also houses two dedicated compensation pumps, which can be cross-connected to the ship's trim and drain system.

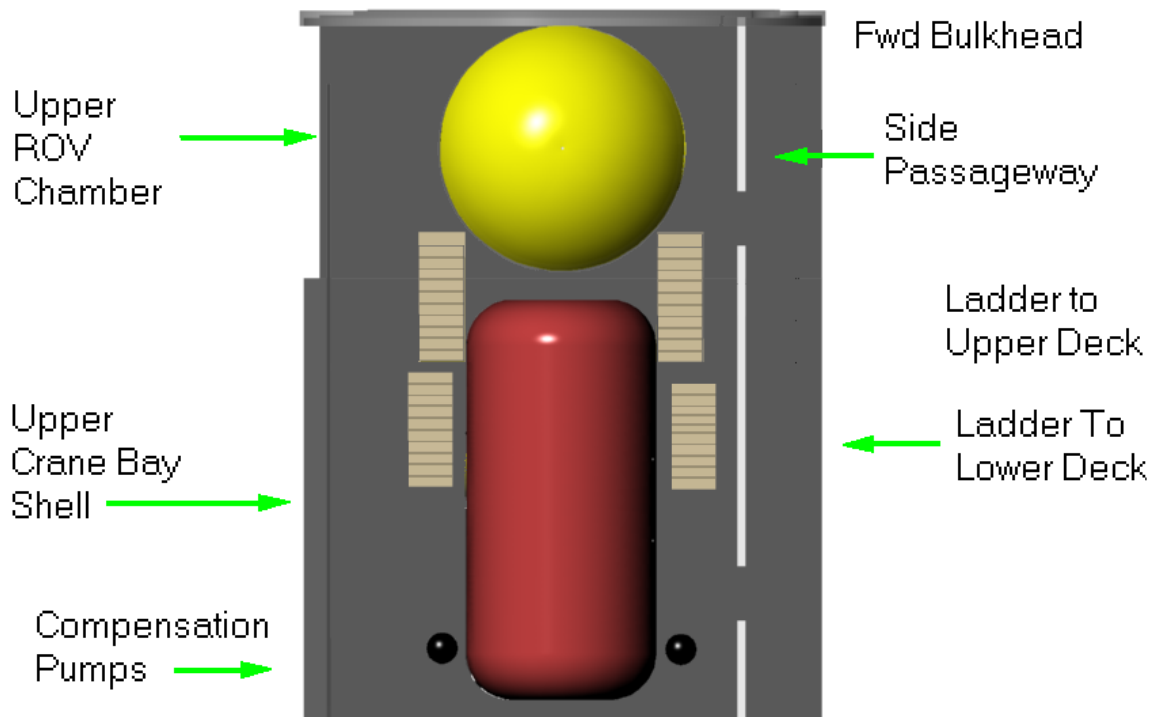


Figure 16. DSOC Middle Level

The lower level at 7.7 ft ABL (Figure 17) is connected by two ladders to the level above. The space contains the DSOC's 3000 psi external hydraulic plant, ROV Chamber access, and the dedicated EMBT Air Flasks. Eighteen vertically-stored EMBT Air Flasks each hold 7 ft³ at 4500 psi.

Though not analyzed in this design, Figure 17 shows a notional access into the Payload Bay area. Also shown are the upper sections of the 65-lton compensation tanks.

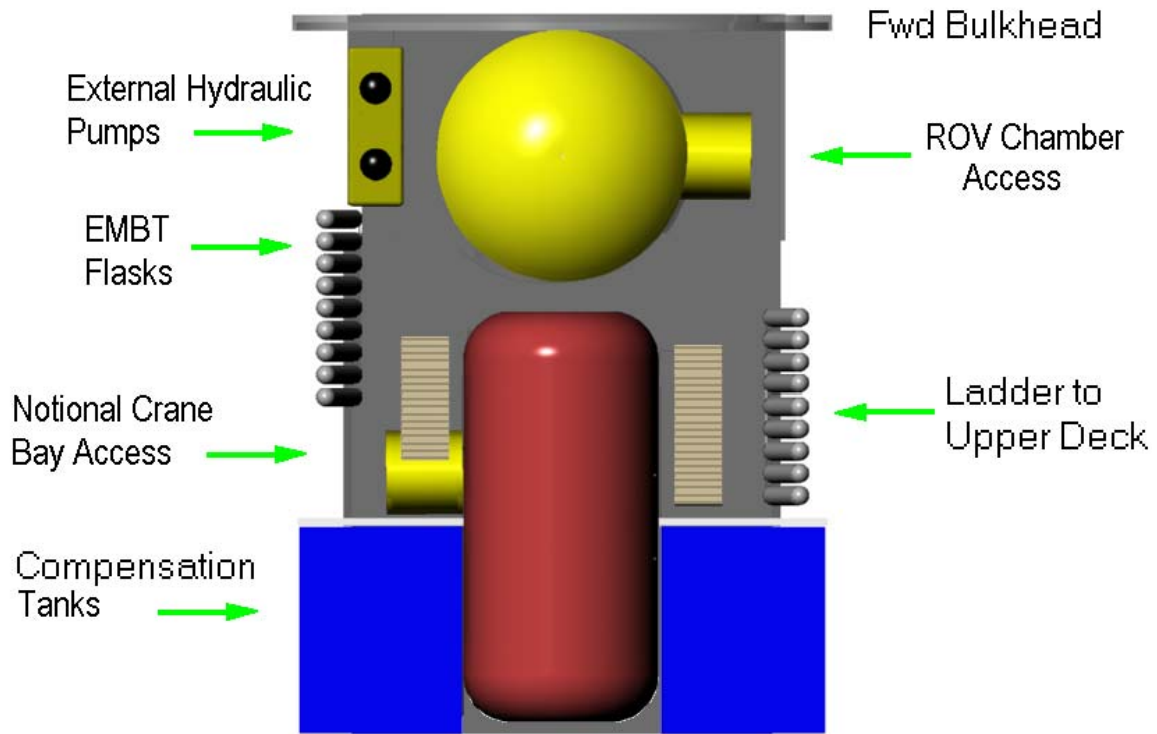


Figure 17. DSOC Lower Level

The lowest level, is merely a piping and tank space between the lower-level deck and the pressure hull. Payload Bay and ROV pressure hull penetrations occur on this level. Additionally, this deck houses the majority of the compensation tank volume. Figure 18 shows a plan view of the area.

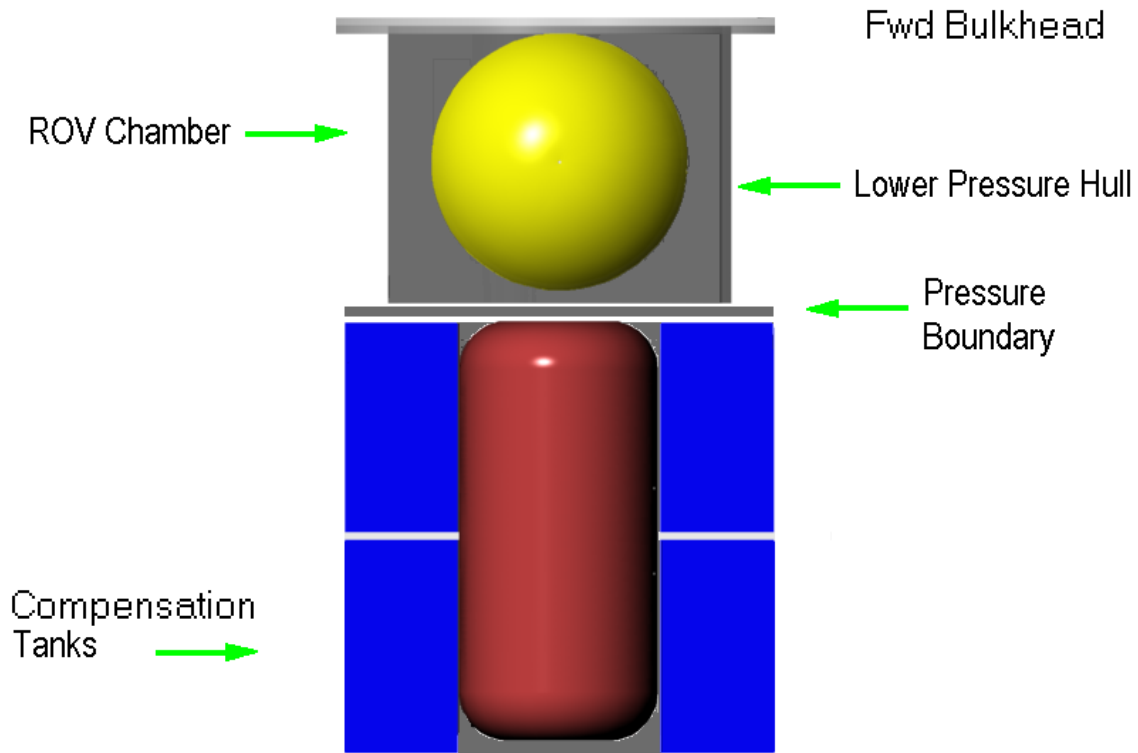


Figure 18. DSOC Tankage Level

4.1.9 Structural Design

The structural feasibility of the PMB concept has been examined in the past.¹⁶ It is well known that any departure from a traditional cylindrical pressure hull will most likely require extensive structural reinforcement. The decision to house payload internally drove the requirement for a large, heavy enclosed bay that is part of the pressure hull. Figure 19 shows the resultant pressure hull geometry.

As expected, the DSOC's asymmetric pressure hull results in substantial structural and weight concerns. One concern is the presence of two significant stress concentrators at the bottom of the pressure hull. Conservative structural weight allowances were factored into the initial calculations in anticipation of these concerns. Analyses showed the design to be feasible based upon very conservative structural selections.

¹⁶. Galvin, et al.

All static load safety margins were satisfied, but detailed dynamic calculations are necessary to show that dynamic safety margins are met. Future design iterations will probably show that the DSOC's structural weight can be greatly reduced.

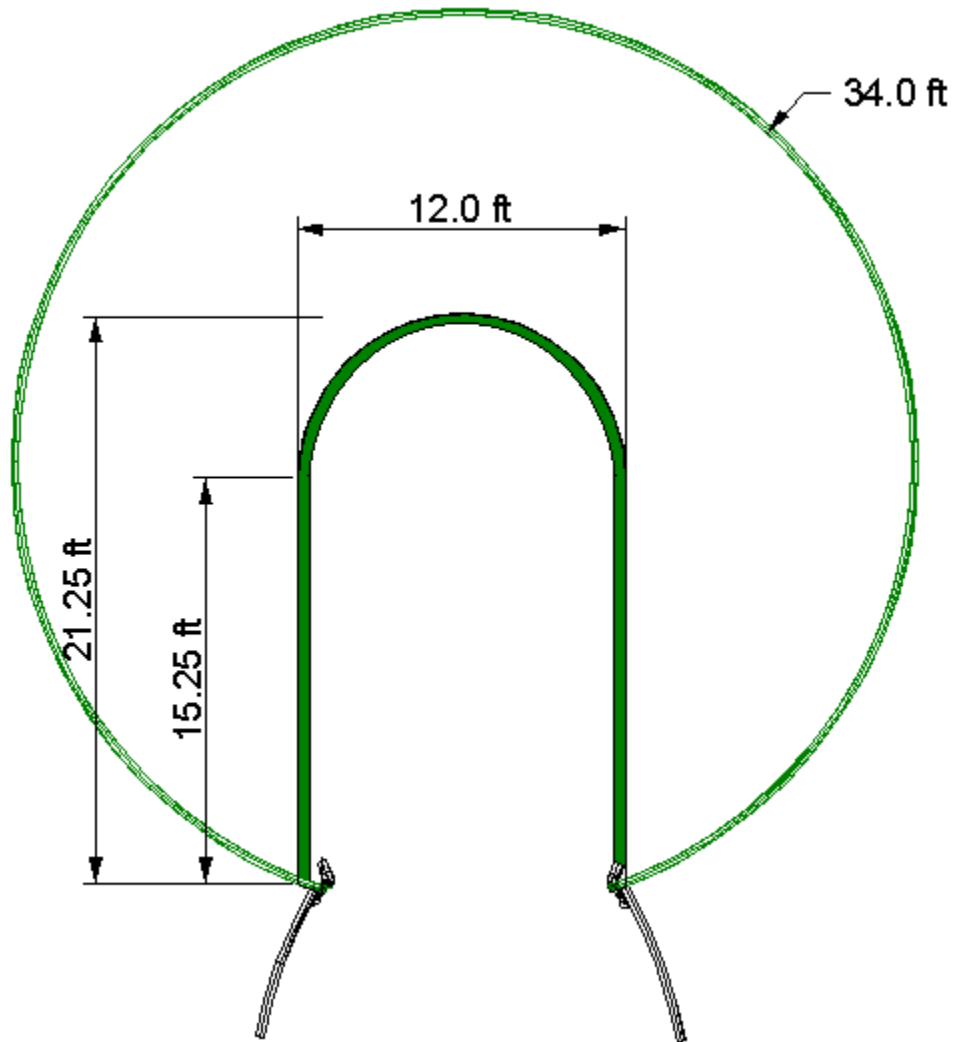


Figure 19. DSOC Cross-Section

4.1.9.1 Main Shell and Framing

The DSOC pressure hull and framing scantlings are based on the current Virginia parallel mid-body design. Reanalysis was considered unnecessary. Use of the existing scantlings also serves to minimize impact on the baseline design and reduce conversion cost.

The payload bay doors introduce a discontinuity into the existing shell form. An elementary moment calculation reveals that bending moment due to hydrostatic pressure at the lower discontinuities will be roughly five times greater than at the top of the cylinder (Table 11). This result suggests that significant reinforcement will be required at the payload bay doors.

Table 11. Bending Moment Due to Hydrostatic Pressure

Location	Bending Moment Due to Hydrostatic Pressure
Top Center	1.77×10^8 lb-ft
Bay Door Hinge	1.09×10^9 lb-ft

The DSOC design could be vulnerable to UNDEX, shock, and torsion loads. Although a complete dynamic analysis was beyond the scope of the feasibility study, the group recognized the issue by installing 3 deep frames: at the forward bulkhead (182'), at the aft bulkhead (220'), and just aft of the ROV Chamber (199'). Additionally, when the bay doors are shut they are hydraulically locked and mechanically secured to provide increased sectional rigidity.

Table 12 shows that the overall sectional modulus is only slightly reduced from the baseline model. (These calculations can be found in Appendix A.C.) Consequently, no difficulties are expected to arise from shear and bending.

Table 12. Moments of Inertia about the Neutral Axis

Sectional Design	Moment of Inertia about Neutral Axis
Baseline Cylinder	2.521×10^4 ft ⁴
DSOC Section	2.433×10^4 ft ⁴

4.1.9.2 Decking and Bulkheads

The DSOC contains three continuous decks supported as shock mounted rafts. For this reason, the decks are not credited as structural reinforcement. The second deck, mounted at 16'4" ABL, is intended to provide only limited longitudinal and lateral

stability for the ROV Lockout Chamber. Additional stiffeners are routed through the third deck that rigidly attach the upper portion of the ROV Chamber to the hull.

Watertight bulkheads enclose the DSOC fore and aft. The aft bulkhead is the existing RC bulkhead from the VIRGINIA Class Submarine design moved 46 ft further aft. The forward bulkhead design is based on a structural model developed in the 2001 design study, The Next Generation Nuclear Attack Submarine.¹⁷ The forward bulkhead incorporates 1.25" HY-80 plating with two 8" transverse beams and seven 3.5" Vertical Stiffeners. Details of this design can be reviewed in Appendix A.C.

4.1.9.3 ROV Chamber

The ROV Chamber is a cylinder 15' 6" in diameter and 22' 6" high with hemispherical upper and lower heads (Figure 20). The chamber was analyzed using an MIT MathCAD Structural Model.¹⁸ This model was used to calculate five hull limit states for the chamber based upon the assumptions that the chamber was a right circular cylinder with a ring-stiffened shell. The shell thickness is 2.00 inches. External 5"-deep ring frames surround the shell at 18" spacing. Table 13 shows the results of the analysis. The scantling selections provide adequacy for the five failure modes to depths far beyond 800 ft.

This model does not consider the effects of shock or UNDEX. Consequently, the scantling design reflects a great deal of conservatism. Future revisions in the chamber design would likely result in a beneficial weight reduction.

¹⁷. Ibid

¹⁸. Dave Johnson. "Program to Compute Suitability of Submarine Design Parameters," May 2001.

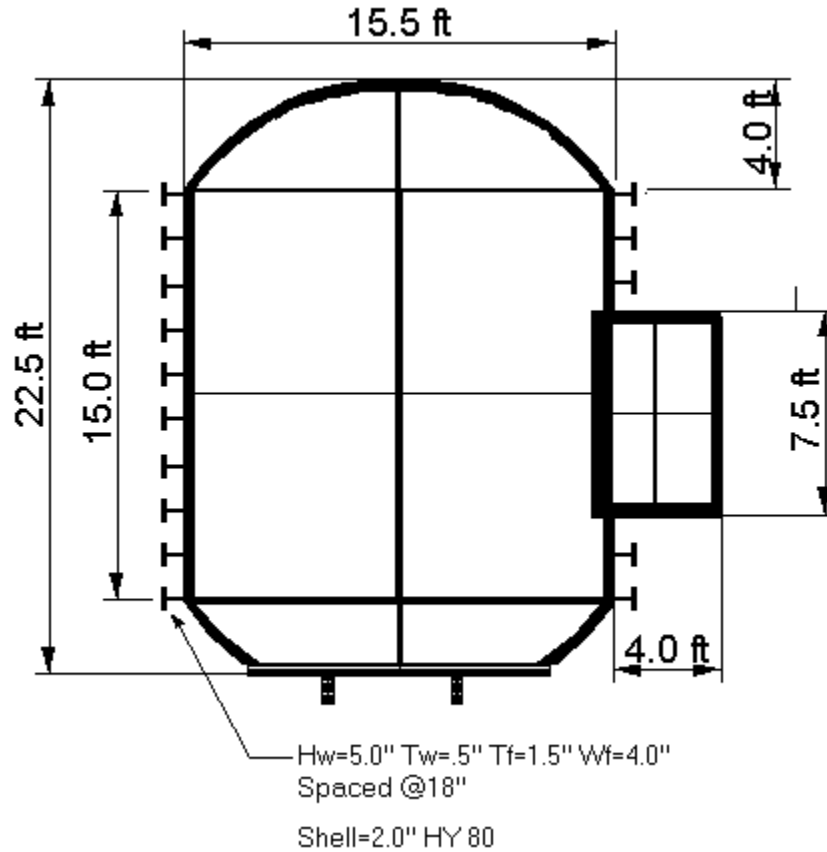


Figure 20. ROV Chamber Scantlings

Table 13. ROV Chamber Failure Mode Stress Ratio Summary

Failure Mode	$\sigma_{mode}/\sigma_{working}$
Lobar Buckling	.056
Shell Yield	.025
General Instability	.219
Frame Yield	.033
Frame Instability	.476

4.1.9.4 Payload Bay

Due to the unique geometry, the payload bay was the most critical and complex portion of the analysis (Figure 21). The side walls of the bay were modeled as a large gridded flat panels rigidly clamped at all edges. The analysis was based on equations

derived in Ship Structural Design that predict the behavior of stiffened panels under hydrostatic load.¹⁹

The Payload Bay cap was modeled as a ring stiffened cylinder using Johnson's MIT MathCAD Structural Model. The final design required HY-80 side and end walls 3 in. thick. Vertical stiffeners 6 in. deep are spaced at 21 in. intervals on the bay ends and at 24 in. intervals on the lateral walls. Transverse frames 8 in. deep are spaced at 4 ft intervals around the circumference of the bay. The bay's shell head uses a 2 in. HY-80 thickness with 3.25 in. ring stiffeners spaced at 14 in. intervals. The 2 in. cylindrical shell plating was selected in order to limit the difference in thickness between the bay wall and the shell head. This set of scantlings also provides structural adequacy to depths well beyond 800 ft.

Table 14. Payload Bay Shell Head Failure Mode Stress Ratio Summary

Failure Mode	$\sigma_{mode}/\sigma_{working}$
Lobar Buckling	.020
Shell Yield	.026
General Instability	.384
Frame Yield	.041
Frame Instability	.474

¹⁹. Owen F. Hughes. Ship Structural Design (Jersey City, New Jersey: The Society of Naval Architects and Engineers, 1988).

Table 15. Payload Bay Lateral Wall Failure Mode Stress Ratio Summary

Failure Mode	$\sigma_{mode}/\sigma_{working}$
Panel Serviceability Plate Transverse Bending	.750
Panel Serviceability Plate Longitudinal Bending	.776
Panel Collapse Membrane Yield	.750
Plate Failure Local Buckling	.030
Panel Yield Tension Flange	.203
Panel Yield Compression Flange	.203
Panel Collapse Stiffener Buckling	.203
Panel Collapse Stiffener Buckling	.804
Panel Collapse Stiffener Buckling 2 (eccentric load)	.653

Table 16. Payload Bay End Wall Failure Mode Stress Ratio Summary

Failure Mode	$\sigma_{mode}/\sigma_{working}$
Panel Serviceability Plate Transverse Bending	.750
Panel Serviceability Plate Longitudinal Bending	.725
Panel Collapse Membrane Yield	.741
Plate Failure Local Buckling	.023
Panel Yield Tension Flange	.996
Panel Yield Compression Flange	.254
Panel Collapse Stiffener Buckling	.031
Panel Collapse Stiffener Buckling	.798
Panel Collapse Stiffener Buckling 2 (eccentric load)	.652

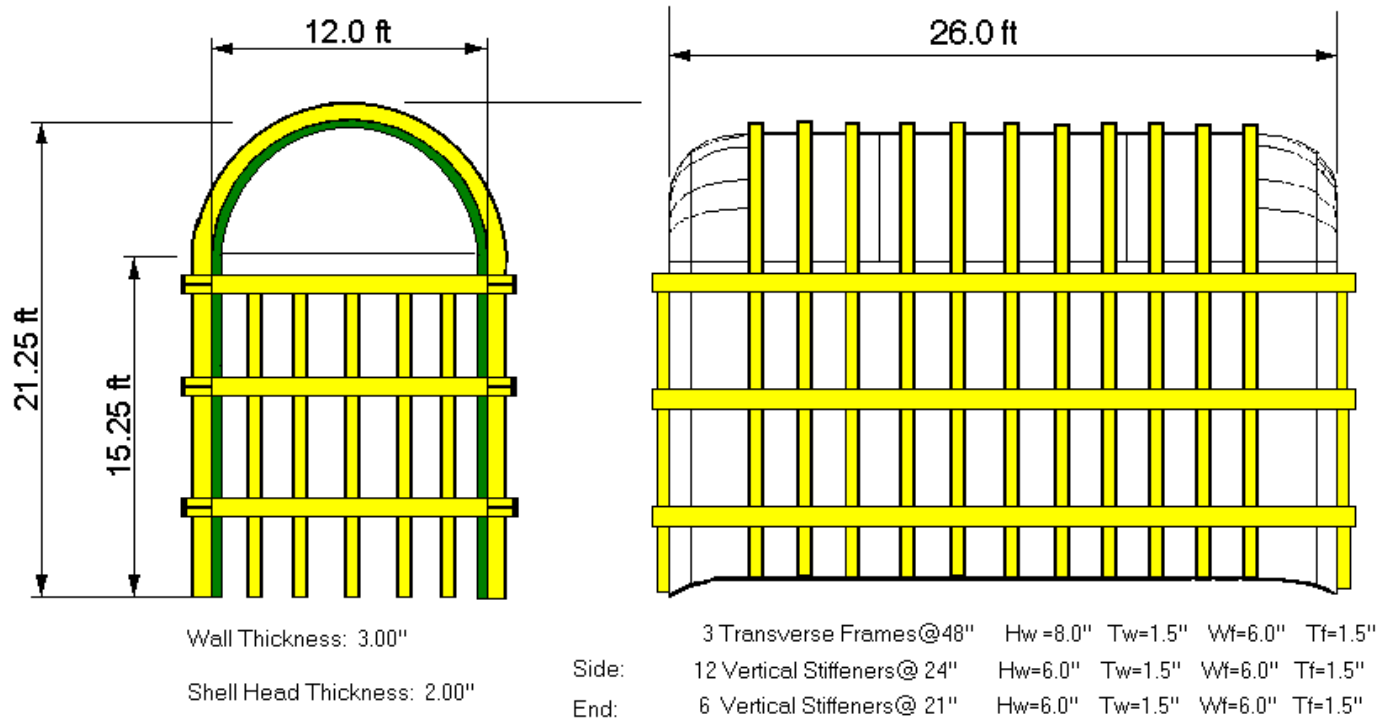


Figure 21. Payload Bay Scantlings

4.1.10 Weights and Stability

4.1.10.1 Baseline Ship Balance

The MIT Submarine MathCAD Model of the balanced VIRGINIA Class Submarine was used in the analysis.²⁰ This model was based upon parametrically derived data.

4.1.10.2 DSOC Balance

The DSOC weight was calculated on an item-by-item basis that required detailed, evolved drawings. Weight estimates for specific pieces of equipment or structure were based on known data from existing platforms. Parametric weight group calculations were used as a second check, but due to its unique function and arrangement, the DSOC was not expected to fall within historical design lanes. In fact, the DSOC weighs approximately 40% more than predicted by historical parameters.

Vertical and longitudinal locations and moments were also estimated and tracked with assistance of the drawing. The A-1 vertical center of gravity (VCG) is 16.63 ft and the longitudinal center of gravity (LCG) is 18.62 ft aft of the DSOC's forward bulkhead. Table 17 shows the DSOC Weight and Stability characteristics. Detailed weight and moment data is included as Appendix E.

Table 17. DSOC Weight Summary

Weight Condition	PLUG Weight (lton)	VCG (ft)	LCG (ft)
A-1	881.20	16.63	200.62
Lead	25.32	4.00	203.00
A	906.52	16.28	200.69
Variable Load	32.53	12.69	201.71
Variable Ballast	60.00	9.45	217.61
NSC	999.05	15.75	201.74
MBT	159.61	10.70	213.50
SUBMERGED	1158.66	15.15	209.07

²⁰. Reed and Walsh

4.1.10.3 Modified Ship Balance

The addition of the DSOC plug and its additional Main Ballast Tank (MBT) had a significant impact on the ship's overall longitudinal balance. The section's submerged center of gravity is 16.7 ft aft of the ship's submerged longitudinal center of buoyancy (LCB). MBT modifications were necessary in order to both balance the ship and to preserve the required 12.5% Reserve Buoyancy (ROB).

An Integrated Bow Conformal Array (IBC) sonar was selected to replace the spherical array, since this modification is already planned for future platforms. This allows the forward bulkhead of MBT 1 to be moved forward by 2.9 ft. This alteration, combined with the removal of the sonar sphere access tunnel results in a 48-ton increase in the ship's MBT capacity centered at 19.58 ft aft of the forward perpendicular (FP). The IBC modification was not sufficient to correct the ship's submerged trim condition. Syntactic foam was inserted into the after-most MBT (formerly MBT 5). The 3643 ft³ (77.8 lton) foam volume permanently displaces 103.8 tons of MBT capacity, bringing the ship's new ROB to 12.8%. Additionally, the foam provides a net buoyancy of 26 lton centered at 374.63 ft. Figure 22 summarizes the modifications. Trim lead and the ship's variable ballast brought the ship to a final longitudinal balance.

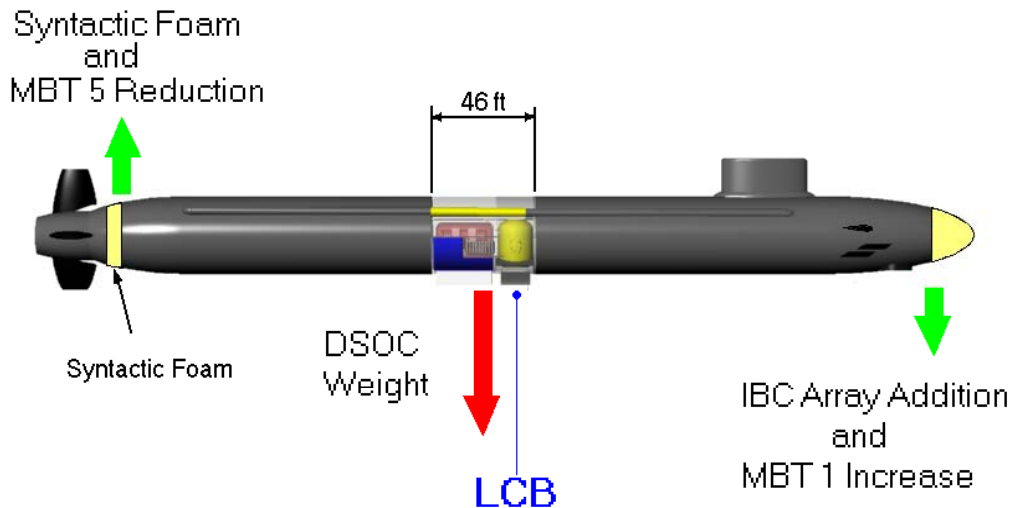


Figure 22. Longitudinal Balance Corrections

4.1.10.4 Equilibrium Polygon

The group analyzed for worst-case variable load conditions according to standard design practice as specified in NSTM 9290. Since this platform carries a particularly large payload item, two 65-ton DSOC compensation tanks were necessary in order for the ship to conduct retrieval operations in all environments and load conditions, including arctic conditions. Figure 23 shows the Equilibrium Polygon with the addition of payload compensation tanks. In the Heavy 2 condition, the ship maintains a 70-lton margin. The extreme Light Condition remains close to the trim system limits (5-lton margin). It is important to note however, that the Light Condition design water density (64.3 lb/ft^3) is normally encountered at deeper depths, which implies that the Light Condition will migrate downward on the Equilibrium Polygon due to hull and SHT compression. In short, the small Light Condition margin was viewed as an acceptable compromise in preserving the ship's arctic capabilities. Table 18 shows the seawater densities assumed for the various load conditions. Detailed variable load calculations can be found in Appendix E.

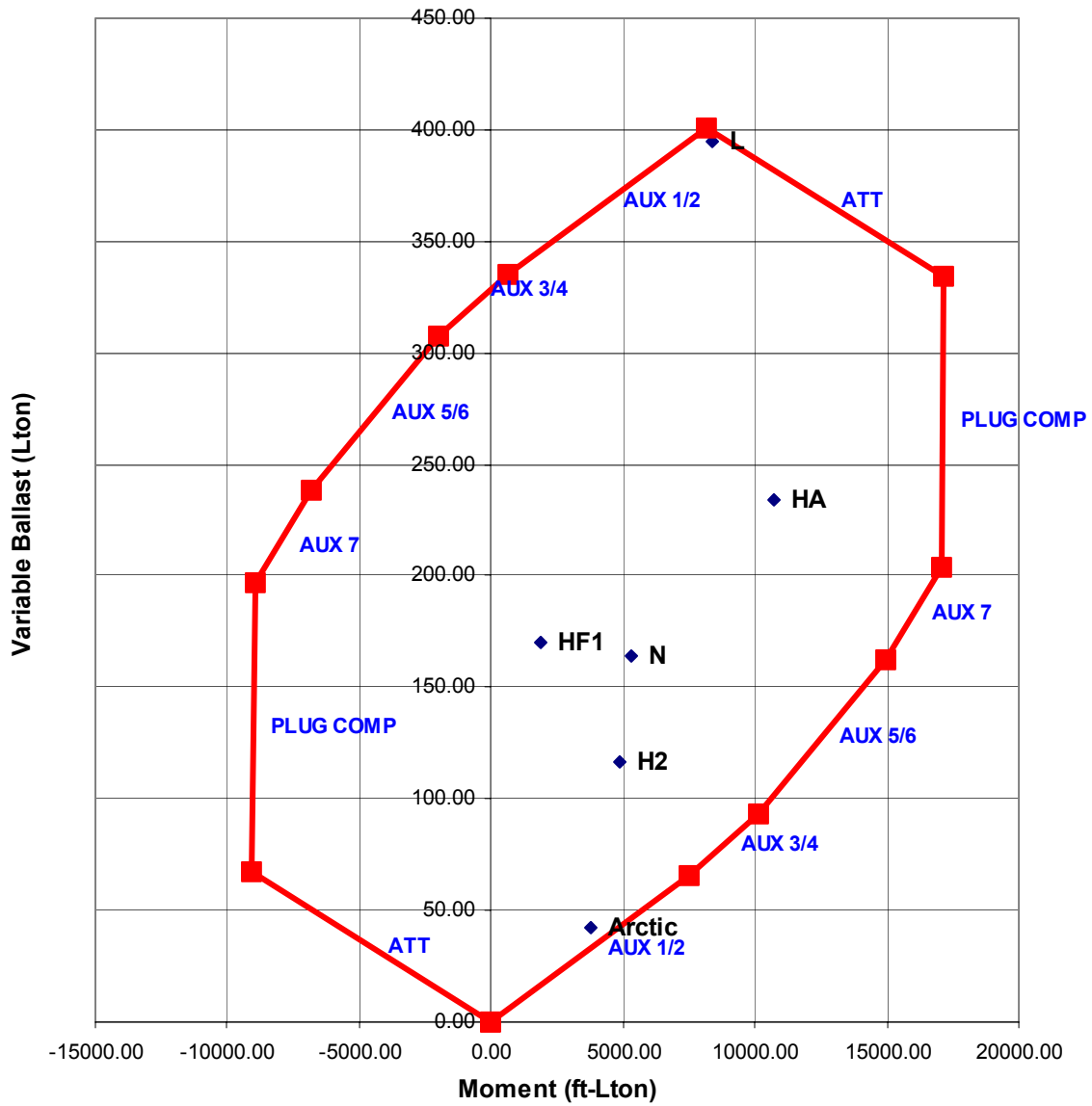


Figure 23. Equilibrium Polygon

Table 18. Seawater Density Assumptions

Condition	Density (lb/ft³)
Normal (N)	64.0
Heavy aft (HA)	63.6
Heavy Forward (HF1)	63.6
Heavy Overall (H2)	63.6
Arctic	63.0
Light (L)	64.3

4.1.10.5 Lead Solution

The lead solution requires 209.7 lton of Stability Lead centered at 221.56 Ft and 290.5 lton of Margin Lead centered at 192.06 ft (for an overall total of 500.27 lton centered at 204.43 ft). The modified design increases the baseline ship's overall lead weight by 145.9 lton. This lead addition is offsets the DSOC's excess buoyancy and fine-tunes the longitudinal balance. If the need arose, stability lead could easily be replaced by permanent weight additions to the DSOC Module. Table 19 summarizes the complete lead solution. Final Ship Weights and Centers of Gravity are shown in Table 20.

Table 19. Lead Solution Summary

Lead	Weight (lton)	LCG (ft)	VCG (ft)
Stability	209.76	221.56	3.00
Margin	290.51	192.06	17.00
Overall	500.27	204.43	11.13

Table 20. Ship Weights and Centers

	Weight (lton)	L. Arm (ft)	V. Arm (ft)	Weight (lton)	L. Arm (ft)	V. Arm (ft)
Group / Condition	Baseline			DSRS		
100	2778.5			3454.69		
200	1348.6			1348.55		
300	246.6			268.22		
400	167.3			199.05		
500	741.8			893.58		
600	505.4			504.45		
700	260.3			260.35		
Condition A-1:	6048.4	182.9	16.2	6903.93	197.88	16.63
Lead:	354.4	158.6	14.2	500.27	204.43	9.90
Condition A:	6402.8	181.5	16.1	7404.20	198.32	16.18
VL	562.2	121.4	13.2	456.97	195.44	11.39
NSC:	6965.1	176.7	15.9	7861.17	198.15	15.98
MBT:	875.8	148	16.8	1009.55	144.63	16.19
Submerged:	7840.8	173.4	16.0	8870.72	192.06	16.00

4.1.10.6 Surfaced Stability During Extreme Load Cases

Trim and stability were analyzed in the surfaced condition in various ballasted and unballasted load conditions. The arrangement of the DSOC raises several issues regarding surface stability. On the surface the ship must compensate for the full dry weight of the retrieved payload (56 lton), rather than the waterborn weight of 14.7 ltons. The ship must also compensate for the free surface effect in the mid-ship MBT. The free surface correction (FSC) due to the additional MBT was calculated to be quite small, 0.01 ft, because the tank is long and narrow in its dimensions. Since the DSOC section is located close to the ship's LCB, extreme load cases in the DSOC plug have very little effect on

the ship's trim. Table 21 and Table 22 show the results of the stability analyses. The ship is stable under all load conditions.

Table 21. Extreme Load Case Stability Parameters

Payload (lton)	Midship Ballast (lton)	Draft (ft)	Trim by Stern (ft)	GM_T (ft)
56	220 (ROV Tank Full)	29.4	7.7	1.80
56	130	29.0	7.0	1.50
56	0	28.4	6.2	1.00
0	0	28.1	5.9	.93

Table 22. Normal Surface Condition Stability Parameters

	Baseline	Variant (With Payload)	Variant (Without Payload)
Normal Δ_{Surf} (lton)	6965	8003	7961
Mean Draft (ft)	28.18	28.55	28.30
Trim (ft)	5.52	6.40	6.00
KM_T (ft)	17.01	17.00	17.00
KG (ft)	15.85	15.86	15.98
GM_T (ft)	1.16	1.12	1.05
Roll Period (sec)	11.1	12.3	13.9

4.2 Performance Analysis

The addition of the DSOC will affect the performance of the submarine primarily by making it more stable and slower. The DSRS will be expected to turn slower and have a larger turning radius than the VIRGINIA Class Submarine. The DSRS will also be 11% slower than the VIRGINIA Class Submarine. The speed reduction is based upon the increased friction drag due to more wetted surface area. The complete calculations

regarding speed are contained in the Submarine MathCAD model contained in Appendix B.²¹

4.3 Operation and Support

The DSRS will require additional support to unload the recovered object at its destination. This process will be complicated because the only way to unload the object is out the bottom of the ship. This can be performed by having the lift frame lower the object beneath the ship and carefully transfer the load to a crane. This can also be accomplished by lowering the object onto the sea floor in a safe, shallow area and having a crane lift it directly from the bottom.

The DSRS will also require additional support in the form of parts and technicians to maintain the added equipment.

4.4 Cost

The DSRS estimated to cost \$650 Million above the cost of the Baseline VIRGINIA Class Submarine. Cost was estimated using the Very Simplified Cost Model portion of the MIT Submarine Math Model. Table 23 shows the parameters used.

Labor rate is the key parameter in determining the total cost of the ship. However, the DSRS conversion represents only a 20% increase over the cost of the Baseline VIRGINIA Class Submarine regardless of the labor cost selected (Figure 24). This team looked at labor costs ranging from \$50 to \$150 per man-hour. The lower rate comes from a study performed in 1991 and does not reflect inflation or other variables such as changes in the labor market. The higher rate comes from a new construction design performed recently and includes significantly more of the expensive new design labor than the DSRS conversion will require.

²¹ Galvin et al.

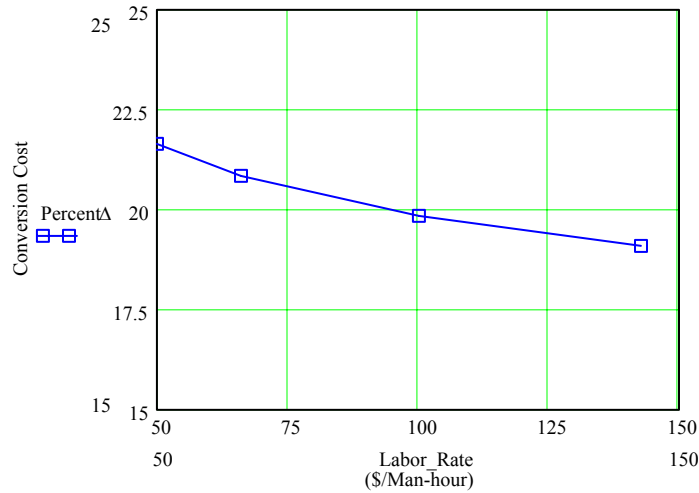


Figure 24. Percentage Change in Baseline VIRGINIA Submarine Cost due to DSRS Conversion

Table 23. Cost Estimating Parameters

Labor Rate	\$50 - \$150 per man-hour
Overhead Factor	1.5
Profit Rate	.11

The cost of the ROV and lift equipment will not be significant in the overall cost of the ship. Table 24 shows the cost of the various portions of the ROV System. The Lift System is expected to cost a similar amount.

Table 24. ROV and Support Equipment Cost

Item	Cost
TRITON ZX ROV	\$775,000
ROV Optional Equipment	\$250,000
Control Consoles	\$300,000
Tether Management System	\$350,000
Power System	\$60,000
System Spares	\$250,000
Total Cost	\$1,985,000

5.0 Design Conclusions

5.1 Summary of Final Concept Design

The Deep Sea Research Submarine final concept design consists of VIRGINIA Class Submarine design modified by the insertion of a 46-ft Deep Sea Operations Compartment. Table 25 gives the principle characteristics. The DSRS is capable of supporting ROV operations and heavy lift operations in addition to performing all the combat missions of a standard VIRGINIA Class Submarine. The DSRS meets the requirements of the study.

Table 25. Deep Sea Research Submarine and Deep Sea Operations Compartment Characteristics

Deep Sea Research Submarine	
Length	423 ft
Diameter	34 ft
Speed Reduction	11%
Surfaced Displacement	7861 lton
Submerged Displacement	8870 lton
LCG	192.06 ft
VCG	15.98 ft
GM _T	1.05 ft
Reserve Buoyancy	12.8%
Deep Sea Operations Compartment	
Length	46 ft
NSC Weight	999.1 lton
Submerged Lifting Capacity	14.7 lton
Maximum ROV Depth	9800 ft
Maximum Retrieval Depth	> 2400 ft
Conversion Cost	\$650 million

5.1.1 ROV Operations

The capability to perform ROV operations allows the submarine to perform missions far deeper than warships have been able to go before. These deep-sea missions include:

- Object inspection
- Object manipulation
- Small object retrieval
- Water sample retrieval
- Biological observation
- Geological sampling.

All of these missions can be performed at depths up to 9800 ft using the TRITON ZX ROV.

5.1.2 Heavy Lift Capability

The ship's heavy lift system permits it to perform missions of interest to both the military and scientific communities. The DSRS's specific capabilities include:

- Submerged lifting capacity of 14.7 tons from depths greater than 2400 ft
- Storage within the submarine's envelope for retrieved objects up to 23.5 ft L x 10.5 ft H x 6 ft W
- Remote operation of the lifting frame.

5.2 Final Conversion Design Assessment

This study responds to the need for a multi-mission submarine capable of performing deep-sea scientific and military missions. Based on the results of this study, the design group concludes that the U.S. Navy should expand research and funding in support of the Deep Sea Research Submarine. The group recommends reinforcing relationships with commercial ROV builders and oceanographic research institutions and including experienced deep sea salvors in the design process.

The proposed VIRGINIA modification incorporates very little high-risk technology. The departure from use of the traditional cylindrical hull section represents a design challenge, but the skills and analytical tools exist to overcome these basic engineering issues. Although the large-scale investment in ROV equipment presents some

uncertainty, the technology required to successfully carry out the proposed DSRS mission is mature.

5.3 Areas for Further Study

This study examines the deep-sea concept for preliminary feasibility. Many areas still require additional attention. Specific items for further study and analysis, including detailed engineering studies, include:

- In depth structural analysis (including dynamic loading) of the Payload Bay and ROV Chamber, specifically in the region of the hull-bay unions.
- Detailed survey of ROV manufacturers to determine existing and future ROV capabilities as well as the suitability of those ROV's for the missions of interest.
- Detailed cost model formulation for installation of heavy lift and ROV equipment.
- Survey of deep sea salvage experts to fully assess the current state of technology and the current and projected needs of the salvage community
- Comprehensive assessment of ROV maneuvering and control problems from a submerged platform
- Comprehensive study of precise submarine stationkeeping when operating with an ROV or performing a heavy lift.
- Hydrodynamic and maneuvering analyses of the modified ship
- Analysis of flow and transient noise
- Analysis of DSOC effects on ship systems such as HVAC.

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Appendices

A. Mission Need Statement

For

Deep Sea Research Submarine

1. Defense Planning Guidance Element

A. This Mission Need Statement (MNS) provides requirements for a multi-mission submarine with deep-sea research capability for the 21st century battle force vision. Through technology investment and insertion, the Deep Sea Research Submarine (DSRS) will be able to perform deep-sea research missions in addition to all the missions of a fast attack submarine. This submarine must operate wherever required to enable joint maritime expeditionary force operations, project precise strike power ashore, and conduct scientific and military research missions. The mission capabilities must be fully interoperable with other naval, interagency, joint and allied forces.

B. This unclassified MNS in part addresses Joint Vision 2020 published in June 2000. This document outlines the vision for creation of a force that “is dominant across the spectrum full spectrum of military operations – persuasive in peace, decisive in war, preeminent in any form of conflict”. Additionally, the document addresses “the need to prepare now for an uncertain future”.^[22]

C. The deep sea research functions described in this MNS address the requirements set forth in Joint Vision 2020 to have “access to and freedom to operate in all domains”^[23] as well as support the information superiority that has been regarded as a key enabler of victory.^[24]

D. This MNS should guide 21st century DSRS design, research, development and acquisition program decisions, service and joint doctrine, and cooperative efforts with U.S. allies.

²². Chairman of the Joint Chiefs of Staff, Joint Vision 2020 (Washington, D.C.: US Government Printing Office, 2000). 1

²³. *Ibid.*, 8

²⁴. *Ibid.*, 10

2. Adversary Capabilities Analysis

As a result of the 2001 Quadrennial Defense Review, the basis of defense planning has been shifted from a threat-based model to a capabilities-based model. The capabilities-based model focuses on how an adversary might fight instead of who that adversary might be. This model recognizes that planning for large wars in distant theaters is not sufficient. The United States must also plan for adversaries who will rely on surprise, deception and asymmetric warfare to meet their objectives. ^[25] Adversary capabilities will include asymmetric approaches to warfare that include terrorism and weapons of mass destruction.

In the past, the large distances between adversaries and the United States have provided a significant level of protection. As the events of September 11, 2001 illustrate, the U.S. can no longer rely upon this geographic protection. The rise of international travel and trade has made even the United States homeland vulnerable to hostile attack. ^[26]

Makers of national strategy will need to consider the rise and decline of regional powers. Some of these states are vulnerable to overthrow by radical or extremist internal forces. Many of these states have large armies and the capability to possess weapons of mass destruction. ^[27] In some states, the governments are unable to their territories from serving as sanctuaries for terrorists and criminals which may pose threats to the safety of the United States. In these cases, “threats can grow out of weakness of governments as much as out of their strength.” ^[28]

Asymmetric warfare, reduced protection from geographical distances, and vulnerabilities of foreign governments result in the need for the United States to maintain the ability to gather intelligence in all forms and in all areas of the globe. A key element in intelligence gathering is the ability to recover objects from the sea floor.

²⁵. Department of Defense, Quadrennial Defense Review Report (Washington, D.C.: US Government Printing Office, 2001). iv

²⁶. Ibid., 4

²⁷. Ibid.

²⁸. Ibid., 5

3. Mission Analysis

A. Mission. The general mission of this ship is to perform specialized military and scientific missions in deep water and on the ocean floor. The ship must be able to independently transit to the mission location, perform military and scientific missions of interest, and return to its base of operations without additional support from other vessels. In addition, the ship must be able to perform all of the missions of a modern fast attack submarine.

B. Military Mission Needs

- 1) Systems Manipulation/Implantation/Control. The vessel must be able to implant mission related objects in precise locations and manipulate objects found in the ocean.
- 2) Recovering Objects. The vessel must be able to recover objects that have been located by onboard or off-board sensors.
- 3) Disabling/Removing Objects. The vessel must be able to manipulate and/or remove objects of military interest.
- 4) Area Sanitization/Investigation. The vessel must be able to locate other vessels or objects within its operating area.
- 5) Intelligence, Surveillance and Reconnaissance. The vessel must be able to monitor a region of interest and communicate the results of that monitoring with higher authority.
- 6) Support to Military Research and Development. The vessel will be an integral part of Department of Defense research and development related to the ocean.
- 7) Gatekeeper. The vessel must be able to alert higher authority of the passage of vessels of interest through its operating area.
- 8) Diver/Special Operations Forces Support. The vessel must be able to transport divers or Special Forces to their launch points, remain on location while the mission is being conducted, conduct launch and recovery operations, and transport the divers or Special Forces to their destination.
- 9) Search and Rescue. The vessel must be able to conduct search and rescue operations.

C. Scientific Mission Needs. The vessel must be able to conduct research in a variety of scientific fields including:

- 1) Physical Oceanography.
- 2) Ice Science.
- 3) Geology/Geophysics.
- 4) Marine Biology.
- 5) Atmospheric Science.
- 6) Ocean Engineering
- 7) Chemical Oceanography
- 8) Maritime Archeology
- 9) Environmental Science

D. Capabilities and Requirements of the Deep Sea Research Submarine or a Remote Operated Vehicle

- 1) Access to three times the Virginia Class maximum operating depth. Deeper excursions are dependent on the ROV.
- 2) Operation in 1.5 knot beam current at ROV depth.
- 3) Endurance same as Virginia Class.
- 4) Heavy lift to 33,000 lbs net at the maximum operating depth. Carrying capability of 23'L x 10.5'H x 6'W.
- 5) Assume Quest and Triton as minimum requirements for ROV's.
- 6) Maximize modularity.
- 7) Maintain the current stealth level of the host submarine in transit.
- 8) Maintain UNDEX capability of host ship. Payload does not have to be shock hardened.
- 9) Maintain minimum required values for host GM, BG, reserve buoyancy, non-nuclear margin, seawater density range, and loads provided for. If this is not feasible, quantify trade-offs.

4. Potential Non-Materiel Alternatives

Potential non-materiel alternatives were examined based upon the military and scientific mission needs. Changes in doctrine or service life extension were not sufficient to address mission requirements.

A. U.S. or Allied Doctrine: Doctrine changes required without a Deep Submergence Research Submarine include: Inability to search for objects of interest on the ocean floor in all weather and for extended periods of time. Inability to recover and manipulate objects of interest on the ocean floor in all weather and for extended periods of time. A deep submergence research submarine is the only type of platform capable of performing these missions. Changes in operational doctrine will not accomplish these missions.

B. Extension of rated hull life: The current deep-sea nuclear submarine is nearing the end of its life. The operating depth could be reduced and the hull life extended, but this reduces the capabilities of the vessel and does not provide a long-term solution.

5. Potential Materiel Alternatives

A. Alternative design concepts include:

- 1) Design of an entirely new class of submarine.
- 2) Modification of an Improved Los Angeles Class Design to meet the mission requirements.
- 3) Modification of a Ohio Class Design to meet the mission
- 4) Modification of a Seawolf Class Design to meet the mission requirements.
- 5) Modification of a Virginia Class Design to meet the mission requirements.

B. The ongoing Virginia acquisition program could potentially address this need through a modified repeat program by capitalizing on advanced technology. However, to do this, it would need to employ a significantly different architectural approach in the design.

C. As part of their shipbuilding programs, various Allies have combat, hull, mechanical and electrical system programs ongoing or under development that offer possible cooperative opportunities. These subsystem designs will be examined. All meaningful cooperative opportunities can be realized without a formal cooperative development program for a research vessel.

6. Constraint

A. Key Boundary Conditions.

- 1) Architecture - The ship design must employ a total ship architectural/engineering approach that optimizes life cycle cost and performance, minimizes operating conflicts, permits rapid upgrade and change in response to evolving operational requirements, and allows computational and communication resources to keep technological pace with commercial capabilities. More specifically, this implies physical element modularity; functional sharing of hardware; open systems information architecture; ship wide resource management; automation of Command, Control, Communications, and Computers (C4I), and navigation functions; integrated ship wide data management; automation and minimization of maintenance and administrative functions; and embedded training.
- 1) Design - Consideration should be given to the maximum use of modular designs in the research vessel's infrastructure. Emerging technologies must be accounted for during the developmental phase. Since communication and data systems hold the greatest potential for growth, and therefore obsolescence, their installations must be modularized as much as possible to allow for future upgrades. Systems onboard must use standard man-to-machine interfaces. The man-to-machine interfaces should be consistent with existing user-friendly systems.
- 2) Personnel - The ship must be automated to a sufficient degree to realize significant manpower reductions in engineering, ship support and watchstanding requirements. Preventive maintenance manpower requirements must be reduced by incorporating self-analysis features in equipment designs and by selecting materials and preservatives that minimize corrosion.

B. Operational Constraints.

- 1) The DSRS must remain fully functional and operational in all environments, whether conducting independent or force operations; in heavy weather; or in


the presence of electromagnetic, nuclear, biological and chemical contamination.

- 2) The DSRS must provide ROV launching and recovery facilities.
- 3) The DSRS must be able to operate in U.S., foreign, and international waters in full compliance with existing U.S. and international pollution control laws and regulations.
- 4) All ship system elements must use standard subsystems and meet required development practices.
- 5) The DSRS must be able to embark Special Operations Forces (SOF) when required for selected missions.
- 6) The DSRS must be able to transit through the Panama Canal.

B. MIT XIII MathCAD Submarine Model

Results included in report. Refer to 13A Program Office at MIT.

TRITON ZX Parameters




TRITON[®] ZX

Heavy Duty Work Class ROV

- Depth Rating3000 MSW
- Power.....100/150 Hp
- Through Frame Lift3000kg
- Control SystemSingle Mode
Fibre Optic P.C. Based
- Lift Point.....Variable
- Payload Capacity.....200kg

ERRY



PERRY & SON

TECHNICAL SPECIFICATION

Dimensions	
Length (mm)	2400
Width (mm)	1520
Height (mm)	1850
Depth Rating (m)	3000
Weight in Air (kg)	3000
Payload Capacity (kg)	200
Power Pack (Shaft kW/HP)	75/100
Thruster Horizontal (mm Ø)	4 x 305
Thruster Vertical (mm Ø)	3 x 305

Ballast Pull (Neutral)	
Forward (kgf)	450
Lateral (kgf)	450
Vertical (Up) (kgf)	400
Lift Capacity (kg)	3000

- Standard Fit
 - Gyro/Fluxgate Compass
 - Pitch/Roll Sensor
 - Digiquartz Depth Gauge
 - Auto Functions (Heading/Depth/Altitude)
 - General Function Valve Pack (12 Functions)
- Interfaces For
 - Manipulator (Left/Right)
 - Sonar
 - Hydraulic tool interfaces
- Telemetry
 - Realtime video channels (8)
 - Spare fibre optic interface card slot (1)
 - Customer solenoid valve drivers (pre-wired) (8)
 - 13" colour video monitor (1)
 - Customer digital out (8)
 - Customer digital in (8)
 - Customer analogue out (4)
 - Customer analogue in (8)
 - Full duplex RS232 @11.5kpbs data channels (4)
 - Full/half duplex RS485/422/232 @11.5kpbs channels (4)
 - Voltage meters for input power and all switching controls
 - Customer analogue in (8)
- Power Distribution
 - 140 KVA transformer for vehicle hydraulics (1)
 - 6.5 KVA transformer for vehicle electronics (1)
 - 7.5 KVA transformer for TMS-HPU (1)
 - Ground fault detection circuits
 - Deck Cable Interface



VEHICLE OPTIONS

- Four function thruster manifold (proportional valves) (1)
- Ten function auxiliary valve manifolds (2)
- Hydraulic pump control manifold
- Heading Control, automatic or manual
- Depth Control (automatic) 115 cm
- Lighting system (3000 watts total)
- 500 watt lights on dimming circuits available (8)
 - Circuits w/2x250 watt lights per standard (8)
- Pan and tilt - standard (1)
- Depth Sensor
 - High accuracy sensor, 0.1% over full scale for depth control (auto depth) and depth determination

SYSTEM OPTIONS

- Main Umbilical
 - Arched/Soft
- Surface Handling
 - 'X' Frame/Crane System
 - Winch to Customer Specification
- Control Cabin
 - Certified/Zone Rated
- Control Console
 - 5 Bay Ergonomically Designed
 - Graphics/Video/Sonar Monitors
 - Video Overlay/Switching/Recording
 - Surface Communications
 - Manipulator Control
- Tether Management System
 - Tophat or Garage
 - 200 metres Tether (Tophat)
 - 750 metres Tether (Garage)
 - 3000 metres Depth Rating
- Workholds
 - Survey & Bathymetric suites
 - Tether Management Systems
 - Launch and Recovery systems
 - Umbilical Winch
 - Control/Work Yarn

Ings Lane, Kirkstynesside, York YO62 0EJ, England
 Tel: +44 (0) 1751 431751 Fax: +44 (0) 1751 431388
 email: post@uk.perry.com



PERRY SLINGSBY SYSTEMS
 Air, Sea & Space Services

821 Jupiter Park Drive, Jupiter, Florida 33458-3046 USA
 Tel: +1 561 743 7000 Fax: +1 561 743 1313
 email: post@us.perry.com

www.perryslingsbysystems.com

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01/2001

C. Structural Design

ROV Chamber Shell Analysis

**PROGRAM TO COMPUTE SUITABILITY
OF SUBMARINE DESIGN PARAMETERS.**

Ref: "Hull Material Trade Off Study", D Fox, Jan 94
PNA 1967, CAPT Harry Jackson Submarine Design Trends

*Revised June 2000
CDR Dave Johnson*

ROV CHAMBER SHELL ANALYSIS

This program computes the safety factors of the following criteria given hull material, scantlings and dimensions:

- a. Shell Yielding;
- b. Shell Lobar Buckling;
- c. Elastic General Instability;
- d. Frame Yielding; and
- e. Frame Instability.

Define input parameters:

Note: Global variables are used for iteration purposes. Inputs are at the end of this spreadsheet.

Compute areas: $R_f := R - \frac{t_p}{2}$ Frame Radius $R_f = 94.4\text{in}$ *Frame Area = Flange + Web*

Frame flange, web area: $A_f := t_f \cdot w_f$ $A_w := t_w \cdot h_w$ $A := A_f + A_w$ $A = 8.5\text{in}^2$

Compute structural efficiency (buoyancy ratios):

$$\Delta := \frac{\rho \cdot R^2 \cdot L_f}{2 \cdot \rho_{st} \cdot \left[\left(R - \frac{t_p}{2} \right) \cdot L_f \cdot t_p + \left(R - t_p - \frac{h_w}{2} \right) \cdot t_w \cdot h_w + \left(R - t_p - h_w - \frac{t_f}{2} \right) \cdot w_f \cdot t_f \right]}$$

$\Delta = 2.605$ Shell Weig ht Frame Web Weight Frame Flange Weight

$\frac{1}{\Delta} \cdot 100 = 38.382$ % - Shell and Frame Weight of 1 Frame Bay as a % of Displaced Water

PART 1 SHELL YIELDING

Safety factor is (1.5 oper depth): $SF_{sy} := 1.5$

Von Sanden and Gunther (1952)
PNA Section 8.4

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{sy}$ $P = 669.799 \text{ psi}$

Area ratio $B := \frac{t_w \cdot t_p}{A + t_w \cdot t_p}$ Slenderness parameter: $\theta := L_f \cdot \left[\frac{3 \cdot (1 - \nu^2)}{(R \cdot t_p)^2} \right]^{\frac{1}{4}}$ Deflection coefficient: $N := \frac{\cosh(\theta) - \cos(\theta)}{\sinh(\theta) + \sin(\theta)}$

$B = 0.105$ $\theta = 1.675$

Frame flexibility parameter: $\beta := \frac{2 \cdot N}{A + t_w \cdot t_p} \cdot \left[\frac{1}{3 \cdot (1 - \nu^2)} \right]^{0.25} \cdot \sqrt{R \cdot t_p^3}$ Frame deflection parameter: $\Gamma := \frac{\left(1 - \frac{\nu}{2}\right) - B}{1 + \beta}$

$\beta = 3.633$

Bending effect (mem): $H_M := -2 \cdot \frac{\sinh\left(\frac{\theta}{2}\right) \cdot \cos\left(\frac{\theta}{2}\right) + \cosh\left(\frac{\theta}{2}\right) \cdot \sin\left(\frac{\theta}{2}\right)}{\sinh(\theta) + \sin(\theta)}$ $\Gamma = 0.161$

$H_M = -0.923$

Bending effect (bend): $H_E := -2 \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot \frac{\sinh\left(\frac{\theta}{2}\right) \cdot \cos\left(\frac{\theta}{2}\right) - \cosh\left(\frac{\theta}{2}\right) \cdot \sin\left(\frac{\theta}{2}\right)}{\sinh(\theta) + \sin(\theta)}$ $H_E = 0.397$

Midbay shell stress is calculated:

Bending effect near frame:

$$K := \frac{\sinh(\theta) - \sin(\theta)}{\sinh(\theta) + \sin(\theta)}$$

Circumferential Stress

PNA #

Longitudinal Stress

$$\sigma_{\phi\phi o} := \frac{-P \cdot R}{t_p} \cdot [1 + \Gamma \cdot (H_M + \nu \cdot H_E)]$$

outer

$$\sigma_{xxso} := \frac{-P \cdot R}{t_p} \cdot (0.5 + \Gamma \cdot H_E)$$

(20b)

$$\sigma_{\phi\phi i} := \frac{-P \cdot R}{t_p} \cdot [1 + \Gamma \cdot (H_M - \nu \cdot H_E)]$$

inner

$$\sigma_{xxsi} := \frac{-P \cdot R}{t_p} \cdot (0.5 - \Gamma \cdot H_E)$$

Shell stress at frames is:

$$\sigma_{\phi\phi o} := \frac{-P \cdot R}{t_p} \cdot \left[1 - \Gamma \cdot \left[1 + \nu \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot K \right] \right]$$

outer

$$\sigma_{xxfo} := \frac{-P \cdot R}{t_p} \cdot \left[0.5 - \Gamma \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot K \right]$$

(20d)

$$\sigma_{\phi\phi i} := \frac{-P \cdot R}{t_p} \cdot \left[1 - \Gamma \cdot \left[1 - \nu \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot K \right] \right]$$

inner

$$\sigma_{xxfi} := \frac{-P \cdot R}{t_p} \cdot \left[0.5 + \Gamma \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot K \right]$$

$$\sigma_{sy} := \begin{pmatrix} \sigma_{\phi\phi so} \\ \sigma_{\phi\phi si} \\ \sigma_{xxso} \\ \sigma_{xxsi} \\ \sigma_{\phi\phi fo} \\ \sigma_{\phi\phi fi} \\ \sigma_{xxfo} \\ \sigma_{xxfi} \end{pmatrix} \quad \sigma_{sy} = \begin{pmatrix} -2.782 \times 10^4 \\ -2.66 \times 10^4 \\ -1.802 \times 10^4 \\ -1.393 \times 10^4 \\ -2.558 \times 10^4 \\ -2.805 \times 10^4 \\ -1.185 \times 10^4 \\ -2.01 \times 10^4 \end{pmatrix} \text{ psi}$$

sy_0 Midbay, circumferential stress, outer shell surface $j := 1..8$
 \vdots
 \vdots
 \vdots
 \vdots
 \vdots
 \vdots
 sy_7 At Frame, longitudinal stress, inner shell surface

← key for Henky-Von Mises calculation below

Now according to Henky-Von Mises (max distortion theory) applied at mid bay(outer) and frame(inner):

HJ Notes, p. 22

$$\sigma_1 := \sigma_{sy_0} \quad \sigma_2 := \sigma_{sy_2} \quad \sigma_{SYM} := \left(\sigma_1^2 - \sigma_1 \cdot \sigma_2 + \sigma_2^2 \right)^{\frac{1}{2}}$$

Circum & Long. Stress at Midbay, Outer surface

$$\sigma_3 := \sigma_{sy_5} \quad \sigma_4 := \sigma_{sy_7} \quad \sigma_{SYF} := \left(\sigma_3^2 - \sigma_3 \cdot \sigma_4 + \sigma_4^2 \right)^{\frac{1}{2}}$$

Circum & Long Stress at Frame, Inner Surface

This represents how much of the safety factor was actually used:

$$\sigma_{SYM} = 2.444 \times 10^4 \text{ psi} \quad \text{Shell Yield, Midbay}$$

$$\sigma_{SYF} = 2.504 \times 10^4 \text{ psi} \quad \text{Shell Yield, Frame}$$

$$\sigma_{SY} := \max \left(\begin{pmatrix} \sigma_{SYM} \\ \sigma_{SYF} \end{pmatrix} \right)$$

$$\sigma_{SY} = 2.504 \times 10^4 \text{ psi}$$

$$\gamma_{SY} := \frac{\sigma_{SY}}{\sigma_y}$$

$$\gamma_{SY} = 0.025$$

PART 2 LOBAR BUCKLING

Windenberg Approx of Von Mises (1933)
Assumes n lobes = $\pi \cdot D/L$

Collapse
pressure:

$$P_{CLB} := \frac{2.42 E \cdot \left(\frac{t_p}{D}\right)^{2.5}}{\left(\frac{L_f}{D} - 0.45 \sqrt{\frac{t_p}{D}}\right) \cdot (1 - \nu^2)^{0.75}}$$

Safety factor is (2.25 oper depth) : $SF_{lb} := 2.25$

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{lb}$

$$P = 1.005 \times 10^3 \text{ psi}$$

HJ Notes, p.14

$$P_{CLB} = 1.786 \times 10^4 \text{ psi}$$

This represents
how much of the
safety factor was
actually used:

$$\gamma_{LB} := \frac{P}{P_{CLB}}$$

$$\gamma_{LB} = 0.056$$

PART 3 GENERAL INSTABILITY

Corrected Bryant Formula (1954) for
better model test correlation

Compute effective frame spacing:

$$\gamma := \frac{P}{2 \cdot E} \cdot \left(\frac{R}{t_p}\right)^2 \cdot \sqrt{3 \cdot (1 - \nu^2)} \quad \gamma = 0.107$$

Safety factor is (3.75 oper depth): $SF_{gi} := 3.75$

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{gi}$ $P = 1.674 \times 10^3 \text{ psi}$

Compute clear length:

$$L_c := L_f - t_w$$

$$n_1 := 0.5 \cdot \sqrt{1 - \gamma} \quad n_1 = 0.473$$

Web thickness:

$$t_w = 0.5 \text{ in}$$

$$n_2 := 0.5 \cdot \sqrt{1 + \gamma} \quad n_2 = 0.526$$

Effective shell plate length:

$$L_{eff} := L_c \cdot F_1 + t_w$$

$$L_{eff} = 17.26 \text{ in}$$

$$F_1 := \frac{4}{\theta} \cdot \left| \frac{\cosh(n_1 \cdot \theta)^2 - \cos(n_2 \cdot \theta)^2}{\frac{\cosh(n_1 \cdot \theta) \cdot \sinh(n_1 \cdot \theta)}{n_1} + \frac{\cos(n_2 \cdot \theta) \cdot \sin(n_2 \cdot \theta)}{n_2}} \right|$$

$$F_1 = 0.958 \quad \text{must be less than 1.00}$$

Theoretical critical lobe
number values are:

$$i := 0..2$$

Effective
plate
area:

$$A_{eff} := L_{eff} \cdot t_p$$

$$A_{eff} = 34.52 \text{ in}^2$$

Circumferential:
Lobes

$$n := \begin{pmatrix} 2 \\ 3 \\ 4 \end{pmatrix}$$

Frame-plate neutral axis
(ref web centre+ toward flange):

Longitudinal Lobes:

$$m := \pi \cdot \frac{R}{L_s} \quad m = 1.665$$

Moment of Inertia corrected for neutral axis.
 Uses Parallel Axis Theorem: $I_{cor} = I + Ad^2$

$$y_{na} := \frac{\left(\frac{h_w + t_f}{2}\right) \cdot A_f - \left(\frac{h_w + t_p}{2}\right) \cdot A_{eff}}{A_{eff} + A_w + A_f} \quad y_{na} = -2.355 \text{ in}$$

Moments of inertia for plate, flange, web:

$$I_p := \frac{I_{eff} \cdot t_p^3}{12} \quad I_w := \frac{t_w \cdot h_w^3}{12} \quad I_f := \frac{w_f \cdot t_f^3}{12}$$

$$I_{pcor} := I_p + A_{eff} \cdot \left[\left(\frac{t_p + h_w}{2} \right) + y_{na} \right]^2$$

$$I_{wcor} := I_w + A_w \cdot (y_{na})^2$$

$$I_{fcor} := I_f + A_f \cdot \left(\frac{t_f + h_w}{2} - y_{na} \right)^2$$

Total: $I_{eff} := I_{pcor} + I_{wcor} + I_{fcor}$

$I_{eff} = 265.457 \text{ in}^4$

The critical Elastic Gen'l Instability pressure is:

$$P_{cGI_i} := \frac{E \cdot t_p}{R} \cdot \frac{m^4}{\left[(n_i)^2 - 1 + \frac{m^2}{2} \right] \cdot \left[(n_i)^2 + m^2 \right]^2} + \frac{\left[(n_i)^2 - 1 \right] \cdot E \cdot I_{eff}}{R^3 \cdot L_f}$$

HJ Notes, p. 24

$$P_{cGI} = \begin{pmatrix} 2.513 \times 10^4 \\ 7.663 \times 10^3 \\ 8.339 \times 10^3 \end{pmatrix} \text{ psi} \quad n := \begin{pmatrix} 2 \\ 3 \\ 4 \end{pmatrix}$$

Min Pressure:

$$P_{cGI} := \min(P_{cGI})$$

This represents how much of the safety factor was actually used:

$P_{cGI} = 7.663 \times 10^3 \text{ psi}$

Use n for minimum P_{cGI} here to calculate Frame Bending Stress In Part 4 below

$$\gamma_{GI} := \frac{P}{P_{cGI}}$$

$\gamma_{GI} = 0.219$

PART 4 FRAME YIELDING

Safety factor is (1.5 Oper Depth): $SF_{fy} := 1.5$

Based on Salerno and Pulos. Accounts for Direct Stress on Face of Frame Flange. HJ Notes use Von Sanden Gunther for Direct Bending Stress from Kendrick (1953)

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{fy}$

$P = 669.799 \text{ psi}$

Compute direct frame stress:

$$\beta_f := \frac{t_w}{L_f}$$

Radius to frame NA:

$$R_{fna} := \frac{D}{2} - t_p - \frac{h_w}{2} - y_{na}$$

$$\alpha_p := \frac{A}{L_f \cdot t_p} \cdot \frac{\frac{D-t_p}{2}}{R_{fna} \cdot \frac{1}{2}}$$

$$\Gamma_p := \frac{P}{2 \cdot E} \cdot \left(\frac{\frac{D-t_p}{2}}{t_p} \right) \cdot \left[3 \cdot (1 - \nu^2) \right]^{\frac{1}{2}}$$

$$n_1 := \frac{1}{2} \cdot (1 - \Gamma_p)^2$$

$$n_2 := \frac{1}{2} \cdot (1 + \Gamma_p)^2$$

Stress Function

$$F_1 := \frac{4}{\theta} \cdot \frac{\cosh(n_1 \cdot \theta)^2 - \cos(n_2 \cdot \theta)^2}{\frac{\cosh(n_1 \cdot \theta) \cdot \sinh(n_1 \cdot \theta)}{n_1} + \frac{\cos(n_2 \cdot \theta) \cdot \sin(n_2 \cdot \theta)}{n_2}}$$

Stress

adjuster:

$$SA := 1 - \frac{\alpha_p}{\alpha_p + \beta_f + (1 - \beta_f) \cdot F_1}$$

$$SA = 0.801$$

$$\sigma_{\text{direct}} := \frac{\left(1 - \frac{\nu}{2}\right) \cdot P \cdot \left(\frac{D}{2} - \frac{t_p}{2}\right)^2}{t_p \cdot \left(\frac{D}{2} - t_p - h_w - t_f\right)} \cdot SA$$

$$\sigma_{\text{direct}} = 2.337 \times 10^4 \text{ psi}$$

Direct (Compressive)
Frame Stress on Flange

Compute bending stress due to eccentricity:

Shell-frame

length:

$$c := \frac{t_p}{2} + h_w + t_f \quad c = 7.5 \text{ in}$$

Define n lobes based on minimum P_{cGI} for
Elastic General Instability (Part 3 Calculation)

$$n := 3$$

HJ Notes, p. 18

Bending
stress:

$$\sigma_{\text{bend}} := \frac{E \cdot c \cdot e \cdot [(n)^2 - 1]}{R^2} \cdot \frac{P}{P_{cGI} - P}$$

$$\sigma_{\text{bend}} = 9.314 \times 10^3 \text{ psi}$$

Bending Frame
Stress on Flange

Total
stress:

$$\sigma_{fr} := \sigma_{\text{direct}} + \sigma_{\text{bend}}$$

$$\sigma_{fr} = 3.268 \times 10^4 \text{ psi}$$

$$\gamma_{fy} := \frac{\sigma_{fr}}{\sigma_y}$$

This represents how much of
the safety factor was actually
used:

$$\gamma_{fy} = 0.033$$

PART 5 FRAME INSTABILITY

Safety factor is (1.8 Oper Depth): $SF_{fy} := 1.8$

Area of plate: $A_p := t_p \cdot L_f$

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{fy}$ $P = 803.759 \text{ psi}$

Frame-plate neutral axis (ref web centre+ toward flange):

$$y_{na2} := \frac{\left(\frac{t_f}{2} + \frac{h_w}{2}\right) \cdot A_f - \left(\frac{t_p}{2} + \frac{h_w}{2}\right) \cdot A_p}{A_p + A_w + A_f} \quad y_{na2} = -2.393 \text{ in}$$

Moments of inertia for shell plate, frame flange & web

(compute I_p using actual shell plate length [frame spacing]):

$$I_p := \frac{L_f \cdot t_p^3}{12} \quad I_p = 12 \text{ in}^4$$

Correct the individual moments from the na:

$$I_{pcor} := I_p + A_p \cdot \left(\frac{t_p}{2} + \frac{h_w}{2} + y_{na2}\right)^2 \quad I_{pcor} = 56.096 \text{ in}^4$$

$$I_{wcor} := I_w + A_w \cdot y_{na2}^2 \quad I_{wcor} = 19.528 \text{ in}^4$$

$$I_{fcor} := I_f + A_f \cdot \left(\frac{h_w}{2} + \frac{t_f}{2} - y_{na2}\right)^2 \quad I_{fcor} = 192.203 \text{ in}^4$$

Then total shell plate & frame moment of inertia is:

$$I := I_{pcor} + I_{wcor} + I_{fcor} \quad I = 267.826 \text{ in}^4$$

Diameter

to NA is:

$$D_{na} := D - 2 \cdot t_p - h_w - 2 \cdot y_{na2} \quad D_{na} = 15.549 \text{ ft}$$

Compute pressure limit:

$$P_{cFI} := \frac{25 \cdot E \cdot I}{D_{na}^3 \cdot L_f}$$

$$P_{cFI} = 1.689 \times 10^3 \text{ psi}$$

HJ Notes, p. 26

This represents how much of the safety factor was actually used:

$$\gamma_{FI} := \frac{P}{P_{cFI}}$$

$$\gamma_{FI} = 0.476$$

Global Variable Inputs:

Operating depth: $D_t \equiv 1000 \text{ ft}$

$$\rho \equiv 1030 \frac{\text{kg}}{\text{m}^3}$$

$e \equiv 0.5 \text{ in}$ (Eccentricity)

Material: $\sigma_y \equiv 1000000 \frac{\text{lbf}}{\text{in}^2}$

$$\rho_{st} \equiv 7.8 \cdot 10^3 \frac{\text{kg}}{\text{m}^3}$$

$E \equiv 29.5 \cdot 10^6 \frac{\text{lbf}}{\text{in}^2}$ $\nu \equiv 0.3$

Geometry:

shell diameter $D \equiv 15.9 \text{ ft}$

$$R \equiv \frac{D}{2}$$

flange tickness $t_f \equiv 1.5 \text{ in}$

frame spacing $L_f \equiv 18 \text{ in}$

flange width $w_f \equiv 4.0 \text{ in}$

bulkhead spacing $L_s \equiv 15 \text{ ft}$

web thickness $t_w \equiv .5 \text{ in}$

shell thickness $t_p \equiv 2.00 \text{ in}$

web height $h_w \equiv 5.0 \text{ in}$

Results:

$$\gamma_{SY} = 0.025$$

$$\gamma_{LB} = 0.056$$

$$\gamma_{GI} = 0.219$$

$$\gamma_{fy} = 0.033$$

$$\gamma_{FI} = 0.476$$

$$\frac{1 \cdot 100}{\Delta} = 38.382$$

$$\text{Slenderness Ratio: } \lambda := \left[\frac{\left(\frac{L_f}{D} \right)}{\left[\left(\frac{t_p}{D} \right)^{1.5} \right] \left(\frac{\sigma_y}{E} \right)} \right]^{.5}$$

$$\lambda = 1.726$$

Design Checks

Good Design Values

Frame Web Height/ Frame Web Thickness:	$\frac{h_w}{t_w} = 10$	< 18
Flange Width/Web Height:	$\frac{w_f}{h_w} = 0.8$	0.7 - 0.8
Frame Space/Dia:	$\frac{L_f}{D} = 0.094$.07-.10
Flange Thickness/Shell t:	$\frac{t_f}{t_p} = 0.75$	0.75 - 1.0

Shell Thickness From Hoop Stress Only:

$$P := \rho \cdot g \cdot D_t \cdot S F_{Sy}$$

$$t := \frac{(P)(D)}{2\sigma_y} \quad t = 0.064 \text{ in}$$

$$\text{Compt Length/Dia: } \frac{L_s}{D} = 0.943 \quad 1.5 - 2.0$$

Check number of lobes at failure for Elastic General Instability from Part 3 above. If required Change n in Frame Yielding Calculation (Part 4)

$$\text{Frame Area/Mom of I: } \frac{A + (t_w \cdot t_p)}{I} = 0.035 \text{ in}^{-2}$$

$$\text{Approx Equal to: } \frac{E}{\sigma_y \cdot R_f^2} = 3.31 \times 10^{-3} \text{ in}^{-2}$$

$$\text{Area of Frame/Area of Shell: } \frac{A}{L_f \cdot t_p} = 0.236 \quad .333$$

Initial Sizing (t from hoop stress only)

Design

Initial Frame Spacing:	22t = 1.406in	HY-80, 1000ft
	26t = 1.661in	HY-100, 1000ft

Shell thickness/Dia.:

$$\frac{t_p}{D} = 0.01$$

$$\text{Initial Frame Web Thickness: } .4t = 0.026 \text{ in}$$

$$t_w = 0.5 \text{ in}$$

$$\text{Initial Frame Web Height: } 7t = 0.447 \text{ in}$$

$$h_w = 5 \text{ in}$$

$$\text{Initial Frame Flg Thickness: } .85t = 0.054 \text{ in}$$

$$t_f = 1.5 \text{ in}$$

$$\text{Initial Frame Flg Width: } 5.25t = 0.335 \text{ in}$$

$$w_f = 4 \text{ in}$$

$$\text{Initial I of shell and plate: } 264.5t^4 = 4.41 \times 10^{-3} \text{ in}^4$$

$$I = 267.826 \text{ in}^4$$

$$\text{Initial Frame Area: } 7.2625t^2 = 0.03 \text{ in}^2$$

$$A = 8.5 \text{ in}^2$$

$$\text{Mom of Inertia/Frame Area: } 36.42t^2 = 0.149 \text{ in}^2$$

$$\frac{I}{A} = 31.509 \text{ in}^2$$

Payload Bay Shell Analysis

PAYLOAD BAY SHELL ANALYSIS

This program computes the safety factors of the following criteria given hull material, scantlings and dimensions:

- a. Shell Yielding;
- b. Shell Lobar Buckling;
- c. Elastic General Instability;
- d. Frame Yielding; and
- e. Frame Instability.

Define input parameters:

Note: Global variables are used for iteration purposes. Inputs are at the end of this spreadsheet.

Compute areas: $R_f := R - \frac{t_p}{2}$ Frame Radius $R_f = 73.4\text{in}$ *Frame Area = Flange + Web*

Frame flange, web area: $A_f := t_f \cdot w_f$ $A_w := t_w \cdot h_w$ $A := A_f + A_w$ $A = 5.05\text{in}^2$

Compute structural efficiency (buoyancy ratios):

$$\Delta := \frac{\rho \cdot R^2 \cdot L_f}{2 \cdot \rho_{st} \cdot \left[\left(R - \frac{t_p}{2} \right) \cdot L_f \cdot t_p + \left(R - t_p - \frac{h_w}{2} \right) \cdot t_w \cdot h_w + \left(R - t_p - h_w - \frac{t_f}{2} \right) \cdot w_f \cdot t_f \right]}$$

$\Delta = 2.129$ Shell Weight Frame Web Weight Frame Flange Weight

$\frac{1}{\Delta} \cdot 100 = 46.978$ % - Shell and Frame Weight of 1 Frame Bay as a % of Displaced Water

PART 1 SHELL YIELDING

Safety factor is (1.5 oper depth): $SF_{sy} := 1.5$

Von Sanden and Gunther (1952)
PNA Section 8.4

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{sy}$ $P = 669.799 \text{psi}$

Area ratio $B := \frac{t_w \cdot t_p}{A + t_w \cdot t_p}$ Slenderness parameter: $\theta := L_f \cdot \left[\frac{3 \cdot (1 - \nu^2)}{(R \cdot t_p)^2} \right]^{\frac{1}{4}}$ Deflection coefficient: $N := \frac{\cosh(\theta) - \cos(\theta)}{\sinh(\theta) + \sin(\theta)}$

$B = 0.137$ $\theta = 1.475$

Frame flexibility parameter: $\beta := \frac{2 \cdot N}{A + t_w \cdot t_p} \cdot \left[\frac{1}{3 \cdot (1 - \nu^2)} \right]^{0.25} \cdot \sqrt{R \cdot t_p^3}$ Frame deflection parameter: $\Gamma := \frac{\left(1 - \frac{\nu}{2}\right) - B}{1 + \beta}$

$\beta = 4.665$

Bending effect (mem): $H_M := -2 \cdot \frac{\sinh\left(\frac{\theta}{2}\right) \cdot \cos\left(\frac{\theta}{2}\right) + \cosh\left(\frac{\theta}{2}\right) \cdot \sin\left(\frac{\theta}{2}\right)}{\sinh(\theta) + \sin(\theta)}$ $\Gamma = 0.126$

$H_M = -0.952$

Bending effect (bend): $H_E := -2 \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot \frac{\sinh\left(\frac{\theta}{2}\right) \cdot \cos\left(\frac{\theta}{2}\right) - \cosh\left(\frac{\theta}{2}\right) \cdot \sin\left(\frac{\theta}{2}\right)}{\sinh(\theta) + \sin(\theta)}$ $H_E = 0.316$

Midbay shell stress is calculated:

Circumferential Stress **PNA #**

outer $\sigma_{\phi\phi so} := \frac{-P \cdot R}{t_p} \cdot [1 + \Gamma \cdot (H_M + \nu \cdot H_E)]$ (20a)

inner $\sigma_{\phi\phi si} := \frac{-P \cdot R}{t_p} \cdot [1 + \Gamma \cdot (H_M - \nu \cdot H_E)]$

Bending effect near frame:

Longitudinal Stress $K := \frac{\sinh(\theta) - \sin(\theta)}{\sinh(\theta) + \sin(\theta)}$

outer $\sigma_{xx so} := \frac{-P \cdot R}{t_p} \cdot (0.5 + \Gamma \cdot H_E)$ (20b)

inner $\sigma_{xx si} := \frac{-P \cdot R}{t_p} \cdot (0.5 - \Gamma \cdot H_E)$

Shell stress at frames is:

outer $\sigma_{\phi\phi fo} := \frac{-P \cdot R}{t_p} \cdot \left[1 - \Gamma \cdot \left[1 + \nu \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot K \right] \right]$ (20c)

inner $\sigma_{\phi\phi fi} := \frac{-P \cdot R}{t_p} \cdot \left[1 - \Gamma \cdot \left[1 - \nu \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot K \right] \right]$

outer $\sigma_{xx fo} := \frac{-P \cdot R}{t_p} \cdot \left[0.5 - \Gamma \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot K \right]$ (20d)

inner $\sigma_{xx fi} := \frac{-P \cdot R}{t_p} \cdot \left[0.5 + \Gamma \cdot \left(\frac{3}{1 - \nu^2}\right)^{0.5} \cdot K \right]$

$$\sigma_{sy} := \begin{pmatrix} \sigma_{\phi\phi so} \\ \sigma_{\phi\phi si} \\ \sigma_{xxso} \\ \sigma_{xxsi} \\ \sigma_{\phi\phi fo} \\ \sigma_{\phi\phi fi} \\ \sigma_{xxfo} \\ \sigma_{xxfi} \end{pmatrix} \quad \sigma_{sy} = \begin{pmatrix} -2.223 \times 10^4 \\ -2.163 \times 10^4 \\ -1.345 \times 10^4 \\ -1.147 \times 10^4 \\ -2.118 \times 10^4 \\ -2.238 \times 10^4 \\ -1.046 \times 10^4 \\ -1.446 \times 10^4 \end{pmatrix} \text{ psi}$$

sy_0 Midbay, circumferential stress, outer shell surface $j := 1..8$
 sy_7 At Frame, longitudinal stress, inner shell surface
 <- key for Henky-Von Mises calculation below

Now according to Henky-Von Mises (max distortion theory) applied at mid bay(outer) and frame(inner):

HJ Notes, p. 22

$$\sigma_1 := \sigma_{sy_0} \quad \sigma_2 := \sigma_{sy_2} \quad \sigma_{SYM} := \left(\sigma_1^2 - \sigma_1 \cdot \sigma_2 + \sigma_2^2 \right)^{\frac{1}{2}}$$

Circum & Long. Stress at Midbay, Outer surface

$$\sigma_3 := \sigma_{sy_5} \quad \sigma_4 := \sigma_{sy_7} \quad \sigma_{SYF} := \left(\sigma_3^2 - \sigma_3 \cdot \sigma_4 + \sigma_4^2 \right)^{\frac{1}{2}}$$

Circum & Long Stress at Frame, Inner Surface

This represents how much of the safety factor was actually used:

$$\sigma_{SYM} = 1.939 \times 10^4 \text{ psi} \quad \text{Shell Yield, Midbay}$$

$$\sigma_{SYF} = 1.965 \times 10^4 \text{ psi} \quad \text{Shell Yield, Frame}$$

$$\sigma_{SY} := \max \left(\begin{pmatrix} \sigma_{SYM} \\ \sigma_{SYF} \end{pmatrix} \right)$$

$$\sigma_{SY} = 1.965 \times 10^4 \text{ psi}$$

$$\gamma_{SY} := \frac{\sigma_{SY}}{\sigma_y}$$

$$\gamma_{SY} = 0.02$$

PART 2 LOBAR BUCKLING

Windenberg Approx of Von Mises (1933)
Assumes n lobes = $\pi \cdot D/L$

Safety factor is (2.25 oper depth) : $SF_{lb} := 2.25$

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{lb}$

$$P = 1.005 \times 10^3 \text{ psi}$$

Collapse
pressure:

$$P_{cLB} := \frac{2.42 E \cdot \left(\frac{t_p}{D}\right)^{2.5}}{\left(\frac{L_f}{D} - 0.45 \sqrt{\frac{t_p}{D}}\right) \cdot (1 - \nu^2)^{0.75}}$$

HJ Notes, p.14

$$P_{cLB} = 3.829 \times 10^4 \text{ psi}$$

This represents
how much of the
safety factor was
actually used:

$$\gamma_{LB} := \frac{P}{P_{cLB}}$$

$$\gamma_{LB} = 0.026$$

PART 3 GENERAL INSTABILITY

Corrected Bryant Formula (1954) for
better model test correlation

Safety factor is (3.75 oper depth): $SF_{gi} := 3.75$

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{gi}$ $P = 1.674 \times 10^3 \text{ psi}$

Compute effective frame spacing:

$$\gamma := \frac{P}{2 \cdot E} \cdot \left(\frac{R}{t_p}\right)^2 \cdot \sqrt{3 \cdot (1 - \nu^2)} \quad \gamma = 0.065$$

Compute clear length:

$$L_c := L_f - t_w$$

$$n_1 := 0.5 \cdot \sqrt{1 - \gamma} \quad n_1 = 0.484$$

Web thickness:

$$t_w = 0.4 \text{ in}$$

$$n_2 := 0.5 \cdot \sqrt{1 + \gamma} \quad n_2 = 0.516$$

Effective shell plate length:

$$L_{eff} := L_c \cdot F_1 + t_w$$

$$L_{eff} = 13.651 \text{ in}$$

$$F_1 := \frac{4}{\theta} \cdot \left| \frac{\cosh(n_1 \cdot \theta)^2 - \cos(n_2 \cdot \theta)^2}{\frac{\cosh(n_1 \cdot \theta) \cdot \sinh(n_1 \cdot \theta)}{n_1} + \frac{\cos(n_2 \cdot \theta) \cdot \sin(n_2 \cdot \theta)}{n_2}} \right|$$

$$F_1 = 0.974 \quad \text{must be less than 1.00}$$

Theoretical critical lobe
number values are:

$$i := 0..2$$

Effective
plate
area:

$$A_{eff} := L_{eff} \cdot t_p \quad A_{eff} = 27.301 \text{ in}^2$$

Circumferential:
Lobes

$$n := \begin{pmatrix} 2 \\ 3 \\ 4 \end{pmatrix}$$

Frame-plate neutral axis
(ref web centre+ toward flange):

Longitudinal Lobes: $m := \pi \cdot \frac{R}{L_s} \quad m = 0.749$

Moment of Inertia corrected for neutral axis.
 Uses Parallel Axis Theorem: $I_{cor} = I + Ad^2$

$$y_{na} := \frac{\left(\frac{h_w + t_f}{2}\right) \cdot A_f - \left(\frac{h_w + t_p}{2}\right) \cdot A_{eff}}{A_{eff} + A_w + A_f} \quad y_{na} = -1.94in$$

Moments of inertia for plate, flange, web:

$$I_p := \frac{L_{eff} \cdot t_p^3}{12} \quad I_w := \frac{t_w \cdot h_w^3}{12} \quad I_f := \frac{w_f \cdot t_f^3}{12}$$

$$I_{pcor} := I_p + A_{eff} \cdot \left[\left(\frac{t_p + h_w}{2} \right) + y_{na} \right]^2$$

$$I_{wcor} := I_w + A_w \cdot (y_{na})^2$$

$$I_{fcor} := I_f + A_f \cdot \left(\frac{t_f + h_w}{2} - y_{na} \right)^2$$

Total: $I_{eff} := I_{pcor} + I_{wcor} + I_{fcor}$

$$I_{eff} = 98.473in^4$$

The critical Elastic Gen'l Instability pressure is:

$$P_{cGI_1} := \frac{E \cdot t_p}{R} \cdot \frac{m^4}{\left[(n_i)^2 - 1 + \frac{m^2}{2} \right] \cdot \left[(n_i)^2 + m^2 \right]^2} + \frac{\left[(n_i)^2 - 1 \right] \cdot E \cdot I_{eff}}{R^3 \cdot L_f}$$

HJ Notes, p. 24

$$P_{cGI} = \begin{pmatrix} 5.171 \times 10^3 \\ 4.361 \times 10^3 \\ 7.617 \times 10^3 \end{pmatrix} \text{ psi} \quad n := \begin{pmatrix} 2 \\ 3 \\ 4 \end{pmatrix}$$

Min Pressure:

$$P_{cGI} := \min(P_{cGI})$$

This represents how much of the safety factor was actually used:

$$P_{cGI} = 4.361 \times 10^3 \text{ psi}$$

Use n for minimum P_{cGI} here to calculate Frame Bending Stress In Part 4 below

$$\gamma_{GI} := \frac{P}{P_{cGI}}$$

$$\gamma_{GI} = 0.384$$

PART 4 FRAME YIELDING

Safety factor is (1.5 Oper Depth): $SF_{fy} := 1.5$

Based on Salerno and Pulos. Accounts for Direct Stress on Face of Frame Flange. HJ Notes use Von Sanden Gunther for Direct Bending Stress from Kendrick (1953)

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{fy}$ $P = 669.799psi$

Compute direct frame stress:

$$\beta_f := \frac{t_w}{L_f}$$

Radius to frame NA:

$$R_{fna} := \frac{D}{2} - t_p - \frac{h_w}{2} - y_{na}$$

$$\alpha_p := \frac{A}{L_f \cdot t_p} \cdot \frac{\frac{D-t_p}{2}}{R_{fna}}$$

$$\Gamma_p := \frac{P}{2 \cdot E} \cdot \left(\frac{\frac{D-t_p}{2}}{t_p} \right)^2 \cdot \left[3 \cdot (1 - \nu^2) \right]^{\frac{1}{2}}$$

$$n_1 := \frac{1}{2} \cdot (1 - \Gamma_p)^2$$

$$n_2 := \frac{1}{2} \cdot (1 + \Gamma_p)^2$$

Stress Function

$$F_1 := \frac{4}{\theta} \cdot \frac{\cosh(n_1 \cdot \theta)^2 - \cos(n_2 \cdot \theta)^2}{\frac{\cosh(n_1 \cdot \theta) \cdot \sinh(n_1 \cdot \theta)}{n_1} + \frac{\cos(n_2 \cdot \theta) \cdot \sin(n_2 \cdot \theta)}{n_2}}$$

Stress adjuster:

$$SA := 1 - \frac{\alpha_p}{\alpha_p + \beta_f + (1 - \beta_f) \cdot F_1} \quad SA = 0.843$$

$$\sigma_{\text{direct}} := \frac{\left(1 - \frac{\nu}{2}\right) \cdot P \cdot \left(\frac{D}{2} - \frac{t_p}{2}\right)^2}{t_p \cdot \left(\frac{D}{2} - t_p - h_w - t_f\right)} \cdot SA$$

$$\sigma_{\text{direct}} = 1.91 \times 10^4 \text{ psi}$$

Direct (Compressive) Frame Stress on Flange

Compute bending stress due to eccentricity:

Shell-frame length:

$$c := \frac{t_p}{2} + h_w + t_f \quad c = 5.75 \text{ in}$$

Define n lobes based on minimum P_{cGI} for Elastic General Instability (Part 3 Calculation)

$$n := 3$$

HJ Notes, p. 18

Bending stress:

$$\sigma_{\text{bend}} := \frac{E \cdot c \cdot e \cdot [(n)^2 - 1]}{R^2} \cdot \frac{P}{P_{cGI} - P}$$

$$\sigma_{\text{bend}} = 2.224 \times 10^4 \text{ psi}$$

Bending Frame Stress on Flange

Total stress:

$$\sigma_{\text{fr}} := \sigma_{\text{direct}} + \sigma_{\text{bend}}$$

$$\sigma_{\text{fr}} = 4.135 \times 10^4 \text{ psi}$$

This represents how much of the safety factor was actually used:

$$\gamma_{fy} := \frac{\sigma_{\text{fr}}}{\sigma_y}$$

$$\gamma_{fy} = 0.041$$

PART 5 FRAME INSTABILITY

Safety factor is (1.8 Oper Depth): $SF_{fy} := 1.8$

Area of plate: $A_p := t_p \cdot L_f$

Pressure loading is: $P := \rho \cdot g \cdot D_t \cdot SF_{fy}$ $P = 803.759 \text{ psi}$

Frame-plate neutral axis (ref web centre+ toward flange): $y_{na2} := \frac{\left(\frac{t_f}{2} + \frac{h_w}{2}\right) \cdot A_f - \left(\frac{t_p}{2} + \frac{h_w}{2}\right) \cdot A_p}{A_p + A_w + A_f}$ $y_{na2} = -1.954 \text{ in}$

Moments of inertia for shell plate, frame flange & web (compute I_p using actual shell plate length [frame spacing]): $I_p := \frac{L_f \cdot t_p^3}{12}$ $I_p = 9.333 \text{ in}^4$

Correct the individual moments from the na:

$$I_{pcor} := I_p + A_p \cdot \left(\frac{t_p}{2} + \frac{h_w}{2} + y_{na2}\right)^2 \quad I_{pcor} = 21.924 \text{ in}^4$$

$$I_{wcor} := I_w + A_w \cdot y_{na2}^2 \quad I_{wcor} = 6.11 \text{ in}^4 \quad I_{fcor} := I_f + A_f \cdot \left(\frac{h_w}{2} + \frac{t_f}{2} - y_{na2}\right)^2 \quad I_{fcor} = 70.993 \text{ in}^4$$

Then total shell plate & frame moment of inertia is: $I := I_{pcor} + I_{wcor} + I_{fcor}$ $I = 99.027 \text{ in}^4$

Diameter to NA is: $D_{na} := D - 2 \cdot t_p - h_w - 2 \cdot y_{na2}$ $D_{na} = 12.122 \text{ ft}$

Compute pressure limit:

$$P_{cFI} := \frac{25 \cdot E \cdot I}{D_{na}^3 \cdot L_f}$$

$$P_{cFI} = 1.695 \times 10^3 \text{ psi}$$

HJ Notes, p. 26

This represents how much of the safety factor was actually used:

$$\gamma_{FI} := \frac{P}{P_{cFI}}$$

$$\gamma_{FI} = 0.474$$

Global Variable Inputs:

Operating depth: $D_t \equiv 1000 \text{ ft}$ $\rho \equiv 1030 \frac{\text{kg}}{\text{m}^3}$ $e \equiv 0.5 \text{ in}$ (Eccentricity)

Material: $\sigma_y \equiv 1000000 \frac{\text{lbf}}{\text{in}^2}$ $\rho_{st} \equiv 7.8 \cdot 10^3 \frac{\text{kg}}{\text{m}^3}$ $E \equiv 29.5 \cdot 10^6 \frac{\text{lbf}}{\text{in}^2}$ $\nu \equiv 0.3$

Geometry:

shell diameter	$D \equiv 12.4 \text{ ft}$	$R \equiv \frac{D}{2}$	flange tickness	$t_f \equiv 1.5 \text{ in}$
frame spacing	$L_f \equiv 14 \text{ in}$		flange width	$w_f \equiv 2.5 \text{ in}$
bulkhead spacing	$L_s \equiv 26 \text{ ft}$		web thickness	$t_w \equiv .4 \text{ in}$
shell thickness	$t_p \equiv 2.00 \text{ in}$		web height	$h_w \equiv 3.25 \text{ in}$

Results:

$$\gamma_{SY} = 0.02$$

$$\gamma_{LB} = 0.026$$

$$\gamma_{GI} = 0.384$$

$$\gamma_{fy} = 0.041$$

$$\gamma_{FI} = 0.474$$

$$\frac{1 \cdot 100}{\Delta} = 46.978$$

Slenderness Ratio: $\lambda :=$

$$\lambda := \left[\frac{\left(\frac{L_f}{D} \right) \left(\frac{\sigma_y}{E} \right)}{\left[\left(\frac{t_p}{D} \right)^{1.5} \right]} \right]^{.5}$$

$$\lambda = 1.431$$

Design Checks

Good Design Values

Frame Web Height/
Frame Web Thickness: $\frac{h_w}{t_w} = 8.125 < 18$

Flange Width/Web Height: $\frac{w_f}{h_w} = 0.769 \quad 0.7 - 0.8$

Frame Space/Dia: $\frac{L_f}{D} = 0.094 \quad .07 - .10$

Flange Thickness/Shell t: $\frac{t_f}{t_p} = 0.75 \quad 0.75 - 1.0$

Frame Area/Mom of I: $\frac{A + (t_w \cdot t_p)}{I} = 0.059 \text{in}^{-2}$

Approx
Equal to: $\frac{E}{\sigma_y \cdot R_f^2} = 5.476 \times 10^{-3} \text{in}^{-2}$

Area of Frame/Area of Shell: $\frac{A}{L_f \cdot t_p} = 0.18 \quad .333$

Shell Thickness From Hoop Stress Only:

$$P := \rho \cdot g \cdot D_t \cdot S F_{sy}$$

$$t := \frac{(P)(D)}{2\sigma_y} \quad t = 0.05 \text{in}$$

Compt Length/Dia: $\frac{L_s}{D} = 2.097 \quad 1.5 - 2.0$

Check number of lobes at failure for Elastic General Instability from Part 3 above. If required Change n in Frame Yielding Calculation (Part 4)

Initial Sizing (t from hoop stress only)

Design

Initial Frame Spacing: $22t = 1.096 \text{in} \quad \text{HY-80, 1000ft}$

$26t = 1.296 \text{in} \quad \text{HY-100, 1000ft}$

Initial Frame Web Thickness: $.4t = 0.02 \text{in}$

Initial Frame Web Height: $7t = 0.349 \text{in}$

Initial Frame Flg Thickness: $.85t = 0.042 \text{in}$

Initial Frame Flg Width: $5.25t = 0.262 \text{in}$

Initial I of shell and plate: $264.5t^4 = 1.631 \times 10^{-3} \text{in}^4$

Initial Frame Area: $7.2625t^2 = 0.018 \text{in}^2$

Mom of Inertia/Frame Area: $36.42t^2 = 0.09 \text{in}^2$

$L_f = 14 \text{in}$

$t_w = 0.4 \text{in}$

$h_w = 3.25 \text{in}$

$t_f = 1.5 \text{in}$

$w_f = 2.5 \text{in}$

$I = 99.027 \text{in}^4$

$A = 5.05 \text{in}^2$

$\frac{I}{A} = 19.609 \text{in}^2$

Shell thickness/Dia.:

$$\frac{t_p}{D} = 0.013$$

Payload Bay Lateral Wall Analysis

PAYLOAD BAY LATERAL WALL ANALYSIS

$$\text{ksi} := 1000 \frac{\text{lb}}{\text{in}^2} \quad \text{lton} := 2240 \text{ lb}$$

MATERIALS

For HY-80 Components:

$$\sigma_Y := 80 \cdot \text{ksi} \quad \gamma_S := 1.25 \quad \gamma_C := 1.5 \quad \sigma_{\text{MAX}} := \frac{\sigma_Y}{2}$$

$$E := 29.6 \cdot 10^3 \cdot \text{ksi} \quad \nu := .30 \quad G := \frac{E}{2 \cdot (1 + \nu)}$$

$$\sigma_{\text{MAX}} = 40 \text{ ksi} \quad \sigma_T := -\sigma_{\text{MAX}} \quad \sigma_C := \sigma_{\text{MAX}}$$

LOCAL LOADS: **For non-continuous internal decks analyze dead load plus live load**

$$H_{\text{LCL}} = 1000 \text{ ft}$$

Select number of stiffeners, N so that $23 \text{ in} < b < 28 \text{ in}$:

$$b := \frac{B}{N + 1} \quad b = 24 \text{ in}$$

Select Frame space and panel thickness:

$$a = 4 \text{ ft} \quad t = 3.000 \text{ in}$$

PLATE LIMIT STATES - assume values for b,t; refine t as required so all $\gamma R_u \leq 1$

$$\sigma_{\text{ax}} := \sigma_{\text{MAX}} \quad \tau := 0 \cdot \text{ksi} \quad D := \frac{E \cdot (t)^3}{12 \cdot (1 - \nu^2)} \quad \text{conv} := .444 \frac{\text{psi}}{\text{ft}}$$

$$p := H_{\text{LCL}} \cdot \text{conv}$$

$$p = 444 \text{ psi}$$

PSPBT - Panel Serviceability Plate Bending Transverse -

$$\sigma_{bx} := 0 \cdot \text{ksi} \quad \sigma_x := \sigma_{ax} + \sigma_{bx} \quad \sigma_{by} := - \left(.5 \cdot \left[p \cdot \left(\frac{b}{t} \right)^2 \right] \right) \quad \sigma_y := \sigma_{by}$$

$$\sigma_{VM} := \sqrt{.5 \cdot \left[(\sigma_x - \sigma_y)^2 + (\sigma_y)^2 + (\sigma_x)^2 \right] + 3 \cdot \tau^2} \quad \gamma_{R_{PSPBT}} := \gamma_S \cdot \frac{\sigma_{VM}}{\sigma_Y}$$

PSPBL - Panel Serviceability Plate Bending Longitudinal

$$\sigma_{bx} := .34 \cdot \left(\left[p \cdot \left(\frac{b}{t} \right)^2 \right] \right) \quad \sigma_x := \sigma_{ax} + \sigma_{bx} \quad \sigma_{by} := 0 \cdot \text{psi} \quad \sigma_y := \sigma_{by}$$

$$\sigma_{VM} := \sqrt{.5 \cdot \left[(\sigma_x - \sigma_y)^2 + (\sigma_y)^2 + (\sigma_x)^2 \right] + 3 \cdot \tau^2} \quad \gamma_{R_{PSPBL}} := \gamma_S \cdot \frac{\sigma_{VM}}{\sigma_Y}$$

PCMY - Panel Collapse Membrane Yield (or PFMY)

$$\sigma_x := \sigma_{ax} \quad \sigma_y := 0 \cdot \text{psi} \quad \gamma_C := 1.5$$

$$\sigma_{VM} := \sqrt{.5 \cdot \left[(\sigma_x - \sigma_y)^2 + (\sigma_y)^2 + (\sigma_x)^2 \right] + 3 \cdot \tau^2} \quad \gamma_{R_{PCMY}} := \gamma_C \cdot \frac{\sigma_{VM}}{\sigma_Y}$$

PFLB - Plate Failure Local Buckling

$$\sigma_{axcr} := -4 \cdot \frac{\pi^2 \cdot D}{b^2 \cdot t} \quad k_S := 5.35 + 4 \cdot \left(\frac{b}{a} \right)^2 \quad \tau := 0 \cdot \text{psi} \quad \tau_{cr} := -k_S \cdot \frac{\pi^2 \cdot D}{b^2 \cdot t} \quad R_S := \frac{\tau}{\tau_{cr}}$$

interaction

formula: $R_C := 1 - R_S^2$ $\sigma_o := -R_C \cdot \sigma_{axcr}$ $R_{PFLB} := \frac{\sigma_C}{\sigma_o}$ $\gamma_{R_{PFLB}} := \gamma_S \cdot R_{PFLB}$

STIFFENED PANEL LIMIT STATES

Stiffener Sizing:

$$\text{HSW} := \text{DEPTH} - \text{TSF} \quad A_w := (\text{DEPTH} - \text{TSF}) \cdot \text{TSW} \quad A_f := \text{BSF} \cdot \text{TSF} \quad (6-1)$$

$$A_s := A_w + A_f \quad A_p := b \cdot t \quad L := a$$

Combination of plate and stiffeners (from p287, equation 8.3.6 in text):

$$d := \text{DEPTH} - \frac{\text{TSF}}{2} + \frac{t}{2} \quad A := A_s + A_p \quad C_1 := \frac{A_w \cdot \left(\frac{A}{3} - \frac{A_w}{4} \right) + A_f \cdot A_p}{(A)^2} \quad I := A \cdot d^2 \cdot C_1$$

$$y_f := - \left(d \cdot \frac{\frac{A_w}{2} + A_p}{A} \right) \quad y_p := d \cdot \left(1 - \frac{\frac{A_w}{2} + A_p}{A} \right) \quad M_{\text{bend}} := - \left(p \cdot b \cdot \frac{L^2}{12} \right) \quad M_{\text{bcen}} := p \cdot b \cdot \frac{L^2}{12} \quad (6-2)$$

$$c_f := y_f - .5 \cdot \text{TSF} \quad c_p := .5 \cdot t + y_p \quad (\text{y is to mid-point})$$

PYTF - Panel Yield Tension Flange $\gamma_S := 1.25$

$$\sigma_{ax} := \sigma_T \quad \sigma_{bx} := \frac{-(M_{\text{bcen}} \cdot c_f)}{I} \quad \sigma_x := \sigma_{ax} + \sigma_{bx} \quad (6-3)$$

$$R_{\text{PYTF}} := \frac{\sigma_x}{\sigma_Y} \quad \gamma R_{\text{PYTF}} := \gamma_S \cdot R_{\text{PYTF}}$$

PYCF - Panel Yield Compression Flange

$$\sigma_{ax} := \sigma_C \quad \sigma_{bx} := \frac{-(M_{\text{bend}} \cdot c_f)}{I} \quad \sigma_x := \sigma_{ax} + \sigma_{bx} \quad R_{\text{PYCF}} := \frac{\sigma_x}{\sigma_Y} \quad (6-4)$$

$$\gamma R_{\text{PYCF}} := \gamma_S \cdot R_{\text{PYCF}}$$

PCCB - Panel Collapse Combined Buckling

$$b_{\text{rat}} := .7 \quad \nu = 0.3$$

$$\text{let: } b_e := b_{\text{rat}} \cdot b \quad A_e := A_s + b_e \cdot t \quad C_1 := \frac{A_w \cdot \left(\frac{A_e}{3} - \frac{A_w}{4} \right) + A_f \cdot b_e \cdot t}{A_e^2} \quad I_e := A_e \cdot d^2 \cdot C_1$$

$$\rho_e := \sqrt{\frac{I_e}{A_e}} \quad \gamma_x := \frac{12 \cdot (1 - \nu^2) \cdot I_e}{b_e \cdot t^3}$$

$$C_\pi := \min \left[\left[\frac{B}{a} \cdot \frac{\sqrt{\frac{\gamma_x}{2 \cdot (1 + \sqrt{1 + \gamma_x})}}}{1} \right] \right] \quad \sigma_{\text{ecr}} := \frac{\pi^2 \cdot E}{\left(\frac{C_\pi \cdot L}{\rho_e} \right)^2} \quad b_e := \frac{C_\pi \cdot L \cdot t}{\rho_e \cdot \sqrt{3 \cdot (1 - \nu^2)}} \quad \frac{b_e}{b} = 1.563 \quad \text{Check, must equal } b_{\text{rat}}$$

$$\sigma_{\text{axcr}} := \left(\frac{b_e \cdot t + A_s}{b \cdot t + A_s} \right) \cdot \sigma_{\text{ecr}} \quad \gamma_{\text{RPCCB}} := \gamma_C \cdot \frac{\sigma_C}{\sigma_{\text{axcr}}}$$

- PCSB - Panel Collapse Stiffener Buckling

$$I_{sz} := \frac{1}{12} \cdot (\text{HSW} \cdot \text{TSW}^3 + \text{TSF} \cdot \text{BSF}^3) \quad I_{sp} := d^2 \cdot \left(A_f + \frac{A_w}{3} \right) \quad J := \frac{\text{BSF} \cdot \text{TSF}^3 + (\text{HSW}) \cdot \text{TSW}^3}{3}$$

$$C_r := \frac{1}{1 + .4 \cdot \left(\frac{t}{\text{TSW}} \right)^3 \cdot \frac{d}{b}} \quad m := \frac{a}{\pi} \cdot \left(\frac{4 \cdot D \cdot C_r}{E \cdot I_{sz} \cdot d^2 \cdot b} \right)^{\frac{1}{4}}$$

recalling that; if $1 < m < 2$, value obtained is conservative

$$\text{for } m=1: \quad \sigma_{at1} := \frac{1}{I_{sp} + \frac{2 \cdot C_r \cdot b^3 \cdot t}{\pi^4}} \cdot \left[G \cdot J + \frac{\pi^2 \cdot E \cdot I_{sz} \cdot d^2}{a^2} + \frac{4 \cdot D \cdot C_r \cdot (a^2 + b^2)}{\pi^2 \cdot b} \right]$$

$$\text{for } m=2: \quad \sigma_{at2} := \frac{1}{I_{sp} + \frac{2 \cdot C_r \cdot b^3 \cdot t}{\pi^4}} \cdot \left(G \cdot J + 4 \cdot \sqrt{\frac{D \cdot C_r \cdot E \cdot I_{sz} \cdot d^2}{b}} + \frac{4 \cdot D \cdot C_r \cdot b}{\pi^2} \right)$$

$$\sigma_{at} := \min \left(\left(\begin{array}{l} \sigma_{at1} \\ \sigma_{at2} \end{array} \right) \right) \quad \gamma_{R_{PCSB}} := \gamma_C \cdot \frac{\sigma_C}{\sigma_{at}}$$

PCSF - Panel Collapse Stiffener Flexure. Use limiting mode (Mode I, II).

Rule of thumb for eccentricity of welded panels: $\Delta := \frac{a}{750}$ $\sigma_{ax} := \sigma_C$ (6-16)

a. Mode I (Point E of fig. 14.2) Compression failure of flange: $M_o := 0 \cdot \text{lbf} \cdot \text{in}$ $\delta_o := 0 \cdot \text{in}$ $\Delta_I := -\Delta$ (6-17)

Beam column parameters:

$$\rho_I := \sqrt{\frac{I}{A}} \quad \lambda_I := \frac{a}{\pi \cdot \rho_I} \cdot \sqrt{\frac{\sigma_Y}{E}} \quad \eta_I := \frac{(\delta_o + \Delta_I) \cdot y_f}{(\rho_I)^2} \quad \mu_I := \frac{M_o \cdot y_f}{I \cdot \sigma_Y} \quad \zeta_I := 1 - \mu_I + \frac{1 + \eta_I}{(\lambda_I)^2}$$

$$R := \frac{\zeta_I}{2} - \sqrt{\frac{(\zeta_I)^2}{4} - \frac{1 - \mu_I}{(\lambda_I)^2}} \quad \text{limit state} \quad \sigma_{axu} := R \cdot \sigma_Y \quad R_{PCSF1} := \frac{\sigma_{ax}}{\sigma_{axu}} \quad \gamma R_{PCSF1} := \gamma_C \cdot R_{PCSF1} \quad (6-18)$$

b. Mode II Compression failure of plate:

For maximum moment and center deflection assume simply supported beam:

$$q := p \cdot b \quad M_o := \frac{q \cdot a^2}{8} \quad \delta_o := \frac{5 \cdot q \cdot a^4}{384 E \cdot I} \quad (6-23)$$

determine failure stress using plate parameters

$$\beta := \frac{b}{t} \cdot \sqrt{\frac{\sigma_Y}{E}} \quad \xi := 1 + \frac{2.75}{(\beta)^2} \quad T := .25 \cdot \left[2 + \xi - \sqrt{(\xi)^2 - \frac{10.4}{(\beta)^2}} \right] \quad (6-19)$$

$$b_{tr} := T \cdot b \quad \sigma_F := \frac{T - .1}{T} \cdot \sigma_Y \cdot \sqrt{1 - 3 \cdot \left(\frac{\tau}{\sigma_Y} \right)^2} \quad (6-20)$$

For combination (from equation 8.3.6 in text) and transformed plate:

$$A_{ptr} := b_{tr} \cdot t \quad A_{tr} := A_s + A_{ptr} \quad C_{1tr} := \frac{A_w \cdot \left(\frac{A_{tr}}{3} - \frac{A_w}{4} \right) + A_f \cdot A_{ptr}}{(A_{tr})^2} \quad I_{tr} := A_{tr} \cdot (d)^2 \cdot C_{1tr} \quad (6-21)$$

$$y_{ftr} := -d \cdot \frac{\frac{A_w}{2} + b_{tr} \cdot t}{A_{tr}} \quad y_{ptr} := d \cdot \left(1 - \frac{\frac{A_w}{2} + b_{tr} \cdot t}{A_{tr}} \right) \quad \rho_{tr} := \sqrt{\frac{I_{tr}}{A_{tr}}} \quad \lambda := \frac{a}{\pi \cdot \rho_{tr}} \cdot \sqrt{\frac{\sigma_F}{E}} \quad (6-22)$$

Correction for load eccentricity:

$$h := \text{SCG} + \frac{t}{2} \quad \Delta_p := h \cdot A_s \cdot \left(\frac{1}{A_{tr}} - \frac{1}{A} \right) \quad \eta_p := \Delta_p \cdot \frac{y_{ptr}}{(\rho_{tr})^2} \quad (6-24)$$

Beam column with σ_F and transformed geometry

$$\eta := \frac{(\delta_o + \Delta) \cdot y_{ptr}}{(\rho_{tr})^2} \quad \mu := \frac{M_o \cdot y_{ptr}}{I_{tr} \cdot \sigma_F} \quad \zeta := \frac{1 - \mu}{1 + \eta_p} + \frac{1 + \eta_p + \eta}{(1 + \eta_p) \cdot (\lambda)^2} \quad R := \frac{\zeta}{2} - \sqrt{\frac{(\zeta)^2}{4} - \frac{1 - \mu}{(1 + \eta_p) \cdot (\lambda)^2}} \quad (6-25)$$

limit state

$$\sigma_{axtru} := R \cdot \sigma_F \quad \sigma_{axu} := \frac{A_{tr}}{A} \cdot \sigma_{axtru} \quad R_{PCSF2} := \frac{\sigma_{ax}}{\sigma_{axu}} \quad \gamma R_{PCSF2} := R_{PCSF2} \quad (6-26)$$

RESULTS:

t = 3 in

b = 24 in

$$\gamma R_{PCMY} = 0.75$$

$$\gamma R_{PSPBT} = 0.761$$

$$\gamma R_{PSPBL} = 0.776$$

$$\gamma R_{PYTF} = 0.203$$

$$\gamma R_{PFLB} = 0.03$$

$$\gamma R_{PCCB} = 0.06$$

$$\gamma R_{PCSB} = 0.037$$

$$\gamma R_{PYCF} = 0.203$$

$$\gamma R_{PCSF1} = 0.804$$

$$\gamma R_{PCSF2} = 0.653$$

DEPTH = 6in

TSW = 1.5in

BSF = 6in

TSF = 2in

SCG = 5-in

Payload Bay End Wall Analysis

PAYLOAD BAY END WALL ANALYSIS

$$\text{ksi} := 1000 \frac{\text{lbf}}{\text{in}^2} \quad \text{lton} := 2240 \cdot \text{lb}$$

MATERIALS

For HY-80 Components:

$$\sigma_Y := 80 \cdot \text{ksi} \quad \gamma_S := 1.25 \quad \gamma_C := 1.5 \quad \sigma_{\text{MAX}} := \frac{\sigma_Y}{2}$$

$$E := 29.6 \cdot 10^3 \cdot \text{ksi} \quad \nu := .30 \quad G := \frac{E}{2 \cdot (1 + \nu)}$$

$$\sigma_{\text{MAX}} = 40 \text{ ksi} \quad \sigma_T := -\sigma_{\text{MAX}} \quad \sigma_C := \sigma_{\text{MAX}}$$

LOCAL LOADS:

For non-continuous internal decks analyze dead load plus live load

$$H_{\text{LCL}} = 1000 \text{ ft}$$

Select number of stiffeners, N so that $23\text{in} < b < 28\text{in}$:

$$b := \frac{B}{N + 1} \quad b = 21 \text{ in}$$

Select Frame space and panel thickness:

$$a = 4 \text{ ft} \quad t = 3.000 \text{ in}$$

PLATE LIMIT STATES - assume values for b,t; refine t as required so all

$$\gamma R_L \leq 1$$

$$\sigma_{\text{ax}} := \sigma_{\text{MAX}} \quad \tau := 0 \cdot \text{ksi} \quad D := \frac{E \cdot (t)^3}{12 \cdot (1 - \nu^2)} \quad \text{conv} := .444 \frac{\text{psi}}{\text{ft}}$$

$$p := H_{\text{LCL}} \cdot \text{conv}$$

$$p = 444 \text{ psi}$$

PSPBT - Panel Serviceability Plate Bending Transverse -

$$\sigma_{bx} := 0 \cdot \text{ksi} \quad \sigma_x := \sigma_{ax} + \sigma_{bx} \quad \sigma_{by} := - \left(.5 \cdot \left[p \cdot \left(\frac{b}{t} \right)^2 \right] \right) \quad \sigma_y := \sigma_{by}$$

$$\sigma_{VM} := \sqrt{.5 \cdot \left[(\sigma_x - \sigma_y)^2 + (\sigma_y)^2 + (\sigma_x)^2 \right] + 3 \cdot \tau^2} \quad \gamma_{R_{PSPBT}} := \gamma_S \cdot \frac{\sigma_{VM}}{\sigma_Y}$$

PSPBL - Panel Serviceability Plate Bending Longitudinal

$$\sigma_{bx} := .34 \cdot \left(\left[p \cdot \left(\frac{b}{t} \right)^2 \right] \right) \quad \sigma_x := \sigma_{ax} + \sigma_{bx} \quad \sigma_{by} := 0 \cdot \text{psi} \quad \sigma_y := \sigma_{by}$$

$$\sigma_{VM} := \sqrt{.5 \cdot \left[(\sigma_x - \sigma_y)^2 + (\sigma_y)^2 + (\sigma_x)^2 \right] + 3 \cdot \tau^2} \quad \gamma_{R_{PSPBL}} := \gamma_S \cdot \frac{\sigma_{VM}}{\sigma_Y}$$

PCMY - Panel Collapse Membrane Yield (or PFMY)

$$\sigma_x := \sigma_{ax} \quad \sigma_y := 0 \cdot \text{psi} \quad \gamma_C := 1.5$$

$$\sigma_{VM} := \sqrt{.5 \cdot \left[(\sigma_x - \sigma_y)^2 + (\sigma_y)^2 + (\sigma_x)^2 \right] + 3 \cdot \tau^2} \quad \gamma_{R_{PCMY}} := \gamma_C \cdot \frac{\sigma_{VM}}{\sigma_Y}$$

PFLB - Plate Failure Local Buckling

$$\sigma_{axcr} := -4 \cdot \frac{\pi^2 \cdot D}{b^2 \cdot t} \quad k_S := 5.35 + 4 \cdot \left(\frac{b}{a} \right)^2 \quad \tau := 0 \cdot \text{psi} \quad \tau_{cr} := -k_S \cdot \frac{\pi^2 \cdot D}{b^2 \cdot t} \quad R_S := \frac{\tau}{\tau_{cr}}$$

interaction

formula: $R_C := 1 - R_S^2$ $\sigma_o := -R_C \cdot \sigma_{axcr}$ $R_{PFLB} := \frac{\sigma_C}{\sigma_o}$ $\gamma_{R_{PFLB}} := \gamma_S \cdot R_{PFLB}$

STIFFENED PANEL LIMIT STATES

Stiffener Sizing:

$$\text{HSW} := \text{DEPTH} - \text{TSF} \quad A_w := (\text{DEPTH} - \text{TSF}) \cdot \text{TSW} \quad A_f := \text{BSF} \cdot \text{TSF} \quad (6-1)$$

$$A_s := A_w + A_f \quad A_p := b \cdot t \quad L := a$$

Combination of plate and stiffeners (from p287, equation 8.3.6 in text):

$$d := \text{DEPTH} - \frac{\text{TSF}}{2} + \frac{t}{2} \quad A := A_s + A_p \quad C_1 := \frac{A_w \cdot \left(\frac{A}{3} - \frac{A_w}{4} \right) + A_f \cdot A_p}{(A)^2} \quad I := A \cdot d^2 \cdot C_1$$

$$y_f := - \left(d \cdot \frac{\frac{A_w}{2} + A_p}{A} \right) \quad y_p := d \cdot \left(1 - \frac{\frac{A_w}{2} + A_p}{A} \right) \quad M_{\text{bend}} := - \left(p \cdot b \cdot \frac{L^2}{12} \right) \quad M_{\text{bcen}} := p \cdot b \cdot \frac{L^2}{12} \quad (6-2)$$

$$c_f := y_f - .5 \cdot \text{TSF} \quad c_p := .5 \cdot t + y_p \quad (\text{y is to mid-point})$$

PYTF - Panel Yield Tension Flange $\gamma_S := 1.25$

$$\sigma_{ax} := \sigma_T \quad \sigma_{bx} := \frac{(M_{\text{bcen}} \cdot c_f)}{I} \quad \sigma_x := \sigma_{ax} + \sigma_{bx} \quad (6-3)$$

$$R_{\text{PYTF}} := \frac{-\sigma_x}{\sigma_Y} \quad \gamma R_{\text{PYTF}} := \gamma_S \cdot R_{\text{PYTF}}$$

PYCF - Panel Yield Compression Flange

$$\sigma_{ax} := \sigma_C \quad \sigma_{bx} := \frac{-(M_{\text{bend}} \cdot c_f)}{I} \quad \sigma_x := \sigma_{ax} + \sigma_{bx} \quad R_{\text{PYCF}} := \frac{\sigma_x}{\sigma_Y} \quad (6-4)$$

$$\gamma R_{\text{PYCF}} := \gamma_S \cdot R_{\text{PYCF}}$$

PCCB - Panel Collapse Combined Buckling

$$b_{\text{rat}} := .7 \quad \nu = 0.3$$

$$\text{let: } b_e := b_{\text{rat}} \cdot b \quad A_e := A_s + b_e \cdot t \quad C_1 := \frac{A_w \cdot \left(\frac{A_e}{3} - \frac{A_w}{4} \right) + A_f \cdot b_e \cdot t}{A_e^2} \quad I_e := A_e \cdot d^2 \cdot C_1$$

$$\rho_e := \sqrt{\frac{I_e}{A_e}} \quad \gamma_x := \frac{12 \cdot (1 - \nu^2) \cdot I_e}{b_e \cdot t^3}$$

$$C_\pi := \min \left[\left[\frac{B}{a} \cdot \frac{\sqrt{\gamma_x}}{\sqrt{2 \cdot (1 + \sqrt{1 + \gamma_x})}} \right], \left[\frac{1}{1} \right] \right] \quad \sigma_{\text{ecr}} := \frac{\pi^2 \cdot E}{\left(\frac{C_\pi \cdot L}{\rho_e} \right)^2} \quad b_e := \frac{C_\pi \cdot L \cdot t}{\rho_e \cdot \sqrt{3 \cdot (1 - \nu^2)}} \quad \frac{b_e}{b} = 1.715 \quad \text{Check, must equal } b_{\text{rat}}$$

$$\sigma_{\text{axcr}} := \left(\frac{b_e \cdot t + A_s}{b \cdot t + A_s} \right) \cdot \sigma_{\text{ecr}} \quad \gamma_{\text{RCCB}} := \gamma_C \cdot \frac{\sigma_C}{\sigma_{\text{axcr}}}$$

- PCSB - Panel Collapse Stiffener Buckling

$$I_{sz} := \frac{1}{12} \cdot (\text{HSW} \cdot \text{TSW}^3 + \text{TSF} \cdot \text{BSF}^3) \quad I_{sp} := d^2 \cdot \left(A_f + \frac{A_w}{3} \right) \quad J := \frac{\text{BSF} \cdot \text{TSF}^3 + (\text{HSW}) \cdot \text{TSW}^3}{3}$$

$$C_r := \frac{1}{1 + .4 \left(\frac{t}{\text{TSW}} \right)^3 \cdot \frac{d}{b}} \quad m := \frac{a}{\pi} \cdot \left(\frac{4 \cdot D \cdot C_r}{E \cdot I_{sz} \cdot d^2 \cdot b} \right)^{\frac{1}{4}}$$

recalling that; if $1 < m < 2$, value obtained is conservative

$$\text{for } m=1: \quad \sigma_{at1} := \frac{1}{I_{sp} + \frac{2 \cdot C_r \cdot b^3 \cdot t}{\pi^4}} \cdot \left[G \cdot J + \frac{\pi^2 \cdot E \cdot I_{sz} \cdot d^2}{a^2} + \frac{4 \cdot D \cdot C_r \cdot (a^2 + b^2)}{\pi^2 \cdot b} \right]$$

$$\text{for } m=2: \quad \sigma_{at2} := \frac{1}{I_{sp} + \frac{2 \cdot C_r \cdot b^3 \cdot t}{\pi^4}} \cdot \left(G \cdot J + 4 \cdot \sqrt{\frac{D \cdot C_r \cdot E \cdot I_{sz} \cdot d^2}{b}} + \frac{4 \cdot D \cdot C_r \cdot b}{\pi^2} \right)$$

$$\sigma_{at} := \min \left(\left(\begin{array}{l} \sigma_{at1} \\ \sigma_{at2} \end{array} \right) \right) \quad \gamma_{R_{PCSB}} := \gamma_C \cdot \frac{\sigma_C}{\sigma_{at}}$$

PCSF - Panel Collapse Stiffener Flexure. Use limiting mode (Mode I, II).

Rule of thumb for eccentricity of welded panels: $\Delta := \frac{a}{750}$ $\sigma_{ax} := \sigma_C$ (6-16)

a. Mode I (Point E of fig. 14.2) Compression failure of flange: $M_o := 0 \cdot \text{lbf} \cdot \text{in}$ $\delta_o := 0 \cdot \text{in}$ $\Delta_I := -\Delta$ (6-17)

Beam column parameters:

$$\rho_I := \sqrt{\frac{I}{A}} \quad \lambda_I := \frac{a}{\pi \cdot \rho_I} \cdot \sqrt{\frac{\sigma_Y}{E}} \quad \eta_I := \frac{(\delta_o + \Delta_I) \cdot y_f}{(\rho_I)^2} \quad \mu_I := \frac{M_o \cdot y_f}{I \cdot \sigma_Y} \quad \zeta_I := 1 - \mu_I + \frac{1 + \eta_I}{(\lambda_I)^2}$$

$$R := \frac{\zeta_I}{2} - \sqrt{\frac{(\zeta_I)^2}{4} - \frac{1 - \mu_I}{(\lambda_I)^2}} \quad \text{limit state} \quad \sigma_{axu} := R \cdot \sigma_Y \quad R_{PCSF1} := \frac{\sigma_{ax}}{\sigma_{axu}} \quad \gamma R_{PCSF1} := \gamma C \cdot R_{PCSF1} \quad (6-18)$$

b. Mode II Compression failure of plate:

For maximum moment and center deflection assume simply supported beam:

$$q := p \cdot b \quad M_o := \frac{q \cdot a^2}{8} \quad \delta_o := \frac{5 \cdot q \cdot a^4}{384 E \cdot I} \quad (6-23)$$

determine failure stress using plate parameters

$$\beta := \frac{b}{t} \cdot \sqrt{\frac{\sigma_Y}{E}} \quad \xi := 1 + \frac{2.75}{(\beta)^2} \quad T := .25 \left[2 + \xi - \sqrt{(\xi)^2 - \frac{10.4}{(\beta)^2}} \right] \quad (6-19)$$

$$b_{tr} := T \cdot b \quad \sigma_F := \frac{T - .1}{T} \cdot \sigma_Y \cdot \sqrt{1 - 3 \cdot \left(\frac{\tau}{\sigma_Y} \right)^2} \quad (6-20)$$

For combination (from equation 8.3.6 in text) and transformed plate:

$$A_{ptr} := b_{tr} \cdot t \quad A_{tr} := A_s + A_{ptr} \quad C_{1tr} := \frac{A_w \cdot \left(\frac{A_{tr}}{3} - \frac{A_w}{4} \right) + A_f \cdot A_{ptr}}{(A_{tr})^2} \quad I_{tr} := A_{tr} \cdot (d)^2 \cdot C_{1tr} \quad (6-21)$$

$$y_{ftr} := -d \cdot \frac{\frac{A_w}{2} + b_{tr} \cdot t}{A_{tr}} \quad y_{ptr} := d \cdot \left(1 - \frac{\frac{A_w}{2} + b_{tr} \cdot t}{A_{tr}} \right) \quad \rho_{tr} := \sqrt{\frac{I_{tr}}{A_{tr}}} \quad \lambda := \frac{a}{\pi \cdot \rho_{tr}} \cdot \sqrt{\frac{\sigma_F}{E}} \quad (6-22)$$

Correction for load eccentricity:

$$h := SCG + \frac{t}{2} \quad \Delta_p := h \cdot A_s \cdot \left(\frac{1}{A_{tr}} - \frac{1}{A} \right) \quad \eta_p := \Delta_p \cdot \frac{y_{ptr}}{(\rho_{tr})^2} \quad (6-24)$$

Beam column with σ_F and transformed geometry

$$\eta := \frac{(\delta_o + \Delta) \cdot y_{ptr}}{(\rho_{tr})^2} \quad \mu := \frac{M_o \cdot y_{ptr}}{I_{tr} \cdot \sigma_F} \quad \zeta := \frac{1 - \mu}{1 + \eta_p} + \frac{1 + \eta_p + \eta}{(1 + \eta_p) \cdot (\lambda)^2} \quad R := \frac{\zeta}{2} - \sqrt{\frac{(\zeta)^2}{4} - \frac{1 - \mu}{(1 + \eta_p) \cdot (\lambda)^2}} \quad (6-25)$$

limit state

$$\sigma_{axtru} := R \cdot \sigma_F \quad \sigma_{axu} := \frac{A_{tr}}{A} \cdot \sigma_{axtru} \quad R_{PCSF2} := \frac{\sigma_{ax}}{\sigma_{axu}} \quad \gamma_{R_{PCSF2}} := R_{PCSF2} \quad (6-26)$$

RESULTS:

$$t = 3 \text{ in}$$

$$b = 21 \text{ in}$$

$$\gamma_{R_{PCMY}} = 0.750$$

$$\gamma_{R_{PSPBT}} = 0.725$$

$$\gamma_{R_{PSPBL}} = 0.741$$

$$\gamma_{R_{PYTF}} = 0.996$$

$$\gamma_{R_{PFLB}} = 0.023$$

$$\gamma_{R_{PCCB}} = 0.052$$

$$\gamma_{R_{PCSB}} = 0.031$$

$$\gamma_{R_{PYCF}} = 0.254$$

$$\gamma_{R_{PCSF1}} = 0.798$$

$$\gamma_{R_{PCSF2}} = 0.652$$

$$\text{DEPTH} \equiv 6 \text{ in}$$

$$\text{TSW} \equiv 1.5 \text{ in}$$

$$\text{BSF} \equiv 6 \text{ in}$$

$$\text{TSF} \equiv 2.00 \text{ in}$$

$$\text{SCG} \equiv 5 \text{ in}$$

$$N \equiv 6$$

$$B \equiv 12.25 \text{ ft}$$

$$a \equiv 4 \text{ ft}$$

$$t \equiv 3.00 \text{ in}$$

$$H_{LCL} \equiv 1000 \text{ ft}$$

Forward Watertight Bulkhead Design

FORWARD WATERTIGHT BULKHEAD DESIGN

$$D := 34 \text{ ft} \quad \rho := 64 \frac{\text{lb}}{\text{ft}^3} \quad D_t := 1000 \text{ ft} \quad g := 32.2 \frac{\text{ft}}{\text{sec}^2} \quad \text{SF} := 1.5$$

$$P := \rho \cdot g \cdot D_t \cdot \text{SF} \quad R := \frac{D}{2}$$

Transverse Shear Beams

$$N_{\text{TSB}} := 2$$

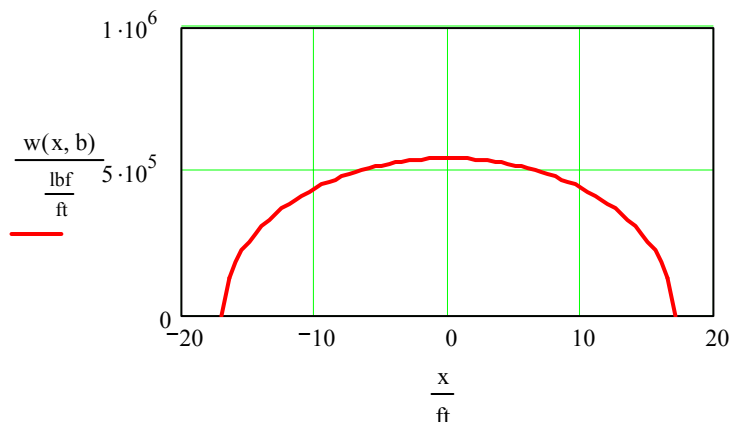
$$F_{\text{TSB}} := \frac{P \cdot \pi \cdot R^2}{2 + 4(N_{\text{TSB}} - 1)} \quad F_{\text{TSB}} = 1.454 \times 10^7 \text{ lbf}$$

$$y(x, b) := \sqrt{b^2 \cdot \left(1 - \frac{x^2}{R^2}\right)} \quad w(x, b) := y(x, b) \cdot \frac{\text{lbf}}{\text{ft}^2}$$

$$x := -R, -R + .5 \cdot \text{ft} .. R$$

$$b_{\text{guess}} := 1 \cdot \text{ft}$$

$$b := \text{root} \left(\int_{-R}^R w(x, b_{\text{guess}}) dx - F_{\text{TSB}}, b_{\text{guess}} \right) \quad b = 5.444 \times 10^5 \text{ ft}$$



$$t_w = 1.25 \text{ in}$$

$$t_f = 1.25 \text{ in}$$

$$t_{bkhd} = 1.25 \text{ in}$$

$$h_w = 84 \text{ in}$$

$$w_f = 132 \text{ in}$$

$$h_{na} := \frac{\left[t_f w_f \left(h_w + \frac{t_f}{2} \right) - R \cdot \frac{t_{bkhd}^2}{4} + t_w \frac{h_w^2}{2} \right]}{t_w h_w + t_{bkhd} \frac{R}{2} + t_f w_f} \quad h_{na} = 46.021 \text{ in}$$

$$I := t_w \frac{h_w^3}{12} + t_w h_w (t_w - h_{na})^2 + \frac{R}{24} t_{bkhd}^3 + \frac{R}{2} t_{bkhd} \left(\frac{-t_{bkhd}}{2} \right)^2 \dots$$
$$+ w_f \frac{t_f^3}{12} + w_f t_f \left(t_w + \frac{t_f}{2} - h_{na} \right)^2$$

$$I = 28.639 \text{ ft}^4$$

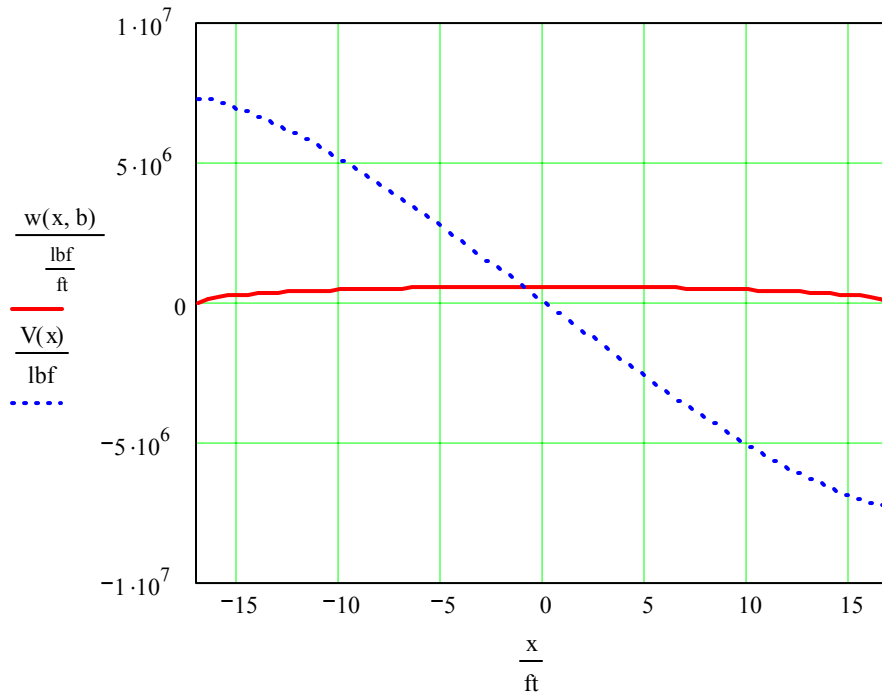
$$V(x) := \frac{F_{TSB}}{2} - \int_{-R}^x w(x, b) dx$$

$$V(-R) = 7.269 \times 10^6 \text{ lbf}$$

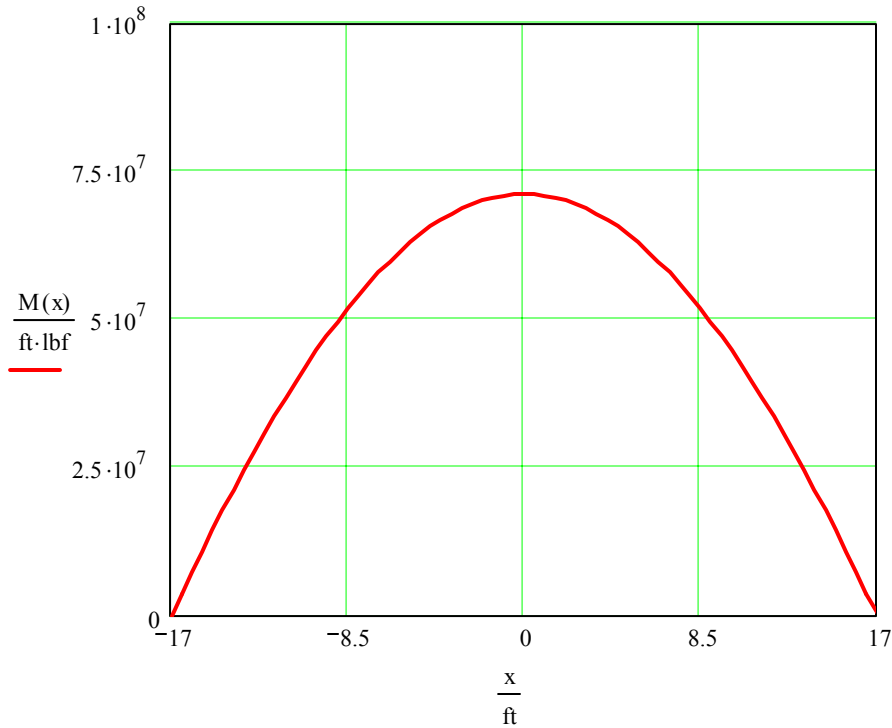
$$M(x) := \int_{-R}^x V(x) dx$$

$$M(0) = 7.113 \times 10^7 \text{ ft} \cdot \text{lbf}$$

Shear Girder Load and Shear Diagram:



Shear Girder Moment Diagram:



Shear Girder Working Stress Summary

$$t_w = 1.25 \text{ in}$$

$$t_f = 1.25 \text{ in}$$

$$t_{bkhd} = 1.25 \text{ in}$$

$$h_w = 84 \text{ in}$$

$$w_f = 132 \text{ in}$$

$$\sigma_{bkhd} := M(0\text{-ft}) \cdot \frac{(h_{na} + t_{bkhd})}{I}$$

$$\sigma_{bkhd} = 6.794 \times 10^4 \text{ psi}$$

$$\sigma_{flange} := M(0\text{-ft}) \cdot \frac{(h_w + t_f + -h_{na})}{I}$$

$$\sigma_{flange} = 5.638 \times 10^4 \text{ psi}$$

$$\sigma_{xy} := \frac{V(-R)}{t_w \cdot h_w + t_f \cdot w_f}$$

$$\sigma_{xy} = 2.692 \times 10^4 \text{ psi}$$

Verticle Stiffeners:

$$N_s = 7$$

$$L_{\text{stiff}} = 11 \cdot \text{ft}$$

$$F_{\text{stiff}} := \frac{F_{\text{TSB}}}{N_s + 1}$$

$$F_{\text{stiff}} = 1.817 \times 10^6 \text{ lbf}$$

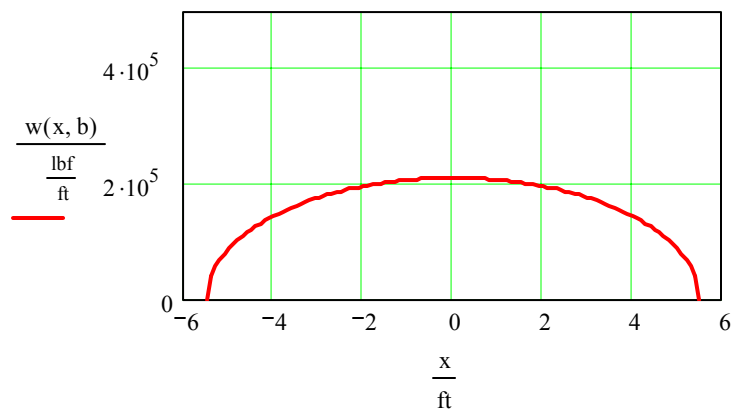
$$y(x, b) := \sqrt{b^2 \cdot \left[1 - \frac{x^2}{\left(\frac{L_{\text{stiff}}}{2}\right)^2} \right]}$$

$$w(x, b) := y(x, b) \cdot \frac{\text{lbf}}{\text{ft}^2}$$

$$x := \frac{-L_{\text{stiff}}}{2}, \frac{-L_{\text{stiff}}}{2} + .1 \cdot \text{ft}.. \frac{L_{\text{stiff}}}{2}$$

$$b_{\text{guess}} := 1 \cdot \text{ft}$$

$$b := \text{root} \left(\int_{\frac{-L_{\text{stiff}}}{2}}^{\frac{L_{\text{stiff}}}{2}} w(x, b_{\text{guess}}) \, dx - F_{\text{stiff}}, b_{\text{guess}} \right) \quad b = 2.104 \times 10^5 \text{ ft}$$



$$t_{ws} = 1 \text{ in}$$

$$t_{fs} = 2 \text{ in}$$

$$h_{ws} = 32 \text{ in}$$

$$w_{fs} = 18 \text{ in}$$

$$h_{na} := \frac{\left[t_{fs} \cdot w_{fs} \cdot \left(h_{ws} + \frac{t_{fs}}{2} \right) - D \cdot \frac{t_{bkhd}^2}{2 \cdot (N_s + 1)} + t_{ws} \cdot \frac{h_{ws}^2}{2} \right]}{t_{ws} \cdot h_{ws} + t_{bkhd} \cdot \frac{D}{N_s + 1} + t_{fs} \cdot w_{fs}} \quad h_{na} = 12.601 \text{ in}$$

$$I := t_{ws} \cdot \frac{h_{ws}^3}{12} + t_{ws} \cdot h_{ws} \cdot (t_{ws} - h_{na})^2 + \frac{R}{24} \cdot t_{bkhd}^3 + \frac{R}{2} \cdot t_{bkhd} \cdot \left(\frac{-t_{bkhd}}{2} \right)^2 \dots$$

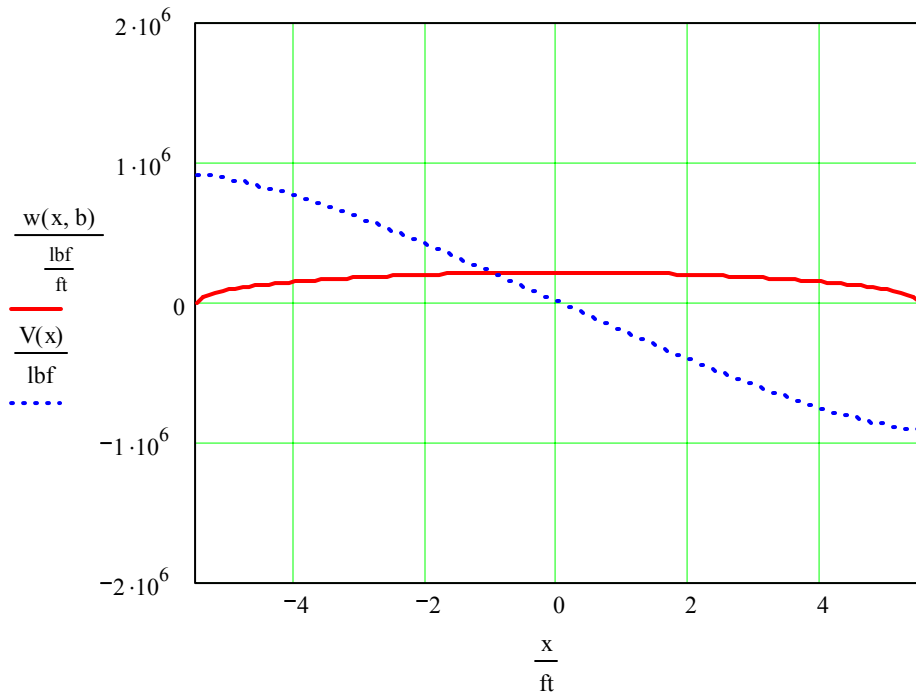
$$+ w_{fs} \cdot \frac{t_{fs}^3}{12} + w_{fs} \cdot t_{fs} \cdot \left(t_{ws} + \frac{t_{fs}}{2} - h_{na} \right)^2$$

$$I = 0.538 \text{ ft}^4$$

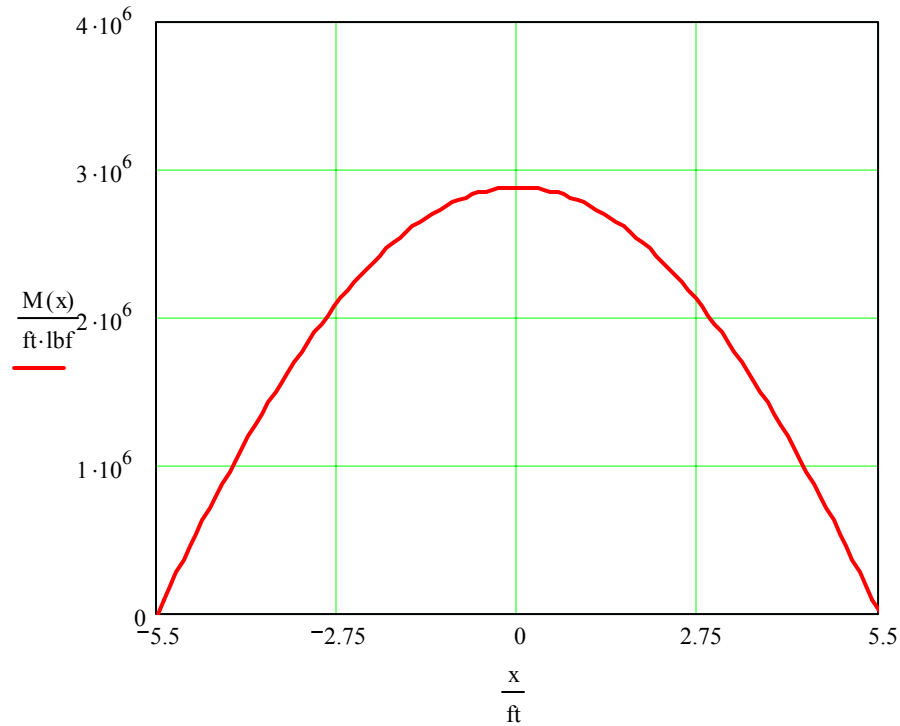
$$V(x) := \frac{F_{stiff}}{2} - \int_{\frac{-L_{stiff}}{2}}^x w(x, b) \, dx \quad V\left(\frac{-L_{stiff}}{2}\right) = 9.087 \times 10^5 \text{ lbf}$$

$$M(x) := \int_{\frac{-L_{stiff}}{2}}^x V(x) \, dx \quad M(0\text{-ft}) = 2.877 \times 10^6 \text{ ft}\cdot\text{lbf}$$

Vertical Stiffener Load and Shear Diagram



Vertical Stiffener Moment Diagram



Vertical Stiffener Working Stress Summary

$$t_{ws} = 1.0 \text{ in}$$

$$t_{fs} = 2.0 \text{ in}$$

$$h_{ws} = 32 \text{ in}$$

$$w_{fs} = 18 \text{ in}$$

$$\sigma_{bkhd} := M(0 \text{ ft}) \cdot \frac{(h_{na} + t_{bkhd})}{I}$$

$$\sigma_{bkhd} = 4.284 \times 10^4 \text{ psi}$$

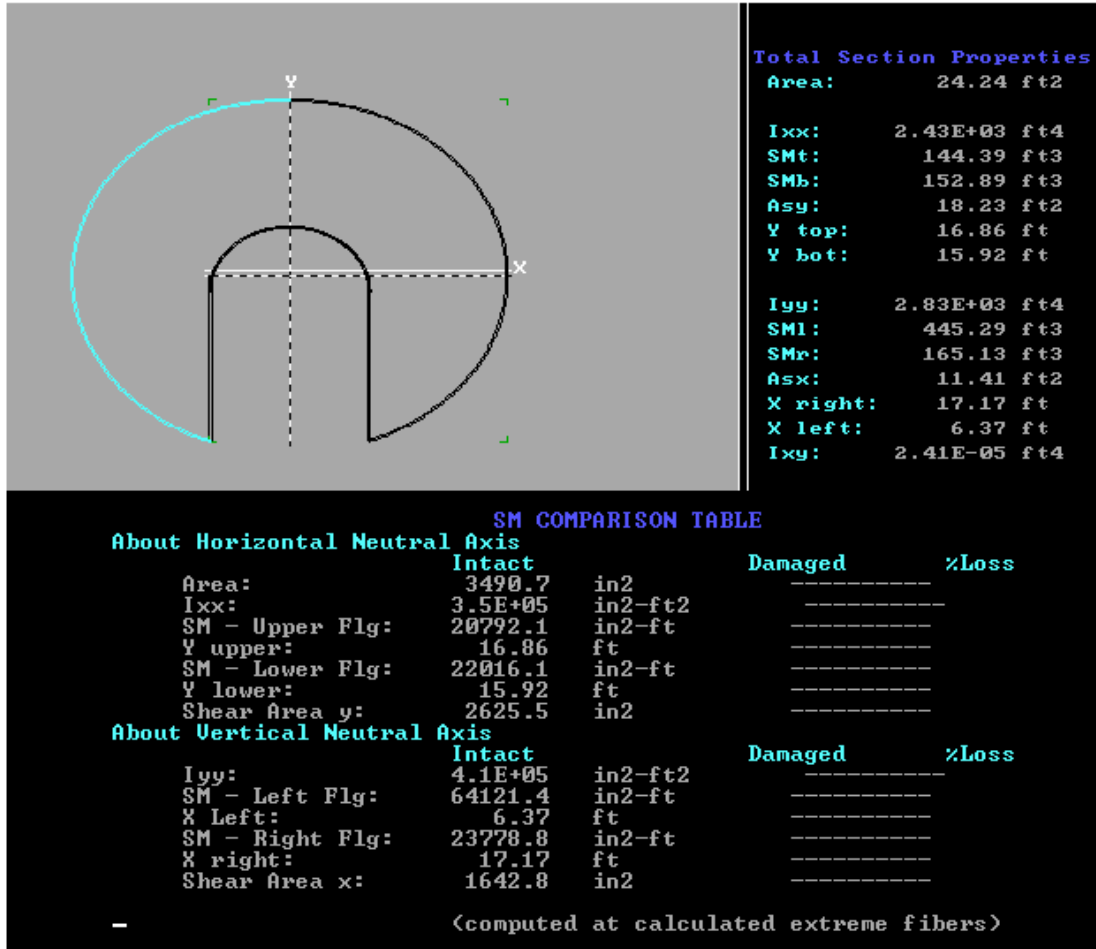
$$\sigma_{flange} := M(0 \text{ ft}) \cdot \frac{(h_{ws} + t_{fs} + -h_{na})}{I}$$

$$\sigma_{flange} = 6.618 \times 10^4 \text{ psi}$$

$$\sigma_{xy} := \frac{V \left(\frac{-L_{stiff}}{2} \right)}{t_{ws} \cdot h_{ws} + t_{fs} \cdot w_{fs}}$$

$$\sigma_{xy} = 1.336 \times 10^4 \text{ psi}$$

D. POSSE Section Calculations



E. Bending Moment Calculation for Asymmetric Hull Section

Moment at Top Center of Shell:

$$P := 440\text{psi} \quad \text{Length} := 26\text{ft} \quad r := 17\text{ft}$$

$$M_{\text{hull}} := \int_0^{2.7925} P \cdot \text{Length} \cdot r \cdot (r - r \cdot \cos(\theta)) \cdot (\sin(\theta)) \, d\theta$$

$$M_{\text{hull}} = 1.214 \times 10^9 \text{ J}$$

$$\text{Arm}_{\text{crane}} := 24\text{ft} \quad A_{\text{crane}} := 25\text{ft} \cdot 18\text{ft}$$

$$M_{\text{crane}} := P \cdot A_{\text{crane}} \cdot \text{Arm}_{\text{crane}}$$

$$M_{\text{crane}} = 9.278 \times 10^8 \text{ J}$$

$$\text{Moment}_{\text{top}} := M_{\text{hull}} - M_{\text{crane}}$$

$$\text{Moment}_{\text{top}} = \blacksquare \text{ lbf} \cdot \text{ft}$$

Moment at Top of a Traditional Ring Stiffened Cylinder

$$M_{\text{cyl_hull}} := \int_0^{2.7925} P \cdot \text{Length} \cdot r \cdot (r - 1\text{ft} + r \cdot \cos(\theta)) \cdot (\sin(\theta)) \, d\theta$$

$$M_{\text{cyl_hull}} = \blacksquare \text{ lbf} \cdot \text{ft}$$

Moment at Hull/Payload Bay Union

$$M_{\text{crane2}} := P \cdot A_{\text{crane}} \cdot 8\text{ft}$$

$$M_{\text{bottom}} := M_{\text{cyl_hull}} + M_{\text{crane2}}$$

$$M_{\text{bottom}} = \blacksquare \text{ ft} \cdot \text{lbf}$$

$$\frac{M_{\text{bottom}}}{\text{Moment}_{\text{top}}} = \blacksquare$$

F. Detailed Weight and Moment Data

PLUG Weight and Gravity Center Calculations

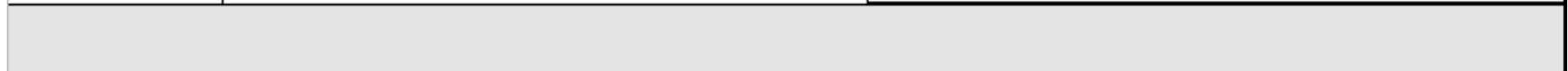
PLUG Length (ft)								
46				Weight (Lton)	VCG (ft)	V _{moment} (ft*Lton)	LCG (ft)	L _{moment} (ft*Lton)
Shell	Thickness (in)	Diameter (ft)						
	2.25	34		201.25	17.40	3501.74	205.00	41256.13
Main Frame Space	Frame Space (in)	Avg Frame Weight (Tons)						
	22.00	3.6		79.53	18.80	1495.11	205.00	16303.09
King Frames	Number of King Frames	Avg Frame Weight (Tons)						
	1.00	3.87		3.87	17.60	68.11	182.50	706.28
	2.00	3.87		3.87	17.60	68.11	198.81	769.39
	3.00	3.87		3.87	17.60	68.11	227.50	880.43
Crane Space Structure	Surface Area (sq.ft)							
	1666.50			68.35	12.20	833.90	213.50	14593.27
Additional Structural Stiffeners				12.00	0.77	9.24	213.50	2562.00
Variable Ballast Control	Pumps +Foundation	Piping, Hangars						
	10.20	5.8		16.00	18.40	294.40	224.00	3584.00
Ventillation	Piping							
	3.50			3.50	22.81	79.84	205.00	717.50
FWD Water Tight Bulkhead	Area (sq. ft)							
	907.92			198.61	17.00	3376.33	182.00	36146.57
Decking and Support Structure	Number Decks	Square feet						
	4.00	2286.04		62.51	23.10	1578.94	204.50	13978.09
ROV Pressure Cylinder	Cylinder (Lton)	34.30		80.04	12.29	421.51	191.04	6552.10
	Upper Head (Lton)	17.20			21.64	372.21	191.04	3285.89
	Tunnel Access & Hatch (B23Lton)	11.00			12.18	133.98	191.04	2101.44
	Lower Head (Lton)	12.40			4.28	53.07	191.04	2368.90
	Hatch(Lton)	5.15			2.66	13.69	191.04	982.90
ROV Lifting Motor	Motor (Lton)	Hangars and Assembly (Lton)						
	4.60	2.2		6.80	21.50	146.20	190.31	1294.11
Lower Cylindrical Pressure Boundary	Arc Length (deg)	Length(ft)						
	75.00	17		21.62	5.40	116.74	191.04	4129.86
Hydraulic Plant	Pumps+Foundation (Lton)	Piping, Hangars, & Oil (Lton)						
	17.60	9.5		27.10	12.95	350.95	189.55	5136.81
Crane Reel	Reel Cage (lton)	Cable (Lton)						
	4.80	2.9		7.75	15.82	122.55	213.50	1653.86
Crane Motor	Motor Weight (Lton)	Hangars and Support (Lton)						
	9.80	4.8		14.60	17.20	251.12	213.50	3117.10
4500# Air Flasks	Starboard Flasks (Lton)	Port Flasks (Lton)						
	14.30	14.3		28.60	14.40	411.84	207.41	5931.93
Lifting Rack	Length (ft)	Width (ft)						
	23.00	12		6.04	12.55	75.77	213.50	1289.01
ROV Control Stations	Number Stations	Weight per Station (Lton)						
	4.00	2.1		8.40	27.20	228.48	220.96	1856.06

PLUG Weight and Gravity Center Calculations (cont...)

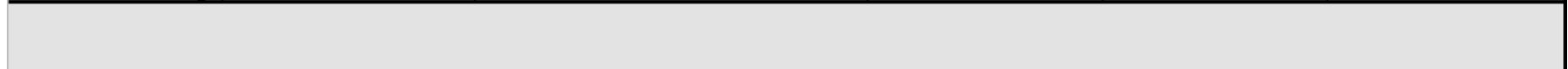
Crane Control Stations	Number Stations	Weight per Station (Lton)						
	4.00	1.2		4.80	27.20	130.56	220.96	1060.61
Electrical Cabling and Switch Boards				22.10	20.50	453.05	205.00	4530.50
			A-1(PLUG Weight)	881.20				
				Moment Sum:		14655.54		176787.81
					A-1 _{VCG}	16.63		
					A-1 _{LCG}	200.62		
LEAD				25.32	4.00	101.28	203.00	5139.96
			A (PLUG with Lead)	906.52				
				Moment Sum:		14756.82		181927.77
					A _{VCG}	16.28		
					A _{LCG}	200.69		
Variable Load Items								
ROV	3.80			32.53	6.99	26.56	191.35	727.13
Consumables	5.00				26.48	132.40	192.00	960.00
Stores	3.00				26.46	79.38	197.00	591.00
Oil	5.00				8.90	44.50	189.30	946.50
Cargo	14.73				7.00	103.11	213.50	3144.86
Personnel	1.00				27.00	27.00	192.00	192.00
			PLUG with Variable Load Items	939.05				
				Moment Sum:		15169.77		188489.25
					VCG	16.15		
					LCG	200.72		
Variable Ballast	Port (Lton)	Stbd (Lton)						
	30.00	30		60.00	9.45	567.00	217.61	13056.60
			NSC (PLUG with Variable Load and Ballast)	999.05				
				Moment Sum:		15736.77		201545.85
					NSC _{VCG}	15.75		
					NSC _{LCG}	201.74		
ROV Space	Length (ft) 17.00	Width (ft) 19	Height (ft) 5	34.61	3.20	110.74	191.25	6618.62
Free Flood								
			PLUG with Free Flood Weight	1033.66				
				Moment Sum:		15847.52		208164.47
					VCG	15.33		
					LCG	201.39		
MBT								
Crane Space	Length (ft) 26.00	Width (ft) 12	Height (ft) 22.5	159.61	10.70	1707.83	213.50	34076.74
			Submerged Plug	1158.66				
				Moment Sum:		17555.34		242241.20
					SUB _{VCG}	15.15		
					SUB _{LCG}	209.07		
			TOTAL Submerged Section	1158.66	Lton			
			Envelope Bouyancy	1158.66	Lton			

Master Balance Sheet

L:	423.33 ft	Color Code	
D:	34 ft	RED:	Input from MathCad
BG Submerged:	1 ft	GREEN:	User variable
ROB	12.84%	BLACK:	Internal calculation



	Weight (lton)	L. Arm (ft)	L. Moment (ft-lton)	V. Arm (ft)	V. Moment (ft-lton)
Condition A-1:	6903.93	197.88	1366149.52	16.63	114812.35
Lead:	500.27	204.43	102270.20	11.13	5568.01
Condition A:	7404.20	198.32	1468419.72	16.26	120380.36
VLI:	292.97	204.46	59902.25	13.45	3941.47
V. Ballast:	164.00	179.31	29406.84	7.71	1264.00
VL	456.97	195.44	89309.09	11.39	5205.47
NSC:	7861.17	198.15	1557728.80	15.98	125585.83
MBT:	1009.55	144.63	146007.17	16.19	16344.46
Subm Disp:	8870.72	192.06	1703737.43	16.00	141931.59



Weight Error (lton):	0.00	if + Reduce lead and/or VB
LCG Error (ft):	0.00	if + Move lead and/or VB forward
LCG Error (ft):	0.00	if + Move lead lower

PROPOSED "FIXES"	
0.00	lead (or VB) increase
0.00	lead LCG increase
0.00	lead VCG increase

REQUIREMENTS

Endurance:	55	days
Chill Stores Endurance:	30	days

	Length (ft)	Packing Factor
NFO Tank	12	0.6

Provisions	Util Factor	lb/man/day	Density	Wt (lbs)	Vol (ft³)
Dry	0.7	4.52	35	24114.2	984.3
Freeze	0.5	1.62	39	8642.7	443.2
Chill	0.5	0.87	23	2531.7	220.1

		Weight	Weight		Space	
Crew	Number	lbs allowed	lbs per man	Totals	Allowed	Total
Officers	10	240	160	4000	30	300
CPO	12	170	160	3960	25	300
Enlisted	75	70	160	17250	10	750
Total	97			25210		1350

Torpedos		
Number	28	
Weight	1.65	LT
Volume	70	ft ³

Variable Load Items

Variable Load Items							
PLUG Length:	46	ft					
NSTM	Factor	Weight (lton)	L. Arm (ft)	L. Moment(ft-lton)	Vol (ft ³)	V. Arm (ft)	V. Moment (ft-lton)
Group 1							
Crew	Calc from Requirements	11.25	137.24	1544.60	0.00	17.00	191.33
San Tanks	0.167	16.17	133.39	2156.49	582.00	10.20	164.90
Dep. Con.	Given	0.00	0.00	0.00	0.00	0.00	0.00
L. O. Sump	Given	9.00	329.21	2962.87	518.25	10.20	91.80
Nitrogen	Given	0.50	96.65	48.32	18.00	10.20	5.10
Group 2							
Pot. Wtr	0.167	16.17	101.22	1636.36	582.00	6.80	109.93
RFT	Given	50.00	318.29	15914.29	1800.00	11.90	595.00
Bat. FW	Given	1.20	163.57	196.29	43.20	6.80	8.16
Pure Wtr.	Given	10.00	264.18	2641.84	360.00	17.00	170.00
Group 3							
Provision		15.75	166.07	2616.28	1647.62	17.00	267.82
Gen. Stores	Given	15.00	240.48	3607.17	540.00	17.00	255.00
Oxygen	Given	0.80	143.25	114.60	28.80	11.90	9.52
O ₂ Candles	Given	0.50	143.25	71.63	18.00	13.60	6.80
Group 4							
L. O. Stow.	Given	10.00	329.21	3292.08	575.84	10.20	102.00
Group 5							
NF Oil	L given in Requirements	52.45	196.90	10327.80	2136.28	17.00	891.71
Oil Collecting	Given	5.00	196.90	984.48	203.64	13.60	68.00
Oil Expansion	Given	5.00	196.90	984.48	203.64	13.60	68.00
Fuel Ballast	Given	0.00	0.00	0.00	0.00	0.00	0.00
Group 6							
Torpedos	1.650	46.20	109.05	5038.10	1960.00	13.60	628.32
Cargo	Given	0.00	0.00	0.00	0.00	13.60	0.00
Small Arm	Given	0.25	97.45	24.36	100.00	15.30	3.83
Hyd. Oil	Given	5.00	356.51	1782.56	270.53	13.60	68.00
Group 7							
Pass.	Given	0.00	0.00	0.00	0.00	17.00	0.00
Misc.	Given	0.00	0.00	0.00	0.00	0.00	0.00
Group 8							
Cargo Comp	Given	14.73	213.50	3144.86	1449.00	10.50	154.67
Group 9							
WRT & tube	2 LT/tank	4.00	101.60	406.40	140.00	10.20	40.80
Impulse Tanks	2 LT/tank	4.00	101.60	406.40	140.00	10.20	40.80
Group 10							
"D" TANK	Safety Tank	0.00	0.00	0.00	0.00	0.00	0.00
Totals		292.97	204.46	59902.25	13316.79	13.45	3941.47

Variable Ballast Tank Worksheet

Tank	Max Capacity	VB	% Full	L. Arm	L. Moment	V. Arm	V. Moment	Volume	Max Moment
	(lton)	(lton)		(ft)		(ft)		(ft3)	+ fwd, - aft
Aux1	32.79	16.00	48.80%	97.53	1560.48	8	128.00	1147.65	3742.49
Aux2	32.89	16.00	48.65%	97.54	1560.64	6	96.00	1151.15	3753.57
Aux3	17.71	6.50	36.70%	116.67	758.355	6	39.00	619.85	1682.36
Aux4	9.98	6.50	65.13%	116.66	758.29	6	39.00	349.3	948.15
Aux5	38.30	14.00	36.55%	141.67	1983.38	6	84.00	1340.5	2680.81
Aux6	30.78	14.00	45.48%	141.22	1977.08	6	84.00	1077.3	2168.30
Aux7	41.64	14.00	33.62%	160.82	2251.48	6	84.00	1457.4	2117.19
Plug Comp 1	65.00	30.00	46.15%	211.00	6330	9	270.00	2275	43.22
Plug Comp2	65.00	30.00	46.15%	211.00	6330	9	270.00	2275	43.22
ATT:	66.94	17.00	25.40%	346.89	5897.13	10	170.00	2342.9	-9051.96
Total:	401.03	164.00	40.89%	179.31	29406.84	7.71	1264.00	14036.05	

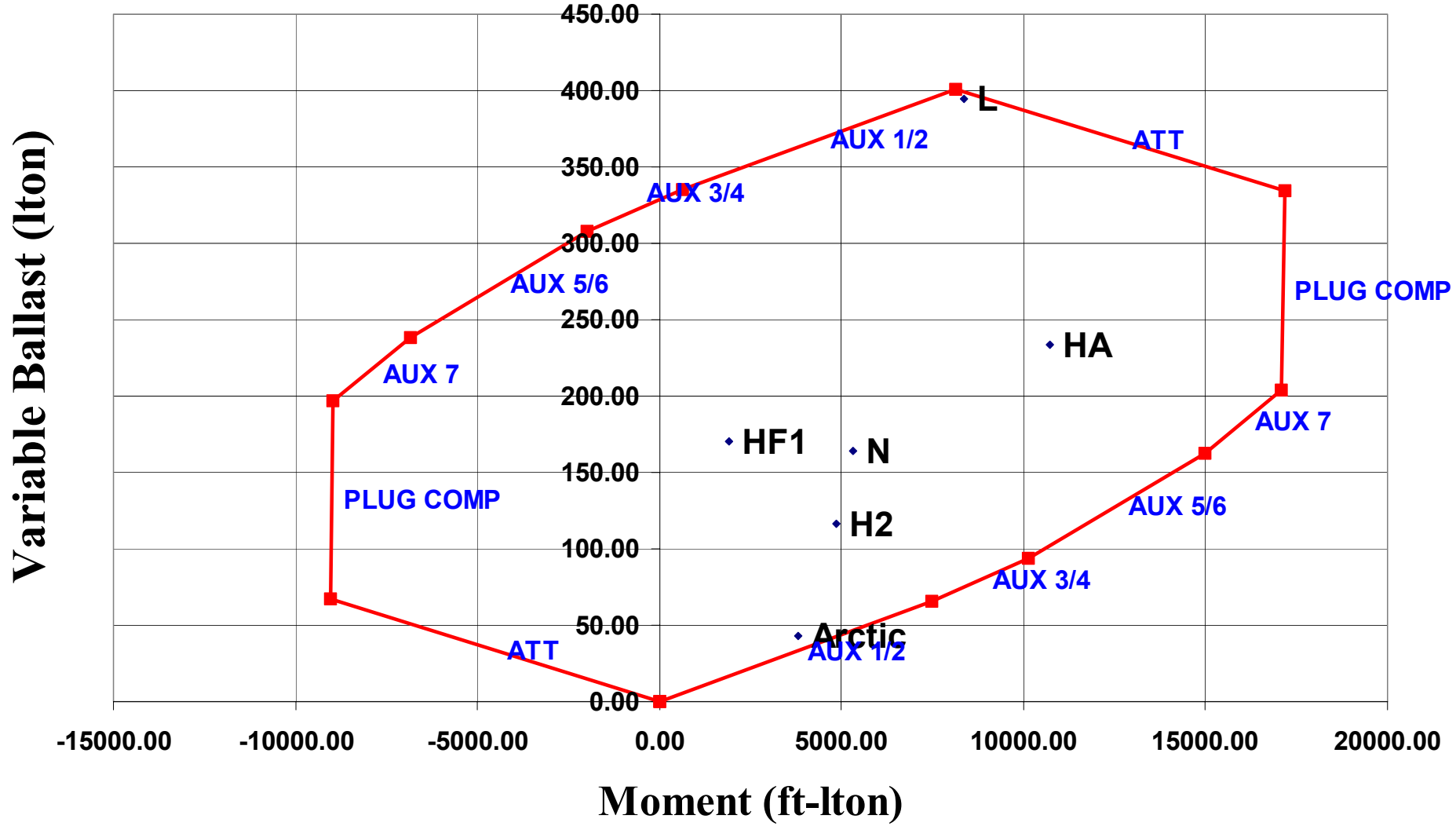
LOAD CONDITION COMPUTATION

	CONDITION N			HEAVY #2			HEAVY FWD #1			HEAVY AFT			LIGHT #2			ARCTIC		
	% FULL	weight	moment	% FULL	weight	moment	% FULL	weight	moment	% FULL	weight	moment	% FULL	weight	moment	% FULL	weight	moment
Group 1																		
Crew	100.00	11.25	1544.60	100.00	11.25	1544.60	100.00	11.25	1544.60	50.00	5.63	772.30	100.00	11.25	1544.60	100.00	11.25	1544.60
San Tanks	100.00	16.17	2156.49	100.00	16.17	2156.49	100.00	16.17	2156.49	50.00	8.08	1078.25	100.00	16.17	2156.49	100.00	16.17	2156.49
Dep. Con.	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00
L. O. Sump	100.00	9.00	2962.87	100.00	9.00	2962.87	100.00	9.00	2962.87	100.00	9.00	2962.87	100.00	9.00	2962.87	100.00	9.00	2962.87
Nitrogen	100.00	0.50	48.32	100.00	0.50	48.32	100.00	0.50	48.32	50.00	0.25	24.16	100.00	0.50	48.32	100.00	0.50	48.32
Group 2																		
Pot. Wtr	100.00	16.17	1636.36	100.00	16.17	1636.36	100.00	16.17	1636.36	100.00	16.17	1636.36	50.00	8.08	818.18	100.00	16.17	1636.36
RFT	100.00	50.00	15914.29	100.00	50.00	15914.29	50.00	25.00	7957.15	100.00	50.00	15914.29	50.00	25.00	7957.15	100.00	50.00	15914.29
Bat. FW	100.00	1.20	196.29	100.00	1.20	196.29	100.00	1.20	196.29	100.00	1.20	196.29	50.00	0.60	98.14	100.00	1.20	196.29
Pure Wtr.	100.00	10.00	2641.84	100.00	10.00	2641.84	50.00	5.00	1320.92	100.00	10.00	2641.84	50.00	5.00	1320.92	100.00	10.00	2641.84
Group 3																		
Provision	100.00	15.75	2616.28	100.00	15.75	2616.28	75.00	11.82	1962.21	50.00	7.88	1308.14	0.00	0.00	0.00	100.00	15.75	2616.28
Gen. Stores	100.00	15.00	3607.17	100.00	15.00	3607.17	75.00	11.25	2705.38	50.00	7.50	1803.58	0.00	0.00	0.00	100.00	15.00	3607.17
Oxygen	100.00	0.80	114.60	100.00	0.80	114.60	75.00	0.60	85.95	50.00	0.40	57.30	0.00	0.00	0.00	100.00	0.80	114.60
O2 Candles	100.00	0.50	71.63	100.00	0.50	71.63	75.00	0.38	53.72	50.00	0.25	35.81	0.00	0.00	0.00	100.00	0.50	71.63
Group 4																		
L. O. Stow.	100.00	10.00	3292.08	100.00	10.00	3292.08	75.00	7.50	2469.06	75.00	7.50	2469.06	50.00	5.00	1646.04	100.00	10.00	3292.08
Group 5																		
NF Oil	100.00	52.45	10327.80	100.00	52.45	10327.80	75.00	39.34	7745.85	50.00	26.23	5163.90	0.00	0.00	0.00	100.00	52.45	10327.80
Oil Collecting	100.00	5.00	984.48	100.00	5.00	984.48	100.00	5.00	984.48	SW	6.11	1203.28	111.43	5.57	1096.99	100.00	5.00	984.48
Oil Expansion	100.00	5.00	984.48	100.00	5.00	984.48	100.00	5.00	984.48	100.00	5.00	984.48	100.00	5.00	984.48	100.00	5.00	984.48
Fuel Ballast	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00
Group 6																		
Torpedos	100.00	46.20	5038.10	100.00	46.20	5038.10	100.00	46.20	5038.10	0.00	0.00	0.00	0.00	0.00	0.00	100.00	46.20	5038.10
Cargo	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	100.00	0.00	0.00
Small Arm	100.00	0.25	24.36	100.00	0.25	24.36	100.00	0.25	24.36	0.00	0.00	0.00	0.00	0.00	0.00	100.00	0.25	24.36
Hyd. Oil	100.00	5.00	1782.56	100.00	5.00	1782.56	100.00	5.00	1782.56	100.00	5.00	1782.56	0.00	0.00	0.00	100.00	5.00	1782.56
Group 7																		
Pass.	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	100.00	0.00	0.00
Misc.	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	100.00	0.00	0.00
Group 8																		
Cargo Comp	100.00	14.73	3144.86	100.00	14.73	3144.86	100.00	14.73	3144.86	0.00	0.00	0.00	0.00	0.00	0.00	100.00	14.73	3144.86
Group 9																		
WRT & tube	100.00	4.00	406.40	REQ'D	2.15	218.44	REQ'D	2.15	218.44	100.00	4.00	406.40	100.00	4.00	406.40	NORM	2.57	261.11
Impulse Tanks	100.00	4.00	406.40	100.00	4.00	406.40	100.00	4.00	406.40	100.00	4.00	406.40	100.00	4.00	406.40	100.00	4.00	406.40
Group 10																		
"D" TANK	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00	100.00	0.00	0.00

TOTALS:

Sum Wt:		292.97			291.12			237.50			174.19			99.18			291.54
Sum Mom:		59902.25			59714.29			45428.84			40847.28			21446.98			59756.97
Net LCG:		204.46			205.12			191.28			234.50			216.25			204.97
Net Arm:		7.20			6.55			20.38			-22.83			-4.59			6.70
Density:		64.00			63.60			63.60			63.60			64.30			63.00
Subm Displ ':		8870.72			8815.28			8815.28			8815.28			8912.31			8732.12
Wt to Subm ':		1466.52			1411.08			1411.08			1411.08			1508.11			1327.92
Wt in MBT ':		1009.55			1003.24			1003.24			1003.24			1014.28			993.78
LCG Wt to Subm ':		160.46			159.22			159.22			159.22			161.33			157.16
VB:		164.00			116.71			170.34			233.65			394.65			42.60
VB Moment:		29408			19860			34146			38727			75165			5214
VB arm:		179.32			170.16			200.46			165.75			190.46			122.41

Equilibrium Polygon



G. Cable Calculations

Cable Worksheet

Constants and Design Inputs

$$\rho_{SW} := 64 \frac{\text{lb}}{\text{ft}^3}$$

$$\rho_{HTS} := 490 \frac{\text{lb}}{\text{ft}^3}$$

$$1\text{ton} := 2240\text{lb}$$

$$v := 1.5 \cdot 10^{-5} \frac{\text{ft}^2}{\text{sec}}$$

$$D_{\text{cable}} := 1.5\text{ in}$$

$$g := 32.2 \frac{\text{ft}}{\text{sec}^2}$$

$$L_{\text{cable}} := 3000\text{ ft}$$

$$\text{HaulTime} := 2\text{ hr}$$

$$\text{Haul_Rate} := \frac{L_{\text{cable}}}{\text{HaulTime}}$$

$$\text{Haul_Rate} = 0.417 \frac{\text{ft}}{\text{sec}}$$

Object Dimensions

$$h := 10.5\text{ ft}$$

$$b := 6\text{ ft}$$

$$L := 23\text{ ft}$$

$$W_{\text{wet_object}} := 33000\text{ lb}$$

$$\text{Vol}_{\text{object}} := h \cdot b \cdot L$$

$$W_{\text{bouy_obj}} := \rho_{SW} \cdot \text{Vol}_{\text{object}}$$

$$W_{\text{bouy_obj}} = 9.274 \times 10^4 \text{ lb}$$

$$W_{\text{bouy_obj}} = 9.274 \times 10^4 \text{ lb}$$

$$W_{\text{dry_object}} := W_{\text{wet_object}} + W_{\text{bouy_obj}}$$

$$W_{\text{dry_object}} = 56.132\text{ton}$$

$$W_{\text{object}} := W_{\text{wet_object}}$$

$$M_{\text{object}} := \frac{W_{\text{object}}}{32.2 \frac{\text{ft}}{\text{sec}^2}}$$

Drag Force

$$U := \frac{L_{\text{cable}}}{\text{HaulTime}} \quad U = 0.417 \frac{\text{ft}}{\text{sec}} \quad \text{Reynolds} := U \cdot \frac{b}{\nu}$$

$$\text{Reynolds} = 1.667 \times 10^5 \quad C_d := .5$$

$$\rho_{\text{SW}} := 1.9905 \text{lb} \cdot \frac{\text{sec}^2}{\text{ft}^4}$$

$$F_{\text{drag}} := .5 \cdot C_d \cdot U^2 \cdot (b \cdot L) \cdot \rho_{\text{SW}}$$

$$F_{\text{drag}} = 11.922 \text{lb}$$

Cable Weight

$$A_{\text{cable}} := \pi \cdot \frac{D_{\text{cable}}^2}{4} \quad A_{\text{cable}} = 1.767 \text{in}^2$$

$$\text{Volume} := L_{\text{cable}} \cdot A_{\text{cable}} \quad \text{Volume} = 36.816 \text{ft}^3$$

$$W_{\text{cable}} := \rho_{\text{HTS}} \cdot \text{Volume} \quad \rho_{\text{SW}} := 64 \frac{\text{lb}}{\text{ft}^3} \quad W_{\text{cable}} = 1.804 \times 10^4 \text{lb}$$

$$\text{Bouy}_{\text{cable}} := \text{Volume} \cdot \rho_{\text{SW}}$$

$$W_{\text{netcable}} := W_{\text{cable}} - \text{Bouy}_{\text{cable}} \quad W_{\text{netcable}} = 1.568 \times 10^4 \text{lb}$$

$$M_{\text{netcable}} := \frac{(W_{\text{cable}} - \text{Bouy}_{\text{cable}})}{32.2 \frac{\text{ft}}{\text{sec}^2}} \quad M_{\text{netcable}} = 487.063 \frac{\text{lb sec}^2}{\text{ft}}$$

Forces Due To Acceleration

$$\rho_{SW} := 1.9905 \text{ lb} \cdot \frac{\text{sec}^2}{\text{ft}^4}$$

$$M_a := .5 \cdot \frac{4 \cdot \pi \cdot b^3 \cdot \rho_{SW}}{3} \quad M_a = 900.481 \frac{\text{lb sec}^2}{\text{ft}}$$

$$\text{Accel} := g$$

$$F_{Ma} := (M_a + M_{\text{netcable}} + M_{\text{object}}) \cdot \text{Accel}$$

$$F_{Ma} = 7.768 \times 10^4 \text{ lb}$$

Cable Stress

$$W_{\text{total}} := W_{\text{object}} + W_{\text{netcable}} + F_{\text{drag}} + F_{Ma}$$

$$W_{\text{total}} = 56.417 \text{ ton}$$

$$F_{\text{cable}} := W_{\text{total}}$$

$$\sigma_{\text{cable}} := \frac{F_{\text{cable}}}{A_{\text{cable}}}$$

$$\sigma_{\text{cable}} = 7.151 \times 10^4 \frac{\text{lb}}{\text{in}^2}$$

Reel Sizing and Weight

$$D_{\text{inner}} := .75 \cdot \text{ft}$$

$$\text{width} := 5 \cdot \text{ft}$$

$$D_{\text{reel}} := 1.5 \sqrt{\frac{4 \left[\frac{\pi \cdot (D_{\text{inner}})^2}{4} + \frac{\text{Volume}}{\text{width}} \right]}{\pi}}$$

$$D_{\text{reel}} = 4.729 \text{ft}$$

$$\rho_{\text{SW}} := 64 \frac{\text{lb}}{\text{ft}^3}$$

$$W_{\text{reel}} := 1.25 \cdot (\text{Volume} \rho_{\text{HTS}})$$

$$W_{\text{reel}} = 10.067 \text{ton}$$

Motor Sizing

$$\text{Power} := \frac{W_{\text{total}}}{\text{HaulTime}} \cdot L_{\text{cable}} \cdot 32.2 \frac{\text{ft}}{\text{sec}^2}$$

$$\text{Power} = 95.815 \text{hp}$$