

(1)

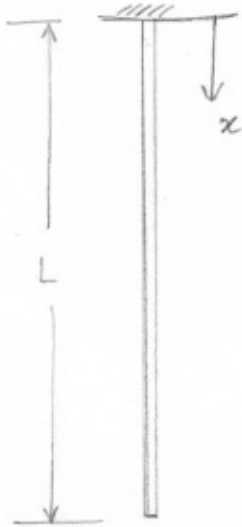
**MASSACHUSETTS INSTITUTE OF TECHNOLOGY**  
**Department of Mechanical Engineering**

**2.001 - Mechanics of Materials I**  
**Spring, 2003**

**Solutions for Problem Set 6**

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PROBLEM 1



a) Maximum length of wire that can be reeled out:

$A$  = area of cross-section

Max. tensile stress occurs at  $x=0$ .

since the weight of the whole cable acts at this section.

$$F = AL\rho g$$

$$g = 9.81 \text{ m/sec}^2$$

$$\rho = 2800 \text{ kg/m}^3$$

$$\sigma = \frac{F}{A}$$

$$\sigma = L\rho g$$

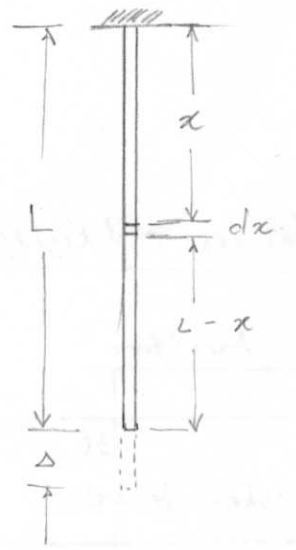
$$\begin{aligned}\sigma_{\max} &= 200 \text{ MPa} \\ &= 200 \times 10^6 \text{ N/m}^2\end{aligned}$$

$$\Rightarrow 200 \times 10^6 = L\rho g$$

$$L = \frac{200 \times 10^6}{2800 \times 9.81}$$

$$L = 7281.2 \text{ m}$$

(b) What is the total deformation of wire (total elongation) at the threshold of failure?



$$u = \int \epsilon dx$$

$$\Delta = \int_0^L \epsilon dx$$

$$= \int_0^L \frac{\rho(L-x)g}{E} dx$$

$$= \int_0^L \left( \rho \frac{L}{E} g - \rho \frac{xg}{E} \right) dx$$

$$\epsilon = \frac{\sigma'}{E}$$

$$\sigma' = \frac{\rho(L-x)Ag}{A} = \rho(L-x)g$$

$$E = 69 \times 10^6 \text{ KN/m}^2$$

$$= 69 \times 10^9 \text{ N/m}^2$$

(from book CDL page 83)

$$\Delta = \rho \frac{L^2}{E} g - \frac{\rho}{2E} L^2 g$$

$$\Delta = \frac{1}{2} \frac{\rho L^2}{E} g$$

$$= \frac{1}{2} \times \frac{2800 \times (7281.2)^2 \times 9.81}{69 \times 10^9}$$

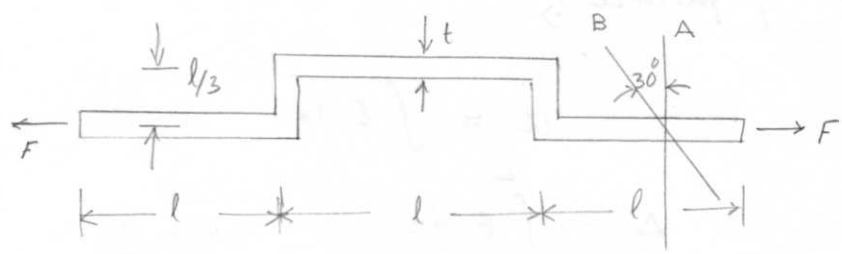
$$= 10.55 \text{ m}$$

(c) The wire will become skinnier as you go up. The stresses are higher up in the wire since more weight is being supported by sections which are higher. Higher stresses mean higher strains (longitudinal strains).

Lateral strains =  $-\nu$  x longitudinal strain  
Poisson's Ratio

Hence higher the stretching, the skinnier will be the wire.

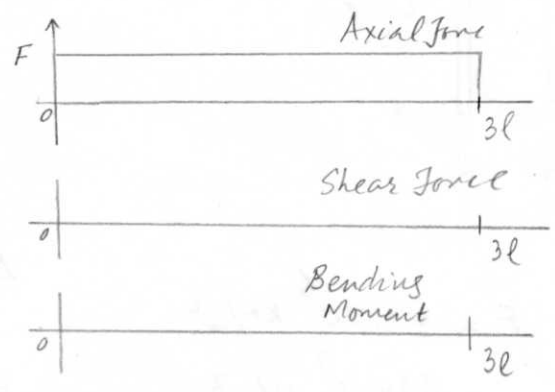
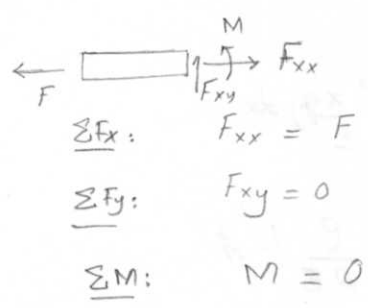
# Problem 2



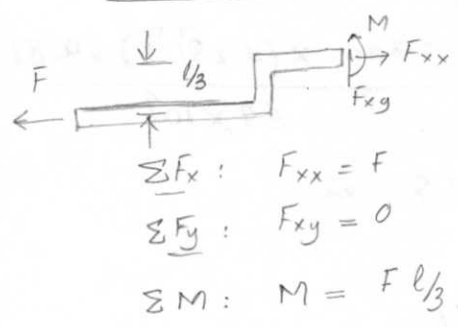
a)

For Left and Right segments

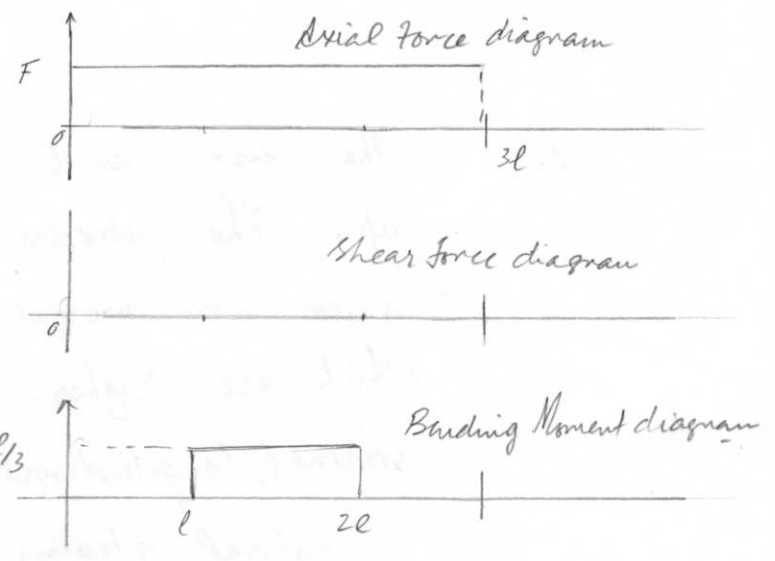
For left segment



For Middle segment



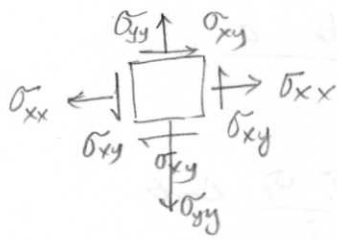
For Middle segment



For Right segment

Same as for left segment by symmetry

(b) On section (A)



$$\sigma_{xx} = \frac{F}{t}$$

Assume the dimension  $\perp$  to paper is unity

$$\sigma_{xy} = 0$$

← since no shear force acts on this face

$$\sigma_y = 0$$

Also this means that

$\sigma_x = \frac{F}{t}$  and  $\sigma_y = 0$  are principal stresses

(c) On section (B)

$$\theta = 30^\circ$$

$$\sigma_{xx} = F/t ; \sigma_{yy} = 0 ; \sigma_{xy} = 0$$

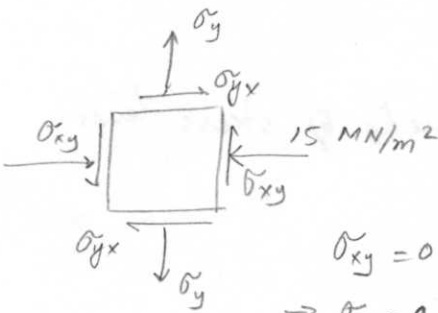
$$\sigma_{x'} = ? \quad \sigma_{xy'} = ?$$

$$\sigma_{x'} = \frac{\sigma_{xx} + \sigma_{yy}}{2} + \frac{\sigma_{xx} - \sigma_{yy}}{2} \cos 2\theta + \sigma_{xy} \sin 2\theta$$

$$= \frac{F}{2t} + \frac{F}{2t} \cos 60^\circ + 0$$

$$= \frac{F}{2t} + \frac{F}{4t} = \frac{3}{4} \frac{F}{t}$$

PROBLEM 3 (4.15)

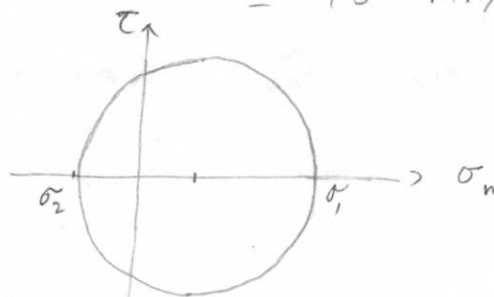


$$\sigma_{xy} = 0$$

$$\Rightarrow \sigma_{yx} = 0$$

(by symmetry of stress tensor)

Maximum tensile stress = 75 MN/m<sup>2</sup>



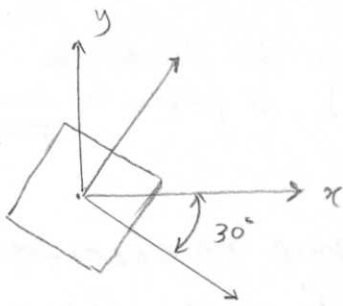
From Mohr's circle, the extreme values of the normal stresses are the principal stresses, and the corresponding shear stress is zero.

Therefore

$$\sigma_1 = 75 \text{ MN/m}^2$$

$$\sigma_2 = -15 \text{ MN/m}^2$$

} Also solution of part B of this problem.



For face  $\perp$  to a.

$$\theta = -30^\circ$$

$$\begin{aligned}\sigma_{aa} &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2} \cos \theta \\ &= \frac{-15 + 75}{2} + \frac{-15 - 75}{2} \cos(-60)\end{aligned}$$

$$\sigma_{aa} = 30 - 22.5 = 7.5 \text{ MN/m}^2$$

$$\sigma_{ab} = - \frac{\sigma_1 - \sigma_2}{2} \sin 2\theta$$

$$= - \frac{-15 - 75}{2} \sin(-60) = -38.97 \text{ MN/m}^2$$

For face  $\perp$  to b

$$\theta = -30 + 90 = 60^\circ$$

$$\sigma_{bb} = \frac{-15 + 75}{2} + \frac{-15 - 75}{2} \cos(120)$$

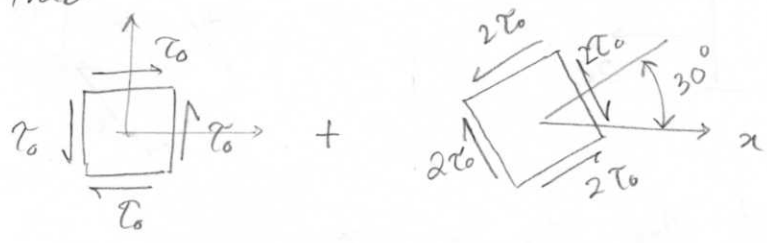
$$= 30 - 45 \cos(120)$$

$$= 52.5 \text{ MN/m}^2$$

$$\sigma_{ba} = \sigma_{ab} \text{ from symmetry of stress tensor.}$$

PROBLEM 4 . 4.26

Case (a)



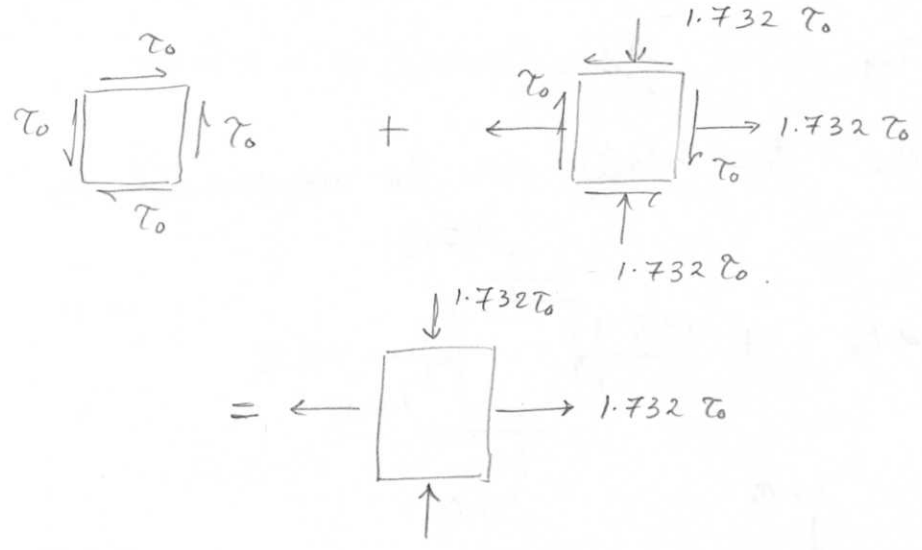
For the state on the right

$$\sigma_x = -2\tau_0 \sin(-2 \times 30) = 1.732 \tau_0$$

$$\sigma_y = -(-2\tau_0) \sin(-2 \times 30) = -1.732 \tau_0$$

$$\tau_{xy} = -2\tau_0 \cos(-2 \times 30) = -\tau_0$$

Therefore the two states can be represented as



Therefore the principal stresses are

$$\sigma_1 = 1.732 \tau_0$$

$$\sigma_2 = -1.732 \tau_0$$

(b)



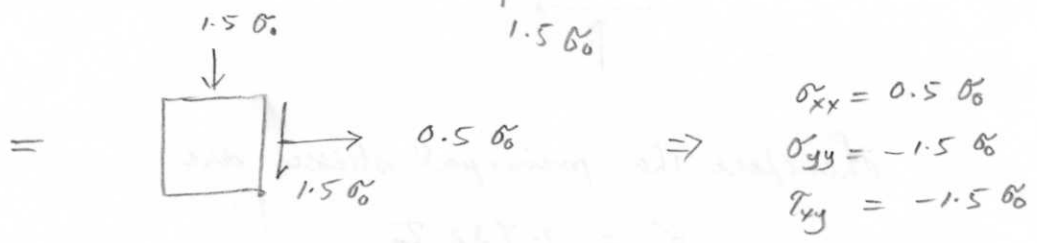
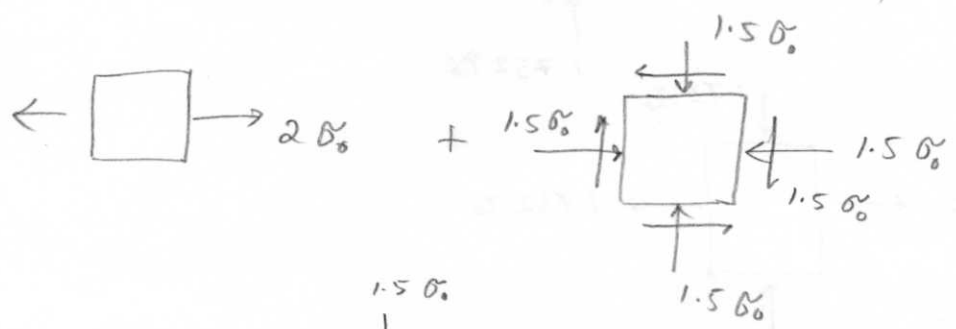
We find  $\sigma_{xx}$ ,  $\sigma_{yy}$  and  $\tau_{xy}$  for the stress state on the right

$$\begin{aligned} \sigma_{xx} &= -\frac{3\sigma_0}{2} + -\frac{3\sigma_0}{2} \cos(2 \times 45) \\ &= -1.5\sigma_0 \end{aligned}$$

$$\begin{aligned} \sigma_{yy} &= -\frac{3\sigma_0}{2} + \frac{3\sigma_0}{2} \cos(2 \times 45) \\ &= -1.5\sigma_0 \end{aligned}$$

$$\tau_{xy} = -\frac{3\sigma_0}{2} \sin(2 \times 45) = -1.5\sigma_0$$

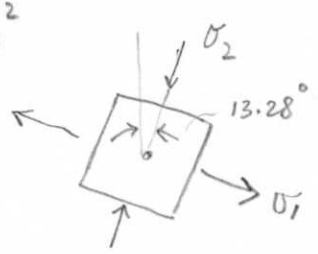
Therefore the two states can be represented by



$$\begin{aligned} \sigma_{xx} &= 0.5\sigma_0 \\ \sigma_{yy} &= -1.5\sigma_0 \\ \tau_{xy} &= -1.5\sigma_0 \end{aligned}$$

$$\begin{aligned} \sigma_1 &= \sqrt{\left(\sigma_{xx} - \frac{\sigma_{xx} + \sigma_{yy}}{2}\right)^2 + \tau_{xy}^2} + \frac{\sigma_{xx} + \sigma_{yy}}{2} \\ &= \sqrt{\sigma_0^2 + 2.25\sigma_0^2} = 1.8\sigma_0 + -0.5\sigma_0 \\ &= 1.3\sigma_0 \end{aligned}$$

$$\begin{aligned} \sigma_2 &= \frac{\sigma_{xx} + \sigma_{yy}}{2} - \sqrt{\left(\frac{\sigma_{xx} - \sigma_{yy}}{2}\right)^2 + \tau_{xy}^2} \\ &= -2.3\sigma_0 \\ \theta &= 13.28 \end{aligned}$$

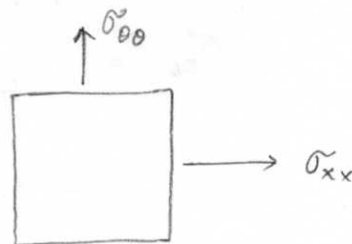
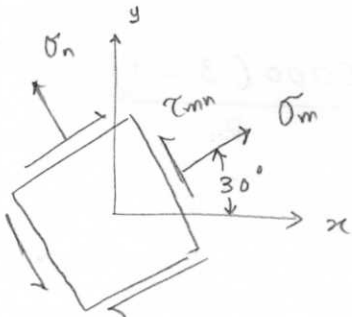


PROBLEM 5

a)  $\sigma_m = 15000 \text{ psi}$  ,  $\sigma_n = 5000 \text{ psi}$   $\tau_{mn} = ?$

$\sigma_{xx}$  and  $\sigma_{\theta\theta}$  are principal stresses

since  $\sigma_{x\theta} = \sigma_{\theta x} = 0$  , from shown loading



$$\sigma_m = \frac{\sigma_{xx} + \sigma_{\theta\theta}}{2} + \frac{\sigma_{xx} - \sigma_{\theta\theta}}{2} \cos(2 \times 30)$$

$$\sigma_m = 0.75 \sigma_{xx} + 0.25 \sigma_{\theta\theta} \quad \text{--- (1)}$$

$$\sigma_n = \frac{\sigma_{xx} + \sigma_{\theta\theta}}{2} - \frac{\sigma_{xx} - \sigma_{\theta\theta}}{2} \cos(2 \times 30)$$

$$\sigma_n = 0.25 \sigma_{xx} + 0.75 \sigma_{\theta\theta} \quad \text{--- (2)}$$

From (1) and (2)

$$\sigma_{xx} = \frac{3}{2} \sigma_m - \frac{\sigma_n}{2}$$

$$\sigma_{\theta\theta} = \frac{3\sigma_n - \sigma_m}{2}$$

$$\Rightarrow \sigma_{xx} = 1.5 \times 15000 - 0.5 \times 5000$$

$$= 20,000 \text{ psi}$$

$$\sigma_{\theta\theta} = 0$$

$$\sigma_{xx} = \frac{F}{2\pi r t} \Rightarrow F = 2\pi r t \times 20,000$$

$$= 2\pi \times 10 \times 0.1 \times 20,000$$

$$= 125,663.7 \text{ lb}$$

$$\sigma_{\theta\theta} = 0 \Rightarrow p = 0$$



b)  $\sigma_m = 15,000 \text{ psi}$        $\sigma_n = 15000 \text{ psi}$

$$\begin{aligned} \sigma_{xx} &= \frac{3}{2} \sigma_m - \frac{\sigma_n}{2} \\ &= 15000 \left( \frac{3}{2} - \frac{1}{2} \right) \\ &= 15000 \text{ psi} \end{aligned}$$

$$\begin{aligned} \sigma_{\theta\theta} &= \frac{3\sigma_n - \sigma_m}{2} = \frac{15000(3-1)}{2} \\ &= 15000 \text{ psi} \end{aligned}$$

$$\begin{aligned} F &= 2\pi r t \times \sigma_{xx} \\ &= 2\pi \times 10 \times 0.1 \times 15000 \\ &= 94,247.8 \text{ lb.} \end{aligned}$$

$$\begin{aligned} \sigma_{\theta\theta} &= \frac{Pr}{2t} \Rightarrow P = \frac{2t}{r} \sigma_{\theta\theta} \\ &= \frac{2 \times 0.1}{10} \times 15000 \\ &= 300 \text{ psi} \end{aligned}$$

PROBLEM 6    4.28

$\sigma_1 = 20 \text{ MN/m}^2$        $\sigma_2 = -45 \text{ MN/m}^2$

$$\begin{aligned} \tau_{xy} &= - \frac{\sigma_1 - \sigma_2}{2} \sin 2\theta \\ 20 &= - \frac{20 + 45}{2} \sin 2\theta \end{aligned}$$

$$\begin{aligned} \sin 2\theta &= -0.615 \\ \Rightarrow \theta &= -18.99^\circ \end{aligned}$$

