

RISK-INFORMED DESIGN CHANGES FOR A PASSIVE COOLING SYSTEM

by

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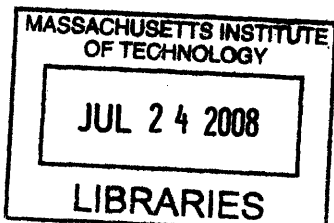
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ABSTRACT

The failure probability of a passive decay heat removal system after a LOCA is evaluated as part of a risk-informed design process for a helium-cooled fast reactor. The system was modeled using RELAP5-3D. The epistemic uncertainties in input parameters as well as the epistemic model uncertainties in the code were assessed and propagated through the model using Latin hypercube sampling. The changes in the design that we investigated reduced the overall failure probability of the system by reducing the impact of the major contributor to the failure probability. Sensitivity analyses led to two unexpected results. First, the key factors affecting the system failure probability are the location of the thermal insulation (inside or outside the hot leg) and the uncertainty in the insulation thermal conductivity. Second, the heat transfer coefficient in the core is not as important as one might expect. Our results show that the heat transfer coefficient in the containment structures is more important. Different methods for sensitivity analysis were applied and gave consistent results.

Thesis supervisor: George E. Apostolakis
Title: Professor of Nuclear Science and Engineering

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I. INTRODUCTION

Of particular promise in terms of improving the reliability for new nuclear plant designs is the use of passive systems that rely on natural phenomena such as gravity, convection, and conduction. The relevant forces are generally weak and, as a result, passive systems are more sensitive to small changes in their environment [1] than active systems.

The concept of passive function failure has been introduced in [2] as the probability that a system will fail to perform its function, i.e., failure occurs when the “capacity” of the system is exceeded by the “load” imposed on the system. Whenever the load exceeds the capacity the system no longer behaves as expected. The load is represented by a set of measurable parameters of the system (e.g., temperature in the fuel, pressure in the pipes) and the capacity is the limit those parameters should not exceed. Reference [3] outlines a systematic approach to the evaluation of the reliability of a passive system.

There are two major sources of uncertainty affecting our ability to predict the exact values of loads and capacities. The first type of uncertainty is due to the fact that we do not know the exact value of each input parameter. We can only assume a range of values and a corresponding probability distribution. Second, there are uncertainties due to the model we use to simulate the behavior of the system. These uncertainties are related to the inevitable approximations in the constitutive equations, to the numerical solution methods built in the codes, and other computational possible errors [4]. These uncertainties are usually called epistemic uncertainties to distinguish them from the aleatory uncertainties that refer to the random occurrence of events such as loss of coolant accidents (LOCAs) [5].

Probabilistic Safety Assessment (PSA) is a powerful tool that allows us to identify potential accident scenarios and to estimate their probabilities of occurrence over a defined

time period. Originally, PSA was primarily used to measure the level of risk associated with an operating facility. More recently, the value of PSA as an important contributor to the design process has been recognized [6-7]. In this paper, PSA is used to guide the designer by comparing different designs and evaluating the risk for each design.

This work presents an example of a risk-informed design change and the evaluation of the failure probability of a passive decay heat removal system after a LOCA including epistemic uncertainties due to both input parameters and the best estimate code used. It also provides the time-dependent reliability of the passive system. In this application, failure limits are fixed values with no uncertainties. We only consider uncertainties on the “loads”.

The design of a helium-cooled fast reactor constitutes the case study. It is part of the MIT studies on a Gas-cooled Fast Reactor (GFR) design. The system and its components were simulated using RELAP5-3D. The computational effort was significant because the complexity of the system required long simulation times (up to 10 hours). The entire system operates as one passive system whose initiation is triggered by the reactor scram after a LOCA. Section II describes the system.

An overview of the methodology is given in Section III. The analysis is presented in Section IV. The reliability evaluation is in Section IV. Finally, conclusions on various aspects of the work and future research suggestions are provided in Section V.

II. GFR SYSTEM DESCRIPTION

II.A. Basic Design

The GFR design that we use [8] consists of a 600 MW_{th} helium-cooled fast reactor core inside the Pressure Vessel (PV), a Brayton power cycle within the Power Conversion Unit (PCU), and two 100% Decay Heat Removal (DHR) loops.

As shown in Figure 1, the PCU has a vertical arrangement and is connected to the reactor vessel through a coaxial duct. The PCU consists of three different kinds of components: the turbine, compressors, and heat exchangers.

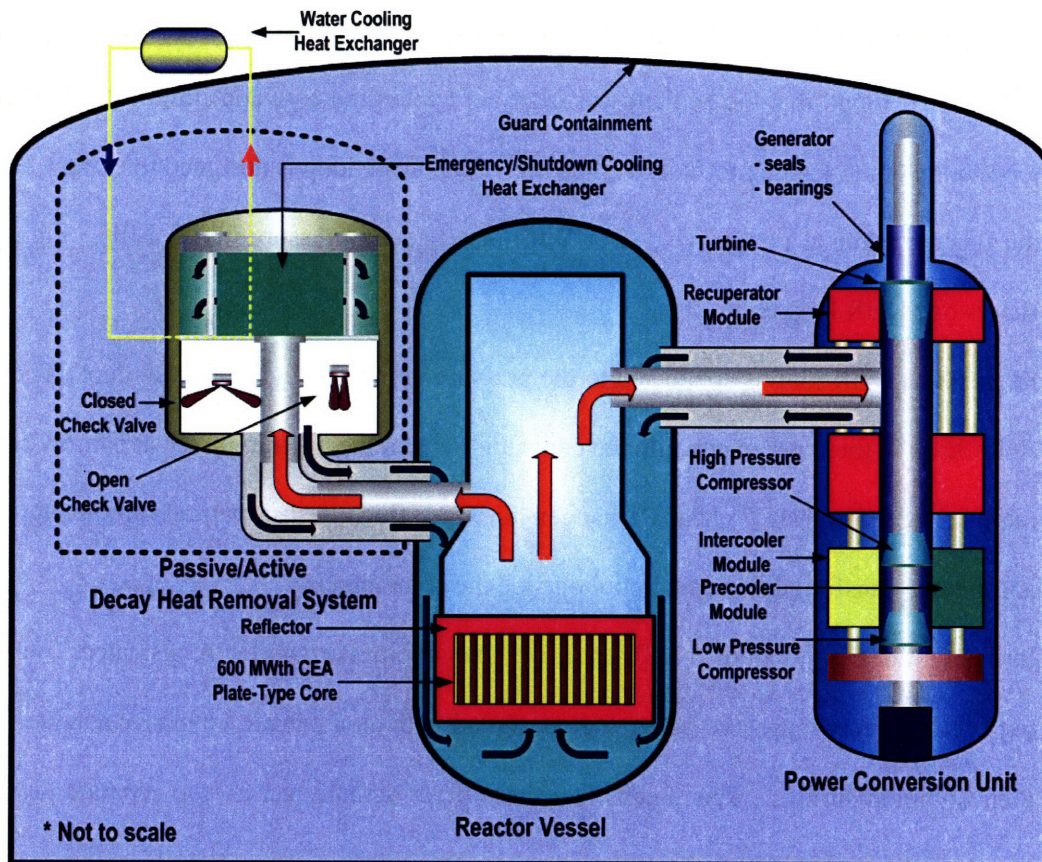


Figure 1 Schematic diagram of GFR systems. Reactor Vessel, PCU and one DHR loop are shown.

The core design is based on a early fully passive Commissariat à l'Énergie Atomique (CEA) design [8]; it employs CERCER 70/30 plate type technology in order to reach

higher outlet temperatures. The core is designed to have a very low pressure drop to maximize the natural circulation capability.

All these systems are protected by a guard-containment at high design pressure (2 MPa). Since in a LOCA accident scenario the system is depressurized, the high guard-containment pressure is intended to provide sufficient backup pressure to sustain the natural circulation in the DHR loops.

The passive decay heat removal system relies on natural circulation of the gas coolant flowing between the low pressure-drop core and gas/water heat exchangers placed at higher elevation and it does not rely on any active safety systems. The initial design consisted of two 50% DHR loops, working in parallel; this configuration was modified [9] since it was found that the coolant was likely to bypass the core and flow from one DHR loop to the other, leading to fuel overheating. Each DHR loop is designed to extract 2% of the reactor nominal power (i.e., 12 MWth) at a backup pressure of 1.3 MPa. Figure 1 shows one DHR loop only.

Each 100% DHR loop is connected to the pressure vessel through a coaxial duct. The hot fluid flows in the inner duct while the cool fluid runs in the outer duct. Heat is transferred, through the HEATRIC™ heat exchanger, to water flowing in a natural circulating loop and finally transferred to a water pool outside the containment.

In this first design, as studied in [9], the two coaxial pipes are perfectly insulated. We will explain later how these two pipes were designed with an adiabatic boundary condition on their common surface. This means that these pipes actually act as two separate pipes in the ideal case of perfect insulation.

In normal operation, the DHR loops are kept closed by check valves that are located between the heat exchanger and the cold leg duct. During normal operation the compressor-driven flow from the main cross duct into the downcomer maintains higher

pressure under the check valve keeping it shut and no flow proceeds through the DHR loop. In addition, the helium gas above the check valve is cooler since it is in contact with the water-cooled heat exchanger while the DHR hot leg (on the other side of the check valve), contains hot gas as it is in direct communication with the reactor upper plenum. After a LOCA and following the coastdown of the shaft, the compressor driven flow through the cross-duct stops, the pressure under the check valves is reduced and the check valves open due to a positive pressure differential between the cold and hot DHR legs. Note that the check valves cannot open until the compressor flow stops neither is it desirable to open the check valves before the shaft coasts down to prevent a reversed flow in the DHR loop.

II.B. Accident Scenario

Our transient analysis considers the consequences of a LOCA due to a small break on the cold leg that connects the PV to the PCU. We are interested in the conditional failure probability of the decay heat removal system after the LOCA occurs.

The system must be able to remove the core decay heat during the transient. The main issue is to verify that the backup pressure evolution in time is sufficient to extract the decay heat from the core. This evolution is driven by various parameters, e.g., the coolant heat exchange with the core and the containment structure – a phenomenon that becomes especially important after equilibrium backup pressure is reached.

The LOCA happens when the system is in a steady-state condition; therefore, the initial conditions for the transient analysis come from the steady-state initialization. Figure 2 shows the sequence of events and the resulting fuel temperature.

At time $t = 0$, the cold leg pipe connecting the PCU to the pressure vessel breaks and the turbine is shut off. Since this is a small break, only a portion of the gas will go through the break into the containment. The other fraction will continue to flow through the

downcomer and to cool the core. Although the turbine is off, the shaft will keep turning for a certain time. During the coastdown of the shaft (region A in Figure 2), the PCU is the only cooling system removing decay heat from the core and the fuel temperature decreases due to higher heat removal capacity than power generated after reactor scram. This action lasts for about 10 minutes. In the meantime, the DHR loops are still closed, i.e., the check valves have not opened yet.

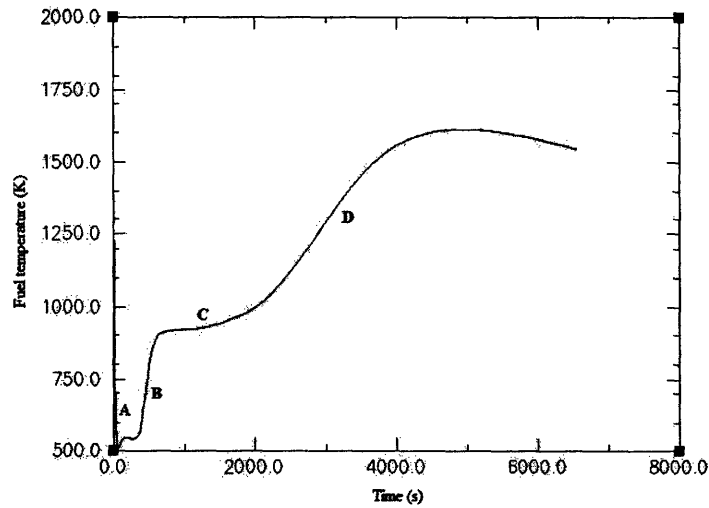


Figure 2 The fuel temperature as the accident scenario unfolds.

Region A corresponds to the shaft still spinning; region B represents the time during which the shaft is at a halt and DHR loops haven't opened yet; region C represents the time when DHR system is working; in region D DHR system removes heat at its backup pressure (1.3 MPa)

When the shaft stops, there is no cooling system working and the temperature in the fuel increases (region B). The stopped compressor flow eliminates the negative pressure differential across a check valve causing it to open due to the gravity head difference between the DHR cold and hot legs.

The system has two DHR loops; therefore, there are two check valves, one for each loop. The design is such that, when one valve opens, the other will stay closed and only one loop will be working. This is because the pressure loss through the emergency heat exchanger is significantly smaller than that in the core and one loop becomes a bypass (see

[9] for details) with reverse flow that shuts the check valves in that loop preventing backflow.

After one valve opens, the DHR loop starts removing heat from the core through the natural circulation of the coolant (region C). At first, the cooling system is oversized since it is working at a pressure higher than the backup pressure. Therefore, it is capable to remove almost all of the heat produced in the core, for that reason the fuel temperature has a plateau. As shown in Figure 3, the depressurization process ends in about 50 minutes, reaching the value of about 1.3 MPa. At this point, the outlet coolant temperature keeps rising until it reaches its operating condition (region D in Figure 2). However, the decay heat is below $12 \text{ MW}_{\text{th}}$ and the system is able to remove that power at this level of backup pressure (see II.A).

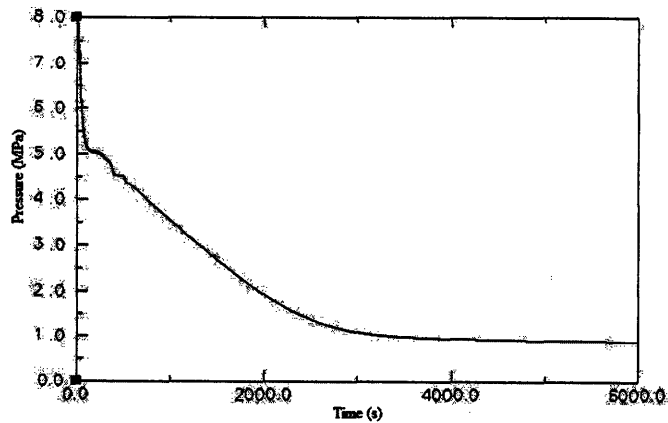


Figure 3 Pressure versus time in the DHR system; the operating condition is reached in about 50 minutes, when the curve reaches its plateau.

II.C. Success Criteria

The failure criterion can be established as a single value target, as a time dependent target, or as an integral value over the mission time [10]. As we stated in Section I, we only consider single-value criteria for the “capacity” of the system. In this case, the maximum fuel temperature should be below $1600 \text{ }^{\circ}\text{C}$ (1873.15 K) and the temperature in the DHR steel structure below $850 \text{ }^{\circ}\text{C}$ (1123.15 K). The first limit comes from the capability of this

type of fuel to prevent significant escape of fission products at temperatures up to 1600 °C*. The second limit is related to the structural resistance of stainless steel used for the DHR hot duct pipes: the inner surface of the hot gas line is in contact with the gas and the duct must withstand the highest coolant temperature. Although probability distributions could be associated with those two limits, we view them as fixed regulatory limits.

II.D. Simulation Code

The RELAP5-3D code [11] was selected to predict the transient response of the GFR to the postulated scenario as well the steady-state performance under nominal conditions.

This code is a best-estimate thermal-hydraulic code developed to perform transient simulations of nuclear reactor cooling systems during postulated accidents. The code models the coupled behavior of the reactor coolant system and the core for LOCAs and operational transients such as anticipated transients without scram, loss of offsite power, loss of feed-water, and loss of flow.

The nodalization of the system in RELAP5-3D is shown in Figure 4. In this diagram, lines represent connections and rectangles represent fluid and structures. Block A represents the Power Conversion Unit; Blocks B1 and B2 are the water secondary loops; Block C is the reactor core; Blocks D1 and D2 are the DHR loops. The check valves connecting the DHR loops to the downcomer are circled. In parallel with the check valves, there are channels to simulate the valve leakages (counter flow).

The importance of including the structures in the simulation has been emphasized in [8]: the structures can store a large amount of energy and this energy is transferred later to the coolant with significant time delay. This is very important in the DHR steel structures; we

* The 1600°C limit was adopted for this study but this innovative GFR uranium carbide plate type fuel with silicon carbide cladding will require irradiation testing before a final limit can be established. The limit pertains to the fuel/cladding plate, but the term fuel limit will be used throughout this paper for simplicity.

will later see that this effect is the major contributor to the overall failure probability of the passive decay heat removal system.

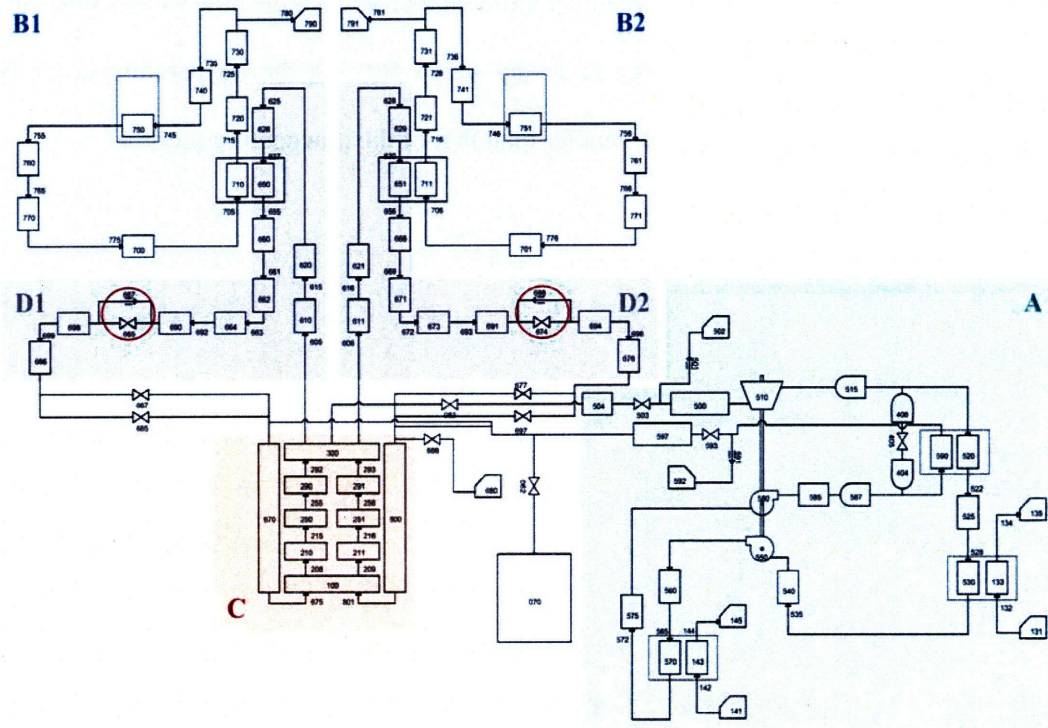


Figure 4 Nodalization of the entire system used in the RELAP5-3D

Also the heat structures in the containment are very important since they absorb heat brought into the containment by the coolant flowing through the break, and so they reduce the backup pressure available to sustain the natural circulation.

Check valves are critical hydrodynamic components; one characteristic is that they leak and sometimes they are designed to leak on purpose. As we have already said, this leakage is simulated by imposing connections which are kept open during the steady state; those connections close once check valves open. This effect of prolonged lead during normal operation was not simulated in this study. We assume that a valve starts leaking at the beginning of transient, i.e., each transient is initiated from the identical steady state conditions.

The leakage results in a small reversed coolant flow and in a reversed temperature profile along the loop, which may eventually prevent natural circulation from starting.

During steady state operation, a small backflow proceeds from the downcomer through the heat exchanger and after a prolonged steady state operation the temperature in the riser section of the DHR loop becomes smaller than that of the downcomer section.

III. METHODOLOGY OVERVIEW

The methodology we use to evaluate the reliability of passive systems is consistent with that of [3] and consists of the following steps:

Definition of the system, its mission and failure modes.

Identification of the source of uncertainties (epistemic uncertainties) and the important parameters, including the definition of specific failure criteria.

Quantification of uncertainties by selecting the appropriate distributions for the parameters. In some cases, the amount of data is limited and expert opinion is used.

Propagation of uncertainties via Monte Carlo simulation using a thermal-hydraulic model (e.g., RELAP5-3D).

Sensitivity analysis.

Evaluation of passive system unreliability to be used in the accident sequence analysis.

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IV. ANALYSIS

IV.A. Preliminary Design Evaluation

A first study on the MIT helium-cooled reactor was presented in [9]. From this point on, we will refer to the design presented in that paper as the basic design or the first design.

In that configuration, the dominant failure mode of the system was the structural failure of the DHR loop. A sensitivity analysis showed that check valve leakages were most important. An adiabatic boundary condition between the two coaxial DHR pipes was assumed, meaning that, for the purpose of that study, they were actually separated.

Some improvements to the system were suggested, such as relaxing the perfect insulation assumption between the two pipes by inserting insulation material on the inner side of the hot leg, combined with an increase in containment backup pressure in order to increase the mass flow rate in the DHR loop.

In our first analysis, we modified the design as suggested in the paper (i.e., insertion of insulation material between the hot and cold pipe) to assess whether this change led to a reduction in the failure probability of the passive system. At first, we did not change the backup pressure in the containment since its increase would affect the cost of the plant and this modification would be the last to make.

Figure 5 presents the different geometries we tested. The various simulations will be described and commented in the next sections.

Design A is the configuration of the basic design: the hot gas flows upward and the cold gas flows downward. The outer and inner ducts are connected by stainless steel but a perfect insulation condition was imposed in the RELAP5-3D code.

Design B is the configuration suggested in [9] as a possible improvement to reduce the system failure probability following a LOCA. The insulation material is placed on the

inner side of the hot pipe. Its thickness was determined using two criteria: a constraint on the overall dimensions and thermal insulation efficiency.

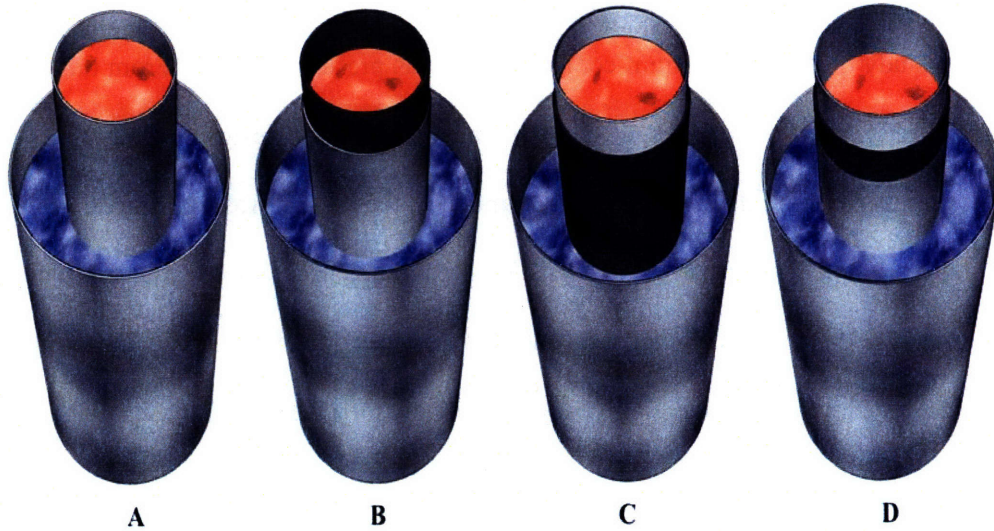


Figure 5 Different configurations for the DHR coaxial pipes; light gray: stainless steel; dark gray: insulation material.

For the second criterion, we evaluated the heat transferred from the fluid to the structure, and calculated the temperature in the steel. Figure 6 shows that the effectiveness of insulation decreases for thicknesses greater than 40 mm. Since this value was also reasonable for the design, we set it as a reference for the insulation thickness.

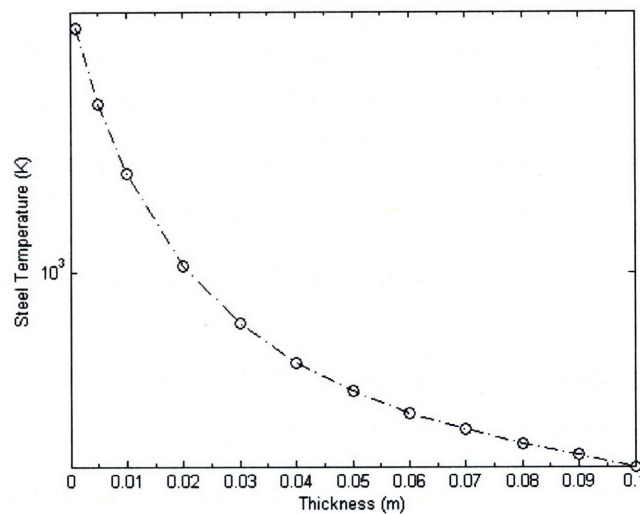


Figure 6 Temperature of stainless steel DHR hot leg pipe is plotted as function of the insulator thickness.

The results given in Figure 7 show that configuration B is worse than the basic configuration: by introducing the thermal insulation between the hot gas and the pipe we reduce the temperature burden on the steel structures but we prevent the gas from transferring heat to the pipe and vice versa.

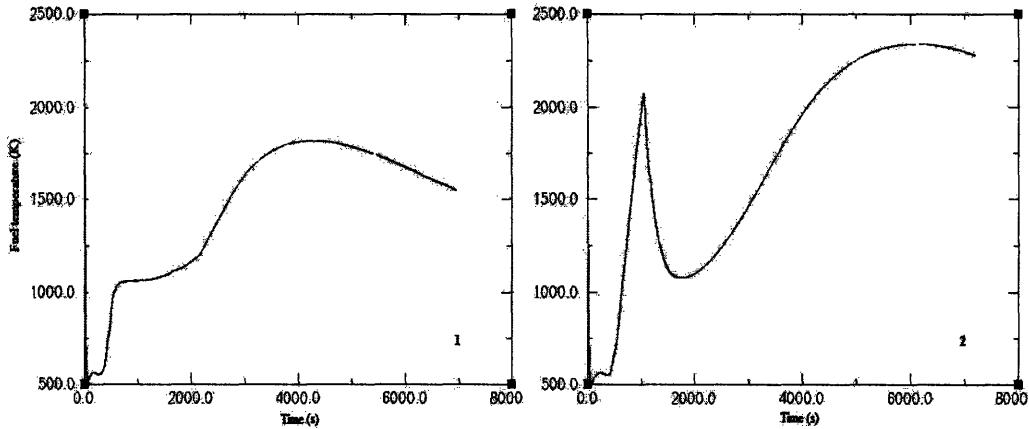


Figure 7 Fuel temperature for design configurations A and B.

The figure on the left corresponds to configuration A and the maximum temperature in the fuel is 1760 K. The figure on the right corresponds to configuration B and the maximum temperature in the fuel is 2250 K.

As discussed in Section II.B, this effect delays the opening of the valves (or may even prevent it) causing a high peak in temperature well above the limit. This is because the hot pipe wall of the hot leg stabilizes the hot-cold leg gas temperature difference necessary to initiate natural circulation. During the transient, a situation can occur in which the hot gas is pushed out of the hot leg and replaced by cooler gas. If the hot pipe wall, which has orders of magnitude higher heat capacity than helium gas is in direct contact with the gas, it can easily heat up gas to high temperature and reestablish desirable density difference between the hot and cold legs. Insulating the hot pipe wall on the inside prevents this rapid heat exchange and results in failure to open the check valve.

From this initial analysis, it seems that only an increase in backup pressure would be beneficial to the reliability of the system. However, before considering this option, we tried other configurations which turned out to be more effective for the system.

Design C shows the configuration where insulating material is placed on the outer surface of the hot leg pipe. This arrangement retains the benefit of stabilization of hot leg gas conditions by exposure to hot pipe walls and, in addition, the steel can now transfer some heat to the cool gas coming down in the cold leg pipe, so that the burden on the structure is partially released. On the other hand, the heat transferred to the cooler downcomer reduces slightly the temperature difference between the hot and cold legs decreasing somewhat the DHR loop flow rate. The overall benefit of this design is a reduced fuel temperature by more than 100 K, compared to design A.

Design D is a more realistic representation of the geometry. The insulation material is on the outer surface of the hot pipe but now it is covered by a 2.7 mm stainless steel foil. This foil prevents small particles from being detached and brought along in the loop by the gas causing damage to the structures or occlusions in the core channels. Design D will be analyzed further.

IV.B. Identification of Important Parameters

By important parameters, we refer to those parameters whose values are not known a priori and whose variability affects system performance. We identify them using expert judgment supported by sensitivity analyses. The probability distributions used for these parameters are listed in Table 1. A qualitative discussion of these parameters is given below.

Core roughness

In order to sustain the natural convection, the mass flow rate has to be high enough to remove enough heat from the core. An increase in core roughness results in an increase in

the friction factor that eventually leads to a higher pressure drop. Roughness is an important parameter in natural circulation and its uncertainty must be considered. The ceramic plate type core proposed by CEA was chosen since it exhibited the best performance due to its small pressure drop.

Check valve leakage

The valve leakage results in a small reversed coolant flow affecting the temperature profile along the loop, which in turn impacts natural circulation flow and may eventually prevent natural circulation from starting. Experimental data for this parameter are very scarce in the literature, given the few facilities working with hot gas at these temperatures. For this particular parameter, expert opinions become even more important.

Moment of inertia of the shaft

We have already stated that the PCU shaft will keep turning for a certain time. The time the shafts stops determines the moment when DHR system starts running. The higher the moment of inertia, the longer the shaft spins and the later the DHR starts operating. In our study, as we will show later, we excluded this parameter from our analysis. In the next chapter, sensitivity calculations will show how this parameter does not affect the failure probability of the system.

Thermal conductivity

In Section I, we mentioned that in our study we introduced some changes in the geometry and we also introduced new elements. The initial design had coaxial pipes in the DHR loops. The perfect insulation (adiabatic) condition between the hot leg and the cold leg pipes made this configuration to look like separate pipes. To keep the coaxial configuration, we relaxed the adiabatic condition and we introduced some insulation material between the two pipes. The geometrical configuration will be explained in the

next section. Here, we only discuss the new parameter we have introduced into our system, the thermal conductivity of the insulation material.

The state of the art [12] of designs for hot gas ducts and their insulations is incomplete with regard to very high temperature performance. The design parameters of the insulation depend strongly on the reactor type. Since the insulating material is in contact with a very hot medium, it has to meet stringent requirements. It must be able to withstand high pressure transients. Damage cannot be repaired because the insulation is installed in areas with difficult access. Ceramic materials seem to be the best option to insulate the hot duct from the cold duct. A range of values was extrapolated to high temperatures [13] and confirmed through expert opinion.

The importance of this parameter lies in the fact that it affects the DHR loop performance significantly. In the adiabatic case, the heat remained entirely in the steel structures of the DHR hot leg. In the present case, the small thermal conductivity of the insulation allows the hot pipe structure to transfer heat to the gas in the cold leg thus reducing the temperature load. This effect is balanced by a negative effect: if the thermal conductivity is too high, the hot gas would transfer heat to the cold gas thereby reducing the temperature differential that drives the natural circulation.

IV.C. MODEL UNCERTAINTY

We have already mentioned that due to unavoidable approximations in the code models, any calculation from a best estimate code, to be meaningful, needs an uncertainty evaluation. These best estimate codes have been developed for pumped circulation systems and their adequacy for natural circulation systems has not been demonstrated. Moreover, many of those best estimate codes have been developed for light water reactor applications and a benchmark comparison with experimental data must be done. Work has been carried out to compare experimental data to numerical predictions from

RELAP5-3D in a gas natural circulation loop [14]. This study shows that the heat transfer correlation for forced convection built in RELAP5-3D does not agree completely with the data. The new correlation developed at MIT demonstrates a better agreement with the data and shows that there is a substantial reduction in the heat transfer coefficient with respect to the previous correlation. This means that the value of the heat transfer coefficient resulting from the RELAP correlation formula, h_{RELAP} , should be adjusted. We do so by multiplying it by a factor ε [5]. This means that the heat transfer coefficient used in our calculations is actually $h = h_{RELAP} \cdot \varepsilon$. In our study, the model uncertainty in the heat transfer coefficient has been translated into an uncertainty in the multiplicative factor ε . The probability distribution of ε is given in Table 1.

Heat transfer coefficient in the core

The heat transfer coefficient is a function of fluid characteristic and system geometry and it is calculated with appropriate correlations. These correlations, built in the RELAP5-3D code, have been corrected with a multiplicative factor. Therefore, the uncertainty in the heat transfer coefficient was put in the multiplicative factor.

Heat transfer coefficient with containment structures

As for the previous parameter, we also use a multiplicative factor to account for uncertainty on the heat transfer to the structures in the containment. This model uncertainty is also justified by the fact that we only have a rough design of containment layout and we lack information about the precise amount of structures.

IV.D. Quantification of Uncertainties

In the previous section, we listed all the parameters considered as important contributors to uncertainty of the final result. Our state of knowledge regarding these uncertainties is expressed by (epistemic) probability density functions that represent parameter variability.

We used lognormal distributions for all parameters, except for the moment of inertia (though this parameter will not be considered in this study, as explained later). Table 1 shows the parameter ranges and corresponding percentiles derived from experts.

Table 1 Probability distributions and ranges for key parameters[†].

Parameter	Distribution	Range		Units	Percentiles	
		Low	High		Low	High
Core Roughness	Lognormal	1.00E-05	1.00E-04	[m]	5	85
Check valve leakage (loop 1)	Lognormal	0.05	0.50	[Kg/s]	5	85
Check valve leakage (loop 2)	Lognormal	0.05	0.50	[Kg/s]	5	85
Heat transfer coefficient (structures)	Lognormal	0.50	2.00		20	75
Heat transfer coefficient (core)	Lognormal	0.40	1.60		20	80
Thermal conductivity (insulator)	Lognormal	0.01	0.21	[W/m K]	5	85
Moment of Inertia	Normal	656.88	802.86	[Kg m ²]	20	80

Comparing with [9], we have modified the distribution for check valve leakage from an exponential distribution to a lognormal distribution. Since we assume that the valve is normally leaking, an exponential distribution is not satisfactory because it gives the highest probability to the non-leaking condition.

IV.E. Propagation of Uncertainties

We use Monte Carlo simulation to propagate the uncertainties. A drawback of this method is that a large number of calculations is required. In our case, this creates difficulties because each run of RELAP5-3D takes a long time[‡].

A method to reduce the number of simulations is to use Latin Hypercube Sampling (LHS) [15]. To generate a sample of size N, the range of each variable x_i , ($i = 1 \dots n$), is divided into N disjoint intervals of equal probability and one value is selected at random from each interval. The N values obtained for the variable x_i are paired randomly with the N values

[†] Heat transfer coefficients refer to the multiplicative factors presented in chapter IV.C.

[‡] To simulate the performance of the DHR system for a period of 2 hours, it takes up to 10 hours on a Pentium 4, CPU 3.20 GHz, RAM 3.19 GHz 0.99 GB.

of variable x_j . The process is repeated with all the variables to produce N samples, each of size n . By construction, all samples have the same probability.

If we call a realization the result of a simulation (i.e., the temperature as a function of time) with a certain set of parameter values, then failure occurs when a realization exceeds the corresponding limit. Each realization leads to two possible outcomes A : failure or success ($A = 1$ if it is a failure, $A = 0$ if it is a success). Therefore, the failure probability FP_N with a sample of size N is given by the following equation:

$$FP_N = \frac{\sum_{i=1}^N A(i)}{N} \quad (1)$$

An important issue in LHS is the determination of the number of realizations N . There are no formal rules regarding the sample size. In [16], 12 parameters were studied using a sample of size 500 and 3 parameters were studied with a sample of size 50. In [9], 128 samples were used for 6 parameters. Between these two studies, there is an important difference. In the former, a single value target is defined (i.e., the released dose); therefore, by simulating 500 samples, we obtain the mean and the variance of the target variable we are interested in. On the contrary, in the second case, the target value was considered to be the failure probability of the system and the 128 simulations all together give a point estimate of that target value. This means that in order to obtain complete (1st and 2nd order moments) information about the failure probability of the system, it is required to run multiple samples. Unfortunately, that would be prohibitive in terms of computational times. For this reason, we tried to evaluate the possibility of running smaller samples and repeat these calculations (i.e., the samples) a few times; Table 2 shows the results for the number of failures and the failure probability for different sample sizes.

Table 2 Number of failures for different sample sizes; case 1 refers to Design A (as calculated in Ref. 7); case 2 refers to Design D.

Sample size	# failures case 1	# failures case 2
16	9 56.3%	< 4 21.9%
32	14 43.8%	< 7 19.5%
128	39 30.5%	16 12.5%

This table shows that the failure probability decreases as the sample size increases. In this study, and given the constraint of the long simulation time, the failure probability of the system was obtained by simulating 128 possible realizations for a real time of 7200 s (two hours). In fact, all the failures, if any, occurred in this time window (see also [9]) and there is no need to push further the simulations, as they are very costly in terms of computational time.

We mention here that a high number of simulations are important not only to the evaluation of the failure probability but also to the derivation of more detailed information about the combinations of parameter values that may lead to failure. Moreover large samples are necessary when the probability functions used to model each parameter have long tails. In our case, distribution tails are short enough to justify our sample sizes.

We now give the reasons why we will not consider the moment of inertia in the calculations. We performed a sensitivity analysis using a traditional method for sensitivity analysis. We varied one parameter at a time, leaving all the other parameters at their mean values and we observed the effects on system performance. The simulations showed that the system was not affected at all by the variability in the moment of inertia. All simulations will be performed with the moment of inertia set at its nominal value (mean value).

We also need to comment on some offsets we found when we used different computers to simulate the system (several computers were used in parallel, given the huge number of simulations required and the long running time per simulation). RELAP5-3D was run on Windows machines; depending on the CPU power and RAM speed, the results may differ significantly from one station to another. In order to use different machines we ran the same case on each one to verify that the output curves were identical for all the machines.

IV.F. RESULTS

The parameter and model uncertainties were propagated through the code, using a sample of size 128. As stated earlier, two failure limits were considered, one for the fuel and one for the DHR structure. The purpose of these calculations was to evaluate possible improvements with respect to the basic design and previous findings on the conditional failure probability of the passive system.

The conditional probability, as presented in Ref. 7, was reviewed and re-evaluated, as some small errors in the geometry had underestimated the failure probability, which we estimated to be not 0.305, as reported in that paper, but above 0.50. This value will be the new point of comparison for the following analysis. In order to assess this estimation, we compared a preliminary calculation using nominal values of the characteristic parameters (e.g., their mean values) that showed that the previous analysis had underestimated the fuel temperature by about 200 K. Estimation using a sample of size 16 confirmed that the failure probability was higher than previously found.

Figure 8 and Figure 9 show the results of system behavior after the insertion of insulating material (Design D). Figure 8 presents the maximum fuel temperature evolution in time; the failure limit is 1873.15 K. There are 9 realizations that lead to system failure due to an excessive temperature in the fuel.

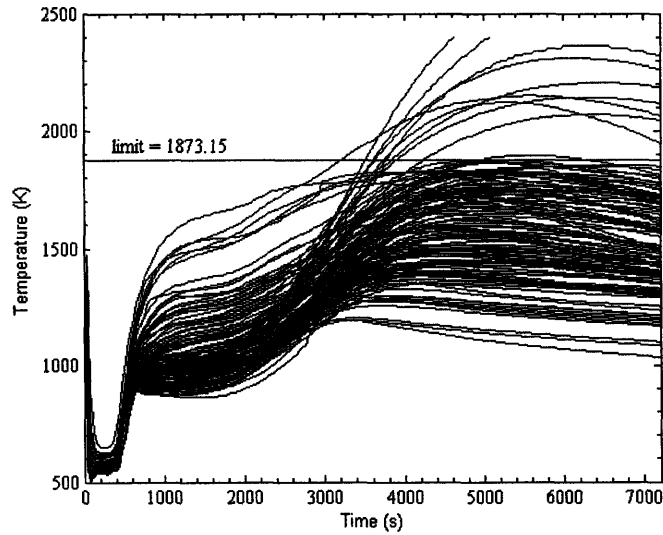


Figure 8 Temperature evolutions in the fuel for 128 samples.

Figure 9 shows the temperature profiles for 128 cases in the steel structure of both DHR loop hot pipes. When we described the system, we mentioned that the DHR system is composed of two 100% loops and only one works while the other remains closed.

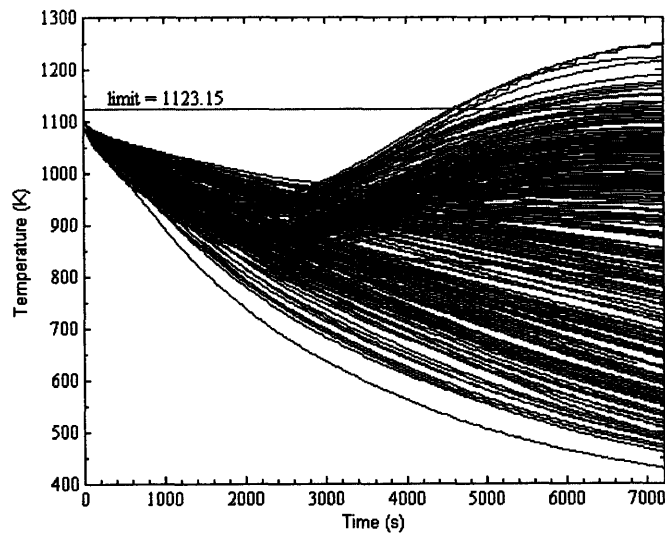


Figure 9 Temperature evolutions in the DHR loop hot pipes for 128 samples.

Consequently, in Figure 9 we actually have 256 curves: the always-decreasing temperature profiles are those for the closed loop, in which the temperature decreases because the hot helium is passing only through the open loop. The curves with a local minimum point (which corresponds to the end of region C in Figure 1) between 2000 and 3000 seconds

are the temperature evolutions of the hot leg pipe in the open loop. The failure criterion is 1123.15 K. There are 14 realizations that exceed the limit and lead to structural failure of the DHR pipes.

It can be easily inferred from these two figures that the DHR failures occur later in time than the failures in the fuel. Those realizations that lead to failure because both limit criteria are not met are counted as a single failure; in particular, all failures in the fuel also lead to mechanical failure of the DHR pipe walls and only 7 of the 14 are failures in Figure 9 are failures of the DHR pipes only. This means that the total failure probability, as expressed in equation 1, is:

$$FP_N = \frac{\sum_{i=1}^N A(i)}{N} = \frac{9 + 7}{128} = 0.125$$

This total failure probability confirms that there is an important reduction with respect to the basic design (at least a factor 4) due to the insulation. In addition, if we look closer to the different contributors, we get even more interesting results. In the initial design, the major contributor (at least 66%) to the total failure probability was the structural failure of the DHR pipes, while in the current configuration this contributor is much less important. The new design succeeds in reducing the impact of the previous major failure mode.

IV.G. Sensitivity Analysis

According to [17], the aims of sensitivity analysis are “priority setting, to determine what factor most needs better determination, and to identify the weak links of the assessment chain (those that propagate most variance in the output.” Monte Carlo evaluations create a mapping between the inputs and the outputs (y_i , $i = 1, 2$, the fuel and DHR temperatures).

To represent the uncertainty in the output parameter we use the expected value and the variance. These are estimated by the following equations, where m is the number of Latin hypercube samples (128):

$$E(y) = \frac{\sum_{i=1}^m y_i}{m} \quad (2)$$

$$\text{var}(y) = \frac{\sum_{i=1}^m (y_i - E(y))^2}{m-1} \quad (3)$$

The use of the first and second moment to characterize the distribution is very helpful even if some information is lost. The distribution of the maximum temperature in the fuel is presented in Figure 10. The mean and standard deviation of the maximum temperatures both in the fuel and in the DHR structure are as follows:

$$E(T_{\max}^{\text{fuel}}) = 1622.8 \text{ K} \quad \text{std}(T_{\max}^{\text{fuel}}) = 248.9 \text{ K}$$

$$E(T_{\max}^{\text{DHR}}) = 1105.0 \text{ K} \quad \text{std}(T_{\max}^{\text{DHR}}) = 29.3 \text{ K}$$

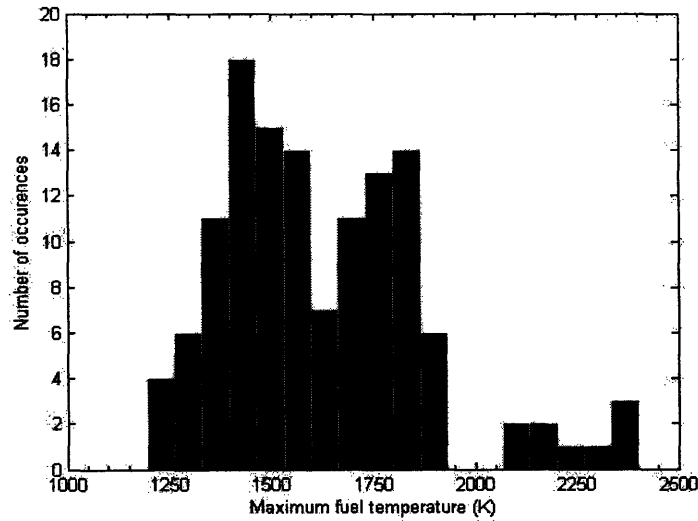


Figure 10 Distribution of the maximum temperatures in the fuel for 128 trials.

We observe that, in the case of maximum fuel temperature, the distribution is quite wide about its mean value, while it is narrower for the maximum DHR temperature distribution. The choice of methods to use in the sensitivity analysis is determined by a number of factors; in our case the most important one was the number of model evaluations we could perform. Since we are using a model that requires long times, we are forced to choose methods that require a relatively low number of model evaluations.

We used two types of analysis and four different methods. The first type of analysis is based on a repeated number of simulations. The objective here is to identify the factor which, if fixed at a point value, would result in the greatest reduction in the output uncertainty. Though this method is time consuming, it provides a fairly reliable indication of the relative importance of different parameters. The second type of analysis does not require additional simulations as it is based on the mapping between input factors and output variables calculated in 128 simulations. The first method consists of generating 2D or 3D scatter plots for the pairs (x_{ji}, y_i) or the triplet (x_{ji}, x_{ki}, y_i) with $i = 1, 2 \dots 128$ and j and k being the indices of given input parameters. Scatter plots offer a qualitative measure of sensitivity. The second method is the entropy or mutual information analysis [18] which addresses the issue of identifying important nonrandom patterns and ranking the association of input-output. The third method is a non-linear regression-based analysis, in which the goal is to identify input variables that have the highest correlation (or partial correlation) with the output of interest. Given the high non-linearity of our system, we were able to reproduce the observed data from 128 trials and the best nonlinear model we could find had a R^2 value of 0.46, which means that it accounts for 46% of the variability in the dependent variable. We did not pursue this method further.

IV.G.1. Parameter Ranking

The method used here is based on repeated simulations where input parameters are fixed one at a time. Our model has 6 input parameters, thus requiring 6 sets of runs. The actual number of sets was 7 since one set of simulations was performed fixing the two check valve leakage parameters at the same value in order to verify any possible relation between these two input factors. The fixed value for each parameter was its mean value. The number of simulations to perform was selected using insights from Table 2. Seven sets of 32 runs were performed.

Table 3 and Table 4 show the results of the analysis and the impact of fixing one parameter at a time on the mean and the variance of the output distributions. The nominal set refers to the case where all the parameters vary according to their distributions. The other cases correspond to the situation where only one parameter (on the left side of the table) is fixed at its mean value.

Table 3 Sensitivity analysis for the maximum cladding temperature; for each set of trials, one parameter is fixed at its mean value.

		Max fuel temperature		
		mean	st. dev.	st. dev. reduction %
nominal set		1651.17	332.29	
fixed parameters	roughness	1656.21	345.45	104%
	check valve loop 1	1515.06	224.52	68%
	check valve loop 2	1515.13	224.59	68%
	HTC containment	1559.09	180.72	54%
	HTC core	1470.92	208.27	63%
	thermal conductivity	1555.12	156.12	47%
	check valve loops 1&2	1516.06	226.52	68%

The important result from Table 3 is that the parameter whose reduction in uncertainty would reduce the output uncertainty the most is the thermal conductivity of the insulation. The second most important parameter is the heat transfer coefficient in the containment. All the parameters have an impact on the mean maximum temperature. It appears that the roughness is an irrelevant parameter with respect to the output.

Table 4 Sensitivity analysis for the maximum DHR temperature; for each set of trials, one parameter is fixed at its mean value.

		Max DHR temperature		
		mean	st. dev.	st. dev. reduction %
nominal set		1080.07	41.12	
fixed parameters	roughness	1075.99	42.38	103%
	check valve loop 1	1062.47	33.32	81%
	check valve loop 2	1059.99	33.64	82%
	HTC containment	1053.00	27.90	68%
	HTC core	1058.18	26.89	65%
	thermal conductivity	1059.32	11.79	29%
	check valve loops 1&2	1055.33	35.65	87%

For the maximum DHR temperature we obtain similar results to those for the fuel temperature (Table 4). Again the thermal conductivity uncertainty is the most important contributor to the output uncertainty. It is also clear that the roughness does not contribute to the uncertainty in the maximum DHR temperature.

IV.G.2. Scatter Plots

The simplest qualitative sensitivity analysis consists of generating scatter plots associated with sampled variables. Since this is a visual method, only 2D and 3D plots can be visualized. All of the six variables we considered are independent, therefore we look at scatter plots in which the output variables (i.e., maximum fuel temperature and maximum DHR temperature) are plotted against one (2D plots) or two variables (3D plots). A pattern in the plot means that there is a correlation between the plotted variables whereas little or no pattern means that there is no correlation between the plotted variables.

Figure 11 shows scatter plots for the maximum fuel temperature versus the six input parameters, one at a time.

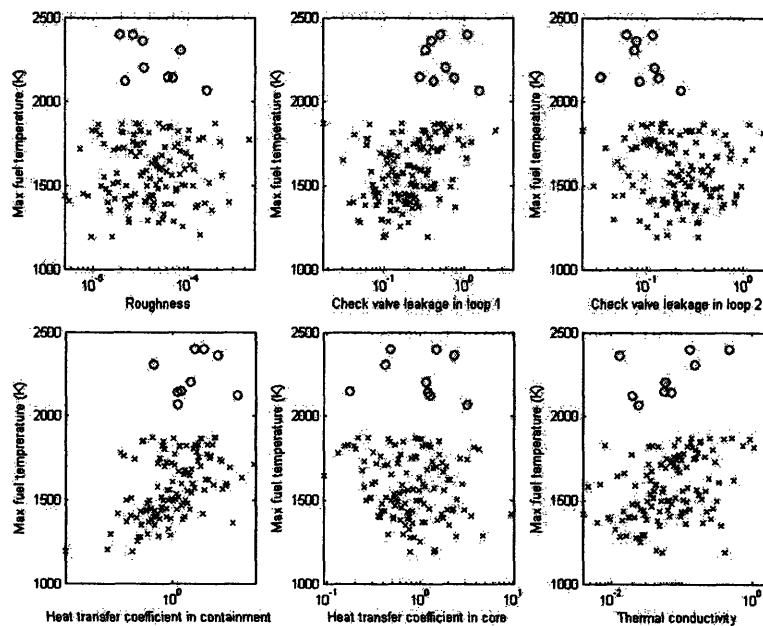


Figure 11 2-D scatter plots for maximum fuel temperature; circles denote failures.

A qualitative evaluation of the plots suggests a possible threshold effect with respect to the heat transfer coefficient in the containment. There are no other clear patterns appearing in the plots. Figure 12 shows a possible threshold effect for the maximum DHR temperature with respect to the heat transfer coefficient in the containment.

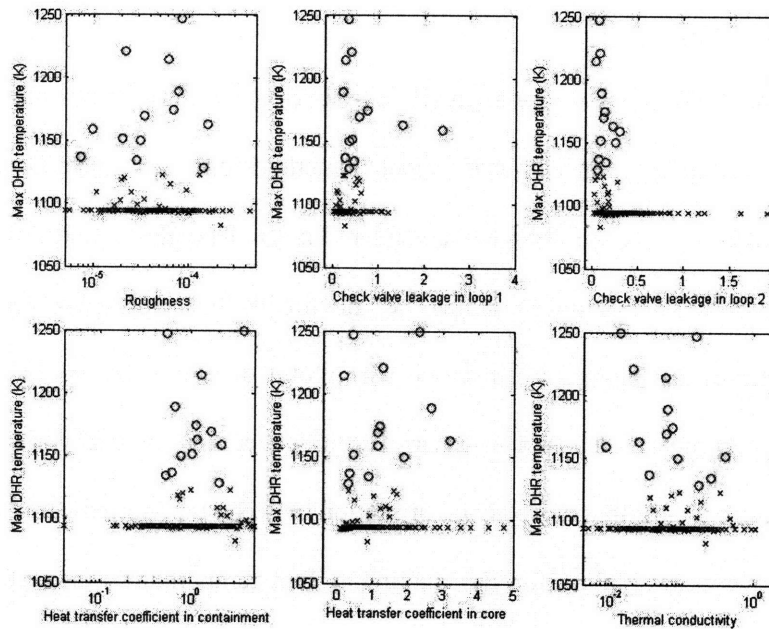


Figure 12 2-D scatter plots for maximum DHR temperature; circles denote failures.

The 3D scatter plots in Figure 13 show the only parameter combinations that exhibit some pattern. The relationship between the two check valves shows that there is a threshold effect between the maximum of the two leakages and the minimum, which confirms what was found in [9].

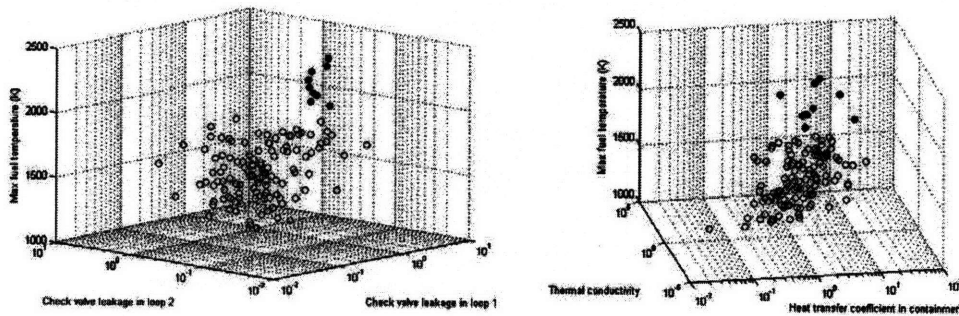


Figure 13 3-D scatter plots for maximum fuel temperature; dark circles denote failures.

The second graph on the right shows a region with low values of the heat transfer coefficient in the containment with no failures and exhibits a possible pattern suggesting a relationship involving these parameters. In the regression section, we will use these parameters to model the system.

Similar plots have been generated for the maximum DHR temperature, though they do not show any particular pattern.

IV.G.3. Entropy Analysis

The entropy-based measure for sensitivity analysis measures the uncertainty reduction in an uncertain output if an uncertain input is perfectly known. Here, the entropy method is combined with a contingency table analysis.

Contingency tables are used to test whether there is any relationship between two or more variables. For the following discussion, we will consider only one output: the maximum fuel temperature. For the second system output (i.e., the maximum DHR temperature), the method works exactly the same.

There are k variables x_k (e.g. in our case $k = 1, 2 \dots 6$) with i possible states and a single output variable y with j possible states. By state, we refer to the intervals in which we divide the range of each variable. For each input variable and the output, we can build a table with i rows and j columns where the matrix elements are integers giving the number of observed events for each combination of row and column. In our study, the input data were grouped into five different states with the same probability (hence $i = 5$ in our case).

The output was divided in four possible states.

We give here a few definitions (Ref. 17): N_{ij} is the number of events occurring when x_k assumes its i -th and y assumes its j -th value; N_i is the total number of events for a given i regardless the state of y ; N_j is the total number of events for a given j regardless the state of x_k .

We also define three different probabilities: the probability of each element in the contingency table is given by $p_{ij} = N_{ij} / N$; the probability of state x_{ki} is $p_i = N_i / N$; the probability of state y_j is $p_j = N_j / N$.

For both x_k and y , we can define their entropy functions, which give the average information in observing x_k and y . Entropy functions for x_k and y are given in Equation 4.[§] The joint entropy function is given in Equation 5.

$$H(x) = -\sum_i p_i \cdot \ln p_i \quad \text{and} \quad H(y) = -\sum_j p_j \cdot \ln p_j \quad (4)$$

$$H(x, y) = -\sum_{i,j} p_{ij} \cdot \ln p_{ij} \quad (5)$$

The mutual information, $I(x, y)$, between x and y measures how knowledge of x would reduce the uncertainty on y .

$$I(x, y) = H(x) + H(y) - H(x, y) = \sum_i \sum_j p_{ij} \cdot \ln \frac{p_{ij}}{p_i \cdot p_j} \quad (6)$$

Different indicators are built using the entropy functions and the mutual information function. The first indicator is a quantitative measure called uncertainty coefficient.

$$U(x, y) = 2 \frac{I(x, y)}{H(x) + H(y)} \quad (7)$$

U ranges from 0 to 1. A 0 value means that there is no association between the input and the output, while a value of 1 means that knowledge of x completely predicts y .

Another indicator to measure the association between two variables is the R-statistic defined as follows:

$$R(x, y) = \sqrt{1 - \exp(-2I(x, y))} \quad (8)$$

R also ranges from 0 to 1. R is 1 if there is an exact (linear or nonlinear) relationship between x and y ; it is zero when x and y are independent.

[§] From now on, we will simply refer to x_k as x

In our study, we built a contingency table for each variable with respect to both the maximum temperature in the fuel and the maximum temperature in the DHR structures.

Table 5 gives the values for $I(x, y)$, $U(x, y)$, and $R(x, y)$ where x is an independent input parameter and y is the maximum fuel temperature. All the indicators give the same ranking for the variables. The thermal conductivity of the insulation is the most important parameter followed by the heat transfer coefficient in the containment and check valve leakages. The heat transfer coefficient in the core and roughness are the least important parameters.

Table 5 Indicators of input variable importance with respect to the maximum cladding temperature.

	Max fuel temperature		
	I	U	R
roughness	0.0482	0.0326	0.3030
check valve loop 1	0.1350	0.0916	0.4864
check valve loop 2	0.1063	0.0723	0.4377
HTC containment	0.1118	0.0757	0.4477
HTC core	0.0350	0.0237	0.2601
thermal conductivity	0.1758	0.1190	0.5445

Table 6 Indicators of input variable importance with respect to the maximum cladding temperature.

	Max fuel temperature		
	I	U	R
roughness	0.0482	0.0326	0.3030
check valve loop 1	0.1350	0.0916	0.4864
check valve loop 2	0.1063	0.0723	0.4377
HTC containment	0.1118	0.0757	0.4477
HTC core	0.0350	0.0237	0.2601
thermal conductivity	0.1758	0.1190	0.5445

Table 6 gives the values of $I(x, y)$, $U(x, y)$, and $R(x, y)$ for the second output variable of the system, the maximum DHR temperature. Also in this case, all the indicators give the same ranking for the different parameters, although the most important variables are now the check valve leakages. This is explained by the fact that the temperature in the DHR

structures depends a lot on the moment the valves open, which is a function of the leakage. Whereas for the fuel temperature there are three important variables, in this case there is a clear dominance of check valve leakage over the other parameters.

The entropy analysis helps to identify those parameters which affect the most the output uncertainty and gives a ranking of those parameters. Moreover, it is in good agreement with the results from the parameter ranking analysis.

IV.H. RELIABILITY EVALUATION

The reliability of a system is defined as the probability that it will perform its function for a given period of time. In particular, the reliability of a passive system should include two principal aspects: the reliability of components (e.g., valves) and the reliability of the passive function.

We use our results to build the reliability curves for the system. We construct the reliability curve at time t by counting the number of failures before t and dividing it by the total number of simulations. These curves are shown in Figure 14 and Figure 15 for 32 trials and 128 trials, respectively.

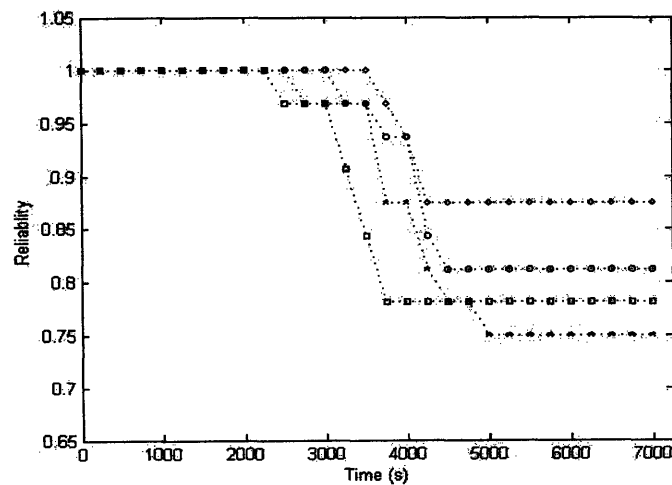


Figure 14 Reliability function; sample size of 32.

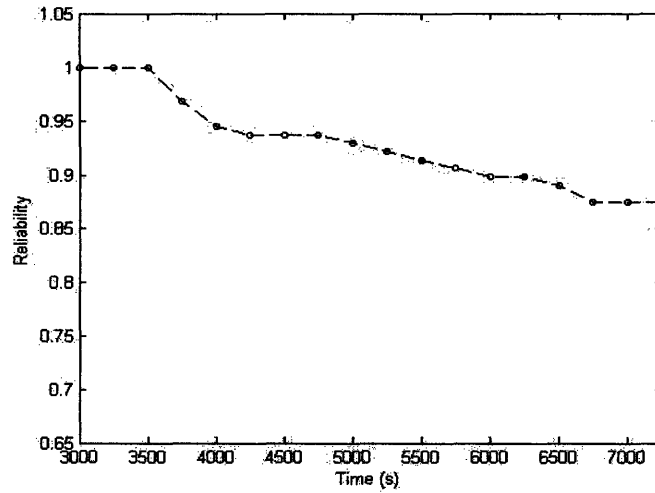


Figure 15 Reliability function for the system; sample size of 128.

For the former, we show multiple curves since multiple sets of 32 trials have been simulated. This gives not only a point estimate on the reliability but also its variability.

At $t = 7200$ s, the average reliability for the first case is $R_{32} = 0.805$ while the value obtained with 128 trials is $R_{128} = 0.875$. The agreement between the two cases suggests that a sample of size 32 gives sufficient information for design purposes with the advantage of being less onerous in terms of calculation time.

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V. CONCLUSIONS

The reliability evaluation process provides useful information to the designer when the uncertainty analysis is carried out in parallel with the design. Important parameters and situations are not easy to be foreseen through only mechanistic analysis with nominal values of the parameters. The probabilistic approach allows the designer to have better insights into the behavior of the system.

The changes in the design that we proposed succeeded at both reducing the overall failure probability of the system and reducing the impact of the major contributor to the failure probability; the system performance was affected positively by the insertion of insulation without any increase in the design containment pressure.

Nonetheless, a purely passive GFR system still has a high conditional probability of failure that is difficult to reduce significantly. In our case, we obtained a reduction by roughly a factor of five in the failure probability. However, the conditional probability is still deemed to be high. Therefore, a reliable active system appears to be better suited for this particular application. Our results have led the MIT team to adopt an active DHR as the main mode of decay heat removal for the GFR.

An important issue is the number of simulations required to perform in order to obtain an accurate failure probability. It seems that the number of trials to simulate is very much dependent on the number of input parameters, their distributions (i.e., long tail distributions need a higher number of simulations) and the targeted failure probability. The issue is even more important in the case of complex systems since the computational time may become prohibitive, as it was in our case. A clear understanding of the relationship between the number of trials and the above mentioned parameters is the next step to better support any PRA study.

Sensitivity analysis gave important insights into the system. The first result is identification of the importance of the thermal conductivity of the insulation material in the DHR pipes. The key parameter affecting the failure probability is the uncertainty in the insulation thermal conductivity and the effect of insulation placement. This is also not what a designer would intuitively expect, especially the issue of placement insulation on the inner hot pipe wall. However, there is a physical explanation for that since the insulation affects the driving force for natural flow, which is responsible for ultimate core cooling.

Another insight from the analysis is that the heat transfer coefficient in the core is not as important as a designer would expect. Our results show that the heat transfer coefficient in the containment structures is more important. This is consistent with [1], where it was found that the containment pressure is key parameter driving the system performance and the heat transfer coefficient in the containment structures is an important parameters affecting containment pressure.

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APPENDIX I – NONLINEAR REGRESSION

The clear non-linearity of the model was approached using a nonlinear regression method. The basic idea of nonlinear regression is the same as that of linear regression, which is to find an output to a vector of input variables. The difficulty here lays in the fact that our system doesn't follow any particular functional form. The fitting tool we used estimates the coefficients of the nonlinear regression function using least squares.

From the previous analysis we identified two input parameters to describe the regression model: heat transfer coefficient in the containment and thermal conductivity, as those are the most significant parameters. Therefore the nonlinear function is given by:

$$y_i = f(x_{4i}, x_{6i}, \underline{\beta}) + \varepsilon_i \quad i = 1, \dots, n$$

In Equation 11, y_i are the outputs (e.g. maximum temperature), x_4 is the heat transfer coefficient in containment and x_6 is the thermal conductivity.

To assess the adequacy of regression models, the R^2 coefficient plays an important role and it is defined as follows:

$$R^2 = \frac{\sum_i (\hat{y}_i - \bar{y})^2}{\sum_i (y_i - \bar{y})^2}$$

In the formula, \hat{y}_i is the estimate of y_i obtained from the model; those values are compared to the mean value of y . The ratio provides a measure to assess the accordance of the model to the observed data. In case the model reproduces completely the data, R^2 is close to 1.

An unsuccessful model has a ratio close to 0.

We tested different model to reproduce the observed data from 128 trials and the best nonlinear model we could find has a R^2 value of 0.46, which means that it accounts for 46% of the variability in the dependent variable.

The low ratio can be explained by the incapability to reproduce the extreme data with very high temperature. However the failure probability (for the only cladding temperature criteria) is close to the observed one: 11 failures in 128 trials instead of 9 failures as observed.

In order to avoid the effects of units, distribution assumptions and nonlinear behavior we also used the technique of rank regression. In this case, data are replaced by their rank and then the nonlinear regression procedure is repeated as we already presented. To determine the rank of each value, the smallest receives rank 1, the next largest has rank 2 and so on. In our case the largest value of each input parameters has rank 128 since we have 128 realizations.

Even in this case we were not able to model the system with good approximation; the best model we could find showed a R^2 value of 0.40. Once again the reason depends on the strongly non linearity of the system we want to model.

APPENDIX II - NOMINAL INPUT DECK

```

= MIT-GCFR Plate DHR
100 newath transnt
101 run
102 si si
105 5.0 6.0
110 air
115 1.0
*
      g=1, no noncond
120 100010000 0.0 he primary 1
121 133010000 0.0 h2o h2opc 1
122 143010000 0.0 h2o h2oit 1
123 700010000 0.0 h2o uhsloop1
124 701010000 0.0 h2o uhsloop2
*crdno end time min dt max dt control minor ed major ed restart
201 6000.0 1.0-10 0.0025 23 4000 3200000 3200000
*
*
-----
* MINOR EDITS
*
-----
* Reactor Coolant System
*
-----
*
301 p 750010000 * Water Loops Data
302 tempf 750010000 *
303 p 751010000 *
304 tempf 751010000 *
305 p 750200000 *
306 tempf 750200000 *
307 p 751200000 *
308 tempf 751200000 *
309 mflowj 750010000 *
310 mflowj 751010000 *
311 cntrlvar 126 * q from 710
312 cntrlvar 127 * q from 711
313 cntrlvar 128 * q from 750
314 cntrlvar 129 * q from 751
315 p 710010000 *
316 tempf 710010000 *
317 p 711010000 *
318 tempf 711010000 *
319 p 710050000 *
320 tempf 710050000 *
321 p 711050000 *
322 tempf 711050000 *
*
*
323 p 650010000 * DHR Loops Data
324 p 651010000 *
325 p 650050000 *
326 p 651050000 *
327 tempg 650010000 *
328 tempg 651010000 *
329 tempg 650050000 *
330 tempg 651050000 *
331 mflowj 665000000 *
332 mflowj 674000000 *
333 cntrlvar 120 * q from 650
334 cntrlvar 125 * q from 651
335 p 610050000 *
336 tempg 610050000 *
337 p 611050000 *
338 tempg 611050000 *
339 p 666010000 *
340 tempg 666010000 *
341 p 676010000 *
342 tempg 676010000 *
343 p 666050000 *
344 tempg 666050000 *
345 p 676050000 *
346 tempg 676050000 *
347 httemp 610100101 *
348 httemp 611100101 *
*
*
349 p 250010000 * Reactor and

```

```

350 p      251010000 * Downcomer Data
351 p      250080000 *
352 p      251080000 *
353 tempg  250010000 *
354 tempg  251010000 *
355 tempg  250080000 *
356 tempg  251080000 *
357 p      670010000 *
358 p      670080000 *
359 p      800010000 *
360 p      800080000 *
361 tempg  670010000 *
362 tempg  670080000 *
363 tempg  800010000 *
364 tempg  800080000 *
365 mflowj  250010000 *
367 mflowj  251010000 *
368 mflowj  670010000 *
369 mflowj  800010000 *
370 mflowj  300040000 *
371 p      300050000 *
372 tempg  300050000 *
373 p      100010000 *
374 tempg  100010000 *
375 cntrlvar 111 * Q extracted from reactor
376 cntrlvar 102 * Estimated Q extracted
377 cntrlvar 123 * Q generated by the reactor
378 cntrlvar 110 * Max temp fuel 251 httemp
379 cntrlvar 103 * MAX temp clad 251 httemp
*
*
380 mflowj  062000000 * Break and Containment Data
381 sonicj  062000000 *
382 p      070010000 *
383 tempg  070010000 *
*
*
384 mflowj  082000000 * PCU Data
385 p      520300000 *
386 tempg  520300000 *
387 cntrlvar 40 *
388 mflowj  550010000 *
389 cntrlvar 42 *
390 mflowj  580010000 *
391 mflowj  597010000 *
392 turvel  510 * Turbine velocity rad/s
393 cntrlvar 32 * q from pc
394 cntrlvar 34 * q from ic

```

20800001 sonicj 062000000

```

*-----*
* TRIPS *
*-----*
*
20600000 expanded
*Time to be taken for Steady-State: 50 seconds
20603500 time 0 ge timeof 522 5. n * trip LP cmpr, HP cmpr and Turbine
20603600 time 0 ge timeof 522 5. l * generator trip
20604810 time 0 ge null 0 5.e6 l * open bypass valve
20604820 time 0 ge null 0 1.0e6 l * close bypass valve
*
20605010 time 0 ge timeof 522 5. l *@Rx Trip'
*20605020 time 0 ge timeof 501 0.0 l -1. *@Rx Trip'
*
20605210 time 0 lt null 0 5.e6 n *trpvlv from tmpdvol
20605220 time 0 ge null 0 5. l *break junction (valve 062)
20605230 time 0 ge timeof 522 180. n

20605240 cntrlvar 102 lt cntrlvar 123 -2.e6 n
20605250 time 0 ge null 0 0. n *valves connecting DHRs to 670
20605260 time 0 lt null 0 5. n *OPEN valve 685 & 686
20605270 time 0 lt null 0 5. n *open valve 082
20605280 cntrlvar 110 gt null 0 900. n
20605290 time 0 ge timeof 1003 0. l *connect external torque
20605300 time 0 ge null 0 20000. n
20605310 time 0 lt null 0 20000. n
20605320 vlvarea 665 eq null 0 0. n

20605340 vlvarea 674 eq null 0 0. n

20605350 turvel 510 lt null 0 0.01 n *trip cprssrs
20605360 mflowj 597010000 gt null 0 1.67 n
20605370 mflowj 082000000 le null 0 1.67 n
20605380 time 0 gt null 0 10. n
20605390 p      690010000 ge p      698010000 0. n
20605400 p      691010000 ge p      694010000 0. n

```

```

20605410 p      690010000 lt p      698010000 0. n
20605420 p      691010000 lt p      694010000 0. n
20605430 time 0 ge timeof 522 40. n

```

```

20610010 530 and 534 n      *valve 694
20610020 530 and 532 n      *valve 692
20610030 523 and 1006 l     *close valve 082
20610040 525 xor 1005 n     *open vlvs 593 & 503
20610050 537 and 538 l     *open vlvs 501 & 591
20610060 524 and 528 n

```

```

*
*
**#####
**
**          §
**      HYDRODYNAMIC COMPONENTS      §
**          §
**#####
*

```

```

*-----
*
* PRIMARY COOLANT SYSTEM
*
*-----
*

```

```

*-----
* Reactor Inlet Plenum
*-----

```

```

* name pipe/annulus
1000000 rx-in-pl pipe
* number of volumes
1000001 5
* area no of vol
1000101 6.7117 5
* length no of vol
1000301 0.2 5
* volume no of vol
1000401 0.0 5
* azi ang no of vol
1000501 90. 5
* ver ang no of vol
1000601 90. 5
* elev. no of vol
1000701 0.1 5
* rough dhydr. no of vol
1000801 1.0e-5 0.15 5
* kforw kbackw no of jun
1000901 0.0 0.0 4
* v-flag no of vol
1001001 00000 5
* j-flag no of jun
1001101 00000 4
* cntrl pressure temperature * * * no of vol
1001201 0 7152053. 2310826. 2310826. 1. 0. 1
1001202 0 7152044. 2310826. 2310826. 1. 0. 2
1001203 0 7152034. 2310826. 2310826. 1. 0. 3
1001204 0 7152024. 2310826. 2310826. 1. 0. 4
1001205 0 7152014. 2310826. 2310826. 1. 0. 5
* cntrl
1001300 0
* w/v.liq w/v.vap w/v.int no of jun
1001301 9.97593 9.97593 0. 1 * 319.2105
1001302 9.97594 9.97594 0. 2 * 319.2105
1001303 9.97595 9.97595 0. 3 * 319.2105
1001304 9.97596 9.97596 0. 4 * 319.2105

```

```

*-----
* Junction: Reactor Inlet Plenum to Lower Reflector
*-----

```

```

* name junction
2080000 rip-lrc sngljun
* from to area kforw kbackw j-flag
2080101 100050002 210000000 1.39801 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
2080201 0 47.4743 47.4743 0. * 316.416
*

```

```

*-----
* Junction: Reactor Inlet Plenum to Lower Reflector
*-----

```

```

* name junction
2090000 rip-lrh sngljun
* from to area kforw kbackw j-flag
2090101 100010000 211000000 0.01259 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
2090201 0 46.5594 46.5594 0. * 2.79462

```

```

*-----
* Reactor Inlet Reflector
*-----
* name volume
2100000 in-rfilt snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
2100101 1.39801 1.0 0.0 90.0 90.0 1.0 5.9409e-005 0.0127 000000
* cntrl press temp
2100200 0 7140967. 2311218. 2311218. 1.
*
*-----
* Reactor Inlet Reflector Hot Channel
*-----
* name volume
2110000 in-rfhc snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
2110101 0.01259 1.0 0.0 90.0 90.0 1.0 5.9409e-005 0.0127 000000
* cntrl press temp
2110200 0 7141388. 2311206. 2311206. 1.
*
*-----
* Junction: Reactor Inlet Reflector to Core
*-----
* name junction
2150000 irf-cor sngljun
* from to area kforw kbackw j-flag
2150101 210010000 250000000 1.39801 3.00 0.00 0000000
* cntrl w/v.liq w/v.vap w/v.int
2150201 0 47.5237 47.5237 0. * 316.416
*
*-----
* Junction: Reactor Inlet Reflector to Core Hot Channel
*-----
* name junction
2160000 irf-chc sngljun
* from to area kforw kbackw j-flag
2160101 211010000 251000000 0.01259 3.00 0.00 0000000
* cntrl w/v.liq w/v.vap w/v.int
2160201 0 46.6061 46.6061 0. * 2.79462
*
*-----
* Reactor Core
*-----
* name pipe/annulus
2500000 rx-core pipe
* number of volumes
2500001 8
* area no of vol
2500101 1.39801 8
* length no of vol
2500301 0.24375 8
* volume no of vol
2500401 0.0 8
* azi ang no of vol
2500501 90. 8
* ver ang no of vol
2500601 90. 8
* elev. no of vol
2500701 0.24375 8
* rough dhydr. no of vol
2500801 5.9409e-005 0.0127 8
* kforw kbackw no of jun
2500901 0.0 0.0 7
* v-flag no of vol
2501001 00000 8
* j-flag no of jun
2501101 000000 7
* cntrl pressure temperature * * * no of vol
2501201 0 7118911. 2407030. 2407030. 1. 0. 1
2501202 0 7116096. 2541886. 2541886. 1. 0. 2
2501203 0 7113010. 2703636. 2703636. 1. 0. 3
2501204 0 7109660. 2879407. 2879407. 1. 0. 4
2501205 0 7106074. 3055207. 3055207. 1. 0. 5
2501206 0 7102302. 3217043. 3217043. 1. 0. 6
2501207 0 7098412. 3352028. 3352028. 1. 0. 7
2501208 0 7094483. 3449417. 3449417. 1. 0. 8

* cntrl
2501300 0
* w/v.liq w/v.vap w/v.int no of jun
2501301 49.585 49.585 0. 1 * 316.416
2501302 52.3795 52.3795 0. 2 * 316.416
2501303 55.7317 55.7317 0. 3 * 316.416
2501304 59.3765 59.3765 0. 4 * 316.416
2501305 63.0252 63.0252 0. 5 * 316.416
2501306 66.3886 66.3886 0. 6 * 316.416
2501307 69.2 69.2 0. 7 * 316.416
*

```



```

*-----
* Reactor Core Hot Channel
*-----
* name pipe/annulus
2510000 rx-core pipe
* number of volumes
2510001 8
* area no of vol
2510101 0.01259 8
* length no of vol
2510301 0.24375 8
* volume no of vol
2510401 0.0 8
* azi ang no of vol
2510501 90. 8
* ver ang no of vol
2510601 90. 8
* elev. no of vol
2510701 0.24375 8
* rough dhydr. no of vol
2510801 5.9409e-005 0.0127 8
* kforw kbackw no of jun
2510901 0.0 0.0 7
* v-flag no of vol
2511001 00000 8
* j-flag no of jun
2511101 000000 7
* cntrl pressure temperature * * * no of vol
2511201 0 7120148. 2423867. 2423867. 1. 0. 1
2511202 0 7117354. 2582030. 2582030. 1. 0. 2
2511203 0 7114255. 2771736. 2771736. 1. 0. 3
2511204 0 7110856. 2977891. 2977891. 1. 0. 4
2511205 0 7107192. 3184081. 3184081. 1. 0. 5
2511206 0 7103315. 3373888. 3373888. 1. 0. 6
2511207 0 7099301. 3532202. 3532202. 1. 0. 7
2511208 0 7095240. 3646411. 3646411. 1. 0. 8

* cntrl
2511300 0
* w/v.liq w/v.vap w/v.int no of jun
2511301 48.9652 48.9652 0. 1 * 2.79462
2511302 52.1772 52.1772 0. 2 * 2.79462
2511303 56.0307 56.0307 0. 3 * 2.79462
2511304 60.2206 60.2206 0. 4 * 2.79462
2511305 64.4151 64.4151 0. 5 * 2.79462
2511306 68.2815 68.2815 0. 6 * 2.79462
2511307 71.5131 71.5131 0. 7 * 2.79462
*
*-----
* Junction: Reactor Core to Outlet Reflector
*-----
* name junction
2550000 cor-orf sngljun
* from to area kforw kbackw j-flag
2550101 250010000 290000000 1.39801 3.00 0.00 0000000
* cntrl w/v.liq w/v.vap w/v.int
2550201 0 71.2362 71.2362 0. * 316.416
*
*-----
* Junction: Reactor Core Hot Channel to Outlet Reflector
*-----
* name junction
2560000 cor-ohc sngljun
* from to area kforw kbackw j-flag
2560101 251010000 291000000 0.01259 3.00 0.00 0000000
* cntrl w/v.liq w/v.vap w/v.int
2560201 0 73.853 73.853 0. * 2.79462
*
*-----
* Reactor Outlet Reflector
*-----
* name volume
2900000 o-rflt snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
2900101 1.39801 1.0 0.0 90.0 90.0 1.0 5.9409e-005 0.0127 000000
* cntrl press temp
2900200 0 7061007. 3448288. 3448288. 1.
*
*-----
* Reactor Outlet Reflector HC
*-----
* name volume
2910000 o-rflt snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
2910101 0.01259 1.0 0.0 90.0 90.0 1.0 5.9409e-005 0.0127 000000
* cntrl press temp
2910200 0 7061106. 3645208. 3645208. 1.
*

```

```

*-----
* Junction: Reactor Core to Outlet Plenum
*-----
* name junction
2920000 cor-orf sngljun
* from to area kforw kbackw j-flag
2920101 290010000 300000000 0.0 0.46 0.46 0000000
* cntrl w/v.liq w/v.vap w/v.int
2920201 0 71.4177 71.4177 0. * 316.416
*
*-----
* Junction: Reactor Core Hot Channel to Outlet Plenum
*-----
* name junction
2930000 cor-ohc sngljun
* from to area kforw kbackw j-flag
2930101 291010000 300000000 0.0 0.46 0.46 0000000
* cntrl w/v.liq w/v.vap w/v.int
2930201 0 74.045 74.045 0. * 2.79462
*-----
* Reactor Outlet Plenum
*-----
* name pipe/annulus
3000000 rx-o-pl pipe
* number of volumes
3000001 5
* area no of vol
3000101 43.0080 5
* length no of vol
3000301 0.2 5
* volume no of vol
3000401 0.0 5
* azi ang no of vol
3000501 90. 5
* ver ang no of vol
3000601 90. 5
* elev. no of vol
3000701 0.20 5
* rough dhydr. no of vol
3000801 4.5e-5 7.4 5
* kforw kbackw no of jun
3000901 0.0 0.0 4
* v-flag no of vol
3001001 00000 5
* j-flag no of jun
3001101 00000 4
* cntrl pressure temperature * * * no of vol
3001201 0 7058110. 3449668. 3449668. 1. 0. 1
3001202 0 7058104. 3449667. 3449667. 1. 0. 2
3001203 0 7058098. 3449666. 3449666. 1. 0. 3
3001204 0 7058092. 3449666. 3449666. 1. 0. 4
3001205 0 7058085. 3449665. 3449665. 1. 0. 5
* cntrl
3001300 0
* w/v.liq w/v.vap w/v.int no of jun
3001301 2.34353 2.34353 0. 1 * 319.2105
3001302 2.34353 2.34353 0. 2 * 319.2105
3001303 2.34353 2.34353 0. 3 * 319.2105
3001304 2.34353 2.34353 0. 4 * 319.2105
*-----
* Junction: Plenum to Pressure controller
*-----
* name junction
*3200000 cor-orf valve
* from to area kforw kbackw j-flag
*3200101 300010000 340000000 1.e5 0. 1.e9 0000000
* cntrl w/v.liq w/v.vap w/v.int
*3200201 1 0. 312.20 0.0
*crdno valve type
*3200300 trpvlv
*crdno open trip
*3200301 521
*
*-----
* Reactor Pressure Controller
*-----
* name volume
*3400000 rx-vent tmdpvvl
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
*3400101 500.0 100.0 0.0 0.0 0.0 0. 0.00046 7.4 000000
* cntrl
*3400200 003
* press temp
*3400201 0.0 6.94220e6 1122.15
*
*-----
* RPV Downcomer #1
*-----

```

```

* name pipe/annulus
6700000 hp-hxcl pipe
* number of volumes
6700001 8
* area no of vol
6700101 3.62855 8
* length no of vol
6700301 1.05625 8
* volume no of vol
6700401 0.0 8
* azi ang no of vol
6700501 -90. 8
* ver ang no of vol
6700601 -90. 8
* elev. no of vol
6700701 -0.68125 8
* rough dhydr. no of vol
6700801 4.5e-5 0.6 8
* kforw kbackw no of jun
6700901 0.0 0.0 7
* v-flag no of vol
6701001 00000 8
* j-flag no of jun
6701101 000000 7
* cntrl pressure temperature * * * no of vol
6701201 0 7151890. 2310802. 2310802. 1. 0. 1
6701202 0 7151917. 2310805. 2310805. 1. 0. 2
6701203 0 7151944. 2310808. 2310808. 1. 0. 3
6701204 0 7151971. 2310812. 2310812. 1. 0. 4
6701205 0 7.152+6 2310816. 2310816. 1. 0. 5
6701206 0 7152025. 2310819. 2310819. 1. 0. 6
6701207 0 7152052. 2310823. 2310823. 1. 0. 7
6701208 0 7152079. 2310827. 2310827. 1. 0. 8
* cntrl
6701300 0
* w/v.liq w/v.vap w/v.int no of jun
6701301 9.22622 9.22622 0. 1 * 319.2105
6701302 9.22622 9.22622 0. 2 * 319.2105
6701303 9.22621 9.22621 0. 3 * 319.2105
6701304 9.2262 9.2262 0. 4 * 319.2105
6701305 9.2262 9.2262 0. 5 * 319.2105
6701306 9.2262 9.2262 0. 6 * 319.2105
6701307 9.22619 9.22619 0. 7 * 319.2105
*
*-----
* RPV Downcomer #2
*-----
* name pipe/annulus
8000000 hp-hxcl pipe
* number of volumes
8000001 8
* area no of vol
8000101 3.62855 8
* length no of vol
8000301 1.05625 8
* volume no of vol
8000401 0.0 8
* azi ang no of vol
8000501 -90. 8
* ver ang no of vol
8000601 -90. 8
* elev. no of vol
8000701 -0.68125 8
* rough dhydr. no of vol
8000801 4.5e-5 0.6 8
* kforw kbackw no of jun
8000901 0.0 0.0 7
* v-flag no of vol
8001001 00000 8
* j-flag no of jun
8001101 000000 7
* cntrl pressure temperature * * * no of vol
8001201 0 7151890. 2310802. 2310802. 1. 0. 1
8001202 0 7151917. 2310805. 2310805. 1. 0. 2
8001203 0 7151944. 2310808. 2310808. 1. 0. 3
8001204 0 7151971. 2310812. 2310812. 1. 0. 4
8001205 0 7.152+6 2310816. 2310816. 1. 0. 5
8001206 0 7152025. 2310819. 2310819. 1. 0. 6
8001207 0 7152052. 2310823. 2310823. 1. 0. 7
8001208 0 7152079. 2310827. 2310827. 1. 0. 8
* cntrl
8001300 0
* w/v.liq w/v.vap w/v.int no of jun
8001301 9.22622 9.22622 0. 1 * 319.2105
8001302 9.22622 9.22622 0. 2 * 319.2105
8001303 9.22621 9.22621 0. 3 * 319.2105
8001304 9.2262 9.2262 0. 4 * 319.2105
8001305 9.2262 9.2262 0. 5 * 319.2105

```

```

8001306 9.2262 9.2262 0. 6 * 319.2105
8001307 9.22619 9.22619 0. 7 * 319.2105
*
-----
* Junction: Pressure Controller to RPV Downcomer
-----
*crdno name type
6850000 j-contr valve
*
*crdno from to area jefvcahs
6850101 680000000 670000000 1.0 0. 0. 00000100
6850110 0.6 0.0 1.0 1.0
*crdno var flowf flowg velj
6850201 0 0. 0. 0. * 0.
*crdno valve type
6850300 trpvlv
*crdno open trip
6850301 526
*
-----
* Junction: Pressure Controller to RPV Downcomer
-----
*crdno name type
6860000 j-contr valve
*
*crdno from to area jefvcahs
6860101 680000000 800000000 1.0 0. 0. 00000100
6860110 0.6 0.0 1.0 1.0
*crdno var flowf flowg velj
6860201 0 0. 0. 0. * 0.
*crdno valve type
6860300 trpvlv
*crdno open trip
6860301 526
*
-----
* Pressure Controller for steady state
-----
* name volume
6800000 p-contr tmdpv01
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6800101 500.00 100.0 0.0 0.0 0.0 0. 0.00046 7.4 000000
* cntrl
6800200 3
* press temp
6800201 0.0 7.08000e6 761.15
*
-----
* SNGLJ: RPV Cold Duct to Rx Inlet Plenum
-----
* name junction
6750000 cd-iplm sngljun
* from to area kforw kbackw j-flag
6750101 670010000 100000000 0.0 1.0 1.0 0000001
* cntrl w/v.liq w/v.vap w/v.int
6750201 0 9.97592 9.97592 0. * 319.2105
*
-----
* SNGLJ: RPV Cold Duct to Rx Inlet Plenum
-----
* name junction
8010000 cd-iplm sngljun
* from to area kforw kbackw j-flag
8010101 800010000 100000000 0.0 1.0 1.0 0000001
* cntrl w/v.liq w/v.vap w/v.int
8010201 0 9.97592 9.97592 0. * 319.2105
*
** Name Valve
5010000 bypass tmdpjun
* from to area j-flag
5010101 500000000 502000000 0.00 0000000
* cntrl trp
5010200 1 1005
*
5010201 -0.1 0. 0. 0.
5010202 0. 0. -10. 0.
*
-----
*crdno name type
5020000 cprbp2 tmdpv01
*
*crdno area lngth vol h-a v-ang delz rgh dhy pvbfe
5020101 78. .9104 0 0 0. .0 0 1.5 00010
*
*crdno ebt
5020200 3
*crdno time press temp
5020201 0.0 5.e6 1150.

```

```

*
***
* 500 Hot Duct volume
***
*
*crdno name type
5000000 hotduct pipe
*
*crdno no.vols.
5000001 4
*
*crdno area vol.no.
5000101 1.606 4
*
*crdno length vol.no.
5000301 1.85 4
*
*crdno v-ang vol.no.
5000601 0.0 4
*
*crdno rough dhy vol.no.
5000801 0. 1.43 4
*
*crdno ff rf jun.no.
5000901 10. 0. 3
*
*crdno tlpvbf vol.no.
5001001 10010 4
*
*crdno jefvcahs jun.no.
5001101 0000000 3
*
*crdno ebt pressure temp qual vol.no.
5001201 0 7001960. 3442779. 3442779. 1. 0. 1
5001202 0 6939344. 3434540. 3434540. 1. 0. 2
5001203 0 6876488. 3425628. 3425628. 1. 0. 3
5001204 0 6813382. 3415980. 3415980. 1. 0. 4
*
*crdno i.c.
5001300 0
*
*crdno flowf flowg velj jun.no.
5001301 62.9543 62.9543 0. 1 * 319.2105
5001302 63.1902 63.1902 0. 2 * 319.2105
5001303 63.4479 63.4479 0. 3 * 319.2105
*
*crdno dhy jun.no
5001401 1.43 1.0 1.0 1.0 3
*
*
*-----$
*hydro component name component type
5100000 turbine1 turbine
*-----$
* no. juns vel/flow
5100001 1 0
*hydro area length volume
5100101 0.4857 4.2 0.0
*
*hydro horz angle vert angle delta z
5100102 0.0 90.0 4.2
*
*hydro roughness hyd diam fe
5100103 6.0e-4 0.7864 10
*
*hydro ebt pressure tempe
5100200 0 3335696. 2520473. 2520473. 1.
* from to area Kf Kr efvcahs
5101101 500010000 510000000 0.193 0.555 0.555 0000010
* velf velg veli
5101201 530.307 530.307 0. * 319.2105
* speed iner fric shaft trip sep eff
5100300 376.991 5478.2 0.39 600 0
* type eff r radius
5100400 2 0.93 0.5 0.6
*-----$
*crdno name type
5150000 trbout branch
5150001 2 0
5150101 0.5 1.3848 0.0
5150102 0.0 -90.0 -1.3848
5150103 0.0 0.7979 11000
5150200 0 2944520. 2419992. 2419992. 1.
*crdno from to area floss loss flag
5151101 510010000 515000000 0.0 3.0 0.0 000100
5152101 515010000 520000000 0.0 3.0 0.0 000000
*crdno flowf flowg velj
5151201 345.128 345.128 0. * 319.2105

```

```

5152201 357.214 357.214 0. * 319.2105
*
*****
5200000 rc-hot pipe
*****
* no. vols
5200001 30
* vol area
5200101 10.98 30
* length
5200301 0.09384 30
* volume
5200401 0.0 30
* azim angle
5200501 0.0 30
* incl angle
5200601 -90.0 30
* roughness hyd dia
5200801 0.3-6 2.4384e-3 30
* kf kr
5200901 0.0 0.0 29
* pvbfe
5201001 00000 30
* fvcchs
5201101 001000 29
* ebt press temp
5201201 0 2706427. 2322732. 2322732. 1. 0. 1
5201202 0 2706121. 2286169. 2286169. 1. 0. 2
5201203 0 2705834. 2249496. 2249496. 1. 0. 3
5201204 0 2705555. 2212712. 2212712. 1. 0. 4
5201205 0 2705283. 2175820. 2175820. 1. 0. 5
5201206 0 2705019. 2138822. 2138822. 1. 0. 6
5201207 0 2704762. 2101724. 2101724. 1. 0. 7
5201208 0 2704513. 2064526. 2064526. 1. 0. 8
5201209 0 2704272. 2027234. 2027234. 1. 0. 9
5201210 0 2704037. 1989851. 1989851. 1. 0. 10
5201211 0 2703810. 1952383. 1952383. 1. 0. 11
5201212 0 2703588. 1914833. 1914833. 1. 0. 12
5201213 0 2703366. 1877206. 1877206. 1. 0. 13
5201214 0 2703143. 1839506. 1839506. 1. 0. 14
5201215 0 2702920. 1801740. 1801740. 1. 0. 15
5201216 0 2702696. 1763912. 1763912. 1. 0. 16
5201217 0 2702473. 1726028. 1726028. 1. 0. 17
5201218 0 2702250. 1688096. 1688096. 1. 0. 18
5201219 0 2702027. 1650121. 1650121. 1. 0. 19
5201220 0 2701805. 1612112. 1612112. 1. 0. 20
5201221 0 2701583. 1574077. 1574077. 1. 0. 21
5201222 0 2701362. 1536022. 1536022. 1. 0. 22
5201223 0 2701141. 1497958. 1497958. 1. 0. 23
5201224 0 2700922. 1459893. 1459893. 1. 0. 24
5201225 0 2700704. 1421836. 1421836. 1. 0. 25
5201226 0 2700487. 1383799. 1383799. 1. 0. 26
5201227 0 2700272. 1345792. 1345792. 1. 0. 27
5201228 0 2700059. 1307826. 1307826. 1. 0. 28
5201229 0 2699848. 1269914. 1269914. 1. 0. 29
5201230 0 2699634. 1232069. 1232069. 1. 0. 30
* vel/flow
5201300 0
* liquid vapor int-face
5201301 16.6594 16.6594 0. 1 * 319.2105
5201302 16.39818 16.39818 0. 2 * 319.2105
5201303 16.13603 16.13603 0. 3 * 319.2105
5201304 15.873 15.873 0. 4 * 319.2105
5201305 15.60912 15.60912 0. 5 * 319.2105
5201306 15.3444 15.3444 0. 6 * 319.2105
5201307 15.0789 15.0789 0. 7 * 319.2105
5201308 14.8126 14.8126 0. 8 * 319.2105
5201309 14.54556 14.54556 0. 9 * 319.2105
5201310 14.2778 14.2778 0. 10 * 319.2105
5201311 14.00935 14.00935 0. 11 * 319.2105
5201312 13.74027 13.74027 0. 12 * 319.2105
5201313 13.4706 13.4706 0. 13 * 319.2105
5201314 13.20037 13.20037 0. 14 * 319.2105
5201315 12.92963 12.92963 0. 15 * 319.2105
5201316 12.6584 12.6584 0. 16 * 319.2105
5201317 12.38676 12.38676 0. 17 * 319.2105
5201318 12.11472 12.11472 0. 18 * 319.2105
5201319 11.84234 11.84234 0. 19 * 319.2105
5201320 11.56968 11.56968 0. 20 * 319.2105
5201321 11.29678 11.29678 0. 21 * 319.2105
5201322 11.02372 11.02372 0. 22 * 319.2105
5201323 10.75055 10.75055 0. 23 * 319.2105
5201324 10.47733 10.47733 0. 24 * 319.2105
5201325 10.20414 10.20414 0. 25 * 319.2105
5201326 9.93105 9.93105 0. 26 * 319.2105
5201327 9.65813 9.65813 0. 27 * 319.2105
5201328 9.38548 9.38548 0. 28 * 319.2105
5201329 9.11317 9.11317 0. 29 * 319.2105

```

```

*hydro jun diam beta intercept slope jun
5201401 2.4384e-3 0.0 1.0 1.0 29
*
*-----$*
*---
*crdno name type
5220000 rc-pr angljun
*
*crdno from to area floss rloss flag
5220101 520010000 525000000 0.0 0. 0. 100
*
*crdno ctl flowf flowg velj
5220201 0 194.1553 194.1553 0. * 319.2105
*
***
* Inlet pipe to precooler
*
*crdno name type
5250000 pr-in pipe
*
*crdno no.vols.
5250001 3
*
*crdno area vol.no.
5250101 0.5 3
*
*crdno length vol.no.
5250301 3.65 3
*
*crdno v-ang vol.no.
5250601 -90.0 3
*
*crdno rough dhy vol.no.
5250801 0. 0.7979 3
*
*crdno ff rf jun.no.
5250901 0. 0. 2
*
*crdno tlpvbf vol.no.
5251001 10010 3
*
*crdno jefvcahs jun.no.
5251101 0000000 2
*
*crdno ebt pressure temp qual vol.no.
5251201 0 2614938. 1219848. 1219848. 1. 0. 1
5251202 0 2613621. 1219651. 1219651. 1. 0. 2
5251203 0 2613715. 1219665. 1219665. 1. 0. 3
*
*crdno i.c.
5251300 0
*
*crdno flowf flowg velj jun.no.
5251301 197.139 197.139 0. 1 * 319.2105
5251302 197.187 197.187 0. 2 * 319.2105
*
*crdno dhy jun.no
5251401 0.7979 1.0 1.0 1.0 2
*
*---
*crdno name type
5280000 pr-inj angljun
*
*crdno from to area floss rloss flag
5280101 525010000 530000000 0.0 0. 0. 100
*
*crdno ctl flowf flowg velj
5280201 0 197.1838 197.1838 0. * 319.2105
*
*-----$*
5300000 precool pipe
*-----$*
* no. vols
5300001 20
* vol area
5300101 28.4 20
* length
5300301 0.2365 20
* volume
5300401 0.0 20
* azim angle
5300501 0.0 20
* incl angle
5300601 -90.0 20
* roughness hyd dia
5300801 4.0e-3 9.924e-3 20
* kf kr
5300901 80.0 80.0 19

```

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* pvbfe
5301001 00000 20
* fvcchs
5301101 001000 19
* ebt press temp
5301201 0 2615890. 1179799. 1179799. 1. 0. 1
5301202 0 2614262. 1144789. 1144789. 1. 0. 2
5301203 0 2612682. 1114443. 1114443. 1. 0. 3
5301204 0 2611144. 1088112. 1088112. 1. 0. 4
5301205 0 2609642. 1065244. 1065244. 1. 0. 5
5301206 0 2608171. 1045368. 1045368. 1. 0. 6
5301207 0 2606727. 1028078. 1028078. 1. 0. 7
5301208 0 2605307. 1013029. 1013029. 1. 0. 8
5301209 0 2603907. 999923. 999923. 1. 0. 9
5301210 0 2602526. 988503. 988503. 1. 0. 10
5301211 0 2601159. 978549. 978549. 1. 0. 11
5301212 0 2599806. 969869. 969869. 1. 0. 12
5301213 0 2598464. 962299. 962299. 1. 0. 13
5301214 0 2597133. 955695. 955695. 1. 0. 14
5301215 0 2595810. 949934. 949934. 1. 0. 15
5301216 0 2594495. 944906. 944906. 1. 0. 16
5301217 0 2593187. 940519. 940519. 1. 0. 17
5301218 0 2591884. 936692. 936692. 1. 0. 18
5301219 0 2590586. 933352. 933352. 1. 0. 19
5301220 0 2589292. 930439. 930439. 1. 0. 20
* vel/flow
5301300 0
* liquid vapor int-face
5301301 3.35547 3.35547 0. 1 * 319.2105
5301302 3.25721 3.25721 0. 2 * 319.2105
5301303 3.17212 3.17212 0. 3 * 319.2105
5301304 3.09839 3.09839 0. 4 * 319.2105
5301305 3.03445 3.03445 0. 5 * 319.2105
5301306 2.97898 2.97898 0. 6 * 319.2105
5301307 2.93084 2.93084 0. 7 * 319.2105
5301308 2.88905 2.88905 0. 8 * 319.2105
5301309 2.85277 2.85277 0. 9 * 319.2105
5301310 2.821274 2.821274 0. 10 * 319.2105
5301311 2.79394 2.79394 0. 11 * 319.2105
5301312 2.77023 2.77023 0. 12 * 319.2105
5301313 2.74967 2.74967 0. 13 * 319.2105
5301314 2.73186 2.73186 0. 14 * 319.2105
5301315 2.716445 2.716445 0. 15 * 319.2105
5301316 2.70312 2.70312 0. 16 * 319.2105
5301317 2.691623 2.691623 0. 17 * 319.2105
5301318 2.68172 2.68172 0. 18 * 319.2105
5301319 2.673206 2.673206 0. 19 * 319.2105
*hydro jun diam beta intercept slope jun
5301401 9.924e-3 0.0 1.0 1.0 19
***
=====*$*
*crdno name type
5350000 pr-lp sngljun
*---
*
*crdno from to area floss rloss flag
5350101 530010000 540000000 0.0 0. 0. 100
*
*crdno ctl flowf flowg velj
5350201 0 31.481 31.481 0. * 319.2105
*
=====*$*
***
* Inlet pipe to low pressure compressor
***
*
*crdno name type
5400000 lp-in pipe
*
*crdno no.vols.
5400001 3
*
*crdno area vol.no.
5400101 2.405 2
5400102 5.983 3
*
*crdno length vol.no.
5400301 2.45 2
5400302 2.38 3
*
*crdno v-ang vol.no.
5400601 90.0 3
*
*crdno rough dhy vol.no.
5400801 0.5e-5 1.75 2
5400802 0.5e-5 2.76 3
*
*crdno ff rf jun.no.

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```

5400901  0.  0.      2
*
*crdno  tlpvbf     vol.no.
5401001 10000      3
*
*crdno  jefvcahs   jun.no.
5401101 0000000      1
5401102 0000100      2
*
*crdno  ebt pressure temp qual vol.no.
5401201  0 2586328. 930098. 930098. 1. 0. 1
5401202  0 2586201. 930087. 930087. 1. 0. 2
5401203  0 2587093. 930191. 930191. 1. 0. 3
*
*crdno  i.c.
5401300  0
*
*crdno  flowf flowg velj jun.no.
5401301 31.4988 31.4988  0.  1 * 319.2105
5401302 31.4997 31.4997  0.  2 * 319.2105
*
*crdno  dhy        jun.no
5401401 1.75      1.0 1.0 1.0  2
*
*
*-----*
* Low pressure compressor
*
*-----*
5500000 lpcmpr cprsr
*-----*
*
*crdno  nj
5500001 2
* area      length  volume
5500101 0.4762    4.2    0.0
* azim angle incl angle delta z pvbfe
5500102 0.00     90.0    4.2    00000
* from jun area Kf  Kr fvcchs
5500108 540010000 0.0  0.0  0.0 001000
* to jun area Kf  Kr fvcchs
5500109 560000000 0.0  0.0  0.0 001000
* hyd dia beta y-int slope
5500110 0.0000  0.00  1.00  1.00
5500111 0.0000  0.00  1.00  1.00
* ebt
5500200 3 4.35e6 377.6
* vel/flow liquid vapor int-face
5500201 1  0.0  312.0  0.
5500202 1  0.0  312.0  0.
* id mtr vel trip rvrs
*5500301 0 -1  0 350 0
5500301 0 -1 -1 350 0
* rated vel sp ratio flow sound inertia density
5500302 376.991 1.000 319.21 781.48 2891.44 4.2425
* mot coeff-tf2 coeff-tf0 coeff-tf1 coeff-tf3
5500303 0.0 0.0 0.0 0.0 0.0
* shaft trip
5500309 600 535
*
5500310 0. 1000. -0.00001
*-----*
* performance curves based directly on mit calculations with
* extrapolations to boundary of adjacent curves; pump efficiencies
* performance data tables
*crdno  Rel Spd  nu  *  Speed
5500910 -0.10  3  *  -37.6991
5500911  0.00  4  *   0.0 rad/s
5500912  0.40 11  * 150.7694
5500913  0.50 14  * 188.4955
5500914  0.60 15  * 226.1946
5500915  0.70 16  * 263.8937
5500916  0.80 15  * 301.5928
5500917  0.90 47  * 339.2919
5500918  1.00 35  * 376.9910
5500919  1.10 36  * 414.6901
5500920  1.20  5  *  452.3892
5500921  1.30  5  *  490.0883
5500922  1.40  4  *  527.7874
5500923  1.50  4  *  565.4865
* relative pr eta pump -10% speed
5501001 -0.1000 0.9000 0.0009 *1.0000 0.0010 * extrapolated
5501002  0.0000 0.8500 0.0009 *0.9701 0.8941 * extrapolated
5501003  0.4216 0.6285 0.0009 *0.9619 0.6641 * extrapolated
* relative pr eta pump 0% speed
5501101 -0.1000 0.9300 0.0009
5501102  0.0000 1.0000 0.0009 *1.0000 0.0010 * extrapolated

```

5501103	0.3736	0.7347	0.8448	*0.9701	0.8941	* extrapolated
5501104	0.4216	0.7285	0.6275	*0.9619	0.6641	* extrapolated
* relative pr eta pump 40% speed						
5501201	-0.1000	0.9500	0.0009			
5501202	0.0000	1.1000	0.0009	*****		
5501203	0.3736	0.8171	0.8448	*1.0789	0.8941	
5501204	0.3745	0.8164	0.8436	*1.0779	0.8929	
5501205	0.3753	0.8158	0.8433	*1.0771	0.8925	
5501206	0.3762	0.8149	0.8423	*1.0759	0.8915	
5501207	0.3770	0.8141	0.8410	*1.0749	0.8901	
5501208	0.3919	0.8006	0.8127	*1.0570	0.8601	
5501209	0.4067	0.7868	0.7546	*1.0388	0.7986	
5501210	0.4216	0.7728	0.6275	*1.0204	0.6641	
5501211	0.4826	0.7157	0.1053	*0.9450	0.1115	* extrapolated
* relative pr eta pump 50% speed						
5501301	0.0000	1.3000	0.0009	*****		
5501302	0.3736	0.9769	0.8769	*1.2898	0.9281	* extrapolated
5501303	0.4026	0.9423	0.8752	*1.2442	0.9263	
5501304	0.4106	0.9328	0.8747	*1.2316	0.9258	
5501305	0.4186	0.9232	0.8734	*1.2189	0.9244	
5501306	0.4266	0.9139	0.8717	*1.2066	0.9226	
5501307	0.4346	0.9036	0.8703	*1.1930	0.9211	
5501308	0.4426	0.8940	0.8688	*1.1804	0.9195	
5501309	0.4506	0.8844	0.8657	*1.1677	0.9162	
5501310	0.4586	0.8742	0.8613	*1.1542	0.9116	
5501311	0.4666	0.8644	0.8562	*1.1413	0.9062	
5501312	0.4746	0.8543	0.8499	*1.1279	0.8995	
5501313	0.4826	0.8445	0.8422	*1.1150	0.8914	
5501314	0.5941	0.7087	0.7363	*0.9357	0.7793	* extrapolated
* relative pr eta pump 60% speed						
5501401	0.0000	1.5000	0.0009	*****		
5501402	0.4026	1.1765	0.8643	*1.5533	0.9148	* extrapolated
5501403	0.4613	1.0935	0.8745	*1.4438	0.9255	
5501404	0.4723	1.0779	0.8763	*1.4232	0.9275	
5501405	0.4834	1.0612	0.8765	*1.4011	0.9277	
5501406	0.4945	1.0447	0.8770	*1.3793	0.9282	
5501407	0.5055	1.0292	0.8782	*1.3589	0.9295	
5501408	0.5166	1.0114	0.8778	*1.3354	0.9290	
5501409	0.5277	0.9922	0.8758	*1.3100	0.9269	
5501410	0.5387	0.9745	0.8732	*1.2867	0.9242	
5501411	0.5609	0.9373	0.8642	*1.2376	0.9146	
5501412	0.5719	0.9188	0.8579	*1.2131	0.9080	
5501413	0.5830	0.9003	0.8504	*1.1887	0.9000	
5501414	0.5941	0.8813	0.8428	*1.1636	0.8920	
5501415	0.7124	0.6786	0.7616	*0.8960	0.8061	* extrapolated
* relative pr eta pump 70% speed						
5501501	0.0000	1.7500	0.0009	*****		
5501502	0.4613	1.4193	0.8507	*1.8740	0.9004	* extrapolated
5501503	0.5447	1.2767	0.8723	*1.6857	0.9232	
5501504	0.5587	1.2528	0.8759	*1.6541	0.9270	
5501505	0.5726	1.2245	0.8781	*1.6168	0.9294	
5501506	0.5866	1.1975	0.8785	*1.5811	0.9298	
5501507	0.6006	1.1687	0.8798	*1.5430	0.9312	
5501508	0.6145	1.1412	0.8796	*1.5067	0.9310	
5501509	0.6285	1.1122	0.8778	*1.4684	0.9290	
5501510	0.6425	1.0825	0.8753	*1.4292	0.9264	
5501511	0.6565	1.0521	0.8716	*1.3891	0.9225	
5501512	0.6704	1.0209	0.8684	*1.3479	0.9191	
5501513	0.6844	0.9892	0.8625	*1.3061	0.9128	
5501514	0.6984	0.9564	0.8532	*1.2628	0.9030	
5501515	0.7124	0.9246	0.8413	*1.2208	0.8904	
5501516	0.8358	0.6436	0.7359	*0.8498	0.7789	* extrapolated
* relative pr eta pump 80% speed						
5501601	0.0000	2.1000	0.0009	*****		
5501602	0.5447	1.7424	0.8600	*2.3005	0.9102	* extrapolated
5501603	0.6638	1.4595	0.8764	*1.9270	0.9276	
5501604	0.6810	1.4187	0.8788	*1.8732	0.9301	
5501605	0.6982	1.3781	0.8799	*1.8195	0.9313	
5501606	0.7154	1.3330	0.8805	*1.7600	0.9319	
5501607	0.7326	1.2883	0.8804	*1.7010	0.9318	
5501608	0.7498	1.2389	0.8780	*1.6357	0.9293	
5501609	0.7670	1.1889	0.8745	*1.5697	0.9256	
5501610	0.7842	1.1375	0.8722	*1.5019	0.9231	
5501611	0.8014	1.0851	0.8648	*1.4327	0.9153	
5501612	0.8186	1.0329	0.8541	*1.3638	0.9040	
5501613	0.8358	0.9789	0.8440	*1.2925	0.8933	
5501614	0.9702	0.5565	0.7651	*0.7347	0.8098	* extrapolated
5501615	1.2390	-.2883	0.6073	*0.7347	0.8098	* extrapolated
* relative pr eta pump 90% speed						
5501701	0.0000	2.4896	0.0009			
5501702	0.6900	2.0358	0.8453			
5501703	0.7000	2.0112	0.8489			
5501704	0.7100	1.9859	0.8521			
5501705	0.7200	1.9599	0.8550			
5501706	0.7300	1.9334	0.8577			
5501707	0.7400	1.9065	0.8600			
5501708	0.7500	1.8792	0.8622			
5501709	0.7600	1.8516	0.8643			

5501710	0.7700	1.8239	0.8663
5501711	0.7800	1.7962	0.8683
5501712	0.7900	1.7685	0.8702
5501713	0.8000	1.7409	0.8722
5501714	0.8100	1.7136	0.8744
5501715	0.8200	1.6863	0.8765
5501716	0.8300	1.6585	0.8785
5501717	0.8400	1.6297	0.8800
5501718	0.8500	1.5993	0.8810
5501719	0.8600	1.5671	0.8815
5501720	0.8700	1.5331	0.8816
5501721	0.8800	1.4975	0.8812
5501722	0.8900	1.4607	0.8806
5501723	0.9000	1.4230	0.8795
5501724	0.9100	1.3846	0.8782
5501725	0.9200	1.3459	0.8766
5501726	0.9300	1.3070	0.8747
5501727	0.9400	1.2679	0.8724
5501728	0.9500	1.2286	0.8694
5501729	0.9600	1.1887	0.8655
5501730	0.9700	1.1480	0.8606
5501731	0.9800	1.1061	0.8543
5501732	0.9900	1.0633	0.8467
5501733	1.0000	1.0198	0.8381
5501734	1.0100	0.9761	0.8291
5501735	1.0200	0.9324	0.8199
5501736	1.0300	0.8885	0.8104
5501737	1.0400	0.8446	0.8007
5501738	1.0500	0.8006	0.7908
5501739	1.0600	0.7566	0.7808
5501740	1.0700	0.7125	0.7706
5501741	1.0800	0.6684	0.7604
5501742	1.0900	0.6242	0.7500
5501743	1.1000	0.5801	0.7396
5501744	1.1100	0.5359	0.7292
5501745	1.1200	0.4917	0.7188
5501746	1.1300	0.4476	0.7084
5501747	1.2812	1.6396	0.5571
* relative pr eta pump 100% speed			
5501801	0.0000	2.8896	0.0009
5501802	0.8100	2.4897	0.8507
5501803	0.8200	2.4586	0.8535
5501804	0.8300	2.4266	0.8561
5501805	0.8400	2.3939	0.8584
5501806	0.8500	2.3605	0.8605
5501807	0.8600	2.3264	0.8624
5501808	0.8700	2.2919	0.8642
5501809	0.8800	2.2570	0.8658
5501810	0.8900	2.2217	0.8673
5501811	0.9000	2.1862	0.8688
5501812	0.9100	2.1505	0.8701
5501813	0.9200	2.1147	0.8715
5501814	0.9300	2.0790	0.8728
5501815	0.9400	2.0434	0.8742
5501816	0.9500	2.0080	0.8756
5501817	0.9600	1.9728	0.8771
5501818	0.9700	1.9373	0.8786
5501819	0.9800	1.9003	0.8798
5501820	0.9900	1.8609	0.8808
5501821	1.0000	1.8188	0.8813
5501822	1.0100	1.7743	0.8814
5501823	1.0200	1.7279	0.8810
5501824	1.0300	1.6800	0.8801
5501825	1.0400	1.6310	0.8789
5501826	1.0500	1.5813	0.8775
5501827	1.0600	1.5308	0.8759
5501828	1.0700	1.4796	0.8741
5501829	1.0800	1.4273	0.8721
5501830	1.0900	1.3738	0.8697
5501831	1.1000	1.3187	0.8665
5501832	1.1100	1.2613	0.8618
5501833	1.1200	1.2013	0.8552
5501834	1.1300	1.1387	0.8467
5501835	1.2811	0.1272	0.6554
* relative pr eta pump 110% speed			
5501901	0.0000	3.2896	0.0009
5501902	0.9500	3.0082	0.8731
5501903	0.9600	2.9685	0.8753
5501904	0.9700	2.9277	0.8773
5501905	0.9800	2.8857	0.8790
5501906	0.9900	2.8425	0.8805
5501907	1.0000	2.7983	0.8818
5501908	1.0100	2.7529	0.8829
5501909	1.0200	2.7064	0.8837
5501910	1.0300	2.6589	0.8844
5501911	1.0400	2.6103	0.8848
5501912	1.0500	2.5607	0.8850
5501913	1.0600	2.5100	0.8851

```

5501914 1.0700 2.4584 0.8849
5501915 1.0800 2.4057 0.8846
5501916 1.0900 2.3521 0.8840
5501917 1.1000 2.2975 0.8833
5501918 1.1100 2.2420 0.8824
5501919 1.1200 2.1855 0.8813
5501920 1.1300 2.1280 0.8800
5501921 1.1400 2.0694 0.8785
5501922 1.1500 2.0097 0.8767
5501923 1.1600 1.9488 0.8748
5501924 1.1700 1.8866 0.8726
5501925 1.1800 1.8232 0.8701
5501926 1.1900 1.7586 0.8675
5501927 1.2000 1.6930 0.8646
5501928 1.2100 1.6265 0.8616
5501929 1.2200 1.5590 0.8584
5501930 1.2300 1.4908 0.8550
5501931 1.2400 1.4218 0.8515
5501932 1.2500 1.3522 0.8479
5501933 1.2600 1.2821 0.8442
5501934 1.2700 1.2115 0.8403
5501935 1.2800 1.1406 0.8365
5501936 1.3982 0.2778 0.7859
*
* relative pr eta pump 120% speed
5502001 0.0000 3.5000 0.0009 *****
5502002 0.6000 4.1500 0.2000
5502003 1.0748 3.4847 0.8746 * * extrapolated
5502004 1.3915 1.1814 0.8336 * * extrapolated
5502005 1.4100 0.6000 0.7000
*
* relative pr eta pump 130% speed
5502101 0.0000 4.0000 0.0009 *****
5502102 0.6000 5.0000 0.2000
5502103 1.2241 3.9712 0.8746 * * extrapolated
5502104 1.5319 1.2322 0.8336 * * extrapolated
5502105 1.5500 0.6000 0.7000
*
* relative pr eta pump 140% speed
5502201 0.0000 4.3000 0.0009 *****
5502202 0.6000 5.6000 0.2000
5502203 1.3734 4.4577 0.8746 * * extrapolated
5502204 1.6723 1.2830 0.8336 * * extrapolated
*
* relative pr eta pump 150% speed
5502301 0.0000 4.7000 0.0009 *****
5502302 0.6000 6.0000 0.2000
5502303 1.5227 4.9442 0.8746 * * extrapolated
5502304 1.8127 1.3338 0.8336 * * extrapolated
*
*5500500
*5500501 0.0 376.991
*5500502 1450. 376.991
*-----$
*hydro component name component type
5600000 lpcout snlvol
*-----$
*hydro area length volume
5600101 4.347 2.45 0.0
*
*hydro horz angle vert angle delta z
5600102 0.0 -90.0 -2.45
*
*hydro roughness hyd diam fe
5600103 0.0 0.0 0
*
*hydro ebt pressure tempe
5600200 0 4357726. 1181832. 1181832. 1.
*-----$
*hydro component name component type
5650000 lpc-ic branch
*-----$
* no. juns vel/flow
5650001 2 0
*hydro area length volume
5650101 4.347 2.45 0.0
*
*hydro horz angle vert angle delta z
5650102 0.0 -90.0 -2.45
*
*hydro roughness hyd diam fe
5650103 0.0 2.353 0
*
*hydro ebt pressure tempe
5650200 0 4357863. 1181846. 1181846. 1.
* from to area Kf Kr efvcahs
5651101 560010000 565000000 0.0 0.0 0.0 0000000
5652101 565010000 570000000 0.0 0.0 0.0 0000000

```

```

* velf velg veli
5651201 12.9294 12.9294 0. * 319.2105
5652201 12.92918 12.92918 0. * 319.2105
* hyd dia beta y-int slope
5651110 2.353 1.00 1.00 1.00
5652110 2.353 1.00 1.00 1.00
*
*-----*
***
* 570 Inter-cooler
***
5700000 intcool pipe
*-----*
* no. vols
5700001 20
* vol area
5700101 28.3 20
* length
5700301 0.2365 20
* volume
5700401 0.0 20
* azim angle
5700501 0.0 20
* incl angle
5700601 -90.0 20
* roughness hyd dia
5700801 4.0e-3 9.924e-3 20
* kf kr
5700901 130.0 130.0 19
* pvbfe
5701001 00000 20
* fvcahs
5701101 001000 19
* ebt press temp
5701201 0 4358364. 1152563. 1152563. 1. 0. 1
5701202 0 4356879. 1126299. 1126299. 1. 0. 2
5701203 0 4355428. 1102891. 1102891. 1. 0. 3
5701204 0 4354008. 1082014. 1082014. 1. 0. 4
5701205 0 4352615. 1063381. 1063381. 1. 0. 5
5701206 0 4351246. 1046744. 1046744. 1. 0. 6
5701207 0 4349898. 1031881. 1031881. 1. 0. 7
5701208 0 4348570. 1018596. 1018596. 1. 0. 8
5701209 0 4347258. 1006716. 1006716. 1. 0. 9
5701210 0 4345962. 996090. 996090. 1. 0. 10
5701211 0 4344678. 986582. 986582. 1. 0. 11
5701212 0 4343408. 978072. 978072. 1. 0. 12
5701213 0 4342148. 970453. 970453. 1. 0. 13
5701214 0 4340898. 963630. 963630. 1. 0. 14
5701215 0 4339656. 957520. 957520. 1. 0. 15
5701216 0 4338423. 952047. 952047. 1. 0. 16
5701217 0 4337196. 947144. 947144. 1. 0. 17
5701218 0 4335976. 942751. 942751. 1. 0. 18
5701219 0 4334760. 938816. 938816. 1. 0. 19
5701220 0 4333550. 935291. 935291. 1. 0. 20
* vel/flow
5701300 0
* liquid vapor int-face
5701301 1.936394 1.936394 0. 1 * 319.2105
5701302 1.892748 1.892748 0. 2 * 319.2105
5701303 1.853877 1.853877 0. 3 * 319.2105
5701304 1.81924 1.81924 0. 4 * 319.2105
5701305 1.78836 1.78836 0. 5 * 319.2105
5701306 1.76082 1.76082 0. 6 * 319.2105
5701307 1.736254 1.736254 0. 7 * 319.2105
5701308 1.71433 1.71433 0. 8 * 319.2105
5701309 1.694765 1.694765 0. 9 * 319.2105
5701310 1.6773 1.6773 0. 10 * 319.2105
5701311 1.661713 1.661713 0. 11 * 319.2105
5701312 1.6478 1.6478 0. 12 * 319.2105
5701313 1.635383 1.635383 0. 13 * 319.2105
5701314 1.624304 1.624304 0. 14 * 319.2105
5701315 1.614422 1.614422 0. 15 * 319.2105
5701316 1.60561 1.60561 0. 16 * 319.2105
5701317 1.59776 1.59776 0. 17 * 319.2105
5701318 1.590767 1.590767 0. 18 * 319.2105
5701319 1.584544 1.584544 0. 19 * 319.2105
*hydro jun diam beta intercept slope jun
5701401 9.924e-3 0.0 1.0 1.0 19
***
*
***
* 572 Junction - IC to HPC
*
*crdno name type
5720000 ic-hpcj sngljun
*
*crdno from to area floss rloss flag
5720101 570010000 575000000 0.0 0.0 0.0 00

```

```

*
*crdno ctl flowf flowg velj
5720201 0 89.372 89.372 0. * 319.2105
*
*
*
*-----*
***
* 575 Inlet pipe to high pressure compressor
***
*
*crdno name type
5750000 ic-hpc pipe
*
*crdno no.vols.
5750001 3
*
*crdno area vol.no.
5750101 0.5 3
*
*crdno length vol.no.
5750301 3.21 3
*
*crdno v-ang vol.no.
5750601 90.0 3
*
*crdno rough dhy vol.no.
5750801 0.5e-5 0.7979 3
*
*crdno ff rf jun.no.
5750901 0. 0. 2
*
*crdno tlpvbf vol.no.
5751001 10000 3
*
*crdno jefvcahs jun.no.
5751101 0000000 2
*
*crdno ebt pressure temp qual vol.no.
5751201 0 4304494. 932850. 932850. 1. 0. 1
5751202 0 4303151. 932810. 932810. 1. 0. 2
5751203 0 4301978. 932785. 932785. 1. 0. 3
*
*crdno i.c.
5751300 0
*
*crdno flowf flowg velj jun.no.
5751301 89.7534 89.7534 0. 1 * 319.2105
5751302 89.7788 89.7788 0. 2 * 319.2105
*
*crdno dhy jun.no
5751401 0.7979 1.0 1.0 1.0 2
*
*
*-----*
* High pressure compressor
*
*-----*
5800000 hpcmpr cprssr
*-----*
*
*crdno nj
5800001 2
* area length volume
*3500101 0.50 2.35 0.0
5800101 0.4762 4.2 0.0
* azim angle incl angle delta z pvbfe
5800102 0.00 90.0 4.2 00000
* from jun area Kf Kr fvcchs
5800108 575010000 0.0 0.0 0.0 001000
* to jun area Kf Kr fvcchs
5800109 585000000 0.0 0.0 0.0 001000
* hyd dia beta y-int slope
5800110 0.0000 0.00 1.00 1.00
5800111 0.0000 0.00 1.00 1.00
* ebt
5800200 3 7.21e6 378.05
* vel/flow liquid vapor int-face
5800201 1 0.0 312.0 0.
5800202 1 0.0 312.0 0.
* id mtr vel trip rvrs
*5800301 0 -1 0 350 0
5800301 0 -1 -1 350 0
* rated vel sp ratio flow sound inertia density
5800302 376.991 1.000 319.21 692.04 2891.44 7.1263
* mot coeff-tf2 coeff-tf0 coeff-tf1 coeff-tf3
5800303 0.0 0.0 0.0 0.0 0.0

```

```

* shaft trip
5800309 600 535
*
5800310 0. 1000. -0.00001
*-----$
* performance curves based directly on mit calculations with
* extrapolations to boundary of adjacent curves; pump efficiencies
* performance data tables
*crdno Rel Spd nu * Speed
5800910 -0.10 3 * -37.6991
5800911 0.00 4 * 0.0 rad/s
5800912 0.40 11 * 150.7694
5800913 0.50 14 * 188.4955
5800914 0.60 15 * 226.1946
5800915 0.70 16 * 263.8937
5800916 0.80 15 * 301.5928
5800917 0.90 47 * 339.2919
5800918 1.00 35 * 376.9910
5800919 1.10 36 * 414.6901
5800920 1.20 3 * 452.3892
5800921 1.30 3 * 490.0883
5800922 1.40 3 * 527.7874
5800923 1.50 3 * 565.4865
* relative pr eta pump -10% speed
5801001 -0.1000 0.9000 0.0009 *1.0000 0.0010 * extrapolated
5801002 0.0000 0.8500 0.0009 *0.9701 0.8941 * extrapolated
5801003 0.4216 0.6285 0.0009 *0.9619 0.6641 * extrapolated
* relative pr eta pump 0% speed
5801101 -0.1000 0.9300 0.0009
5801102 0.0000 1.0000 0.0009 *1.0000 0.0010 * extrapolated
5801103 0.3736 0.7347 0.8448 *0.9701 0.8941 * extrapolated
5801104 0.4216 0.7285 0.6275 *0.9619 0.6641 * extrapolated
* relative pr eta pump 40% speed
5801201 -0.1000 0.9500 0.0009
5801202 0.0000 1.1000 0.0009 *****
5801203 0.3736 0.8171 0.8448 *1.0789 0.8941
5801204 0.3745 0.8164 0.8436 *1.0779 0.8929
5801205 0.3753 0.8158 0.8433 *1.0771 0.8925
5801206 0.3762 0.8149 0.8423 *1.0759 0.8915
5801207 0.3770 0.8141 0.8410 *1.0749 0.8901
5801208 0.3919 0.8006 0.8127 *1.0570 0.8601
5801209 0.4067 0.7868 0.7546 *1.0388 0.7986
5801210 0.4216 0.7728 0.6275 *1.0204 0.6641
5801211 0.4826 0.7157 0.1053 *0.9450 0.1115 * extrapolated
* relative pr eta pump 50% speed
5801301 0.0000 1.3000 0.0009 *****
5801302 0.3736 0.9769 0.8769 *1.2898 0.9281 * extrapolated
5801303 0.4026 0.9423 0.8752 *1.2442 0.9263
5801304 0.4106 0.9328 0.8747 *1.2316 0.9258
5801305 0.4186 0.9232 0.8734 *1.2189 0.9244
5801306 0.4266 0.9139 0.8717 *1.2066 0.9226
5801307 0.4346 0.9036 0.8703 *1.1930 0.9211
5801308 0.4426 0.8940 0.8688 *1.1804 0.9195
5801309 0.4506 0.8844 0.8657 *1.1677 0.9162
5801310 0.4586 0.8742 0.8613 *1.1542 0.9116
5801311 0.4666 0.8644 0.8562 *1.1413 0.9062
5801312 0.4746 0.8543 0.8499 *1.1279 0.8995
5801313 0.4826 0.8445 0.8422 *1.1150 0.8914
5801314 0.5941 0.7087 0.7363 *0.9357 0.7793 * extrapolated
* relative pr eta pump 60% speed
5801401 0.0000 1.5000 0.0009 *****
5801402 0.4026 1.1765 0.8643 *1.5533 0.9148 * extrapolated
5801403 0.4613 1.0935 0.8745 *1.4438 0.9255
5801404 0.4723 1.0779 0.8763 *1.4232 0.9275
5801405 0.4834 1.0612 0.8765 *1.4011 0.9277
5801406 0.4945 1.0447 0.8770 *1.3793 0.9282
5801407 0.5055 1.0292 0.8782 *1.3589 0.9295
5801408 0.5166 1.0114 0.8778 *1.3354 0.9290
5801409 0.5277 0.9922 0.8758 *1.3100 0.9269
5801410 0.5387 0.9745 0.8732 *1.2867 0.9242
5801411 0.5609 0.9373 0.8642 *1.2376 0.9146
5801412 0.5719 0.9188 0.8579 *1.2131 0.9080
5801413 0.5830 0.9003 0.8504 *1.1887 0.9000
5801414 0.5941 0.8813 0.8428 *1.1636 0.8920
5801415 0.7124 0.6786 0.7616 *0.8960 0.8061 * extrapolated
* relative pr eta pump 70% speed
5801501 0.0000 1.7500 0.0009 *****
5801502 0.4613 1.4193 0.8507 *1.8740 0.9004 * extrapolated
5801503 0.5447 1.2767 0.8723 *1.6857 0.9232
5801504 0.5587 1.2528 0.8759 *1.6541 0.9270
5801505 0.5726 1.2245 0.8781 *1.6168 0.9294
5801506 0.5866 1.1975 0.8785 *1.5811 0.9298
5801507 0.6006 1.1687 0.8798 *1.5430 0.9312
5801508 0.6145 1.1412 0.8796 *1.5067 0.9310
5801509 0.6285 1.1122 0.8778 *1.4684 0.9290
5801510 0.6425 1.0825 0.8753 *1.4292 0.9264
5801511 0.6565 1.0521 0.8716 *1.3891 0.9225
5801512 0.6704 1.0209 0.8684 *1.3479 0.9191

```

5801513	0.6844	0.9892	0.8625	*1.3061	0.9128
5801514	0.6984	0.9564	0.8532	*1.2628	0.9030
5801515	0.7124	0.9246	0.8413	*1.2208	0.8904
5801516	0.8358	0.6436	0.7359	*0.8498	0.7789 * extrapolated
* relative pr eta pump 80% speed					
5801601	0.0000	2.1000	0.0009	*****	
5801602	0.5447	1.7424	0.8600	*2.3005	0.9102 * extrapolated
5801603	0.6638	1.4595	0.8764	*1.9270	0.9276
5801604	0.6810	1.4187	0.8788	*1.8732	0.9301
5801605	0.6982	1.3781	0.8799	*1.8195	0.9313
5801606	0.7154	1.3330	0.8805	*1.7600	0.9319
5801607	0.7326	1.2883	0.8804	*1.7010	0.9318
5801608	0.7498	1.2389	0.8780	*1.6357	0.9293
5801609	0.7670	1.1889	0.8745	*1.5697	0.9256
5801610	0.7842	1.1375	0.8722	*1.5019	0.9231
5801611	0.8014	1.0851	0.8648	*1.4327	0.9153
5801612	0.8186	1.0329	0.8541	*1.3638	0.9040
5801613	0.8358	0.9789	0.8440	*1.2925	0.8933
5801614	0.9702	0.5565	0.7651	*0.7347	0.8098 * extrapolated
5801615	1.2390	-2.2883	0.6073	*0.7347	0.8098 * extrapolated
* relative pr eta pump 90% speed					
5801701	0.0000	2.5000	0.0009		
5801702	0.6800	2.0462	0.8453		
5801703	0.6900	2.0216	0.8489		
5801704	0.7000	1.9963	0.8521		
5801705	0.7100	1.9703	0.8550		
5801706	0.7200	1.9438	0.8577		
5801707	0.7300	1.9169	0.8600		
5801708	0.7400	1.8896	0.8622		
5801709	0.7500	1.8620	0.8643		
5801710	0.7600	1.8343	0.8663		
5801711	0.7700	1.8066	0.8683		
5801712	0.7800	1.7789	0.8702		
5801713	0.7900	1.7513	0.8722		
5801714	0.8000	1.7240	0.8744		
5801715	0.8100	1.6967	0.8765		
5801716	0.8200	1.6689	0.8785		
5801717	0.8300	1.6401	0.8800		
5801718	0.8400	1.6097	0.8810		
5801719	0.8500	1.5775	0.8815		
5801720	0.8600	1.5435	0.8816		
5801721	0.8700	1.5079	0.8812		
5801722	0.8800	1.4711	0.8806		
5801723	0.8900	1.4334	0.8795		
5801724	0.9000	1.3950	0.8782		
5801725	0.9100	1.3563	0.8766		
5801726	0.9200	1.3174	0.8747		
5801727	0.9300	1.2783	0.8724		
5801728	0.9400	1.2390	0.8694		
5801729	0.9500	1.1991	0.8655		
5801730	0.9600	1.1584	0.8606		
5801731	0.9700	1.1165	0.8543		
5801732	0.9800	1.0737	0.8467		
5801733	0.9900	1.0302	0.8381		
5801734	1.0000	0.9865	0.8291		
5801735	1.0100	0.9428	0.8199		
5801736	1.0200	0.8989	0.8104		
5801737	1.0300	0.8550	0.8007		
5801738	1.0400	0.8110	0.7908		
5801739	1.0500	0.7670	0.7808		
5801740	1.0600	0.7229	0.7706		
5801741	1.0700	0.6788	0.7604		
5801742	1.0800	0.6346	0.7500		
5801743	1.0900	0.5905	0.7396		
5801744	1.1000	0.5463	0.7292		
5801745	1.1100	0.5021	0.7188		
5801746	1.1200	0.4580	0.7084		
5801747	1.2712	1.6500	0.5571		
* relative pr eta pump 100% speed					
5801801	0.0000	2.9000	0.0009		
5801802	0.8000	2.5001	0.8507		
5801803	0.8100	2.4690	0.8535		
5801804	0.8200	2.4370	0.8561		
5801805	0.8300	2.4043	0.8584		
5801806	0.8400	2.3709	0.8605		
5801807	0.8500	2.3368	0.8624		
5801808	0.8600	2.3023	0.8642		
5801809	0.8700	2.2674	0.8658		
5801810	0.8800	2.2321	0.8673		
5801811	0.8900	2.1966	0.8688		
5801812	0.9000	2.1609	0.8701		
5801813	0.9100	2.1251	0.8715		
5801814	0.9200	2.0894	0.8728		
5801815	0.9300	2.0538	0.8742		
5801816	0.9400	2.0184	0.8756		
5801817	0.9500	1.9832	0.8771		
5801818	0.9600	1.9477	0.8786		
5801819	0.9700	1.9107	0.8798		


```

5801820 0.9800 1.8713 0.8808
5801821 0.9900 1.8292 0.8813
5801822 1.0000 1.7847 0.8814
5801823 1.0100 1.7383 0.8810
5801824 1.0200 1.6904 0.8801
5801825 1.0300 1.6414 0.8789
5801826 1.0400 1.5917 0.8775
5801827 1.0500 1.5412 0.8759
5801828 1.0600 1.4900 0.8741
5801829 1.0700 1.4377 0.8721
5801830 1.0800 1.3842 0.8697
5801831 1.0900 1.3291 0.8665
5801832 1.1000 1.2717 0.8618
5801833 1.1100 1.2117 0.8552
5801834 1.1200 1.1491 0.8467
5801835 1.2711 0.1376 0.6554
*   relative pr eta pump 110% speed
5801901 0.0000 3.2896 0.0009
5801902 0.9400 3.0186 0.8731
5801903 0.9500 2.9789 0.8753
5801904 0.9600 2.9381 0.8773
5801905 0.9700 2.8961 0.8790
5801906 0.9800 2.8529 0.8805
5801907 0.9900 2.8087 0.8818
5801908 1.0000 2.7633 0.8829
5801909 1.0100 2.7168 0.8837
5801910 1.0200 2.6693 0.8844
5801911 1.0300 2.6207 0.8848
5801912 1.0400 2.5711 0.8850
5801913 1.0500 2.5204 0.8851
5801914 1.0600 2.4688 0.8849
5801915 1.0700 2.4161 0.8846
5801916 1.0800 2.3625 0.8840
5801917 1.0900 2.3079 0.8833
5801918 1.1000 2.2524 0.8824
5801919 1.1100 2.1959 0.8813
5801920 1.1200 2.1384 0.8800
5801921 1.1300 2.0798 0.8785
5801922 1.1400 2.0201 0.8767
5801923 1.1500 1.9592 0.8748
5801924 1.1600 1.8970 0.8726
5801925 1.1700 1.8336 0.8701
5801926 1.1800 1.7690 0.8675
5801927 1.1900 1.7034 0.8646
5801928 1.2000 1.6369 0.8616
5801929 1.2100 1.5694 0.8584
5801930 1.2200 1.5012 0.8550
5801931 1.2300 1.4322 0.8515
5801932 1.2400 1.3626 0.8479
5801933 1.2500 1.2925 0.8442
5801934 1.2600 1.2219 0.8403
5801935 1.2700 1.1510 0.8365
5801936 1.3882 0.2882 0.7859
*
*   relative pr eta pump 120% speed
5802001 0.0000 3.5000 0.0009 *****
5802002 1.0748 3.4847 0.8746 * * extrapolated
5802003 1.3915 1.1814 0.8336 * * extrapolated
*
*   relative pr eta pump 130% speed
5802101 0.0000 4.0000 0.0009 *****
5802102 1.2241 3.9712 0.8746 * * extrapolated
5802103 1.5319 1.2322 0.8336 * * extrapolated
*
*   relative pr eta pump 140% speed
5802201 0.0000 4.3000 0.0009 *****
5802202 1.3734 4.4577 0.8746 * * extrapolated
5802203 1.6723 1.2830 0.8336 * * extrapolated
*
*   relative pr eta pump 150% speed
5802301 0.0000 4.7000 0.0009 *****
5802302 1.5227 4.9442 0.8746 * * extrapolated
5802303 1.8127 1.3338 0.8336 * * extrapolated
*
*5800500
*5800501 0.0 376.991
*5800502 1450. 376.991
*-----$
*hydro      component name component type
5850000      hpout      snglvol
*-----$
*hydro      area      length      volume
5850101      0.5      1.0      0.0
*
*hydro      horz angle      vert angle      delta z
5850102      0.0      0.0      0.0
*
*hydro      roughness      hyd diam      fe

```

```

5850103 0.0 0.0 0
*
*hydro ebt pressure tempe
5850200 0 7210130. 1173657. 1173657. 1.
*-----$
*hydro component name component type
5870000 hp-rc branch
*-----$
* no. juns vel/flow
5870001 2 0
*hydro area length volume
5870101 0.5 1.0 0.0
*
*hydro horz angle vert angle delta z
5870102 0.0 0.0 0.0
*
*hydro roughness hyd diam fe
5870103 0.0 0.7979 0
*
*hydro ebt pressure tempe
5870200 0 7209954. 1173663. 1173663. 1.
* from to area Kf Kr efvcahs
5871101 585010000 587000000 0.5 0.0 0.0 0000000
5872101 587010000 590000000 0.0 0.0 0.0 0000000
* velf velg veli
5871201 67.6061 67.6061 0. * 319.2105
5872201 67.6074 67.6074 0. * 319.2104
* hyd dia beta y-int slope
5871110 0.7979 1.00 1.00 1.00
5872110 0.7979 1.00 1.00 1.00
*
*-----$
5900000 rc-hp pipe
*-----*
* no. vols
5900001 30
* vol area
5900101 7.32 30
* length
5900301 0.09384 30
* volume
5900401 0.0 30
* azim angle
5900501 0.0 30
* incl angle
5900601 90.0 30
* roughness hyd dia
5900801 1.5-4 1.067e-3 30
* kf kr
5900901 14.0 14.0 29
* pvbfe
5901001 00000 30
* fvcchs
5901101 001000 29
* ebt
5901201 0 7231182. 1212588. 1212588. 1. 0. 1
5901202 0 7229406. 1250813. 1250813. 1. 0. 2
5901203 0 7227566. 1289093. 1289093. 1. 0. 3
5901204 0 7225664. 1327414. 1327414. 1. 0. 4
5901205 0 7223700. 1365766. 1365766. 1. 0. 5
5901206 0 7221672. 1404137. 1404137. 1. 0. 6
5901207 0 7219580. 1442517. 1442517. 1. 0. 7
5901208 0 7217424. 1480896. 1480896. 1. 0. 8
5901209 0 7215203. 1519265. 1519265. 1. 0. 9
5901210 0 7212918. 1557615. 1557615. 1. 0. 10
5901211 0 7210568. 1595938. 1595938. 1. 0. 11
5901212 0 7208154. 1634226. 1634226. 1. 0. 12
5901213 0 7205674. 1672471. 1672471. 1. 0. 13
5901214 0 7203128. 1710667. 1710667. 1. 0. 14
5901215 0 7200516. 1748806. 1748806. 1. 0. 15
5901216 0 7197838. 1786883. 1786883. 1. 0. 16
5901217 0 7195095. 1824891. 1824891. 1. 0. 17
5901218 0 7192285. 1862826. 1862826. 1. 0. 18
5901219 0 7189408. 1900682. 1900682. 1. 0. 19
5901220 0 7186466. 1938455. 1938455. 1. 0. 20
5901221 0 7183456. 1976141. 1976141. 1. 0. 21
5901222 0 7180379. 2013735. 2013735. 1. 0. 22
5901223 0 7177236. 2051233. 2051233. 1. 0. 23
5901224 0 7174025. 2088632. 2088632. 1. 0. 24
5901225 0 7170748. 2125927. 2125927. 1. 0. 25
5901226 0 7167402. 2163116. 2163116. 1. 0. 26
5901227 0 7163990. 2200194. 2200194. 1. 0. 27
5901228 0 7160510. 2237160. 2237160. 1. 0. 28
5901229 0 7156964. 2274011. 2274011. 1. 0. 29
5901230 0 7153350. 2310746. 2310746. 1. 0. 30
* vel/flow
5901300 0
* liquid vapor int-face

```

```

5901301 4.76433 4.76433 0. 1 * 319.2104
5901302 4.91561 4.91561 0. 2 * 319.2104
5901303 5.06717 5.06717 0. 3 * 319.2104
5901304 5.21897 5.21897 0. 4 * 319.2104
5901305 5.37095 5.37095 0. 5 * 319.2104
5901306 5.52307 5.52307 0. 6 * 319.2104
5901307 5.6753 5.6753 0. 7 * 319.2105
5901308 5.82761 5.82761 0. 8 * 319.2105
5901309 5.97995 5.97995 0. 9 * 319.2105
5901310 6.1323 6.1323 0. 10 * 319.2105
5901311 6.28462 6.28462 0. 11 * 319.2105
5901312 6.4369 6.4369 0. 12 * 319.2105
5901313 6.58909 6.58909 0. 13 * 319.2105
5901314 6.74117 6.74117 0. 14 * 319.2105
5901315 6.89313 6.89313 0. 15 * 319.2105
5901316 7.04494 7.04494 0. 16 * 319.2105
5901317 7.19658 7.19658 0. 17 * 319.2105
5901318 7.34803 7.34803 0. 18 * 319.2105
5901319 7.49927 7.49927 0. 19 * 319.2105
5901320 7.6503 7.6503 0. 20 * 319.2105
5901321 7.80109 7.80109 0. 21 * 319.2105
5901322 7.95163 7.95163 0. 22 * 319.2105
5901323 8.10192 8.10192 0. 23 * 319.2105
5901324 8.25193 8.25193 0. 24 * 319.2105
5901325 8.40165 8.40165 0. 25 * 319.2105
5901326 8.55108 8.55108 0. 26 * 319.2105
5901327 8.7002 8.7002 0. 27 * 319.2105
5901328 8.84901 8.84901 0. 28 * 319.2105
5901329 8.9975 8.9975 0. 29 * 319.2105
*hydro jun diam beta intercept slope jun
5901401 1.067e-3 0.0 1.0 1.0 29
*
** Name Valve
5910000 bypass tmdppjun
* from to area j-flag
5910101 590010000 592000000 0.00 0000000
* cntrl trp
5910200 1 1005
*
5910201 -0.1 0. 0. 0.
5910202 0. 0. 10. 0.
*
-----
*crdno name type
5920000 cprbp2 tmdpv01
*
*crdno area lngth vol h-a v-ang delz rgh dhy pvbfe
5920101 78. .9104 0 0 0. .0 0 1.5 00010
*
*crdno ebt
5920200 3
*crdno time press temp
5920201 0.0 3e5 740.
*
** Name Valve
5930000 RC_Clg valve
* from to area kforw kbackw j-flag
5930101 590010000 595000000 0.00 0. 0. 0000000
* cntrl w/v.liq w/v.vap w/v.int
5930201 1 0. 319.2105 0.0
* valve-type
5930300 trpvlv
* trip# w/v.liq w/v.vap w/v.int
5930301 1004
*
*-----$
*crdno name type
5950000 rcoutj branch
5950001 1 0
5950101 0.5 2.8152 0.0
5950102 0.0 -90.0 -2.8152
5950103 0.0 0.7979 11000
5950200 0 7109896. 2307731. 2307731. 1.
*crdno from to area floss rloss flag
*5951101 590010000 595000000 0.0 0.0 0.0 000000
5951101 595010000 597000000 0.0 0.0 0.0 000000
*crdno flowf flowg velj
*5951201 133.8927 133.8927 0. * 319.2105
5951201 134.1854 134.1854 0. * 319.2105
*
*-----$
*
*
***
* 597 Hot Duct volume
***
*
*crdno name type

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```

5970000  cldduct  pipe
*
*crdno no.vols.
5970001  4
*
*crdno area      vol.no.
5970101  1.885      4
*
*crdno length    vol.no.
5970301  1.85         4
*
*crdno v-ang     vol.no.
5970601  0.0          4
*
*crdno rough dhy  vol.no.
5970801  0.  0.6      4
*
*crdno  ff  rf    jun.no.
5970901  0.  0.        3
*
*crdno tlpvbf     vol.no.
5971001  10010        4
*
*crdno jefvcahs   jun.no.
5971101  0000000     3
*
*crdno  ebt pressure temp qual vol.no.
5971201  0 7149064. 2310600. 2310600. 1. 0. 1
5971202  0 7149072. 2310600. 2310600. 1. 0. 2
5971203  0 7149072. 2310600. 2310600. 1. 0. 3
5971204  0 7149072. 2310600. 2310600. 1. 0. 4
*
*crdno i.c.
5971300  0
*
*crdno flowf flowg  velj  jun.no.
5971301  35.525  35.525  0.  1 * 319.2105
5971302  35.525  35.525  0.  2 * 319.2105
5971303  35.525  35.525  0.  3 * 319.2105
*
*crdno dhy      jun.no
5971401  0.6  1.0  1.0  1.0  3
*
*
*-----*
*** Bypass Line
*
*-----**
*
4040000  bypvo21  branch
4040001  1  0
4040101  0.1039  9.144  0.0
4040102  0.0  0.0  0.0
4040103  3.048-7  0.0  11000
4040200  0  7231534.  1175566.  1175566.  1.
4041101  587010002  404010001  0.0  0.0  0.0  000000
4041110  0.0  0.0  1.0  1.0
4041201  -6.90005-7 -6.90005-7  0.  * -6.76943-7
*
*
4050000  bypsv12  valve
4050101  404010002  406010001  0.1039
4050102  0.5  0.5  000100
4050103  1.0  1.0  1.0
4050201  1  0.  0.  0.  * 0.
4050300  mtrv1v
4050301  481  482  1.0
4050302  0.0  0
*
*
4060000  bypv122  branch
4060001  1  0
4060101  0.1039  9.144  0.0
4060102  0.0  90.0  4.2
4060103  3.048-7  0.0  11000
4060200  0  3049666.  2494429.  2494429.  1.
4061101  406010002  515010001  0.0  0.0  0.0  000000
4061110  0.0  0.0  1.0  1.0
4061201  -1.244698-9 -1.244698-9  0.  * -2.31131-10
*
*
*-----*
****
*
*** Source of cooling water for precooler

```

```

*
*-----**
* 131 Water Source
*
*crdno  name      type
1310000  h2_cd      tmpdpvol
*
*crdno  area  lngth  vol  h-a  v-ang  delz  rgh  dhy  pvbfe
1310101  78.  .9104  0  0  0.  .0  0  1.5  00010
*
*crdno  ebt
1310200  3
*crdno  time  press  temp
1310201  0.0  0.84e6  293.15
*
*
*---
*crdno  name      type
1320000  hecdj  snljun
*
*crdno  from  to  area  floss  rloss  flag
1320101  131000000  133000000  0.0  0.  0.  100
*
*crdno  ctl  flowf  flowg  velj
1320201  0  1.490186  1.520952  0. * 1253.5
*
*-----*
1330000  prech2o  pipe
*-----*
*  no. vols
1330001  20
*  vol area
1330101  0.8423  20
*  length
1330301  0.2365  20
*  volume
1330401  0.0  20
*  azim angle
1330501  0.0  20
*  incl angle
1330601  90.0  20
*  roughness hyd dia
1330801  0.0  2.0e-3  20
*  kf  kr
1330901  13.7  13.7  19
*  pvbfe
1331001  00000  20
*  fvcahs
1331101  001000  19
*  ebt  press  temp
1331201  0  834479.  84988.  2576484.  0.  0.  1
1331202  0  811195.  86349.6  2575659.  0.  0.  2
1331203  0  787915.  87917.5  2574782.  0.  0.  3
1331204  0  764650.  89721.8  2573852.  0.  0.  4
1331205  0  741402.  91796.9  2572900.  0.  0.  5
1331206  0  718173.  94182.4  2571848.  0.  0.  6
1331207  0  694965.  96923.8  2570730.  0.  0.  7
1331208  0  671782.  100073.6  2569583.  0.  0.  8
1331209  0  648627.  103692.4  2568406.  0.  0.  9
1331210  0  625502.  107850.  2567196.  0.  0.  10
1331211  0  602412.  112627.  2565952.  0.  0.  11
1331212  0  579360.  118117.  2564672.  0.  0.  12
1331213  0  556350.  124428.4  2563352.  0.  0.  13
1331214  0  533387.  131686.8  2561992.  0.  0.  14
1331215  0  510475.  140038.7  2560586.  0.  0.  15
1331216  0  487618.  149655.  2559134.  0.  0.  16
1331217  0  464821.  160735.3  2557629.  0.  0.  17
1331218  0  442088.  173512.7  2556068.  0.  0.  18
1331219  0  419421.  188262.  2554324.  0.  0.  19
1331220  0  396824.  205304.8  2552454.  0.  0.  20
*  vel/flow
1331300  0
*  liquid vapor  int-face
1331301  1.490278  1.538892  0.  1  * 1253.5
1331302  1.490396  1.559857  0.  2  * 1253.5
1331303  1.490533  1.58196  0.  3  * 1253.5
1331304  1.49069  1.60508  0.  4  * 1253.5
1331305  1.490873  1.62915  0.  5  * 1253.5
1331306  1.491085  1.654127  0.  6  * 1253.5
1331307  1.491332  1.679986  0.  7  * 1253.5
1331308  1.491623  1.706704  0.  8  * 1253.5
1331309  1.491964  1.734265  0.  9  * 1253.5
1331310  1.492368  1.762648  0.  10  * 1253.5
1331311  1.492847  1.791832  0.  11  * 1253.5
1331312  1.49342  1.821788  0.  12  * 1253.5
1331313  1.494103  1.85248  0.  13  * 1253.5
1331314  1.494926  1.883866  0.  14  * 1253.5
1331315  1.49592  1.915887  0.  15  * 1253.5

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1331316 1.497126 1.92571 0. 16 * 1253.5
1331317 1.498594 1.92763 0. 17 * 1253.5
1331318 1.50039 1.929976 0. 18 * 1253.5
1331319 1.502596 1.93286 0. 19 * 1253.5
*hydro jun diam beta intercept slope jun
1331401 2.0e-3 0.0 1.0 1.0 19
*-----$
*
***
* 134 Junction - cooling outlet
*
1340000 coreij tmdpjun
*crdno from to area jefvcahs
1340101 133010000 135000000 0.0 000000
1340200 1
1340201 0.0 1.2535e3 0.0 0.0
*
*
*
* 135 Water Sink
*
*crdno name type
1350000 hi_cold tmdpvol
*
*crdno area lngth vol h-a v-ang delz rgh dhy pvbfe
1350101 78. .9104 0 0 0. .0 0 1.5 00010
*
*crdno ebt
1350200 3
*crdno time press temp
1350201 0.0 0.54e6 325.15
*
*
****
*
*** Source of cooling water for intercooler
*
*
* 141 Water Source
*
*crdno name type
1410000 h2c_cd tmdpvol
*
*crdno area lngth vol h-a v-ang delz rgh dhy pvbfe
1410101 78. .9104 0 0 0. .0 0 1.5 00010
*
*crdno ebt
1410200 3
*crdno time press temp
1410201 0.0 0.84e6 293.15
*
*
*
*
*crdno name type
1420000 hcdj engljun
*
*crdno from to area floss rloss flag
1420101 141000000 143000000 0.0 0. 0. 100
*
*crdno ctl flowf flowg velj
1420201 0 1.62224 1.65259 0. * 985.
*
*-----*
1430000 intch2o pipe
*-----*
*
* no. vols
1430001 20
* vol area
1430101 0.608 20
* length
1430301 0.2365 20
* volume
1430401 0.0 20
* azim angle
1430501 0.0 20
* incl angle
1430601 90.0 20
* roughness hyd dia
1430801 0.0 2.0e-3 20
* kf kr
1430901 12. 12. 19
* pvbfe
1431001 00000 20
* fvcchs
1431101 001000 19
* ebt press temp
1431201 0 833749. 85647.2 2576458. 0. 0. 1
1431202 0 809012. 87706.5 2575581. 0. 0. 2

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1431203 0 784296. 90010.2 2574638. 0. 0. 3
1431204 0 759605. 92586.7 2573647. 0. 0. 4
1431205 0 734941. 95467.7 2572631. 0. 0. 5
1431206 0 710307. 98689. 2571472. 0. 0. 6
1431207 0 685704. 102290.8 2570276. 0. 0. 7
1431208 0 661137. 106318. 2569046. 0. 0. 8
1431209 0 636608. 110821.3 2567782. 0. 0. 9
1431210 0 612120. 115857.5 2566480. 0. 0. 10
1431211 0 587677. 121490.7 2565138. 0. 0. 11
1431212 0 563283. 127793.2 2563754. 0. 0. 12
1431213 0 538940. 134846.4 2562325. 0. 0. 13
1431214 0 514652. 142742.6 2560846. 0. 0. 14
1431215 0 490423. 151586. 2559314. 0. 0. 15
1431216 0 466255. 161494.7 2557725. 0. 0. 16
1431217 0 442152. 172602.3 2556073. 0. 0. 17
1431218 0 418115.5 185061.3 2554218. 0. 0. 18
1431219 0 394148. 199045.3 2552214. 0. 0. 19
1431220 0 370250. 214750. 2550009. 0. 0. 20
* vel/flow
1431300 0
* liquid vapor int-face
1431301 1.622396 1.67498 0. 1 * 985.
1431302 1.622586 1.69937 0. 2 * 985.
1431303 1.6228 1.725116 0. 3 * 985.
1431304 1.623046 1.752073 0. 4 * 985.
1431305 1.623326 1.78016 0. 5 * 985.
1431306 1.623645 1.809332 0. 6 * 985.
1431307 1.624012 1.839554 0. 7 * 985.
1431308 1.624434 1.8708 0. 8 * 985.
1431309 1.62492 1.903052 0. 9 * 985.
1431310 1.625485 1.93628 0. 10 * 985.
1431311 1.62614 1.970453 0. 11 * 985.
1431312 1.626903 2.00553 0. 12 * 985.
1431313 1.627794 2.04146 0. 13 * 985.
1431314 1.628838 2.07817 0. 14 * 985.
1431315 1.630063 2.09947 0. 15 * 985.
1431316 1.631506 2.101357 0. 16 * 985.
1431317 1.633208 2.103583 0. 17 * 985.
1431318 1.635222 2.106216 0. 18 * 985.
1431319 1.63761 2.10934 0. 19 * 985.
*hydro jun diam beta intercept slope jun
1431401 2.0e-3 0.0 1.0 1.0 19
*-----$
*
***
* 144 Junction - cooling outlet
*
1440000 coreij tmdpjun
*crdno from to area jefvcahs
1440101 143010000 145000000 0.0 000000
1440200 1
1440201 0.0 0.985e3 0.0 0.0
*
*
* 145 Water Sink
*
*crdno name type
1450000 hi_cold tmdpvol
*
*crdno area lngth vol h-a v-ang delz rgh dhy pvbfe
1450101 78. .9104 0 0 0. .0 0 1.5 00010
*
*crdno ebt
1450200 3
*crdno time press temp
1450201 0.0 0.54e6 325.15
*
*-----$
*
* PCU Model Configuration-Hot Side
*
*-----$
* PCU Junction: Reactor Outlet Plenum to PCU Hot Duct
*-----$
* name junction
0820000 RPV-Hdct valve
* from to area kforw kbackw j-flag
0820101 300010000 504000000 1.606 8.0 1.0 00000200
* cntrl w/v.liq w/v.vap w/v.int
0820201 0 62.7588 62.7588 0. * 319.2105
* valve-type
0820300 mtrvlv
* trip# w/v.liq w/v.vap w/v.int
0820301 527 1003 0.0167 1.0
*
** Name Valve

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5030000 cprbp2 valve
* from to area kforw kbackw j-flag
5030101 504010000 500000000 0.00 0. 0. 0000000
* cntrl w/v.liq w/v.vap w/v.int
5030201 1 0. 0. 0.0
* valve-type
5030300 trpvlv
* trip# w/v.liq w/v.vap w/v.int
5030301 1004
*
*-----
*
*-----
*crdno name type
5040000 contnmt snglvol
*crdno area length vol h-a v-ang delz rgh dhy pvbfe
5040101 1.606 0.1 0 0 0. .0 0. 0. 00010 *
*crdno ebt press temp.
5040200 0 7001960. 3442779. 3442779. 1. 0.
*
*-----
* Single Volume: Guard Containment
*-----
*crdno name type
0700000 contnmt snglvol
*crdno area length vol h-a v-ang delz rgh dhy pvbfe
0700101 283.0 10.15 0 0 0. .0 0. 0. 00010 * 283x66.15
*crdno ebt press temp.
0700200 3 1.0e5 303.15
*-----
* Single Volume: nossle
*-----
*crdno name type
*0630000 contnmt snglvol
*crdno area length vol h-a v-ang delz rgh dhy pvbfe
*0630101 0.05 0.01 0 0 0. .0 0. 0. 00010 *
*crdno ebt press temp.
*0630200 3 1.0e5 303.15
*-----
* Single Junction: nossle
*-----
** name junction
*0640000 tocont sngljun
* from to area kforw kbackw j-flag
*0640101 063010000 070000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
*0640201 0 0. 0. 0. *
*-----
* Valve: PCU to Guard Containment
*-----
** Name Valve
0620000 PCU-GC valve
* from to area kforw kbackw j-flag
0620101 597010000 070000000 0.0005 0.84206 0.84206 0000000
* cntrl w/v.liq w/v.vap w/v.int
0620201 1 0. 0.0 0.0
* valve-type
0620300 trpvlv
* trip# w/v.liq w/v.vap w/v.int
0620301 522 *CLOSE until 50 secs
*
*-----
* 083 Junction between PCU and RPV inlet (cold duct)
*-----
*0830000 pcuhot tmdpjun
*crdno from to area jefvcahs
*0830101 597010000 670000000 1.885 000000
*0830200 1 522
*0830201 -1.0 0.0 0.0 0.0
*0830202 0.0 0.0 324.57 0.0
*0830203 1.0 0.0 324.57 0.0
*0830204 50.0 0.0 0.0 0.0
*Note times above are trip tim + given time
*
*-----
* PCU Junction: PCU Cold Duct to RPV Downcomer
*-----
* name junction
9650000 InC-InHP sngljun
* from to area kforw kbackw j-flag
9650101 597010000 670000000 0.0 0.0 0.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
9650201 0 35.525 35.525 0. * 319.2105
*-----
* PCU Junction: PCU Cold Duct to RPV Downcomer
*-----

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* name junction
9660000 InC-InHP sngljun
* from to area kforw kbackw j-flag
9660101 597010000 800000000 0.0 0.0 0.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
9660201 0 35.525 35.525 0. * 319.2105
*
*-----
*
* Passive DHR DECAY HEAT REMOVAL SYSTEM 1
*
*-----
*
* Junction: Reactor Outlet Plenum to Passive DHR System Duct
*-----
** name junction
6050000 opl-hd sngljun
* from to area kforw kbackw j-flag
6050101 300010000 610000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
6050201 0 -1.298463-7 -1.298463-7 0. * -4.31083-7
*-----
* Passive DHR Hot Duct 1x50% loop
*-----
* name pipe/annulus
6100000 hp-hotd pipe
* number of volumes
6100001 5
* area no of vol
6100101 2.0774 5
* length no of vol
6100301 3.8 5
* volume no of vol
6100401 0.0 5
* azi ang no of vol
6100501 90. 5
* ver ang no of vol
6100601 90. 5
* elev. no of vol
6100701 3.0 5
* rough dhydr. no of vol
6100801 4.5e-5 1.6264 5
* kforw kbackw no of jun
6100901 0.0875 0.0875 4
* v-flag no of vol
6101001 00000 5
* j-flag no of jun
6101101 00000 4
* cntrl pressure temperature * * * no of vol
6101201 0 7058062. 3418188. 3418188. 1. 0. 1
6101202 0 7.058+6 3403438. 3403438. 1. 0. 2
6101203 0 7057949. 3400732. 3400732. 1. 0. 3
6101204 0 7057892. 3401820. 3401820. 1. 0. 4
6101205 0 7057836. 3411673. 3411673. 1. 0. 5
* cntrl
6101300 0
* w/v.liq w/v.vap w/v.int no of jun
6101301 -1.256998-7 -1.256998-7 0. 1 * -4.19126-7
6101302 -1.221132-7 -1.221132-7 0. 2 * -4.07489-7
6101303 -1.18709-7 -1.18709-7 0. 3 * -3.96001-7
6101304 -1.156956-7 -1.156956-7 0. 4 * -3.848304-7
*
*-----
* Junction: HP Hot Duct to HX POD Inlet
*-----
* name junction
6150000 hd-hxpin sngljun
* from to area kforw kbackw j-flag
6150101 610010000 620000000 0.0 0.75 0.75 0000001
* cntrl w/v.liq w/v.vap w/v.int
6150201 0 -1.158115-7 -1.158115-7 0. * -3.76676-7
*
*-----
* Passive DHR Heat Exchanger POD Inlet
*-----
* name volume
6200000 hp-hxpin snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6200101 5.4 4.5 0.0 90. 90. 4.5 4.5e-5 1.636 000000 $ 1
* cntrl press temp
6200200 0 7057738. 3488909. 3488909. 1.
*-----
* Junction: Passive DHR HX POD Inlet to Heat Exchanger Inlet
*-----
* name junction
6250000 ihx-hxp sngljun
* from to area kforw kbackw j-flag

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6250101 620010000 626000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
6250201 0 -3.62896-8 -3.62896-8 0. * -2.489533-7
*
*-----
* Passive DHR Heat Exchanger Inlet
*-----
* name volume
6260000 hp-hxin snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6260101 2.1276 1.0 0.0 -90. -90. -0.5 4.5e-5 0.15 000000 $ 1
* cntrl press temp
6260200 0 7057678. 3388292. 3388292. 1.
*-----
* Junction: Passive DHR HX Inlet to Heat Exchanger
*-----
* name junction
6270000 ihx-hx sngljun
* from to area kforw kbackw j-flag
6270101 626010000 650000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
6270201 0 -2.086635-8 -2.086635-8 0. * -2.680236-7
*
*-----
* Passive DHR Heat Exchanger
*-----
* name pipe/annulus
6500000 hp-hx pipe
* number of volumes
6500001 5
* area no of vol
6500101 2.1856 5
* length no of vol
6500301 0.060 5
* volume no of vol
6500401 0.0 5
* azi ang no of vol
6500501 -90. 5
* ver ang no of vol
6500601 -90. 5
* elev. no of vol
6500701 -0.060 5
* rough dhydr. no of vol
6500801 1.e-5 3.055e-3 5
* kforw kbackw no of jun
6500901 0.0 0.0 4
* v-flag no of vol
6501001 00000 5
* j-flag no of jun
6501101 000000 4
* cntrl pressure temperature * * * no of vol
6501201 0 7057689. 932251. 932251. 1. 0. 1
6501202 0 7057696. 932245. 932245. 1. 0. 2
6501203 0 7057702. 932240. 932240. 1. 0. 3
6501204 0 7057710. 932236. 932236. 1. 0. 4
6501205 0 7057716. 932233. 932233. 1. 0. 5
* cntrl
6501300 0
* w/v.liq w/v.vap w/v.int no of jun
6501301 -2.098683-8 -2.098683-8 0. 1 * -2.69573-7
6501302 -2.108813-8 -2.108813-8 0. 2 * -2.708757-7
6501303 -2.11641-8 -2.11641-8 0. 3 * -2.71853-7
6501304 -2.12116-8 -2.12116-8 0. 4 * -2.724644-7
*-----
* Junction: Passive DHR Heat Exchanger to HX Outlet
*-----
* name junction
6550000 hx-ohx sngljun
* from to area kforw kbackw j-flag
6550101 650010000 660000000 0.0 0.50 0.50 0000000
* cntrl w/v.liq w/v.vap w/v.int
6550201 0 -4.34546-8 -4.34546-8 0. * -2.737685-7
*
*-----
* Passive DHR Heat Exchanger Outlet Plenum
*-----
* name volume
6600000 hp-outpl snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6600101 2.1276 1.0 0.0 -90. -90. -0.2 4.5e-5 0.15 000000
* cntrl press temp
6600200 0 7057726. 1896749. 1896749. 1.
*
*-----
* Junction: Passive DHR HX Outlet to Downcomer
*-----
* name junction
6610000 hp-ohx sngljun

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```

* from to area kforw kbackw j-flag
6610101 660010000 662000000 0.0 1.0 1.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6610201 0 -2.273712-8 -2.273712-8 0. * -2.254984-7
*-----
* Passive DHR Heat Exchanger Outlet Pod
*-----
* name volume
6620000 hp-outpp snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6620101 10.995 1.0 0.0 -90. -90. -1.0 4.5e-5 2.026 000000 $
* cntrl press temp
6620200 0 7057754. 2344926. 2344926. 1.
*
*-----
* Junction: Passive DHR HX Outlet Pod
*-----
* name junction
6630000 hp-ohxp sngljun
* from to area kforw kbackw j-flag
6630101 662010000 664000000 0.0 0.0 0.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6630201 0 -4.49314-9 -4.49314-9 0. * -1.282388-7
*
*-----
* Passive DHR BLOWER volume
*-----
* name volume
6640000 hp-outpb snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6640101 6.1576 3.0 0.0 -90. -90. -3.0 4.5e-5 1.4 000000
* cntrl press temp
6640200 0 7057845. 2358240. 2358240. 1.
*
* name junction
6920000 hp-ohxp sngljun
* from to area kforw kbackw j-flag
6920101 664010000 690000000 0.0 0.0 0.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6920201 0 -4.67222-9 -4.67222-9 0. * -1.88798-7
*-----
* name volume
6900000 hp-outpc snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6900101 6.1576 0.5 0.0 -90. 0. 0.0 0. 1.4 000000
* cntrl press temp
6900200 0 7057892. 1666776. 1666776. 1.
*
*-----
* name junction
6650000 hp-blow valve
* from to area kforw kbackw j-flag
6650101 690010000 698000000 6.1576 13.46 13.46 00000200
* cntrl w/v.liq w/v.vap w/v.int
6650201 0 0. 0. 0. * 0.
* valve-type
6650300 mtrvlv
* trip# w/v.liq w/v.vap w/v.int
6650301 539 541 0.025 0.0
*-----
** Name Valve
6870000 leak1 tmdpjun
* from to area j-flag
6870101 698000000 690010000 0.00 0000000
* cntrl trp
6870200 1 541
*
6870201 -0.1 0. 0. 0.
6870202 0. 0. 0.311 0.
*-----
* name volume
6980000 hp-outpd snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6980101 6.1576 0.5 0.0 -90. 0. 0.0 0. 1.4 000000
* cntrl press temp
6980200 0 9623368. 3469112. 3469112. 1.
* name junction
6990000 hp-ohxp sngljun
* from to area kforw kbackw j-flag
6990101 698010000 666000000 0.0 0.0 0.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6990201 0 -4.67222-9 -4.67222-9 0. * -1.88798-7
*-----
* Passive DHR Cold leg 1x50% loop
*-----
* name pipe/annulus
6660000 SCS-CL pipe

```

```

* number of volumes
6660001 5
* area no of vol
6660101 6.1576 5
* length no of vol
6660301 3.7 5
* volume no of vol
6660401 0.0 5
* azi ang no of vol
6660501 -90. 5
* ver ang no of vol
6660601 -90. 5
* elev. no of vol
6660701 -2.9 5
* rough dhydr. no of vol
6660801 4.5e-5 1.546 5
* kforw kbackw no of jun
6660901 0.0875 0.0875 4
* v-flag no of vol
6661001 00000 5
* j-flag no of jun
6661101 00000 4
* cntrl pressure temperature * * * no of vol
6661201 0 9644631. 3497396. 3497396. 1. 0. 1
6661202 0 9644697. 3497396. 3497396. 1. 0. 2
6661203 0 9644763. 3497396. 3497396. 1. 0. 3
6661204 0 9644829. 3497396. 3497396. 1. 0. 4
6661205 0 9644895. 3497397. 3497397. 1. 0. 5
* cntrl
6661300 0
* w/v.liq w/v.vap w/v.int no of jun
6661301 -9.47945-14 -9.47945-14 0. 1 * -2.729385-13
6661302 -1.594003-13 -1.594003-13 0. 2 * -4.58962-13
6661303 -2.3107-13 -2.3107-13 0. 3 * -6.6533-13
6661304 -2.0602-13 -2.0602-13 0. 4 * -5.93211-13
*
*
-----
* Junction connecting Passive Cold Leg to RPV downcomer with valve (simulates
*
* name junction
6670000 hp-ohb valve
* from to area kforw kbackw j-flag
6670101 666010000 670000000 0.0 1.0 1.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6670201 0 0. 0. 0. * 0.
* valve-type
6670300 trpvlv
* trip# w/v.liq w/v.vap w/v.int
6670301 525 * Close Until end of coastdown
*
-----
* Bypass Junction to simulate leakage of check check valve
*
* name junction
6950000 leak_chv valve
* from to area kforw kbackw j-flag
6950101 666010000 670000000 1.e-9 1.e9 1.e9 0000000
* cntrl w/v.liq w/v.vap w/v.int
6950201 0 0. 0. 0. * 0.
* valve-type
6950300 trpvlv
* trip# w/v.liq w/v.vap w/v.int
6950301 525 * Close Until end of coastdown
*
-----
*
* Passive DHR DECAY HEAT REMOVAL SYSTEM 2 (DHR2)
*
-----
*
* Junction: Reactor Outlet Plenum to Passive DHR System Duct (DHR2)
*
* name junction
6060000 opl-hd2 sngljun
* from to area kforw kbackw j-flag
6060101 300010000 611000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
6060201 0 -1.822274-7 -1.822274-7 0. * -6.11274-7
*
-----
* Passive DHR Hot Duct (DHR2)
*
* name pipe/annulus
6110000 hp-hotd2 pipe
* number of volumes
6110001 5
* area no of vol
6110101 2.0774 5

```

```

* length no of vol
6110301 3.8 5
* volume no of vol
6110401 0.0 5
* azi ang no of vol
6110501 90. 5
* ver ang no of vol
6110601 90. 5
* elev. no of vol
6110701 3.0 5
* rough dhydr. no of vol
6110801 4.5e-5 1.6264 5
* kforw kbackw no of jun
6110901 0.0875 0.0875 4
* v-flag no of vol
6111001 00000 5
* j-flag no of jun
6111101 000000 4
* cntrl pressure temperature * * * no of vol
6111201 0 7058062. 3383064. 3383064. 1. 0. 1
6111202 0 7.058+6 3366640. 3366640. 1. 0. 2
6111203 0 7057948. 3341524. 3341524. 1. 0. 3
6111204 0 7057890. 3294012. 3294012. 1. 0. 4
6111205 0 7057830. 3193825. 3193825. 1. 0. 5
* cntrl
6111300 0
* w/v.liq w/v.vap w/v.int no of jun
6111301 -1.7768-7 -1.7768-7 0. 1 * -5.98928-7
6111302 -1.726138-7 -1.726138-7 0. 2 * -5.86226-7
6111303 -1.6624-7 -1.6624-7 0. 3 * -5.72729-7
6111304 -1.569187-7 -1.569187-7 0. 4 * -5.57591-7
*
*-----
* Junction: HP Hot Duct to HX POD Inlet (DHR2)
*-----
* name junction
6160000 hd-hxpi2 sngljun
* from to area kforw kbackw j-flag
6160101 611010000 621000000 0.0 0.75 0.75 0000001
* cntrl w/v.liq w/v.vap w/v.int
6160201 0 -1.378557-7 -1.378557-7 0. * -5.37921-7
*
*-----
* Passive DHR Heat Exchanger POD Inlet (DHR2)
*-----
* name volume
6210000 hp-hxp2 snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6210101 5.4 4.5 0.0 90. 90. 4.5 4.5e-5 1.636 000000 $ 1
* cntrl press temp
6210200 0 7057717. 2908740. 2908740. 1.
*
*-----
* Junction: Passive DHR HX POD Inlet to Heat Exchanger Inlet (DHR2)
*-----
* name junction
6280000 ihx-hxp2 sngljun
* from to area kforw kbackw j-flag
6280101 621010000 629000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
6280201 0 -1.570477-8 -1.570477-8 0. * -3.142066-7
*
*-----
* Passive DHR Heat Exchanger Inlet (DHR2)
*-----
* name volume
6290000 hp-hxin2 snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6290101 2.1276 1.0 0.0 -90. -90. -0.5 4.5e-5 0.15 000000 $ 1
* cntrl press temp
6290200 0 7057657. 1164302. 1164302. 1.
*
*-----
* Junction: Passive DHR HX Inlet to Heat Exchanger (DHR2)
*-----
* name junction
6300000 ihx-hx sngljun
* from to area kforw kbackw j-flag
6300101 629010000 651000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
6300201 0 -2.589013-8 -2.589013-8 0. * -3.32553-7
*
*-----
* Passive DHR Heat Exchanger (DHR2)
*-----
* name pipe/annulus
6510000 hp-hx2 pipe
* number of volumes
6510001 5
* area no of vol

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```

6510101 2.1856 5
* length no of vol
6510301 0.060 5
* volume no of vol
6510401 0.0 5
* azi ang no of vol
6510501 -90. 5
* ver ang no of vol
6510601 -90. 5
* elev. no of vol
6510701 -0.06 5
* rough dhydr. no of vol
6510801 1.e-5 3.055e-3 5
* kforw kbackw no of jun
6510901 0.0 0.0 4
* v-flag no of vol
6511001 00000 5
* j-flag no of jun
6511101 000000 4
* cntrl pressure temperature * * * no of vol
6511201 0 7057684. 932250. 932250. 1. 0. 1
6511202 0 7057690. 932244. 932244. 1. 0. 2
6511203 0 7057698. 932239. 932239. 1. 0. 3
6511204 0 7057704. 932235. 932235. 1. 0. 4
6511205 0 7057711. 932232. 932232. 1. 0. 5
* cntrl
6511300 0
* w/v.liq w/v.vap w/v.int no of jun
6511301 -2.60233-8 -2.60233-8 0. 1 * -3.34266-7
6511302 -2.612243-8 -2.612243-8 0. 2 * -3.35541-7
6511303 -2.618735-8 -2.618735-8 0. 3 * -3.36377-7
6511304 -2.62204-8 -2.62204-8 0. 4 * -3.368025-7
-----
* Junction: Passive DHR Heat Exchanger to HX Outlet (DHR2)
-----
*
* name junction
6560000 hx-ohx2 sngljun
* from to area kforw kbackw j-flag
6560101 651010000 668000000 0.0 0.50 0.50 0000000
* cntrl w/v.liq w/v.vap w/v.int
6560201 0 -4.44103-8 -4.44103-8 0. * -3.37483-7
*
-----
* Passive DHR Heat Exchanger Outlet Plenum (DHR2)
-----
*
* name volume
6680000 hp-outp2 snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6680101 2.1276 1.0 0.0 -90. -90. -0.2 4.5e-5 0.15 000000
* cntrl press temp
6680200 0 7057722. 1573145. 1573145. 1.
*
-----
* Junction: Passive DHR HX Outlet to Downcomer (DHR2)
-----
*
* name junction
6690000 hp-ohx2 sngljun
* from to area kforw kbackw j-flag
6690101 668010000 671000000 0.0 1.0 1.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6690201 0 -2.11582-8 -2.11582-8 0. * -3.063706-7
*
-----
* Passive DHR Heat Exchanger Outlet Pod (DHR2)
-----
*
* name volume
6710000 hp-outp2 snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6710101 10.995 1.0 0.0 -90. -90. -1.0 4.5e-5 2.026 000000
* cntrl press temp
6710200 0 7057762. 1607285. 1607285. 1.
*
-----
* Junction: Passive DHR HX Outlet Pod (DHR2)
-----
*
* name junction
6720000 hp-ohxp sngljun
* from to area kforw kbackw j-flag
6720101 671010000 673000000 0.0 0.0 0.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6720201 0 -4.67222-9 -4.67222-9 0. * -1.88798-7
*
-----
* Passive DHR BLOWER (DHR2)
-----
*
* name volume
6730000 hp-outp2 snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6730101 6.1576 3.0 0.0 -90. -90. -3.0 4.5e-5 1.4 000000
* cntrl press temp

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```

6730200 0 7057892. 1666776. 1666776. 1.
*
-----
* name junction
6930000 hp-ohxp sngljun
* from to area kforw kbackw j-flag
6930101 673010000 691000000 0.0 0.0 0.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6930201 0 -4.67222-9 -4.67222-9 0. * -1.88798-7
* name volume
6910000 hp-outpc snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6910101 6.1576 0.5 0.0 -90. 0. 0.0 0. 1.4 000000
* cntrl press temp
6910200 0 7057892. 1666776. 1666776. 1.
*
-----
* name volume
6940000 hp-outpd snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
6940101 6.1576 0.5 0.0 -90. 0. 0.0 0. 1.4 000000
* cntrl press temp
6940200 0 9623368. 3469112. 3469112. 1.
*
* name junction
6960000 hp-ohxp sngljun
* from to area kforw kbackw j-flag
6960101 694010000 676000000 0.0 0.0 0.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6960201 0 -4.67222-9 -4.67222-9 0. * -1.88798-7
-----
* Valve: Passive DHR Cold Leg Valve junction to RPV downcomer (DHR2)
-----
** name junction
6740000 hp-cl valve
* from to area kforw kbackw j-flag
6740101 691010000 694000000 6.1576 13.46 13.46 00000200
* cntrl w/v.liq w/v.vap w/v.int
6740201 0 0. 0. 0. * 0.
* valve-type
6740300 mtrvlv
* trip# w/v.liq w/v.vap w/v.int
6740301 540 542 0.0125 0.0 0
*
-----
** Name Valve
6880000 leak2 tmdpjun
* from to area j-flag
6880101 694000000 691010000 0.00 0000000
* cntrl trp
6880200 1 542
*
6880201 -0.1 0. 0. 0.
6880202 0. 0. 0.311 0.
*
-----
* Passive DHR Cold leg 1x50# loop (DHR2)
-----
* name pipe/annulus
6760000 SCS-CL pipe
* number of volumes
6760001 5
* area no of vol
6760101 6.1576 5
* length no of vol
6760301 3.7 5
* volume no of vol
6760401 0.0 5
* azi ang no of vol
6760501 -90. 5
* ver ang no of vol
6760601 -90. 5
* elev. no of vol
6760701 -2.9 5
* rough dhydr. no of vol
6760801 4.5e-5 1.546 5
* kforw kbackw no of jun
6760901 0.0875 0.0875 4
* v-flag no of vol
6761001 00000 5
* j-flag no of jun
6761101 00000 4
* cntrl pressure temperature * * * no of vol
6761201 0 9623368. 3469112. 3469112. 1. 0. 1
6761202 0 9623434. 3469112. 3469112. 1. 0. 2
6761203 0 9623500. 3469112. 3469112. 1. 0. 3
6761204 0 9623566. 3469113. 3469113. 1. 0. 4
6761205 0 9623632. 3469113. 3469113. 1. 0. 5

```

```

* cntrl
6761300 0
* w/v.liq w/v.vap w/v.int no of jun
6761301 -6.67305-15 -6.67305-15 0. 1 * -1.928565-14
6761302 -3.19196-14 -3.19196-14 0. 2 * -9.22514-14
6761303 -1.173983-13 -1.173983-13 0. 3 * -3.392996-13
6761304 8.44969-14 8.44969-14 0. 4 * 2.44209-13
*
-----
* Valve: Passive DHR Cold Leg Valve junction to RPV downcomer (DHR2)
*
* name junction
6770000 hp-ohb2 valve
* from to area kforw kbackw j-flag
6770101 676010000 800000000 0.0 1.0 1.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
6770201 0 0. 0. 0. * 0.
* valve-type
6770300 trpvlv
* trip# w/v.liq w/v.vap w/v.int
6770301 525 * Close Until end of coastdown
*
-----
* Bypass Junction to simulate leakage of check check valve
*
* name junction
6970000 leak_chv valve
* from to area kforw kbackw j-flag
6970101 676010000 800000000 1.e-9 1.e9 1.e9 0000000
* cntrl w/v.liq w/v.vap w/v.int
6970201 0 0. 0. 0. * 0.
* valve-type
6970300 trpvlv
* trip# w/v.liq w/v.vap w/v.int
6970301 525 * Close Until end of coastdown
*
=====
*
* Passive DHR DECAY HEAT REMOVAL SYSTEM UHS SYSTEM 1
*
-----
* H2O DHR Heat Exchanger Inlet
*
* name volume
7000000 h2ohxin snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
7000101 0.0873 1.0 0.0 90. 90. 0.5 4.5e-5 0.333 000000
* cntrl press temp
7000200 0 1085604. 104058.9 2584130. 0.
*
-----
* Junction: H2O Passive DHR HX Inlet to Heat Exchanger
*
* name junction
7050000 h2oihxj sngljun
* from to area kforw kbackw j-flag
7050101 700010000 710000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
7050201 0 8.28489-4 8.3558-4 0. * .0721563
*
-----
* Passive H2O DHR Heat Exchanger
*
* name pipe/annulus
7100000 h2ohphx pipe
* number of volumes
7100001 5
* area no of vol
7100101 1.09281 5
* length no of vol
7100301 0.060 5
* volume no of vol
7100401 0.0 5
* azi ang no of vol
7100501 90. 5
* ver ang no of vol
7100601 90. 5
* elev. no of vol
7100701 0.060 5
* rough dhydr. no of vol
7100801 1.e-5 3.055e-3 5
* kforw kbackw no of jun
7100901 0.0 0.0 4
* v-flag no of vol
7101001 00000 5
* j-flag no of jun
7101101 00000 4
* cntrl pressure temperature * * * no of vol
7101201 0 1082864. 104068.4 2584060. 0. 0. 1

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7101202 0 1082277. 104073. 2584045. 0. 0. 2
7101203 0 1081690. 104078.7 2584030. 0. 0. 3
7101204 0 1081103. 104085.5 2584014. 0. 0. 4
7101205 0 1080516. 104093. 2.584+6 0. 0. 5
* cntrl
7101300 0
* w/v.liq w/v.vap w/v.int no of jun
7101301 6.61846-5 6.62321-5 0. 1 * .0721563
7101302 6.61846-5 6.62321-5 0. 2 * .0721563
7101303 6.61846-5 6.62321-5 0. 3 * .0721563
7101304 6.61847-5 6.62322-5 0. 4 * .0721563
*
*-----*
* Junction: H2O Passive DHR Heat Exchanger to HX Outlet
*-----*
* name junction
7150000 h2hxohx sngljun
* from to area kforw kbackw j-flag
7150101 710010000 720000000 0.0 1.00 1.00 0000000
* cntrl w/v.liq w/v.vap w/v.int
7150201 0 8.28492-4 8.35584-4 0. * .0721563
*
*-----*
* Passive H2O DHR Heat Exchanger Outlet Plenum
*-----*
* name volume
7200000 h2ooutpl snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
7200101 0.0873 1.0 0.0 90. 90. 0.2 4.5e-5 0.333 0000000
* cntrl press temp
7200200 0 1079244. 104098. 2583967. 0.
*
*-----*
* Junction: H2O DHR Heat Exchanger Outlet Plenum to UHS Duct
*-----*
* name junction
7250000 h2oplhd sngljun
* from to area kforw kbackw j-flag
7250101 720010000 730000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
7250201 0 8.28492-4 8.35584-4 0. * .0721563
*
*-----*
* Passive DHR Hot Duct
*-----*
* name pipe/annulus
7300000 h2ohotd pipe
* number of volumes
7300001 5
* area no of vol
7300101 0.0873 5
* length no of vol
7300301 1.6 5
* volume no of vol
7300401 0.0 5
* azi ang no of vol
7300501 90. 5
* ver ang no of vol
7300601 90. 5
* elev. no of vol
7300701 1.6 5
* rough dhydr. no of vol
7300801 4.5e-5 0.333 5
* kforw kbackw no of jun
7300901 0.0875 0.0875 4
* v-flag no of vol
7301001 00000 5
* j-flag no of jun
7301101 00000 4
* cntrl pressure temperature * * * no of vol
7301201 0 1070439. 104106.3 2583740. 0. 0. 1
7301202 0 1054786. 104114.7 2583334. 0. 0. 2
7301203 0 1039133. 104123.5 2582923. 0. 0. 3
7301204 0 1023479. 104133.1 2582507. 0. 0. 4
7301205 0 1007826. 104160.4 2582086. 3.71865-6 0. 5
* cntrl
7301300 0
* w/v.liq w/v.vap w/v.int no of jun
7301301 8.28495-4 8.35587-4 0. 1 * .0721562
7301302 8.28501-4 8.35593-4 0. 2 * .0721562
7301303 8.28507-4 8.35599-4 0. 3 * .0721561
7301304 8.28513-4 .00157848 0. 4 * .0721561
*
**
** Junction: Hotleg Duct to surge tank
**
** name type
7800000 h2o-surj sngljun

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```

* from to area kforw kbackw j-flag
7800101 730010000 790000000 0 0.5 0.5 0000000
* cntrl w/v.liq w/v.vap w/v.int
7800201 0 -.00146826 -9.44189-7 0. * -4.00458-7
*
-----
** H2O LOOP surge tank
-----
* name volume
7900000 h2osurge tmdpvoll
* area length vol. a.ang. in.ang. elev. rough. hDe pvbfe
7900101 500.0 10.0 0.0 0.0 0.0 0.0 0.00046 7.4 00010
* cntrl
7900200 003
* press temp
7900201 0.0 1.00000e6 473.0
-----
* Junction: HP Hot Duct to HX Inlet
-----
* name junction
7350000 h2ohxpin sngljun
* from to area kforw kbackw j-flag
7350101 730010000 740000000 0.0 0.75 0.75 0000001
* cntrl w/v.liq w/v.vap w/v.int
7350201 0 8.28526-4 .02027343 0. * .0721564
*
-----
* Passive DHR Heat Exchanger Inlet
-----
* name volume
7400000 h2ohxin snglvoll
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
7400101 0.0873 1.0 0.0 -90. -90. -0.5 4.5e-5 0.333 000000
* cntrl press temp
7400200 0 1002446. 104171.3 2581940. 1.404818-6
-----
* Junction: Passive DHR HX Inlet to Heat Exchanger
-----
* name junction
7450000 h2ohx-h sngljun
* from to area kforw kbackw j-flag
7450101 740010000 750000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
7450201 0 8.28526-4 -.00344602 0. * .0721564
*
-----
* Passive H2O/UHS Heat Exchanger
-----
* name pipe/annulus
7500000 h2hp-hx pipe
* number of volumes
7500001 20
* area no of vol
7500101 9.64974e-2 20
* length no of vol
7500301 1.605 20
* volume no of vol
7500401 0.0 20
* azi ang no of vol
7500501 -90. 20
* ver ang no of vol
7500601 0.0 20
* elev. no of vol
7500701 0.0 20
* rough dhydr. no of vol
7500801 1.e-5 3.5052e-2 20
* kforw kbackw no of jun
7500901 0.0 0.0 19
* v-flag no of vol
7501001 00000 20
* j-flag no of jun
7501101 00000 19
* cntrl pressure temperature * * * no of vol
7501201 0 1004892. 104080.5 2582007. 0. 0. 1
7501202 0 1004892. 104063. 2582007. 0. 0. 2
7501203 0 1004892. 104059.6 2582007. 0. 0. 3
7501204 0 1004891. 104059. 2582007. 0. 0. 4
7501205 0 1004891. 104058.8 2582007. 0. 0. 5
7501206 0 1004891. 104058.8 2582007. 0. 0. 6
7501207 0 1004891. 104058.8 2582007. 0. 0. 7
7501208 0 1004891. 104058.8 2582007. 0. 0. 8
7501209 0 1004891. 104058.8 2582007. 0. 0. 9
7501210 0 1004891. 104058.8 2582007. 0. 0. 10
7501211 0 1004891. 104058.8 2582007. 0. 0. 11
7501212 0 1004891. 104058.8 2582007. 0. 0. 12
7501213 0 1004891. 104058.8 2582007. 0. 0. 13
7501214 0 1004891. 104058.8 2582007. 0. 0. 14
7501215 0 1004891. 104058.8 2582007. 0. 0. 15

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7501216 0 1004891. 104058.8 2582007. 0. 0. 16
7501217 0 1004891. 104058.8 2582007. 0. 0. 17
7501218 0 1004891. 104058.8 2582007. 0. 0. 18
7501219 0 1004891. 104058.8 2582007. 0. 0. 19
7501220 0 1004891. 104058.8 2582007. 0. 0. 20
* cntrl
7501300 0
* w/v.liq w/v.vap w/v.int no of jun
7501301 7.49551-4 7.49551-4 0. 1 * .0721563
7501302 7.4955-4 7.4955-4 0. 2 * .0721563
7501303 7.4955-4 7.4955-4 0. 3 * .0721563
7501304 7.4955-4 7.4955-4 0. 4 * .0721563
7501305 7.4955-4 7.4955-4 0. 5 * .0721563
7501306 7.4955-4 7.4955-4 0. 6 * .0721563
7501307 7.4955-4 7.4955-4 0. 7 * .0721563
7501308 7.4955-4 7.4955-4 0. 8 * .0721563
7501309 7.4955-4 7.4955-4 0. 9 * .0721563
7501310 7.4955-4 7.4955-4 0. 10 * .0721563
7501311 7.4955-4 7.4955-4 0. 11 * .0721563
7501312 7.4955-4 7.4955-4 0. 12 * .0721563
7501313 7.4955-4 7.4955-4 0. 13 * .0721563
7501314 7.4955-4 7.4955-4 0. 14 * .0721563
7501315 7.4955-4 7.4955-4 0. 15 * .0721563
7501316 7.4955-4 7.4955-4 0. 16 * .0721563
7501317 7.4955-4 7.4955-4 0. 17 * .0721563
7501318 7.4955-4 7.4955-4 0. 18 * .0721563
7501319 7.4955-4 7.4955-4 0. 19 * .0721563
*
-----
* Junction: H2O/UHS Passive DHR Heat Exchanger to HX Outlet
*
* name junction
7550000 h2hx-ohx sngljun
* from to area kforw kbackw j-flag
7550101 750010000 760000000 0.0 1.00 1.00 0000000
* cntrl w/v.liq w/v.vap w/v.int
7550201 0 8.28518-4 8.28518-4 0. * .0721563
*
-----
* Passive UHS DHR Heat Exchanger Outlet Plenum
*
* name volume
7600000 h2-outpl snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
7600101 0.0873 1.0 0.0 -90. -90. -0.5 4.5e-5 0.333 000000
* cntrl press temp
7600200 0 1007337. 104058.8 2582073. 0.
*
-----
* Junction: Passive DHR HX Outlet to Downcomer
*
* name junction
7650000 hhp-ohx sngljun
* from to area kforw kbackw j-flag
7650101 760010000 770000000 0.0 1.0 1.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
7650201 0 8.28517-4 8.3561-4 0. * .0721563
*
-----
* Passive DHR Downcomer
*
* name pipe/annulus
7700000 h2ohotd pipe
* number of volumes
7700001 5
* area no of vol
7700101 0.0873 5
* length no of vol
7700301 1.6 5
* volume no of vol
7700401 0.0 5
* azi ang no of vol
7700501 -90. 5
* ver ang no of vol
7700601 -90. 5
* elev. no of vol
7700701 -1.6 5
* rough dhydr. no of vol
7700801 4.5e-5 0.333 5
* kforw kbackw no of jun
7700901 0.0875 0.0875 4
* v-flag no of vol
7701001 00000 5
* j-flag no of jun
7701101 00000 4
* cntrl pressure temperature * * * no of vol
7701201 0 1017609. 104058.8 2582350. 0. 0. 1
7701202 0 1033262. 104058.8 2582768. 0. 0. 2
7701203 0 1048916. 104058.8 2583181. 0. 0. 3

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```

7701204 0 1064569. 104058.8 2583589. 0. 0. 4
7701205 0 1080223. 104058.9 2583992. 0. 0. 5
* cntrl
7701300 0
* w/v.liq w/v.vap w/v.int no of jun
7701301 8.28514-4 8.35606-4 0. 1 * .0721563
7701302 8.28508-4 8.356-4 0. 2 * .0721563
7701303 8.28502-4 8.35594-4 0. 3 * .0721563
7701304 8.28496-4 8.35589-4 0. 4 * .0721563
*
-----
* SNGLJ: Passive DHR Cold Duct to Rx Inlet Plenum
-----
* name junction
7750000 cd-iplm sngljun
* from to area kforw kbackw j-flag
7750101 770010000 700000000 0.0 1.0 1.0 0000001
* cntrl w/v.liq w/v.vap w/v.int
7750201 0 8.2849-4 8.2849-4 0. * .0721563
*
=====
* Passive DHR DECAY HEAT REMOVAL SYSTEM UHS SYSTEM 2-Water loop
*
-----
* H2O DHR Heat Exchanger Inlet (DHR2-Water)
-----
* name volume
7010000 h2ohxin snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
7010101 0.0873 1.0 0.0 90. 90. 0.5 4.5e-5 0.333 000000
* cntrl press temp
7010200 0 1085604. 104059. 2584130. 0.
-----
* Junction: H2O Passive DHR HX Inlet to Heat Exchanger (DHR2-Water)
-----
* name junction
7060000 h2oixj sngljun
* from to area kforw kbackw j-flag
7060101 701010000 711000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
7060201 0 7.98759-4 8.05363-4 0. * .0695671
*
-----
* Passive H2O DHR Heat Exchanger (DHR2-Water)
-----
* name pipe/annulus
7110000 h2ohphx pipe
* number of volumes
7110001 5
* area no of vol
7110101 1.09281 5
* length no of vol
7110301 0.060 5
* volume no of vol
7110401 0.0 5
* azi ang no of vol
7110501 90. 5
* ver ang no of vol
7110601 90. 5
* elev. no of vol
7110701 0.060 5
* rough dhydr. no of vol
7110801 1.e-5 3.055e-3 5
* kforw kbackw no of jun
7110901 0.0 0.0 4
* v-flag no of vol
7111001 00000 5
* j-flag no of jun
7111101 000000 4
* cntrl pressure temperature * * * no of vol
7111201 0 1082864. 104067. 2584060. 0. 0. 1
7111202 0 1082277. 104071.2 2584045. 0. 0. 2
7111203 0 1081690. 104076.7 2584030. 0. 0. 3
7111204 0 1081103. 104083.6 2584014. 0. 0. 4
7111205 0 1080516. 104092. 2.584+6 0. 0. 5
* cntrl
7111300 0
* w/v.liq w/v.vap w/v.int no of jun
7111301 6.38096-5 6.38538-5 0. 1 * .069567
7111302 6.38096-5 6.38538-5 0. 2 * .069567
7111303 6.38097-5 6.38538-5 0. 3 * .069567
7111304 6.38097-5 6.38538-5 0. 4 * .069567
*
-----
* Junction: H2O Passive DHR Heat Exchanger to HX Outlet (DHR2-Water)
-----

```

```

* name junction
7160000 h2hxohx sngljun
* from to area kforw kbackw j-flag
7160101 711010000 721000000 0.0 1.00 1.00 0000000
* cntrl w/v.liq w/v.vap w/v.int
7160201 0 7.98762-4 8.05366-4 0. * .069567
*
-----
* Passive H2O DHR Heat Exchanger Outlet Plenum (DHR2-Water)
*
* name volume
7210000 h2ooutpl snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
7210101 0.0873 1.0 0.0 90. 90. 0.2 4.5e-5 0.333 000000 $
* cntrl press temp
7210200 0 1079244. 104097.8 2583967. 0.
*
-----
* Junction: H2O DHR Heat Exchanger Outlet Plenum to UHS Duct (DHR2-Water)
*
* name junction
7260000 h2opld sngljun
* from to area kforw kbackw j-flag
7260101 721010000 731000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
7260201 0 7.98762-4 8.05366-4 0. * .069567
*
-----
* Passive DHR Hot Duct (DHR2-Water)
*
* name pipe/annulus
7310000 h2ohotd pipe
* number of volumes
7310001 5
* area no of vol
7310101 0.0873 5 $ lumping 2 loops
* length no of vol
7310301 1.6 5
* volume no of vol
7310401 0.0 5
* azi ang no of vol
7310501 90. 5
* ver ang no of vol
7310601 90. 5
* elev. no of vol
7310701 1.6 5
* rough dhydr. no of vol
7310801 4.5e-5 0.333 5
* kforw kbackw no of jun
7310901 0.0875 0.0875 4
* v-flag no of vol
7311001 00000 5
* j-flag no of jun
7311101 000000 4
* cntrl pressure temperature * * * no of vol
7311201 0 1070439. 104108.4 2583740. 0. 0. 1
7311202 0 1054786. 104120.5 2583334. 0. 0. 2
7311203 0 1039133. 104134. 2582923. 0. 0. 3
7311204 0 1023480. 104149.5 2582507. 0. 0. 4
7311205 0 1007826. 104168.6 2582086. 0. 0. 5
* cntrl
7311300 0
* w/v.liq w/v.vap w/v.int no of jun
7311301 7.98765-4 8.0537-4 0. 1 * .069567
7311302 7.98771-4 8.05375-4 0. 2 * .0695669
7311303 7.98776-4 8.05381-4 0. 3 * .0695668
7311304 7.98782-4 8.05387-4 0. 4 * .0695668
*
**
** Junction: Hotleg Duct to Pressure Controller (DHR2-Water)
**
** name type
7810000 htcd-orf sngljun
* from to area kforw kbackw j-flag
7810101 731010000 791000000 0 0.5 0.5 0000000
* cntrl w/v.liq w/v.vap w/v.int
7810201 0 -5.48151-9 -5.4809-9 0. * -4.67351-7
*
-----
** UHS LOOP Pressure Controller (DHR2-Water)
*
* name volume
7910000 h2osurge tmdpvol
* area length vol. a.ang. in.ang. elev. rough. hDe pvbfe
7910101 500.0 10.0 0.0 0.0 0.0 0. 0.00046 7.4 00010
* cntrl
7910200 003

```

```

*      press temp
7910201 0.0 1.00000e6 345.67
*-----
* Junction: HP Hot Duct to HX Inlet (DHR2-Water)
*-----
* name junction
7360000 h2ohxpin sngljun
* from to area kforw kbackw j-flag
7360101 731010000 741000000 0.0 0.75 0.75 0000001
* cntrl w/v.liq w/v.vap w/v.int
7360201 0 7.98793-4 7.98793-4 0. * .0695672
*-----
* Passive DHR Heat Exchanger Inlet (DHR2-Water)
*-----
* name volume
7410000 h2ohxin snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
7410101 0.0873 1.0 0.0 -90. -90. -0.5 4.5e-5 0.333 000000 $
* cntrl press temp
7410200 0 1002446. 104180.8 2581940. 0.
*-----
* Junction: Passive DHR HX Inlet to Heat Exchanger (DHR2-Water)
*-----
* name junction
7460000 h2ohx-h sngljun
* from to area kforw kbackw j-flag
7460101 741010000 751000000 0.0 0.23 0.23 0000000
* cntrl w/v.liq w/v.vap w/v.int
7460201 0 7.98795-4 7.98795-4 0. * .0695671
*-----
* Passive UHS DHR Heat Exchanger (DHR2-Water)
*-----
* name pipe/annulus
7510000 h2hp-hx pipe
* number of volumes
7510001 20
* area no of vol
7510101 9.46497e-2 20
* length no of vol
7510301 1.605 20
* volume no of vol
7510401 0.0 20
* azi ang no of vol
7510501 -90. 20
* ver ang no of vol
7510601 0.0 20
* elev. no of vol
7510701 0.0 20
* rough dhydr. no of vol
7510801 1.e-5 3.5052e-2 20
* kforw kbackw no of jun
7510901 0.0 0.0 19
* v-flag no of vol
7511001 00000 20
* j-flag no of jun
7511101 000000 19
* cntrl pressure temperature * * * no of vol
7511201 0 1004892. 104081.7 2582007. 0. 0. 1
7511202 0 1004892. 104063.2 2582007. 0. 0. 2
7511203 0 1004892. 104059.7 2582007. 0. 0. 3
7511204 0 1004892. 104059. 2582007. 0. 0. 4
7511205 0 1004891. 104058.8 2582007. 0. 0. 5
7511206 0 1004891. 104058.8 2582007. 0. 0. 6
7511207 0 1004891. 104058.8 2582007. 0. 0. 7
7511208 0 1004891. 104058.8 2582007. 0. 0. 8
7511209 0 1004891. 104058.8 2582007. 0. 0. 9
7511210 0 1004891. 104058.8 2582007. 0. 0. 10
7511211 0 1004891. 104058.8 2582007. 0. 0. 11
7511212 0 1004891. 104058.8 2582007. 0. 0. 12
7511213 0 1004891. 104058.8 2582007. 0. 0. 13
7511214 0 1004891. 104058.8 2582007. 0. 0. 14
7511215 0 1004891. 104058.8 2582007. 0. 0. 15
7511216 0 1004891. 104058.8 2582007. 0. 0. 16
7511217 0 1004891. 104058.8 2582007. 0. 0. 17
7511218 0 1004891. 104058.8 2582007. 0. 0. 18
7511219 0 1004891. 104058.8 2582007. 0. 0. 19
7511220 0 1004891. 104058.8 2582007. 0. 0. 20
* cntrl
7511300 0
* w/v.liq w/v.vap w/v.int no of jun
7511301 7.36762-4 7.36762-4 0. 1 * .0695671
7511302 7.36761-4 7.36761-4 0. 2 * .0695671
7511303 7.3676-4 7.3676-4 0. 3 * .0695671
7511304 7.3676-4 7.3676-4 0. 4 * .0695671
7511305 7.3676-4 7.3676-4 0. 5 * .0695671
7511306 7.3676-4 7.3676-4 0. 6 * .0695671

```

```

7511307 7.3676-4 7.3676-4 0. 7 * .0695671
7511308 7.3676-4 7.3676-4 0. 8 * .0695671
7511309 7.3676-4 7.3676-4 0. 9 * .0695671
7511310 7.3676-4 7.3676-4 0. 10 * .0695671
7511311 7.3676-4 7.3676-4 0. 11 * .0695671
7511312 7.3676-4 7.3676-4 0. 12 * .0695671
7511313 7.3676-4 7.3676-4 0. 13 * .0695671
7511314 7.3676-4 7.3676-4 0. 14 * .0695671
7511315 7.3676-4 7.3676-4 0. 15 * .0695671
7511316 7.3676-4 7.3676-4 0. 16 * .0695671
7511317 7.3676-4 7.3676-4 0. 17 * .0695671
7511318 7.3676-4 7.3676-4 0. 18 * .0695671
7511319 7.3676-4 7.3676-4 0. 19 * .0695671
*
*-----*
* Junction: UHS Passive DHR Heat Exchanger to HX Outlet
*-----*
* name junction
7560000 h2hx-ohx sngljun
* from to area kforw kbackw j-flag
7560101 751010000 761000000 0.0 1.00 1.00 0000000
* cntrl w/v.liq w/v.vap w/v.int
7560201 0 7.98788-4 7.98788-4 0. * .0695671
*
*-----*
* Passive UHS DHR Heat Exchanger Outlet Plenum
*-----*
* name volume
7610000 h2-outpl snglvol
* area length vol. a.ang. in.ang. elev. rough. hDe v-flag
7610101 0.0873 1.0 0.0 -90. -90. -0.5 4.5e-5 0.333 000000 $
* cntrl press temp
7610200 0 1007337. 104058.8 2582073. 0.
*
*-----*
* Junction: Passive DHR HX Outlet to Downcomer
*-----*
* name junction
7660000 hhp-ohx sngljun
* from to area kforw kbackw j-flag
7660101 761010000 771000000 0.0 1.0 1.0 0000000
* cntrl w/v.liq w/v.vap w/v.int
7660201 0 7.98787-4 8.05391-4 0. * .0695671
*
*-----*
* Passive DHR Downcomer
*-----*
* name pipe/annulus
7710000 h2ohotd pipe
* number of volumes
7710001 5
* area no of vol
7710101 0.0873 5 $ lumping 2 loops
* length no of vol
7710301 1.6 5
* volume no of vol
7710401 0.0 5
* azi ang no of vol
7710501 -90. 5
* ver ang no of vol
7710601 -90. 5
* elev. no of vol
7710701 -1.6 5
* rough dhydr. no of vol
7710801 4.5e-5 0.333 5
* kforw kbackw no of jun
7710901 0.0875 0.0875 4
* v-flag no of vol
7711001 00000 5
* j-flag no of jun
7711101 00000 4
* cntrl pressure temperature * * * no of vol
7711201 0 1017609. 104058.8 2582350. 0. 0. 1
7711202 0 1033263. 104058.8 2582768. 0. 0. 2
7711203 0 1048916. 104058.8 2583181. 0. 0. 3
7711204 0 1064569. 104058.8 2583589. 0. 0. 4
7711205 0 1080223. 104058.9 2583992. 0. 0. 5
* cntrl
7711300 0
* w/v.liq w/v.vap w/v.int no of jun
7711301 7.98783-4 8.05388-4 0. 1 * .0695671
7711302 7.98778-4 8.05382-4 0. 2 * .0695671
7711303 7.98772-4 8.05376-4 0. 3 * .0695671
7711304 7.98766-4 8.05371-4 0. 4 * .0695671
*
*-----*
* SNGLJ: Passive DHR Cold Duct to Rx Inlet Plenum
*-----*
* name junction

```

```

7760000 cd-iplm sngljun
* from to area kforw kbackw j-flag
7760101 771010000 701000000 0.0 1.0 1.0 0000001
* cntrl w/v.liq w/v.vap w/v.int
7760201 0 7.98761-4 7.98761-4 0. * .0695671
*

```

```

*
*****
*
* HEAT STRUCTURE COMPONENTS *
*
*****
*-----
* RPV Downcomer (Cylinder) #1 *
* # Wall thickness: 0.014m *
*-----
* # -HS # -MP geotype SS-ini L-coord. reflood bvol-ind axial#
16701000 8 10 2 0 4.0
* mesh-loc format-flag
16701100 0 1
* # -Intvl R-coord. (radial info.)
16701101 9 4.19
* comp-# interval-# (radial info.)
16701201 6 9
* source interval-# (radial info.)
16701301 0.0 9
* initial temperature flag (if flag=0 or -1)
16701400 -1
* temp-1 temp-2 temp-3 temp-4 temp-5 temp-6 temp-7 temp-8 temp-9 temp-1
16701401 740.49 740.50 740.50 740.50 740.50 740.50 740.51 740.51 740.51 740.51
16701402 740.50 740.51 740.51 740.51 740.52 740.52 740.52 740.52 740.53 740.53
16701403 740.51 740.52 740.52 740.53 740.53 740.54 740.54 740.54 740.55 740.55
16701404 740.52 740.53 740.54 740.54 740.55 740.56 740.56 740.56 740.57 740.57
16701405 740.53 740.54 740.55 740.55 740.56 740.57 740.57 740.58 740.58 740.59 740.59
16701406 740.54 740.55 740.56 740.57 740.58 740.59 740.60 740.60 740.60 740.61
16701407 740.55 740.56 740.58 740.58 740.59 740.60 740.61 740.62 740.62 740.62
16701408 740.56 740.57 740.59 740.60 740.61 740.62 740.63 740.64 740.64 740.64
* L-B B.Vol.# increment BC option surf.code height NH
16701501 670010000 10000 160 1 1.05625 8
* R-B B.Vol.# increment BC option surf.code height NH
16701601 0 0 0 1 1.05625 8 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16701701 0 0. 0. 0. 8
* 9-words format option
16701800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16701801 8.000 0.528125 20. 0. 0. 0. 0. 1. 1
16701802 8.000 1.584375 20. 0. 0. 0. 0. 1. 2
16701803 8.000 2.640625 20. 0. 0. 0. 0. 1. 3
16701804 8.000 3.696875 20. 0. 0. 0. 0. 1. 4
16701805 8.000 4.753125 20. 0. 0. 0. 0. 1. 5
16701806 8.000 5.809375 20. 0. 0. 0. 0. 1. 6
16701807 8.000 6.865625 20. 0. 0. 0. 0. 1. 7
16701808 8.000 7.921875 20. 0. 0. 0. 0. 1. 8
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16701901 8.380 0.528125 20. 0. 0. 0. 0. 1. 1
16701902 8.380 1.584375 20. 0. 0. 0. 0. 1. 2
16701903 8.380 2.640625 20. 0. 0. 0. 0. 1. 3
16701904 8.380 3.696875 20. 0. 0. 0. 0. 1. 4
16701905 8.380 4.753125 20. 0. 0. 0. 0. 1. 5
16701906 8.380 5.809375 20. 0. 0. 0. 0. 1. 6
16701907 8.380 6.865625 20. 0. 0. 0. 0. 1. 7
16701908 8.380 7.921875 20. 0. 0. 0. 0. 1. 8
*
*-----
* RPV Downcomer (Cylinder) #2 *
* # Wall thickness: 0.014m *
*-----
* # -HS # -MP geotype SS-ini L-coord. reflood bvol-ind axial#
18001000 8 10 2 0 4.0
* mesh-loc format-flag
18001100 0 1
* # -Intvl R-coord. (radial info.)
18001101 9 4.19
* comp-# interval-# (radial info.)
18001201 6 9
* source interval-# (radial info.)
18001301 0.0 9

```



```

*   initial temperature flag (if flag=0 or -1)
18001400 -1
*   temp-1 temp-2 temp-3 temp-4 temp-5 temp-6 temp-7 temp-8 temp-9 temp-1
18001401 740.49 740.50 740.50 740.50 740.50 740.50 740.51 740.51 740.51 740.51
18001402 740.50 740.51 740.51 740.51 740.52 740.52 740.52 740.53 740.53 740.53
18001403 740.51 740.52 740.52 740.53 740.53 740.54 740.54 740.54 740.55 740.55
18001404 740.52 740.53 740.54 740.54 740.54 740.55 740.56 740.56 740.57 740.57
18001405 740.53 740.54 740.55 740.56 740.57 740.57 740.58 740.58 740.59 740.59
18001406 740.54 740.55 740.56 740.57 740.58 740.59 740.60 740.60 740.60 740.61
18001407 740.55 740.56 740.58 740.59 740.60 740.61 740.62 740.62 740.62 740.62
18001408 740.56 740.57 740.59 740.60 740.61 740.62 740.63 740.64 740.64 740.64
* L-B B.Vol.# increment BC option surf.code height NH
18001501 800010000 10000 160 1 1.05625 8
* R-B B.Vol.# increment BC option surf.code height NH
18001601 0 0 0 1 1.05625 8 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
18001701 0 0. 0. 0. 8
*   9-words format option
18001800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
18001801 8.000 0.528125 20. 0. 0. 0. 0. 1. 1
18001802 8.000 1.584375 20. 0. 0. 0. 0. 1. 2
18001803 8.000 2.640625 20. 0. 0. 0. 0. 1. 3
18001804 8.000 3.696875 20. 0. 0. 0. 0. 1. 4
18001805 8.000 4.753125 20. 0. 0. 0. 0. 1. 5
18001806 8.000 5.809375 20. 0. 0. 0. 0. 1. 6
18001807 8.000 6.865625 20. 0. 0. 0. 0. 1. 7
18001808 8.000 7.921875 20. 0. 0. 0. 0. 1. 8
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
18001901 8.380 0.528125 20. 0. 0. 0. 0. 1. 1
18001902 8.380 1.584375 20. 0. 0. 0. 0. 1. 2
18001903 8.380 2.640625 20. 0. 0. 0. 0. 1. 3
18001904 8.380 3.696875 20. 0. 0. 0. 0. 1. 4
18001905 8.380 4.753125 20. 0. 0. 0. 0. 1. 5
18001906 8.380 5.809375 20. 0. 0. 0. 0. 1. 6
18001907 8.380 6.865625 20. 0. 0. 0. 0. 1. 7
18001908 8.380 7.921875 20. 0. 0. 0. 0. 1. 8
*
*-----
* Inlet Plenum (Cylinder) *
* # Wall thickness: 0.004m *
*-----
* #HS #MP geotype SS-ini L-coord. reflood bvol-ind axial#
11001000 5 5 2 0 0.0
* mesh-loc format-flag
11001100 0 1
* #-Intvl R-coord. (radial info.)
11001101 4 0.075
* comp-# interval-# (radial info.)
11001201 6 4
* source value interval-# (radial info.)
11001301 0.0 4
*   initial temperature flag (if flag=0 or -1)
11001400 -1
*   temp-1 temp-2 temp-3 temp-4 temp-5
11001401 740.50 740.50 740.50 740.50 740.50
11001402 740.50 740.50 740.50 740.50 740.50
11001403 740.50 740.50 740.50 740.50 740.50
11001404 740.50 740.50 740.50 740.50 740.50
11001405 740.50 740.50 740.50 740.50 740.50
* L-B B.Vol.# increment BC option surf.code height NH
11001501 0 0 0 1 0.2 5 * Insulate
* R-B B.Vol.# increment BC option surf.code height NH
11001601 100010000 10000 160 1 0.2 5
* Source source-type multiplier DHeat-Left DHeat-Right NH
11001701 0 0. 0. 0. 5
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
11001901 0.150 0.1 20. 0. 0. 0. 0. 1. 1
11001902 0.150 0.3 20. 0. 0. 0. 0. 1. 2
11001903 0.150 0.5 20. 0. 0. 0. 0. 1. 3
11001904 0.150 0.7 20. 0. 0. 0. 0. 1. 4
11001905 0.150 0.9 20. 0. 0. 0. 0. 1. 5
*-----
* Lower Reflector-Entrance of Core Average Channel (Plate)
*-----
* #HS #MP geotype SS-ini L-coord. reflood bvol-ind axial#
12101000 1 3 1 0 0.0
* mesh-loc format-flag
12101100 0 1
* #-Intvl R-coord. (radial info.)
12101101 2 0.002655
* comp-# interval-# (radial info.)
12101201 13 2
* source value interval-# (radial info.)
12101301 0.0 2
*   initial temperature flag (if flag=0 or -1)
12101400 -1
*   temp-1 temp-2 temp-3

```

```

12101401 740.62 740.62 740.62
* L-B B.Vol.# increment BC option surf.code area NH
12101501 0 0 0 1 439.62 1 * Insulat
* R-B B.Vol.# increment BC option surf.code area NH
12101601 210010000 10000 160 1 439.62 1
* Source source-type multiplier DHeat-Left DHeat-Right NH
12101701 0 0. 0. 0. 1
* 9-words format option
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
12101901 0.0127 0.5 20. 0. 0. 0. 0. 1. 1
*
*-----
* Lower Reflector-Entrance of Core Hot Channel (Plate)
*-----
* #HS #MP geotype SS-ini L-coord. reflod bvol-ind axial#
12111000 1 3 1 0 0.0
* mesh-loc format-flag
12111100 0 1
* #-Intvl R-coord. (radial info.)
12111101 2 0.002655
* comp-# interval-# (radial info.)
12111201 13 2
* source value interval-# (radial info.)
12111301 0.0 2
* initial temperature flag (if flag=0 or -1)
12111400 -1
* temp-1 temp-2 temp-3
12111401 740.62 740.62 740.62
* L-B B.Vol.# increment BC option surf.code area NH
12111501 0 0 0 1 3.9581195 1 * Insula
* R-B B.Vol.# increment BC option surf.code area NH
12111601 211010000 10000 160 1 3.9581195 1
* Source source-type multiplier DHeat-Left DHeat-Right NH
12111701 0 0. 0. 0. 1
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
12111901 0.0127 0.5 20. 0. 0. 0. 0. 1. 1
*
*-----
* MATRIX CORE HEAT STRUCTURES: Average Channel (Plate)
*-----
* #HS #MP geotype SS-ini L-coord. reflod bvol-ind axial#
12501000 8 8 1 0 0.0
* mesh-loc format-flag
12501100 0 1
* #-Intvl R-coord. (radial info.)
12501101 6 0.002355 * 1/2 fuel plate dimension
12501102 1 0.002655 * coating thickn dimension
* comp-# interval-# (radial info.)
12501201 1 6 $ UO2
12501202 -13 7 $ Ferritic SS
* source interval-# (radial info.)
12501301 1.0 6
12501302 0.0 7
* initial temperature flag (if flag=0 or -1)
12501400 -1
* temp. mesh point
12501401 934.97 934.24 932.06 928.42 923.33 916.78 908.77 899.31
12501402 1063.8 1062.8 1059.8 1054.8 1047.8 1038.7 1027.7 1014.6
12501403 1172.9 1171.7 1168.1 1162.1 1153.7 1142.9 1129.8 1114.0
12501404 1257.0 1255.8 1251.9 1245.4 1236.4 1224.7 1210.5 1193.4
12501405 1311.0 1309.7 1305.8 1299.4 1290.4 1278.8 1264.6 1247.5
12501406 1332.3 1331.1 1327.5 1321.6 1313.3 1302.7 1289.6 1273.9
12501407 1321.2 1320.2 1317.2 1312.3 1305.4 1296.5 1285.6 1272.5
12501408 1280.3 1279.6 1277.4 1273.8 1268.9 1262.4 1254.6 1245.1
* L-B B.Vol.# increment BC option surf.code surface area NH
12501501 0 0 0 1 107.159 8
* R-B B.Vol.# increment BC option surf.code surface area NH
12501601 250010000 10000 160 1 107.159 8
** Source source-type multiplier DHeat-Left DHeat-Right NH
$ 1.25 chopped cosine shape $ He Core
12501701 1000 0.0844607 0. 0. 1
12501702 1000 0.1171673 0. 0. 2
12501703 1000 0.1405377 0. 0. 3
12501704 1000 0.1527072 0. 0. 4
12501705 1000 0.1527072 0. 0. 5
12501706 1000 0.1405377 0. 0. 6
12501707 1000 0.1171673 0. 0. 7
12501708 1000 0.0844607 0. 0. 8
*
12501900 1
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
12501901 0.0127 0.121875 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 1
12501902 0.0127 0.365625 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 2
12501903 0.0127 0.609375 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 3
12501904 0.0127 0.853125 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 4
12501905 0.0127 1.096875 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 5
12501906 0.0127 1.340625 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 6
12501907 0.0127 1.584375 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 7

```

```

12501908 0.0127 1.828125 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 8
*-----*
* MATRIX CORE HEAT STRUCTURES: Hot Channel (Plate) *
*-----*
* #HS #MP geotype SS-ini L-coord. reflood bvol-ind axial#
12511000 8 8 1 0 0.00
* mesh-loc format-flag
12511100 0 1
* #-Intvl R-coord. (radial info.)
12511101 6 0.002355 * 1/2 fuel plate dimension
12511102 1 0.002655 * coating thckn dimension
* comp-# interval-# (radial info.)
12511201 1 6 $ UO2
12511202 -13 7 $ Ferritic SS
* source interval-# (radial info.)
12511301 1.0 6
12511302 0.0 7
* initial temperature flag (if flag=0 or -1)
12511400 -1
* temp. mesh point
12511401 968.50 967.67 965.17 960.99 955.15 947.64 938.45 927.57
12511402 1120.2 1119.0 1115.6 1109.8 1101.7 1091.4 1078.7 1063.6
12511403 1247.7 1246.4 1242.3 1235.4 1225.8 1213.5 1198.4 1180.3
12511404 1345.6 1344.1 1339.7 1332.3 1322.0 1308.7 1292.4 1272.7
12511405 1407.8 1406.4 1401.9 1394.6 1384.3 1371.0 1354.8 1335.1
12511406 1431.9 1430.6 1426.5 1419.8 1410.3 1398.1 1383.2 1365.1
12511407 1418.6 1417.5 1414.1 1408.5 1400.6 1390.4 1378.0 1362.9
12511408 1371.0 1370.2 1367.8 1363.7 1358.0 1350.6 1341.6 1330.8
* L-B B.Vol.# increment BC option surf.code surface area NH
12511501 0 0 0 1 0.965395 8
* R-B B.Vol.# increment BC option surf.code surface area NH
12511601 251010000 10000 160 1 0.965395 8
** Source source-type multiplier DHeat-Left DHeat-Right NH
$ 1.25 chopped cosine shape $ He Core
12511701 1000 0.0008750 0. 0. 1
12511702 1000 0.0012139 0. 0. 2
12511703 1000 0.0014560 0. 0. 3
12511704 1000 0.0015821 0. 0. 4
12511705 1000 0.0015821 0. 0. 5
12511706 1000 0.0014560 0. 0. 6
12511707 1000 0.0012139 0. 0. 7
12511708 1000 0.0008750 0. 0. 8
*
12511900 1
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
12511901 0.0127 0.121875 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 1
12511902 0.0127 0.365625 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 2
12511903 0.0127 0.609375 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 3
12511904 0.0127 0.853125 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 4
12511905 0.0127 1.096875 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 5
12511906 0.0127 1.340625 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 6
12511907 0.0127 1.584375 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 7
12511908 0.0127 1.828125 20. 0. 0. 0. 0. 1. 0.0 1.1 1.12354 8
*-----*
* reactor kinetics data *
* - ANS 79 Decay Heat Model used *
*-----*
30000000 point separabl
30000001 gamma-ac 600.0e6 0. 352.11268 1.0
30000002 ans79-1 200.0
30000011 100 * scram curve
* Density reactivity feedback
30000501 0. 0.0
30000502 1000. 0.0
*
30000601 100. 0.0
30000602 3000. 0.0
* Doppler reactivity feedback
*
* Volume weighting factor
*
* For transient calculation, the following data should be used
* instead of cards 30000801 - 820
* by SIL
*
*30000801 1701001 0 0.02365 -0.000859212
*30000802 1701002 0 0.031328 -0.000859212
*30000803 1701003 0 0.038502 -0.000997298
*30000804 1701004 0 0.045054 -0.000997298
*30000805 1701005 0 0.050881 -0.001072738
*30000806 1701006 0 0.055887 -0.001072738
*30000807 1701007 0 0.059993 -0.001072738
*30000808 1701008 0 0.063131 -0.001253016
*30000809 1701009 0 0.065252 -0.001253016
*30000810 1701010 0 0.066322 -0.001253016
*30000811 1701011 0 0.066322 -0.000722406
*30000812 1701012 0 0.065252 -0.000722406

```

```

*30000813 1701013 0 0.063131 -0.000722406
*30000814 1701014 0 0.059993 -0.000784413
*30000815 1701015 0 0.055887 -0.000784413
*30000816 1701016 0 0.050881 -0.000784413
*30000817 1701017 0 0.045054 -0.000746697
*30000818 1701018 0 0.038502 -0.000746697
*30000819 1701019 0 0.031328 -0.00052422
*30000820 1701020 0 0.02365 -0.00052422
*
-----*
* scram table *
-----*
*
20210000 reac-t 501
20210001 0.0 0.0
20210002 1.98 -0.052667
20210003 2.31 -0.158001
20210004 2.64 -0.421300
20210005 2.97 -0.974300
20210006 3.30 -2.212000
20210007 3.63 -4.371400
20210008 3.96 -5.029700
20210009 4.29 -5.266700
20210010 2.0e20 -5.266700
*
-----*
* Lower Reflector-Entrance of Core Average Channel (Plate)
-----*
* #-HS #-MP geotype SS-ini L-coord. reflod bvol-ind axial#
12901000 1 3 1 0 0.0
* mesh-loc format-flag
12901100 0 1
* #-Intvl R-coord. (radial info.)
12901101 2 0.002655
* comp-# interval-# (radial info.)
12901201 13 2
* source value interval-# (radial info.)
12901301 0.0 2
* initial temperature flag (if flag=0 or -1)
12901400 -1
* temp-1 temp-2 temp-3
12901401 1105.6 1105.6 1105.6
* L-B B.Vol.# increment BC option surf.code area NH
12901501 0 0 0 1 439.62 1 * Zero hea
* R-B B.Vol.# increment BC option surf.code area NH
12901601 290010000 10000 160 1 439.62 1
* Source source-type multiplier DHeat-Left DHeat-Right NH
12901701 0 0. 0. 0. 1
* 9-words format option
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
12901901 0.0127 0.5 20. 0. 0. 0. 0. 1. 1
*
-----*
* Lower Reflector-Entrance of Core Hot Channel (Plate)
-----*
* #-HS #-MP geotype SS-ini L-coord. reflod bvol-ind axial#
12911000 1 3 1 0 0.0
* mesh-loc format-flag
12911100 0 1
* #-Intvl R-coord. (radial info.)
12911101 2 0.002655
* comp-# interval-# (radial info.)
12911201 13 2
* source value interval-# (radial info.)
12911301 0.0 2
* initial temperature flag (if flag=0 or -1)
12911400 -1
* temp-1 temp-2 temp-3
12911401 1168.8 1168.8 1168.8
* L-B B.Vol.# increment BC option surf.code area NH
12911501 0 0 0 1 3.9581195 1 * Zero
* R-B B.Vol.# increment BC option surf.code area NH
12911601 291010000 10000 160 1 3.9581195 1
* Source source-type multiplier DHeat-Left DHeat-Right NH
12911701 0 0. 0. 0. 1
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
12911901 0.0127 0.5 20. 0. 0. 0. 0. 1. 1
*****
* ***** STRUCTURE 5201 *****
* Recuperator -- plate-fin
-----*
*ht str ht.strs m.pts geom init l.coord refl b.vol ax.incr.
15201000 30 3 1 1 0.0 0
*
* loc flag
15201100 0 1
*

```

```

* # r
15201101 2 0.0004572
* compos. #
15201201 15 2
* source #
15201301 0.0 2
* temperature flag
15201400 -1
* temperature #
15201401 742.40 742.29
15201402 730.64 730.53
15201403 718.84 718.73
15201404 707.00 706.89
15201405 695.13 694.90
15201406 683.11 683.00
15201407 671.28 671.17
15201408 659.31 659.22
15201409 647.31 647.19
15201410 635.28 635.16
15201411 623.21 623.09
15201412 611.13 611.00
15201413 599.01 598.89
15201414 586.87 586.75
15201415 574.71 574.58
15201416 562.53 562.44
15201417 550.33 550.27
15201418 538.11 537.98
15201419 525.88 525.74
15201420 513.63 513.55
15201421 501.38 501.24
15201422 489.12 488.98
15201423 476.85 476.71
15201424 464.58 464.44
15201425 452.32 452.17
15201426 440.05 439.75
15201427 427.8 427.65
15201428 415.55 415.45
15201429 403.33 403.17
15201430 391.12 390.96
* vol inc type code factor #
15201501 520010000 10000 160 0 2192.0 30
* vol inc type code factor #
15201601 590300000 -10000 160 0 2192.0 30
* type mult D-It # source
15201701 0 0.0 0.0 30
*
15201800 1
* Dhe LHRF LHRF LGSF LGSF Krev Rboil nclF pvd ff #
15201801 2.7-4 0.047 2.768 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.1
15201802 2.7-4 0.141 2.674 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.2
15201803 2.7-4 0.235 2.581 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.3
15201804 2.7-4 0.328 2.487 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.4
15201805 2.7-4 0.422 2.393 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.5
15201806 2.7-4 0.516 2.299 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.6
15201807 2.7-4 0.610 2.205 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.7
15201808 2.7-4 0.704 2.111 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.8
15201809 2.7-4 0.798 2.018 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.9
15201810 2.7-4 0.891 1.924 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.10
15201811 2.7-4 0.985 1.830 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.11
15201812 2.7-4 1.079 1.736 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.12
15201813 2.7-4 1.173 1.642 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.13
15201814 2.7-4 1.267 1.548 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.14
15201815 2.7-4 1.361 1.455 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.15
15201816 2.7-4 1.455 1.361 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.16
15201817 2.7-4 1.548 1.267 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.17
15201818 2.7-4 1.642 1.173 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.18
15201819 2.7-4 1.736 1.079 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.19
15201820 2.7-4 1.830 0.985 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.20
15201821 2.7-4 1.924 0.891 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.21
15201822 2.7-4 2.018 0.798 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.22
15201823 2.7-4 2.111 0.704 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.23
15201824 2.7-4 2.205 0.610 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.24
15201825 2.7-4 2.299 0.516 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.25
15201826 2.7-4 2.393 0.422 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.26
15201827 2.7-4 2.487 0.328 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.27
15201828 2.7-4 2.581 0.235 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.28
15201829 2.7-4 2.674 0.141 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.29
15201830 2.7-4 2.768 0.047 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1.30
15201900 1

```

```

*   Dhe LHEF LHEr LGSf LGSr Kfwd Krev Fboil nclf povd ff #
15201901 2.4-4 2.768 0.047 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 1
15201902 2.4-4 2.674 0.141 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 2
15201903 2.4-4 2.581 0.235 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 3
15201904 2.4-4 2.487 0.328 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 4
15201905 2.4-4 2.393 0.422 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 5
15201906 2.4-4 2.299 0.516 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 6
15201907 2.4-4 2.205 0.610 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 7
15201908 2.4-4 2.111 0.704 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 8
15201909 2.4-4 2.018 0.798 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 9
15201910 2.4-4 1.924 0.891 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 10
15201911 2.4-4 1.830 0.985 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 11
15201912 2.4-4 1.736 1.079 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 12
15201913 2.4-4 1.642 1.173 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 13
15201914 2.4-4 1.548 1.267 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 14
15201915 2.4-4 1.455 1.361 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 15
15201916 2.4-4 1.361 1.455 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 16
15201917 2.4-4 1.267 1.548 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 17
15201918 2.4-4 1.173 1.642 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 18
15201919 2.4-4 1.079 1.736 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 19
15201920 2.4-4 0.985 1.830 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 20
15201921 2.4-4 0.891 1.924 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 21
15201922 2.4-4 0.798 2.018 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 22
15201923 2.4-4 0.704 2.111 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 23
15201924 2.4-4 0.610 2.205 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 24
15201925 2.4-4 0.516 2.299 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 25
15201926 2.4-4 0.422 2.393 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 26
15201927 2.4-4 0.328 2.487 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 27
15201928 2.4-4 0.235 2.581 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 28
15201929 2.4-4 0.141 2.674 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 29
15201930 2.4-4 0.047 2.768 10.0 10.0 0.0 0.0 1.0 2.815 1.0 1. 30
*
*
***** COMPOSITION 15*****
* thermal properties of GA design
* distortion in heatric pche
*****$
20101500 tbl/fctn 1 1
*-----*
20101501 2.232611E+02 1.058900E+01
20101502 2.942611E+02 1.158900E+01
20101503 4.220389E+02 1.383203E+01
20101504 5.331500E+02 1.570122E+01
20101505 6.442611E+02 1.744581E+01
20101506 6.998167E+02 1.831810E+01
20101507 8.109278E+02 2.006268E+01
20101508 8.664833E+02 2.093497E+01
20101509 1.255372E+03 2.990710E+01
20101510 1.922039E+03 2.990710E+01
*
20101551 2.002611E+02 3.143784E+06
20101552 2.942611E+02 3.433784E+06
20101553 9.775944E+02 4.694627E+06
20101554 1.922039E+03 4.694627E+06
*
*
***** STRUCTURE 5301 *****
* precoolers -- tube/shell hx
*****$
*ht str ht.strs m.pts geom init l.coord refl b.vol ax.incr.
15301000 20 5 2 1 0.0033 0
*
* loc flag
15301100 0 1
*
* # r
15301101 4 0.0045
*
* compos. #
15301201 16 4
*
* source #
15301301 0.0 4
*
* temperature flag
15301400 -1
*
* temperature #
15301401 324.69 325.27 325.80 326.30 326.76
15301402 320.35 320.86 321.32 321.75 322.15
15301403 316.58 317.02 317.43 317.80 318.15
15301404 313.31 313.69 314.04 314.37 314.67
15301405 310.46 310.80 311.10 311.38 311.65
15301406 307.99 308.28 308.54 308.79 309.02
15301407 305.83 306.08 306.32 306.53 306.73
15301408 303.95 304.17 304.37 304.56 304.74
15301409 302.32 302.51 302.68 302.85 303.00

```

15301410	300.89	301.06	301.21	301.35	301.48
15301411	299.65	299.79	299.92	300.05	300.16
15301412	298.56	298.69	298.80	298.91	299.01
15301413	297.62	297.73	297.83	297.92	298.01
15301414	296.79	296.89	296.98	297.06	297.13
15301415	296.07	296.16	296.23	296.30	296.37
15301416	295.45	295.52	295.59	295.65	295.71
15301417	294.90	294.97	295.02	295.08	295.13
15301418	294.43	294.48	294.53	294.58	294.62
15301419	294.02	294.06	294.11	294.15	294.19
15301420	293.66	293.70	293.74	293.77	293.80

```

*
* vol inc type code factor #
15301501 133200000 -10000 1 1 35500. 20

```

```

*
* vol inc type code factor #
15301601 530010000 10000 1 1 35500. 20

```

```

*
* type mult D-lt D-rt # *source
15301701 0 0.0 0.0 0.0 20

```

```

15301800 1
* Dhe LHEf LHEr LGSf LGSr Kfwd Krev Fboil nclf povd ff #
15301801 0.003394 4.612 0.118 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 1
15301802 0.003394 4.375 0.355 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 2
15301803 0.003394 4.139 0.591 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 3
15301804 0.003394 3.902 0.828 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 4
15301805 0.003394 3.666 1.064 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 5
15301806 0.003394 3.429 1.301 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 6
15301807 0.003394 3.193 1.537 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 7
15301808 0.003394 2.956 1.774 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 8
15301809 0.003394 2.720 2.010 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 9
15301810 0.003394 2.483 2.247 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 10
15301811 0.003394 2.247 2.483 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 11
15301812 0.003394 2.010 2.720 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 12
15301813 0.003394 1.774 2.956 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 13
15301814 0.003394 1.537 3.193 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 14
15301815 0.003394 1.301 3.429 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 15
15301816 0.003394 1.064 3.666 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 16
15301817 0.003394 0.828 3.902 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 17
15301818 0.003394 0.591 4.139 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 18
15301819 0.003394 0.355 4.375 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 19
15301820 0.003394 0.118 4.612 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 20

```

```

15301900 1
* Dhe LHEf LHEr LGSf LGSr Kfwd Krev Fboil nclf povd ff #
15301901 0.003394 0.118 4.612 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 1
15301902 0.003394 0.355 4.375 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 2
15301903 0.003394 0.591 4.139 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 3
15301904 0.003394 0.828 3.902 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 4
15301905 0.003394 1.064 3.666 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 5
15301906 0.003394 1.301 3.429 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 6
15301907 0.003394 1.537 3.193 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 7
15301908 0.003394 1.774 2.956 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 8
15301909 0.003394 2.010 2.720 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 9
15301910 0.003394 2.247 2.483 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 10
15301911 0.003394 2.483 2.247 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 11
15301912 0.003394 2.720 2.010 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 12
15301913 0.003394 2.956 1.774 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 13
15301914 0.003394 3.193 1.537 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 14
15301915 0.003394 3.429 1.301 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 15
15301916 0.003394 3.666 1.064 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 16
15301917 0.003394 3.902 0.828 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 17
15301918 0.003394 4.139 0.591 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 18
15301919 0.003394 4.375 0.355 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 19
15301920 0.003394 4.612 0.118 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 20

```

***** COMPOSITION 16*****

```

* thermal properties of ss-316 modified to compensate for volume
* distortion in heatric pche

```

```

*-----$
20101600 tbl/fctn 1 1 * ss-316

```

```

-----
20101601 283.15 13.70
20101602 310.93 14.14
20101603 533.15 17.63
20101604 699.82 20.24
20101605 810.93 21.99
20101606 1088.71 26.35

```

```

*
20101651 283.15 3.115e06 * divided by 1.140
20101652 310.93 3.237e06
20101653 533.15 3.733e06
20101654 699.82 3.865e06
20101655 810.93 3.958e06
20101656 1088.71 4.309e06

```

```

*
*
***** STRUCTURE 5701 *****
* Inter-cooler -- tube/shell hx
*-----$
*ht str ht.strs m.pts geom init l.coord refl b.vol ax.incr.
15701000 20 5 2 1 0.0033 0
*
*   loc flag
15701100 0 1
*
*   #   r
15701101 4 0.0045
*
*   compos. #
15701201 16 4
*
*   source #
15701301 0.0 4
*
*   temperature flag
15701400 -1
*
*   temperature #
15701401 326.30 326.77 327.19 327.59 327.96
15701402 322.39 322.81 323.19 323.55 323.87
15701403 318.91 319.28 319.62 319.94 320.23
15701404 315.79 316.13 316.43 316.71 316.98
15701405 313.01 313.31 313.58 313.84 314.07
15701406 310.53 310.80 311.04 311.27 311.48
15701407 308.31 308.55 308.77 308.97 309.16
15701408 306.32 306.54 306.73 306.92 307.09
15701409 304.55 304.74 304.92 305.08 305.23
15701410 302.96 303.13 303.29 303.43 303.57
15701411 301.54 301.69 301.83 301.96 302.08
15701412 300.26 300.40 300.53 300.64 300.75
15701413 299.12 299.25 299.36 299.46 299.56
15701414 298.10 298.21 298.31 298.41 298.50
15701415 297.19 297.29 297.38 297.46 297.54
15701416 296.37 296.46 296.54 296.62 296.69
15701417 295.64 295.72 295.79 295.86 295.92
15701418 294.98 295.06 295.12 295.18 295.24
15701419 294.40 294.46 294.52 294.57 294.62
15701420 293.87 293.93 293.98 294.03 294.07
*
*   vol inc type code factor #
15701501 143200000 -10000 1 1 32000. 20
*
*   vol inc type code factor #
15701601 570010000 10000 1 1 32000. 20
*
*   type mult D-lt D-rt # *source
15701701 0 0.0 0.0 0.0 20
*
15701800 1
*   Dhe LHEf LHEr LGSf LGSr Kfwd Krev Fboil nclf povd ff #
15701801 0.003394 4.612 0.118 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 1
15701802 0.003394 4.375 0.355 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 2
15701803 0.003394 4.139 0.591 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 3
15701804 0.003394 3.902 0.828 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 4
15701805 0.003394 3.666 1.064 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 5
15701806 0.003394 3.429 1.301 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 6
15701807 0.003394 3.193 1.537 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 7
15701808 0.003394 2.956 1.774 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 8
15701809 0.003394 2.720 2.010 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 9
15701810 0.003394 2.483 2.247 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 10
15701811 0.003394 2.247 2.483 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 11
15701812 0.003394 2.010 2.720 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 12
15701813 0.003394 1.774 2.956 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 13
15701814 0.003394 1.537 3.193 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 14
15701815 0.003394 1.301 3.429 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 15
15701816 0.003394 1.064 3.666 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 16
15701817 0.003394 0.828 3.902 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 17
15701818 0.003394 0.591 4.139 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 18
15701819 0.003394 0.355 4.375 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 19
15701820 0.003394 0.118 4.612 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 20
*
15701900 1
*   Dhe LHEf LHEr LGSf LGSr Kfwd Krev Fboil nclf povd ff #
15701901 0.003394 0.118 4.612 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 1
15701902 0.003394 0.355 4.375 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 2
15701903 0.003394 0.591 4.139 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 3
15701904 0.003394 0.828 3.902 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 4
15701905 0.003394 1.064 3.666 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 5
15701906 0.003394 1.301 3.429 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 6
15701907 0.003394 1.537 3.193 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 7
15701908 0.003394 1.774 2.956 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 8

```



```

15701909 0.003394 2.010 2.720 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 9
15701910 0.003394 2.247 2.483 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 10
15701911 0.003394 2.483 2.247 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 11
15701912 0.003394 2.720 2.010 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 12
15701913 0.003394 2.956 1.774 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 13
15701914 0.003394 3.193 1.537 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 14
15701915 0.003394 3.429 1.301 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 15
15701916 0.003394 3.666 1.064 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 16
15701917 0.003394 3.902 0.828 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 17
15701918 0.003394 4.139 0.591 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 18
15701919 0.003394 4.375 0.355 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 19
15701920 0.003394 4.612 0.118 10.0 10.0 0.0 0.0 1.0 4.73 1.0 1.1 20
*
*
*-----*
* Hot Leg Duct of Passive DHR System 1 (Cylinder):Wall Thickness (0.027m)
*-----*
* # -HS # -MP geotype SS-ini L-coord. reflow bvol-ind axial#
16101000 5 7 2 0 0.813
* mesh-loc format-flag
16101100 0 1
* # -Intvl R-coord. (radial info.)
16101101 2 0.84
16101102 2 0.88
16101103 2 0.8827
* comp-# interval-# (radial info.)
16101201 6 2
16101202 17 4
16101203 6 6
* source value interval-# (radial info.)
16101301 0.0 6
* initial temperature flag (if flag=0 or -1)
16101400 -1
* temp-1 temp-2 temp-3 temp-4 temp-5 temp-6 temp-7
16101401 1095.9 1095.9 1095.9 1095.9 1095.9 1095.9 1095.9
16101402 1091.2 1091.2 1091.2 1091.2 1091.2 1091.2 1091.2
16101403 1090.3 1090.3 1090.3 1090.3 1090.3 1090.3 1090.3
16101404 1090.7 1090.7 1090.7 1090.7 1090.7 1090.7 1090.7
16101405 1093.8 1093.8 1093.8 1093.8 1093.8 1093.8 1093.8
* L-B B.Vol.# increment BC option surf.code height NH
16101501 610010000 10000 160 1 2.60 5
* R-B B.Vol.# increment BC option surf.code height NH
16101601 666050000 -10000 160 1 2.60 5
*16101601 0 0 0 1 2.60 5 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16101701 0 0. 0. 0. 5
* 9-words format option
16101800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16101801 1.626 1.3 20. 0. 0. 0. 0. 1. 1
16101802 1.626 3.9 20. 0. 0. 0. 0. 1. 2
16101803 1.626 6.5 20. 0. 0. 0. 0. 1. 3
16101804 1.626 9.1 20. 0. 0. 0. 0. 1. 4
16101805 1.626 11.7 20. 0. 0. 0. 0. 1. 5
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16101901 1.765 1.3 20. 0. 0. 0. 0. 1. 1
16101902 1.765 3.9 20. 0. 0. 0. 0. 1. 2
16101903 1.765 6.5 20. 0. 0. 0. 0. 1. 3
16101904 1.765 9.1 20. 0. 0. 0. 0. 1. 4
16101905 1.765 11.7 20. 0. 0. 0. 0. 1. 5
*
*-----*
* Hot Leg Duct of Passive DHR System 2 (Cylinder):Wall Thickness (0.027m)
*-----*
* # -HS # -MP geotype SS-ini L-coord. reflow bvol-ind axial#
16111000 5 7 2 0 0.813
* mesh-loc format-flag
16111100 0 1
* # -Intvl R-coord. (radial info.)
16111101 2 0.84
16111102 2 0.88
16111103 2 0.8827
* comp-# interval-# (radial info.)
16111201 6 2
16111202 17 4
16111203 6 6
* source value interval-# (radial info.)
16111301 0.0 6
* initial temperature flag (if flag=0 or -1)
16111400 -1
* temp-1 temp-2 temp-3 temp-4 temp-5 temp-6 temp-7
16111401 1084.7 1084.7 1084.7 1084.7 1084.7 1084.7 1084.7
16111402 1079.4 1079.4 1079.4 1079.4 1079.4 1079.4 1079.4
16111403 1071.3 1071.3 1071.3 1071.3 1071.3 1071.3 1071.3
16111404 1056.1 1056.1 1056.1 1056.1 1056.1 1056.1 1056.1
16111405 1023.9 1023.9 1023.9 1023.9 1023.9 1023.9 1023.9
* L-B B.Vol.# increment BC option surf.code height NH
16111501 611010000 10000 160 1 2.60 5

```

```

* R-B B.Vol.# increment BC option surf.code height NH
16111601 676050000 -10000 160 1 2.60 5
*16111601 0 0 0 1 2.60 5 * Insulated
* Source source-type multiplier DHeat-Left DHeat-Right NH
16111701 0 0. 0. 0. 5
*
* 9-words format option
16111800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16111801 1.626 1.3 20. 0. 0. 0. 0. 1. 1
16111802 1.626 3.9 20. 0. 0. 0. 0. 1. 2
16111803 1.626 6.5 20. 0. 0. 0. 0. 1. 3
16111804 1.626 9.1 20. 0. 0. 0. 0. 1. 4
16111805 1.626 11.7 20. 0. 0. 0. 0. 1. 5
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16111901 1.765 1.3 20. 0. 0. 0. 0. 1. 1
16111902 1.765 3.9 20. 0. 0. 0. 0. 1. 2
16111903 1.765 6.5 20. 0. 0. 0. 0. 1. 3
16111904 1.765 9.1 20. 0. 0. 0. 0. 1. 4
16111905 1.765 11.7 20. 0. 0. 0. 0. 1. 5
*
*=====
* HX pod Inlet of Passive DHR System 1 (Cylinder):Wall Thickness (0.027m)
*=====
* #HS #MP geotype SS-ini L-coord. reflod bvol-ind axial#
16201000 1 3 2 0 0.818
* mesh-loc format-flag
16201100 0 1
* #-Intvl R-coord. (radial info.)
16201101 2 0.828
* comp-# interval-# (radial info.)
16201201 6 2
* source value interval-# (radial info.)
16201301 0.0 2
* initial temperature flag (if flag=0 or -1)
16201400 -1
* temp-1 temp-2 temp-3
16201401 1118.6 1118.6 1118.6
* L-B B.Vol.# increment BC option surf.code height NH
16201501 620010000 10000 160 1 4.50 1
* R-B B.Vol.# increment BC option surf.code height NH
16201601 0 0 0 1 4.50 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16201701 0 0. 0. 0. 1
*
* 9-words format option
16201800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16201801 1.636 2.25 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16201901 1.656 2.25 20. 0. 0. 0. 0. 1. 1
*
*=====
* HX pod Inlet of Passive DHR System 2 (Cylinder):Wall Thickness (0.027m)
*=====
* #HS #MP geotype SS-ini L-coord. reflod bvol-ind axial#
16211000 1 3 2 0 0.818
* mesh-loc format-flag
16211100 0 1
* #-Intvl R-coord. (radial info.)
16211101 2 0.828
* comp-# interval-# (radial info.)
16211201 6 2
* source value interval-# (radial info.)
16211301 0.0 2
* initial temperature flag (if flag=0 or -1)
16211400 -1
* temp-1 temp-2 temp-3
16211401 932.43 932.43 932.43
* L-B B.Vol.# increment BC option surf.code height NH
16211501 621010000 10000 160 1 4.50 1
* R-B B.Vol.# increment BC option surf.code height NH
16211601 0 0 0 1 4.50 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16211701 0 0. 0. 0. 1
*
* 9-words format option
16211800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16211801 1.636 2.25 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16211901 1.656 2.25 20. 0. 0. 0. 0. 1. 1
*
*=====
* HX Inlet of Passive DHR System 1 (Cylinder):Wall Thickness (0.027m)
*=====
* #HS #MP geotype SS-ini L-coord. reflod bvol-ind axial#
16261000 1 3 2 0 0.075
* mesh-loc format-flag

```

```

16261100 0 1
* #-Intvl R-coord. (radial info.)
16261101 2 0.085
* comp-# interval-# (radial info.)
16261201 6 2
* source value interval-# (radial info.)
16261301 0.0 2
* initial temperature flag (if flag=0 or -1)
16261400 -1
* temp-1 temp-2 temp-3
16261401 1086.5 1086.5 1086.5
* L-B B.Vol.# increment BC option surf.code height NH
16261501 626010000 10000 160 1 1.00 1
* R-B B.Vol.# increment BC option surf.code height NH
16261601 0 0 0 1 1.00 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16261701 0 0. 0. 0. 1
* 9-words format option
16261800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16261801 0.150 0.50 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16261901 0.170 0.50 20. 0. 0. 0. 0. 1. 1
*
*=====
* HX Inlet of Passive DHR System 2 (Cylinder):Wall Thickness (0.027m)
*=====
* #-HS #-MP geotype SS-ini L-coord. reflowd bvol-ind axial#
16291000 1 3 2 0 0.075
* mesh-loc format-flag
16291100 0 1
* #-Intvl R-coord. (radial info.)
16291101 2 0.085
* comp-# interval-# (radial info.)
16291201 6 2
* source value interval-# (radial info.)
16291301 0.0 2
* initial temperature flag (if flag=0 or -1)
16291400 -1
* temp-1 temp-2 temp-3
16291401 372.51 372.51 372.51
* L-B B.Vol.# increment BC option surf.code height NH
16291501 629010000 10000 160 1 1.00 1
* R-B B.Vol.# increment BC option surf.code height NH
16291601 0 0 0 1 1.00 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16291701 0 0. 0. 0. 1
* 9-words format option
16291800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16291801 0.150 0.50 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16291901 0.170 0.50 20. 0. 0. 0. 0. 1. 1
*
*=====
* Passive DHR HEAT EXCHANGER 1
*
*=====
*-----
* Heat Exchanger (model in cylindrical coord)
*-----
* #-HS #-MP geotype SS-ini L-coord. reflowd bvol-ind axial#
16501000 5 3 1 0 1.5275e-3
* mesh-loc format-flag
16501100 0 1
* #-Intvl R-coord. (radial info.)
16501101 2 3.0275e-3
* comp-# interval-# (radial info.)
16501201 6 2
* source value interval-# (radial info.)
16501301 0.0 2
* initial temperature flag (if flag=0 or -1)
16501400 -1
* temp. mesh point temp. mesh point
16501401 298.01 298.01 298.01
16501402 298.01 298.01 298.01
16501403 298.01 298.01 298.01
16501404 298.00 298.00 298.00
16501405 298.00 298.00 298.00
* L-B B.Vol.# increment BC option surf.code surf area NH *H=#of
16501501 650010000 10000 160 1 53.62 5 *139050
* R-B B.Vol.# increment BC option surf.code surf area NH
16501601 710050000 -10000 160 1 53.62 5
*16501601 0 0 1401 1 4171.5 5 *tempera

```

```

* Source source-type multiplier DHeat-Left DHeat-Right NH
16501701 0 0. 0. 0. 5
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16501801 3.0550e-3 0.03 20. 0. 0. 0. 0. 1. 1
16501802 3.0550e-3 0.09 20. 0. 0. 0. 0. 1. 2
16501803 3.0550e-3 0.15 20. 0. 0. 0. 0. 1. 3
16501804 3.0550e-3 0.21 20. 0. 0. 0. 0. 1. 4
16501805 3.0550e-3 0.27 20. 0. 0. 0. 0. 1. 5
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16501901 3.0550e-3 0.03 20. 0. 0. 0. 0. 1. 1
16501902 3.0550e-3 0.09 20. 0. 0. 0. 0. 1. 2
16501903 3.0550e-3 0.15 20. 0. 0. 0. 0. 1. 3
16501904 3.0550e-3 0.21 20. 0. 0. 0. 0. 1. 4
16501905 3.0550e-3 0.27 20. 0. 0. 0. 0. 1. 5
=====
*
* Passive DHR HEAT EXCHANGER 2
*
=====
*
* Heat Exchanger
*
-----
* #HS #MP geotype SS-ini L-coord. reflood bvol-ind axial#
16511000 5 3 1 0 1.5275e-3
* mesh-loc format-flag
16511100 0 1
* #-Intvl R-coord. (radial info.)
16511101 2 3.0275e-3
* comp-# interval-# (radial info.)
16511201 6 2
* source value interval-# (radial info.)
16511301 0.0 2
* initial temperature flag (if flag=0 or -1)
16511400 -1
* temp. mesh point temp. mesh point
16511401 298.01 298.01 298.01
16511402 298.01 298.01 298.01
16511403 298.01 298.01 298.01
16511404 298.00 298.00 298.00
16511405 298.00 298.00 298.00
* L-B B.Vol.# increment BC option surf.code surf area NH
16511501 651010000 10000 160 1 53.62 5
* R-B B.Vol.# increment BC option surf.code surf area NH
16511601 711050000 -10000 160 1 53.62 5
*16511601 0 0 1401 1 4171.5 5 *te
* Source source-type multiplier DHeat-Left DHeat-Right NH
16511701 0 0. 0. 0. 5
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16511801 3.0550e-3 0.03 20. 0. 0. 0. 0. 1. 1
16511802 3.0550e-3 0.09 20. 0. 0. 0. 0. 1. 2
16511803 3.0550e-3 0.15 20. 0. 0. 0. 0. 1. 3
16511804 3.0550e-3 0.21 20. 0. 0. 0. 0. 1. 4
16511805 3.0550e-3 0.27 20. 0. 0. 0. 0. 1. 5
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16511901 3.0550e-3 0.03 20. 0. 0. 0. 0. 1. 1
16511902 3.0550e-3 0.09 20. 0. 0. 0. 0. 1. 2
16511903 3.0550e-3 0.15 20. 0. 0. 0. 0. 1. 3
16511904 3.0550e-3 0.21 20. 0. 0. 0. 0. 1. 4
16511905 3.0550e-3 0.27 20. 0. 0. 0. 0. 1. 5
*
=====
* HX Outlet of Passive DHR System 1 (Cylinder):Wall Thickness (0.027m)
*
-----
* #HS #MP geotype SS-ini L-coord. reflood bvol-ind axial#
16601000 1 3 2 0 0.075
* mesh-loc format-flag
16601100 0 1
* #-Intvl R-coord. (radial info.)
16601101 2 0.085
* comp-# interval-# (radial info.)
16601201 6 2
* source value interval-# (radial info.)
16601301 0.0 2
* initial temperature flag (if flag=0 or -1)
16601400 -1
* temp-1 temp-2 temp-3
16601401 607.58 607.58 607.58
* L-B B.Vol.# increment BC option surf.code height NH
16601501 660010000 10000 160 1 1.00 1
* R-B B.Vol.# increment BC option surf.code height NH
16601601 0 0 0 1 1.00 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16601701 0 0. 0. 0. 1
*
9-words format option
16601800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16601801 0.150 0.50 20. 0. 0. 0. 0. 1. 1

```

```

*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16601901 0.170 0.50 20. 0. 0. 0. 0. 1. 1
*
*=====
* HX Outlet of Passive DHR System 2 (Cylinder):Wall Thickness (0.027m)
*=====
* # -HS # -MP geotype SS-ini L-coord. reflood bvol-ind axial#
16681000 1 3 2 0 0.075
* mesh-loc format-flag
16681100 0 1
* # -Intvl R-coord. (radial info.)
16681101 2 0.085
* comp-# interval-# (radial info.)
16681201 6 2
* source value interval-# (radial info.)
16681301 0.0 2
* initial temperature flag (if flag=0 or -1)
16681400 -1
* temp-1 temp-2 temp-3
16681401 503.73 503.73 503.73
* L-B B.Vol.# increment BC option surf.code height NH
16681501 668010000 10000 160 1 1.00 1
* R-B B.Vol.# increment BC option surf.code height NH
16681601 0 0 0 1 1.00 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16681701 0 0. 0. 0. 0. 1
* 9-words format option
16681800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16681801 0.150 0.50 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16681901 0.170 0.50 20. 0. 0. 0. 0. 1. 1
*
*=====
* HX Outlet Pod of Passive DHR System 1 (Cylinder):Wall Thickness (0.027m)
*=====
* # -HS # -MP geotype SS-ini L-coord. reflood bvol-ind axial#
16621000 1 3 2 0 1.013
* mesh-loc format-flag
16621100 0 1
* # -Intvl R-coord. (radial info.)
16621101 2 1.023
* comp-# interval-# (radial info.)
16621201 6 2
* source value interval-# (radial info.)
16621301 0.0 2
* initial temperature flag (if flag=0 or -1)
16621400 -1
* temp-1 temp-2 temp-3
16621401 751.45 751.45 751.45
* L-B B.Vol.# increment BC option surf.code height NH
16621501 662010000 10000 160 1 1.00 1
* R-B B.Vol.# increment BC option surf.code height NH
16621601 0 0 0 1 1.00 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16621701 0 0. 0. 0. 0. 1
* 9-words format option
16621800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16621801 2.026 0.50 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16621901 2.046 0.50 20. 0. 0. 0. 0. 1. 1
*
*=====
* HX Outlet Pod of Passive DHR System 2 (Cylinder):Wall Thickness (0.027m)
*=====
* # -HS # -MP geotype SS-ini L-coord. reflood bvol-ind axial#
16711000 1 3 2 0 1.013
* mesh-loc format-flag
16711100 0 1
* # -Intvl R-coord. (radial info.)
16711101 2 1.023
* comp-# interval-# (radial info.)
16711201 6 2
* source value interval-# (radial info.)
16711301 0.0 2
* initial temperature flag (if flag=0 or -1)
16711400 -1
* temp-1 temp-2 temp-3
16711401 514.68 514.68 514.68
* L-B B.Vol.# increment BC option surf.code height NH
16711501 671010000 10000 160 1 1.00 1
* R-B B.Vol.# increment BC option surf.code height NH
16711601 0 0 0 1 1.00 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH

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```

16711701 0 0. 0. 0. 1
* 9-words format option
16711800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16711801 2.026 0.50 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16711901 2.046 0.50 20. 0. 0. 0. 0. 1. 1
*
*-----
* Blower Volume of Passive DHR System 1 (Cylinder):Wall Thickness (0.027m)
*-----
* # -HS # -MP geotype SS-ini L-coord. reflood bvol-ind axial#
16641000 1 3 2 0 0.7
* mesh-loc format-flag
16641100 0 1
* # -Intvl R-coord. (radial info.)
16641101 2 0.71
* comp-# interval-# (radial info.)
16641201 6 2
* source value interval-# (radial info.)
16641301 0.0 2
* initial temperature flag (if flag=0 or -1)
16641400 -1
* temp-1 temp-2 temp-3
16641401 755.72 755.72 755.72
* L-B B.Vol.# increment BC option surf.code height NH
16641501 664010000 10000 160 1 3.00 1
* R-B B.Vol.# increment BC option surf.code height NH
16641601 0 0 0 0 1 3.00 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16641701 0 0. 0. 0. 1
* 9-words format option
16641800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16641801 1.400 1.50 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16641901 1.420 1.50 20. 0. 0. 0. 0. 1. 1
*
*-----
* Blower Volume of Passive DHR System 2 (Cylinder):Wall Thickness (0.027m)
*-----
* # -HS # -MP geotype SS-ini L-coord. reflood bvol-ind axial#
16731000 1 3 2 0 0.7
* mesh-loc format-flag
16731100 0 1
* # -Intvl R-coord. (radial info.)
16731101 2 0.71
* comp-# interval-# (radial info.)
16731201 6 2
* source value interval-# (radial info.)
16731301 0.0 2
* initial temperature flag (if flag=0 or -1)
16731400 -1
* temp-1 temp-2 temp-3
16731401 533.78 533.78 533.78
* L-B B.Vol.# increment BC option surf.code height NH
16731501 673010000 10000 160 1 3.00 1
* R-B B.Vol.# increment BC option surf.code height NH
16731601 0 0 0 0 1 3.00 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16731701 0 0. 0. 0. 1
* 9-words format option
16731800 0 *This 9-words format excludes the pitch-to-diameter ratio on 801-
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16731801 1.400 1.50 20. 0. 0. 0. 0. 1. 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16731901 1.420 1.50 20. 0. 0. 0. 0. 1. 1
*
*-----
* Cold Leg Duct of Passive DHR System 1 (Cylinder)
*-----
* # -HS # -MP geotype SS-ini L-coord. reflood bvol-ind axial#
16661000 5 5 2 0 1.655
* mesh-loc format-flag
16661100 0 1
* # -Intvl R-coord. (radial info.)
16661101 4 1.685
* comp-# interval-# (radial info.)
16661201 6 4
* source value interval-# (radial info.)
16661301 0.0 4
* initial temperature flag (if flag=0 or -1)
16661400 -1
* temp-1 temp-2 temp-3 temp-4 temp-5
16661401 717.70 717.70 717.70 717.70 717.70

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16661402 717.70 717.70 717.70 717.70 717.70
16661403 717.70 717.70 717.70 717.70 717.70
16661404 717.70 717.70 717.70 717.70 717.70
16661405 717.70 717.70 717.70 717.70 717.70
* L-B B.Vol.# increment BC option surf.code height NH
16661501 666010000 10000 160 1 12.50 5
* R-B B.Vol.# increment BC option surf.code height NH
16661601 0 0 0 1 12.50 5 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
16661701 0 0. 0. 0. 5
* 9-words format option
16661800 0
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16661801 3.31 1.25 20. 0. 0. 0. 0. 1. 1
16661802 3.31 3.75 20. 0. 0. 0. 0. 1. 2
16661803 3.31 6.25 20. 0. 0. 0. 0. 1. 3
16661804 3.31 8.75 20. 0. 0. 0. 0. 1. 4
16661805 3.31 11.25 20. 0. 0. 0. 0. 1. 5
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16661901 3.37 1.25 20. 0. 0. 0. 0. 1. 1
16661902 3.37 3.75 20. 0. 0. 0. 0. 1. 2
16661903 3.37 6.25 20. 0. 0. 0. 0. 1. 3
16661904 3.37 8.75 20. 0. 0. 0. 0. 1. 4
16661905 3.37 11.25 20. 0. 0. 0. 0. 1. 5
*
*-----
* Cold Leg Duct of Passive DHR System 2 (Cylinder)
*-----
* #HS #MP geotype SS-ini L-coord. reflood bvol-ind axial#
16761000 5 5 2 0 1.655
* mesh-loc format-flag
16761100 0 1
* #-Intvl R-coord. (radial info.)
16761101 4 1.685
* comp-# interval-# (radial info.)
16761201 6 4
* source value interval-# (radial info.)
16761301 0.0 4
* initial temperature flag (if flag=0 or -1)
16761400 -1
* temp-1 temp-2 temp-3 temp-4 temp-5
16761401 717.70 717.70 717.70 717.70 717.70
16761402 717.70 717.70 717.70 717.70 717.70
16761403 717.70 717.70 717.70 717.70 717.70
16761404 717.70 717.70 717.70 717.70 717.70
16761405 717.70 717.70 717.70 717.70 717.70
* L-B B.Vol.# increment BC option surf.code height NH
16761501 676010000 10000 160 1 2.50 5
* R-B B.Vol.# increment BC option surf.code height NH
16761601 0 0 0 1 2.50 5 * Insulated
* Source source-type multiplier DHeat-Left DHeat-Right NH
16761701 0 0. 0. 0. 5
* 9-words format option
16761800 0
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16761801 3.31 1.25 20. 0. 0. 0. 0. 1. 1
16761802 3.31 3.75 20. 0. 0. 0. 0. 1. 2
16761803 3.31 6.25 20. 0. 0. 0. 0. 1. 3
16761804 3.31 8.75 20. 0. 0. 0. 0. 1. 4
16761805 3.31 11.25 20. 0. 0. 0. 0. 1. 5
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
16761901 3.37 1.25 20. 0. 0. 0. 0. 1. 1
16761902 3.37 3.75 20. 0. 0. 0. 0. 1. 2
16761903 3.37 6.25 20. 0. 0. 0. 0. 1. 3
16761904 3.37 8.75 20. 0. 0. 0. 0. 1. 4
16761905 3.37 11.25 20. 0. 0. 0. 0. 1. 5
*
*-----
* Passive UHS DHR HEAT EXCHANGER 1
*
*-----
* Heat Exchanger
*-----
* #HS #MP geotype SS-ini L-coord. reflood bvol-ind axial#
17501000 20 5 2 0 1.7526e-2
* mesh-loc format-flag
17501100 0 1
* #-Intvl R-coord. (radial info.)
17501101 4 2.0182e-2
* comp-# interval-# (radial info.)
17501201 6 4
* source value interval-# (radial info.)
17501301 0.0 4
* initial temperature flag (if flag=0 or -1)
17501400 -1

```

```

* temp. mesh point temp. mesh point
17501401 298.00 298.00 298.00 298.00 298.00
17501402 298.00 298.00 298.00 298.00 298.00
17501403 298.00 298.00 298.00 298.00 298.00
17501404 298.00 298.00 298.00 298.00 298.00
17501405 298.00 298.00 298.00 298.00 298.00
17501406 298.00 298.00 298.00 298.00 298.00
17501407 298.00 298.00 298.00 298.00 298.00
17501408 298.00 298.00 298.00 298.00 298.00
17501409 298.00 298.00 298.00 298.00 298.00
17501410 298.00 298.00 298.00 298.00 298.00
17501411 298.00 298.00 298.00 298.00 298.00
17501412 298.00 298.00 298.00 298.00 298.00
17501413 298.00 298.00 298.00 298.00 298.00
17501414 298.00 298.00 298.00 298.00 298.00
17501415 298.00 298.00 298.00 298.00 298.00
17501416 298.00 298.00 298.00 298.00 298.00
17501417 298.00 298.00 298.00 298.00 298.00
17501418 298.00 298.00 298.00 298.00 298.00
17501419 298.00 298.00 298.00 298.00 298.00
17501420 298.00 298.00 298.00 298.00 298.00
* L-B B.Vol.# increment BC option surf.code height NH
17501501 750010000 10000 160 1 160.5 20
* R-B B.Vol.# increment BC option surf.code Height NH
17501601 0 0 1401 1 160.5 20 *temperature
* Source source-type multiplier DHeat-Left DHeat-Right NH
17501701 0 0. 0. 0. 20
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
17501801 3.5052e-2 0.08025e1 20. 0. 0. 0. 0. 1. 1
17501802 3.5052e-2 0.24075e1 20. 0. 0. 0. 0. 1. 2
17501803 3.5052e-2 0.40125e1 20. 0. 0. 0. 0. 1. 3
17501804 3.5052e-2 0.56175e1 20. 0. 0. 0. 0. 1. 4
17501805 3.5052e-2 0.72225e1 20. 0. 0. 0. 0. 1. 5
17501806 3.5052e-2 0.88275e1 20. 0. 0. 0. 0. 1. 6
17501807 3.5052e-2 1.04325e1 20. 0. 0. 0. 0. 1. 7
17501808 3.5052e-2 1.20375e1 20. 0. 0. 0. 0. 1. 8
17501809 3.5052e-2 1.36425e1 20. 0. 0. 0. 0. 1. 9
17501810 3.5052e-2 1.52475e1 20. 0. 0. 0. 0. 1. 10
17501811 3.5052e-2 1.68525e1 20. 0. 0. 0. 0. 1. 11
17501812 3.5052e-2 1.84575e1 20. 0. 0. 0. 0. 1. 12
17501813 3.5052e-2 2.00625e1 20. 0. 0. 0. 0. 1. 13
17501814 3.5052e-2 2.16675e1 20. 0. 0. 0. 0. 1. 14
17501815 3.5052e-2 2.32725e1 20. 0. 0. 0. 0. 1. 15
17501816 3.5052e-2 2.48775e1 20. 0. 0. 0. 0. 1. 16
17501817 3.5052e-2 2.64825e1 20. 0. 0. 0. 0. 1. 17
17501818 3.5052e-2 2.80875e1 20. 0. 0. 0. 0. 1. 18
17501819 3.5052e-2 2.96925e1 20. 0. 0. 0. 0. 1. 19
17501820 3.5052e-2 3.12975e1 20. 0. 0. 0. 0. 1. 20
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
17501901 4.0364e-2 0.08025e1 20. 0. 0. 0. 0. 1. 1
17501902 4.0364e-2 0.24075e1 20. 0. 0. 0. 0. 1. 2
17501903 4.0364e-2 0.40125e1 20. 0. 0. 0. 0. 1. 3
17501904 4.0364e-2 0.56175e1 20. 0. 0. 0. 0. 1. 4
17501905 4.0364e-2 0.72225e1 20. 0. 0. 0. 0. 1. 5
17501906 4.0364e-2 0.88275e1 20. 0. 0. 0. 0. 1. 6
17501907 4.0364e-2 1.04325e1 20. 0. 0. 0. 0. 1. 7
17501908 4.0364e-2 1.20375e1 20. 0. 0. 0. 0. 1. 8
17501909 4.0364e-2 1.36425e1 20. 0. 0. 0. 0. 1. 9
17501910 4.0364e-2 1.52475e1 20. 0. 0. 0. 0. 1. 10
17501911 4.0364e-2 1.68525e1 20. 0. 0. 0. 0. 1. 11
17501912 4.0364e-2 1.84575e1 20. 0. 0. 0. 0. 1. 12
17501913 4.0364e-2 2.00625e1 20. 0. 0. 0. 0. 1. 13
17501914 4.0364e-2 2.16675e1 20. 0. 0. 0. 0. 1. 14
17501915 4.0364e-2 2.32725e1 20. 0. 0. 0. 0. 1. 15
17501916 4.0364e-2 2.48775e1 20. 0. 0. 0. 0. 1. 16
17501917 4.0364e-2 2.64825e1 20. 0. 0. 0. 0. 1. 17
17501918 4.0364e-2 2.80875e1 20. 0. 0. 0. 0. 1. 18
17501919 4.0364e-2 2.96925e1 20. 0. 0. 0. 0. 1. 19
17501920 4.0364e-2 3.12975e1 20. 0. 0. 0. 0. 1. 20
*-----
*
* Passive UHS DHR HEAT EXCHANGER 2
*
*-----
*
* Heat Exchanger
*-----
* #-HS #-MP geotype SS-ini L-coord. reflood bvol-ind axial#
17511000 20 5 2 0 1.7526e-2
* mesh-loc format-flag
17511100 0 1
* #-Intvl R-coord. (radial info.)
17511101 4 2.0182e-2
* comp-# interval-# (radial info.)
17511201 6 4
* source value interval-# (radial info.)
17511301 0.0 4

```



```

*   initial temperature flag (if flag=0 or -1)
17511400 -1
*   temp. mesh point temp. mesh point
17511401 298.00 298.00 298.00 298.00 298.00
17511402 298.00 298.00 298.00 298.00 298.00
17511403 298.00 298.00 298.00 298.00 298.00
17511404 298.00 298.00 298.00 298.00 298.00
17511405 298.00 298.00 298.00 298.00 298.00
17511406 298.00 298.00 298.00 298.00 298.00
17511407 298.00 298.00 298.00 298.00 298.00
17511408 298.00 298.00 298.00 298.00 298.00
17511409 298.00 298.00 298.00 298.00 298.00
17511410 298.00 298.00 298.00 298.00 298.00
17511411 298.00 298.00 298.00 298.00 298.00
17511412 298.00 298.00 298.00 298.00 298.00
17511413 298.00 298.00 298.00 298.00 298.00
17511414 298.00 298.00 298.00 298.00 298.00
17511415 298.00 298.00 298.00 298.00 298.00
17511416 298.00 298.00 298.00 298.00 298.00
17511417 298.00 298.00 298.00 298.00 298.00
17511418 298.00 298.00 298.00 298.00 298.00
17511419 298.00 298.00 298.00 298.00 298.00
17511420 298.00 298.00 298.00 298.00 298.00
* L-B B.Vol.# increment BC option surf.code height NH
17511501 751010000 10000 160 1 160.5 20
* R-B B.Vol.# increment BC option surf.code height NH
17511601 0 0 1401 1 160.5 20 *temperatu
* Source source-type multiplier DHeat-Left DHeat-Right NH
17511701 0 0. 0. 0. 20
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
17511801 3.5052e-2 0.08025e1 20. 0. 0. 0. 0. 1. 1
17511802 3.5052e-2 0.24075e1 20. 0. 0. 0. 0. 1. 2
17511803 3.5052e-2 0.40125e1 20. 0. 0. 0. 0. 1. 3
17511804 3.5052e-2 0.56175e1 20. 0. 0. 0. 0. 1. 4
17511805 3.5052e-2 0.72225e1 20. 0. 0. 0. 0. 1. 5
17511806 3.5052e-2 0.88275e1 20. 0. 0. 0. 0. 1. 6
17511807 3.5052e-2 1.04325e1 20. 0. 0. 0. 0. 1. 7
17511808 3.5052e-2 1.20375e1 20. 0. 0. 0. 0. 1. 8
17511809 3.5052e-2 1.36425e1 20. 0. 0. 0. 0. 1. 9
17511810 3.5052e-2 1.52475e1 20. 0. 0. 0. 0. 1. 10
17511811 3.5052e-2 1.68525e1 20. 0. 0. 0. 0. 1. 11
17511812 3.5052e-2 1.84575e1 20. 0. 0. 0. 0. 1. 12
17511813 3.5052e-2 2.00625e1 20. 0. 0. 0. 0. 1. 13
17511814 3.5052e-2 2.16675e1 20. 0. 0. 0. 0. 1. 14
17511815 3.5052e-2 2.32725e1 20. 0. 0. 0. 0. 1. 15
17511816 3.5052e-2 2.48775e1 20. 0. 0. 0. 0. 1. 16
17511817 3.5052e-2 2.64825e1 20. 0. 0. 0. 0. 1. 17
17511818 3.5052e-2 2.80875e1 20. 0. 0. 0. 0. 1. 18
17511819 3.5052e-2 2.96925e1 20. 0. 0. 0. 0. 1. 19
17511820 3.5052e-2 3.12975e1 20. 0. 0. 0. 0. 1. 20
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
17511901 4.0364e-2 0.08025e1 20. 0. 0. 0. 0. 1. 1
17511902 4.0364e-2 0.24075e1 20. 0. 0. 0. 0. 1. 2
17511903 4.0364e-2 0.40125e1 20. 0. 0. 0. 0. 1. 3
17511904 4.0364e-2 0.56175e1 20. 0. 0. 0. 0. 1. 4
17511905 4.0364e-2 0.72225e1 20. 0. 0. 0. 0. 1. 5
17511906 4.0364e-2 0.88275e1 20. 0. 0. 0. 0. 1. 6
17511907 4.0364e-2 1.04325e1 20. 0. 0. 0. 0. 1. 7
17511908 4.0364e-2 1.20375e1 20. 0. 0. 0. 0. 1. 8
17511909 4.0364e-2 1.36425e1 20. 0. 0. 0. 0. 1. 9
17511910 4.0364e-2 1.52475e1 20. 0. 0. 0. 0. 1. 10
17511911 4.0364e-2 1.68525e1 20. 0. 0. 0. 0. 1. 11
17511912 4.0364e-2 1.84575e1 20. 0. 0. 0. 0. 1. 12
17511913 4.0364e-2 2.00625e1 20. 0. 0. 0. 0. 1. 13
17511914 4.0364e-2 2.16675e1 20. 0. 0. 0. 0. 1. 14
17511915 4.0364e-2 2.32725e1 20. 0. 0. 0. 0. 1. 15
17511916 4.0364e-2 2.48775e1 20. 0. 0. 0. 0. 1. 16
17511917 4.0364e-2 2.64825e1 20. 0. 0. 0. 0. 1. 17
17511918 4.0364e-2 2.80875e1 20. 0. 0. 0. 0. 1. 18
17511919 4.0364e-2 2.96925e1 20. 0. 0. 0. 0. 1. 19
17511920 4.0364e-2 3.12975e1 20. 0. 0. 0. 0. 1. 20
*
*-----*
* General Table for Surface Temperature of HX
* time temperature
20240100 temp
20240101 0.0 298.00
20240102 1.e5 298.00
*
*-----*
* Containment Ferrit SS perimeter
*-----*
* #-HS #-MP geotype SS-ini L-coord. reflood bvol-ind axial#
10701000 1 7 2 0 15.0
* mesh-loc format-flag
10701100 0 1
* #-Intvl R-coord. (radial info.)
10701101 2 15.025

```

```

10701102 4 15.225
* comp-# interval-# (radial info.)
10701201 17 2
10701202 6 6
* source value interval-# (radial info.)
10701301 0.0 6
* initial temperature flag (if flag=0 or -1)
10701400 -1
* temp-1 temp-2 temp-3
10701401 303.15 303.15 303.15 303.15 303.15 303.15 303.15
* L-B B.Vol.# increment BC option surf.code height NH
10701501 070010000 10000 160 1 25.0 1
* R-B B.Vol.# increment BC option surf.code height NH
10701601 0 0 0 1 25.0 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
10701701 0 0. 0. 0. 1
*
10701800 1 *This 12-words format
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
10701801 0.0 15. 15. 0. 0. 0. 0. 1. 0. 1.1 1.6383 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
10701901 0.0 15. 15. 0. 0. 0. 0. 1. 1
*
*=====  

* Containment Concrete floor  

*=====  

* #-HS #-MP geotype SS-ini L-coord. reflood bvol-ind axial#
10702000 1 5 1 0 15.0
* mesh-loc format-flag
10702100 0 1
* #-Intvl R-coord. (radial info.)
10702101 4 15.5
* comp-# interval-# (radial info.)
10702201 14 4
* source value interval-# (radial info.)
10702301 0.0 4
* initial temperature flag (if flag=0 or -1)
10702400 -1
* temp-1 temp-2 temp-3
10702401 303.15 303.15 303.15 303.15 303.15
* L-B B.Vol.# increment BC option surf.code height NH
10702501 070010000 10000 131 0 700. 1
* R-B B.Vol.# increment BC option surf.code height NH
10702601 0 0 0 0 700.0 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
10702701 0 0. 0. 0. 1
*
10702800 1 *This 12-words format
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
10702801 48.51 15. 15. 0. 0. 0. 0. 1. 0. 1.1 1.6383 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
10702901 48.51 15. 15. 0. 0. 0. 0. 1. 1
*
*=====  

* Containment SS stuctures (Thinner ones)  

*=====  

* #-HS #-MP geotype SS-ini L-coord. reflood bvol-ind axial#
10703000 1 5 1 0 7.5
* mesh-loc format-flag
10703100 0 1
* #-Intvl R-coord. (radial info.)
10703101 4 7.525
* comp-# interval-# (radial info.)
10703201 4 4
* source value interval-# (radial info.)
10703301 0.0 4
* initial temperature flag (if flag=0 or -1)
10703400 -1
* temp-1 temp-2 temp-3
10703401 303.15 303.15 303.15 303.15 303.15
* L-B B.Vol.# increment BC option surf.code height NH
10703501 070010000 10000 160 0 700. 1
* R-B B.Vol.# increment BC option surf.code height NH
10703601 0 0 0 0 700.0 1 * Insulate
* Source source-type multiplier DHeat-Left DHeat-Right NH
10703701 0 0. 0. 0. 1
* 9-words format option
10703800 1 *This 12-words format
* Add L-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
10703801 42.79 15. 15. 0. 0. 0. 0. 1. 0. 1.1 1.6383 1
*
* Add R-B Dh HL-f HL-r grid-f grid-r grid-kf grid-kr L-Boil NH
10703901 42.79 15. 15. 0. 0. 0. 0. 1. 1
*
*
*=====  


```

```

-----
*   heat structures properties   *
-----
*
20100100 tbl/fctn 1 1 * UO-2
20100200 tbl/fctn 3 1 * gap for average rods
20100300 tbl/fctn 1 1 * zircaloy
20100400 s-steel * s. steel (default)
20100500 tbl/fctn 1 1 * inconel
20100600 tbl/fctn 1 1 * ferrit SS
20100700 tbl/fctn 1 1 * austenit SS
20100800 tbl/fctn 3 1 * gap for hot rod
20100900 tbl/fctn 1 1 * inconel for energy balance
20101000 tbl/fctn 1 1 * heater (MgO)
*
20101100 tbl/fctn 1 1 * U-TRU-Zr (90:10 weight fraction)
20101200 tbl/fctn 1 1 * UC-SiC (50:50 volume fraction)
20101300 tbl/fctn 1 1 * SiC for the Lower-Upper Reflector
20101400 tbl/fctn 1 1 * Concrete
20101700 tbl/fctn 1 1 * Insulator
-----
*   fuel UC
*   temp[k] lamda[w/m-k] temp[k] lamda[w/m-k]
20100101 273.15 21.7 373.15 21.4321
20100102 473.15 21.2364 573.15 21.1129
20100103 673.14 21.0616 773.15 21.0825
20100104 873.15 21.1756 973.15 21.3409
20100105 1073.15 21.384 1173.15 21.532
20100106 1273.15 21.68 1373.15 21.828
20100107 1473.15 21.976 1573.15 22.124
20100108 1673.15 22.272 1773.15 22.42
20100109 1873.15 22.568 1973.15 22.716
20100110 2073.15 22.864 2173.15 23.012
20100111 2273.15 23.16 2373.15 23.308 *Extrapolated
20100112 2473.15 23.456 2573.15 23.604 *Extrapolated
20100113 2673.15 23.752 2773.15 23.9 *Extrapolated
20100114 2873.15 24.048 2973.15 24.196 *Extrapolated
20100115 3073.15 24.344 3173.15 24.492 *Extrapolated
20100116 3573.15 25.084 4873.15 27.008 *Extrapolated
-----
*   gap gas average rods
*   gas type mole fraction
20100201 helium 0.9511
20100202 argon 0.0396
20100203 nitrogen 0.0008
20100204 xenon 0.0076
20100205 krypton 0.0008
-----
*   huellerohr zircaloy
*   temp[k] lamda[w/m-k] temp[k] lamda[w/m-k]
*
20100301 273.15 13.6 373.15 14.1
20100302 473.15 14.8 573.15 15.8
20100303 673.15 16.9 773.15 18.1
20100304 873.15 19.5 973.15 21.1
20100305 1073.15 22.8 1173.15 24.6
20100306 1273.15 26.8 1373.15 29.2
20100307 1473.15 31.7 1573.15 34.4
20100308 1673.15 37.3 1773.15 40.4
20100309 1873.15 43.5 1973.15 46.6
20100309 1873.15 43.5 4973.15 46.6 * test
-----
*   inconel
*   temp(k) lamda(w/m3-k) temp(k) lamda(w/m3-k)
20100501 294.3 14.9 366.0 15.7
20100502 477.0 17.5 588.7 19.2
20100503 699.8 20.9 810.9 22.8
20100504 1500.0 22.8
-----
*   ferrit
*   temp[k] lamda[w/m-k] temp[k] lamda[w/m-k]
20100601 73.15 44. 373.15 44. *arbitrarily extended
20100602 473.15 43. 573.15 42.
20100603 673.15 40. 773.15 39.
20100604 873.15 39. 973.15 39.
20100605 1073.15 39. 1173.15 39.
20100605 1073.15 39. 1973.15 39. *arbitrarily extended
20100606 5000.0 39.
-----
*   austenit
*   temp[k] lamda[w/m-k] temp[k] lamda[w/m-k]
20100701 293.15 14.24 413.15 16.7
20100702 523.15 18.6 683.15 18.6
20100703 773.15 20.9 873.15 20.9
20100704 973.15 20.9 2000. 20.9
20100704 973.15 20.9 4000. 20.9 *itest
-----
*   gap gas hot rod

```

```

* gas type mole fraction
20100801 helium 0.9079
20100802 argon 0.0378
20100803 nitrogen 0.0049
20100804 xenon 0.0445
20100805 krypton 0.0050
-----
* Inconel Property Tuning for Energy Balance Factor : 1.55
*
20100901 294.3 23.09 366.0 24.34
20100902 477.0 27.13 588.7 29.76
20100903 699.8 32.39 810.9 35.34
20100904 1500.0 35.34
*
-----
* PZR Heater - MgO (010)
* temp (k) thermal conductivity (w/m.k)
20101001 .29320e+03 .81400e+02
20101002 .12732e+04 .10047e+03
20101003 .22532e+04 .11954e+03
-----
* U-TRU-Zr (90:10 weight fraction)
* temp (k) thermal conductivity (w/m.k)
20101101 373. 21.16 600. 23.1546
20101102 900. 25.0209 938. 25.2094
20101103 938.01 25.2095 1049. 25.707
20101104 1049.01 25.0707 1132.3 26.0308
-----
* UC-SiC (50:50 volume fraction)
* temp (k) thermal conductivity (w/m.k)
20101201 373. 20.9195 600. 20.7434
20101202 900. 20.7767 1200. 20.4998
20101203 1500. 20.3775 1800. 20.2394
20101204 2100. 20.0847 2400. 19.9125
*
-----
* SiC
* temp(k) lamda(w/m.k) temp(k) lamda(w/m.k)
20101301 273. 15. 2400. 15.
-----
* Concrete
20101401 1.4
* Insulator
20101701 0.0737
-----
* volumetric heat capacity *
-----
* fuel UC
* temp[k] cp[j/m3-k] temp[k] cp[j/m3-k]
20100151 273.150 3.536e6 400. 3.536e6 *average
20100152 500. 3.536e6 600. 3.536e6
20100153 700. 3.536e6 800. 3.536e6
20100154 900. 3.536e6 1000. 3.536e6
20100155 1100. 3.536e6 1200. 3.536e6
20100156 1300. 3.536e6 1400. 3.536e6
20100157 1500. 3.536e6 1600. 3.536e6
20100158 1700. 3.536e6 1800. 3.536e6
20100159 1900. 3.536e6 2000. 3.536e6
20100160 2100. 3.536e6 2200. 3.536e6
20100161 2300. 3.536e6 2400. 3.536e6
20100162 2500. 3.536e6 2600. 3.536e6
20100163 3000. 3.536e6 5000. 3.536e6
*
-----
* gap gas
* temp[k] cp[j/m3-k] temp[k] cp[j/m3-k]
20100251 273.15 5.4 3273.15 5.4
-----
* huellerohr zicaloy
* temp[k] cp[j/m3-k] temp[k] cp[j/m3-k]
20100351 273.15 1.881e6 573.15 2.079e6
20100352 773.15 2.211e6 903.15 2.290e6
20100353 923.15 2.376e6 1083.15 2.376e6
20100354 1103.15 3.630e6 1123.15 4.455e6
20100355 1143.15 4.950e6 1163.15 5.115e6
20100356 1183.15 4.950e6 1203.15 4.455e6
20100357 1213.15 3.360e6 1243.15 2.376e6
20100358 2073.15 2.376e6
20100358 4073.15 2.376e6 *test
-----
* inconel
* temp(k) cp(j/m3-k) temp(k) cp(j/m3-k)
20100551 273. 3.988e6 293.0 3.916e6
20100552 373. 4.169e6 473.0 4.418e6
20100553 573. 4.703e6 673.0 5.095e6
20100554 773. 5.593e6 873.0 6.307e6
20100555 973. 7.482e6 1000.0 7.482e6
20100556 2000. 7.482e6 4000. 7.482e6 *Arbitrary Extended

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-----
* ferrit
* temp[k] cp[j/m3-k] temp[k] cp[j/mf-k]
20100651 93.15 3.611e6 373.15 3.847e6 *Arbitrary extended
20100652 473.15 4.082e6 573.15 4.396e6
20100653 673.15 4.788e6 773.15 5.338e6
20100654 2000. 5.338e6 4000.00 5.338e6 *Arbitrary Extended
-----
* austenit
* temp[k] cp[j/m3-k] temp[k] cp[j/m3-k]
20100751 293.15 3.572e6 368. 3.837e6
20100752 478.15 4.102e6 588.15 4.333e6
20100753 698.15 4.465e6 813.15 4.597e6
20100754 873.15 4.465e6 2000. 4.465e6
20100754 873.15 4.465e6 4000. 4.465e6 *test
-----
* gap gas
* temp[k] cp[j/m3-k] temp[k] cp[j/m3-k]
20100851 273.15 5.4 3273.15 5.4
-----
* Inconel
* temp(k) cp(j/m3-k) temp(k) cp(j/m3-k)
*
20100951 273. 3.988e6 294.3 3.740e6
20100952 366.5 3.917e6 477.6 4.094e6
20100953 588.8 4.270e6 699.9 4.446e6
20100954 811.0 4.658e6 2000.0 4.658e6
20100955 4000. 4.65836 *Arbitrary Extended
-----
* PZR Heater - MgO (010)
* temp (k) volumetric heat capacity (j/m3.k)
20101051 .293e+03 .2581e+07
20101052 .450e+03 .2835e+07
20101053 .800e+03 .3402e+07
20101054 .112e+04 .3726e+07
20101055 .144e+04 .4050e+07
-----
* U-TRU-Zr (90:10 weight fraction)
* temp (k) volumetric heat capacity (j/m3.k)
20101151 373. 2.21306e6 600. 2.58049e6
20101152 900. 3.25756e6 938. 3.35867e6
20101153 938.01 3.03142e6 1049. 2.98995e6
20101154 1049.01 2.71774e6 1132.3 3.05993e6
-----
* UC-SiC (50:50 volume fraction)
* temp (k) volumetric heat capacity (j/m3.k)
20101251 373. 2.58160e6 600. 2.74160e6
20101252 900. 3.22160e6 1200. 3.70160e6
20101253 1500. 3.86160e6 1800. 3.95760e6
20101254 2100. 4.02160e6 2400. 4.10160e6
-----
* SiC
* temp(K) Cp(J/kg-K) temp(K) Cp(J/kg-K)
20101351 273. 500. 600. 600.
20101352 900. 900. 1200. 1200.
20101353 1500. 1300. 1800. 1360.
20101354 2100. 1400. 2400. 1450.
-----
* Concrete
20101451 840.
* Insulator
20101751 1050.
-----
* power table
-----
*20210000 power 503 1. 2775.0e6
*20210001 -1. 1.0
*20210002 0. 0.20267
*20210003 5. 0.12720
*20210004 10. 0.11631
*20210005 20. 0.08037
*20210006 30. 0.06289
*20210007 40. 0.05148
*20210008 50. 0.04565
*20210009 70. 0.04097
*20210010 100. 0.03726
*20210011 150. 0.03448
*20210012 200. 0.03268
*20210013 300. 0.03024
*20210014 400. 0.02862
*20210015 500. 0.02741
*20210016 600. 0.02683
*20210017 800. 0.02486
*20210018 1000. 0.02362
*20210019 1300. 0.02211
*20210020 1600. 0.02090
*20210021 2000. 0.01960
*20210022 2500. 0.01836

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*20210023 3000. 0.01736
*20210024 3500. 0.01657
*20210025 4000. 0.01590
*20210026 4500. 0.01537
*20210027 5000. 0.01490
*20210028 6000. 0.01404
-----
* control variables
-----
*
* Temperature Drop core
20510100 DeltT sum 1.0 360. 1
20510101 0.0 -1.0 tempg 100050000
20510102 1.0 tempg 300010000
*
* Estimated extracted Q (Core)
20510200 EstimQ mult 5192.4 6.0e8 1
20510201 cntrlvar 101
20510202 mflowj 100040000
*
* MAX Temperature Cladding: Control variable 103
20510300 max-clad stdfnctn 1.0 1310.995 1
20510301 max htemp 251100107 htemp 251100108
20510302 htemp 251100207 htemp 251100208
20510303 htemp 251100307 htemp 251100308
20510304 htemp 251100407 htemp 251100408
20510305 htemp 251100507 htemp 251100508
20510306 htemp 251100607 htemp 251100608
20510307 htemp 251100707 htemp 251100708
20510308 htemp 251100807 htemp 251100808
** reynolds number (De = 0.0127)
20510800 re-no0 mult 0.0127 2.783415 1
20510801 rhog 250040000 velg 250040000
20510900 re-no div 1.0 67608.9 1
20510901 viscg 250040000 cntrlvar 108
* MAX Temperature Fuel: Control variable 110
20511000 max-fuel stdfnctn 1.0 1310.995 1
20511001 max htemp 251100401 htemp 251100402
20511002 htemp 251100403 htemp 251100404
20511003 htemp 251100501 htemp 251100502
20511004 htemp 251100503 htemp 251100504
20511005 htemp 251100601 htemp 251100602
20511006 htemp 251100603 htemp 251100604
20511007 htemp 251100701 htemp 251100702
20511008 htemp 251100703 htemp 251100704
20511009 htemp 251100801 htemp 251100802
20511010 htemp 251100803 htemp 251100804
* Energy Balance in core 250 and 251
20511100 Core-E sum 1.0 6.+8 1
20511101 0.0 1.0 q 250010000
20511102 1.0 q 250020000
20511103 1.0 q 250030000
20511104 1.0 q 250040000
20511105 1.0 q 250050000
20511106 1.0 q 250060000
20511107 1.0 q 250070000
20511108 1.0 q 250080000
20511109 1.0 q 251010000
20511110 1.0 q 251020000
20511111 1.0 q 251030000
20511112 1.0 q 251040000
20511113 1.0 q 251050000
20511114 1.0 q 251060000
20511115 1.0 q 251070000
20511116 1.0 q 251080000
**
*-----
* Heat loss from the primary wall heat structures
* Hydrodynamic components 100, 210, 211, 290, 291, 610, 611, 666, 676, 670
*-----
* DHR HX 1 (650): Control variable 120
20512000 DhrHX1HS sum 1.0 .1704288 1
20512001 0.0 1.0 q 650010000
20512002 1.0 q 650020000
20512003 1.0 q 650030000
20512004 1.0 q 650040000
20512005 1.0 q 650050000
*Power generated in the core Control variable 123
20512300 corepowg sum 1.0 600.0e6 1
20512301 0.0 1.0 htpowg 2501001
20512302 1.0 htpowg 2501002 1.0 htpowg 2501003
20512303 1.0 htpowg 2501004 1.0 htpowg 2501005
20512304 1.0 htpowg 2501006 1.0 htpowg 2501007
20512305 1.0 htpowg 2501008 1.0 htpowg 2511001
20512306 1.0 htpowg 2511002 1.0 htpowg 2511003
20512307 1.0 htpowg 2511004 1.0 htpowg 2511005
20512308 1.0 htpowg 2511006 1.0 htpowg 2511007
20512309 1.0 htpowg 2511008

```

```

* DHR HX 2 (651): Control variabelbe 125
20512500 DhrHX2HS sum 1.0 .1704288 1
20512501 0.0 1.0 q 651010000
20512502 1.0 q 651020000
20512503 1.0 q 651030000
20512504 1.0 q 651040000
20512505 1.0 q 651050000
* DHR HX 1 (710): Control variabelbe 126
20512600 DhrHX1CS sum 1.0 .665619 1
20512601 0.0 1.0 q 710010000
20512602 1.0 q 710020000
20512603 1.0 q 710030000
20512604 1.0 q 710040000
20512605 1.0 q 710050000
* DHR HX 2 (711): Control variabelbe 127
20512700 DhrHX2CS sum 1.0 .665619 1 *8.60957-6
20512701 0.0 1.0 q 711010000
20512702 1.0 q 711020000
20512703 1.0 q 711030000
20512704 1.0 q 711040000
20512705 1.0 q 711050000
* H2O1 (750): Control variabelbe 128
20512800 H2O1 sum 1.0 8.10906-6 1
20512801 0.0 1.0 q 750010000
20512802 1.0 q 750020000 1.0 q 750030000
20512803 1.0 q 750040000 1.0 q 750050000
20512804 1.0 q 750060000 1.0 q 750070000
20512805 1.0 q 750080000 1.0 q 750090000
20512806 1.0 q 750100000 1.0 q 750110000
20512807 1.0 q 750120000 1.0 q 750130000
20512808 1.0 q 750140000 1.0 q 750150000
20512809 1.0 q 750160000 1.0 q 750170000
20512810 1.0 q 750180000 1.0 q 750190000
20512811 1.0 q 750200000
* H2O2 (751): Control variabelbe 129
20512900 H2O2 sum 1.0 3977.325 1
20512901 0.0 1.0 q 751010000
20512902 1.0 q 751020000 1.0 q 751030000
20512903 1.0 q 751040000 1.0 q 751050000
20512904 1.0 q 751060000 1.0 q 751070000
20512905 1.0 q 751080000 1.0 q 751090000
20512906 1.0 q 751100000 1.0 q 751110000
20512907 1.0 q 751120000 1.0 q 751130000
20512908 1.0 q 751140000 1.0 q 751150000
20512909 1.0 q 751160000 1.0 q 751170000
20512910 1.0 q 751180000 1.0 q 751190000
20512911 1.0 q 751200000
*
20513000 Firder diffrend 1.0 0. 1
20513001 tempg 251080000
*
20513100 Secder diffrend 1.0 0. 1
20513101 cntrivar 130
*
*ctlvar name type factor init f c min max
20560000 shaft1 shaft 1.0 376.991 1 1 0.1
*
*ctlvar cv iner fric type comp type comp
20560001 990 729.87 0.0 turbine 510
20560002 cprsr 550
20560003 cprsr 580
20560004 generatr 600
*
iner fric trip discon
20560006 376.991 376.991 1270.95 0.0 360 0
*
*****
* added shaft torque from a control variable representing a resistor bank
*****
20599000 shftTrql function 1.0 1.0 1
20599001 time 0 990
*
*****
* Table giving resistor bank torque versus time for 1x shaft
20299000 reac-t 529
*
time torque
20299001 0.0 0.
20299002 3.5 -100000.
*****
$=====
* compute generator torque (N-m) and power (mw)
$=====
*ctlvar name type factor init f c min max
20560200 gentrql sum 1.0 407472.4 1
*
*ctlvar a0 a1 v1 pl a2 v2 p2
20560201 0.0 1.0 turtrq 510 1.0 cprtrq 550
20560202 1.0 cprtrq 580
*
*ctlvar name type factor init f c min max

```

```

20560400 genpow1 mult 1.0 153613424.1
*
*ctlvar v1 p1 v2 p2
20560401 cntrlvar 600 cntrlvar 602
*
$=====
* compute turbine shaft power in MW
$=====
*ctlvar name type factor init f c min max
20562000 turpow1 sum 1.e-6 411.063 1 1 1.e-6
*
*ctlvar a0 a1 v1 p1 a2 v2 p2
20562001 0.0 1.0 turpow 510
*
$=====
*control variables to calculate total power transfered in recuperator
*
20503000 rc_hQ1 sum 1.0 -6.00586+8 1
20503001 0.0 1.0 q 520010000 1.0 q 520020000 1.0 q 520030000
20503002 1.0 q 520040000 1.0 q 520050000 1.0 q 520060000 1.0 q 520070000
20503003 1.0 q 520080000 1.0 q 520090000 1.0 q 520100000 1.0 q 520110000
20503004 1.0 q 520120000 1.0 q 520130000 1.0 q 520140000 1.0 q 520150000
20503005 1.0 q 520160000 1.0 q 520170000 1.0 q 520180000 1.0 q 520190000
20503006 1.0 q 520200000 1.0 q 520210000 1.0 q 520220000 1.0 q 520230000
20503007 1.0 q 520240000 1.0 q 520250000 1.0 q 520260000 1.0 q 520270000
20503008 1.0 q 520280000 1.0 q 520290000 1.0 q 520300000
*
20503100 rc_cQ1 sum 1.0 6.00586+8 1
20503101 0.0 1.0 q 590010000 1.0 q 590020000 1.0 q 590030000
20503102 1.0 q 590040000 1.0 q 590050000 1.0 q 590060000 1.0 q 590070000
20503103 1.0 q 590080000 1.0 q 590090000 1.0 q 590100000 1.0 q 590110000
20503104 1.0 q 590120000 1.0 q 590130000 1.0 q 590140000 1.0 q 590150000
20503105 1.0 q 590160000 1.0 q 590170000 1.0 q 590180000 1.0 q 590190000
20503106 1.0 q 590200000 1.0 q 590210000 1.0 q 590220000 1.0 q 590230000
20503107 1.0 q 590240000 1.0 q 590250000 1.0 q 590260000 1.0 q 590270000
20503108 1.0 q 590280000 1.0 q 590290000 1.0 q 590300000
*
$=====
*control variables to calculate total power transfered in pre-cooler
*
20503200 pc_hQ1 sum 1.0 -152171632.1
20503201 0.0 1.0 q 530010000 1.0 q 530020000 1.0 q 530030000
20503202 1.0 q 530040000 1.0 q 530050000 1.0 q 530060000 1.0 q 530070000
20503203 1.0 q 530080000 1.0 q 530090000 1.0 q 530100000 1.0 q 530110000
20503204 1.0 q 530120000 1.0 q 530130000 1.0 q 530140000 1.0 q 530150000
20503205 1.0 q 530160000 1.0 q 530170000 1.0 q 530180000 1.0 q 530190000
20503206 1.0 q 530200000
*
20503300 pc_cQ1 sum 1.0 152171632.1
20503301 0.0 1.0 q 133010000 1.0 q 133020000 1.0 q 133030000
20503302 1.0 q 133040000 1.0 q 133050000 1.0 q 133060000 1.0 q 133070000
20503303 1.0 q 133080000 1.0 q 133090000 1.0 q 133100000 1.0 q 133110000
20503304 1.0 q 133120000 1.0 q 133130000 1.0 q 133140000 1.0 q 133150000
20503305 1.0 q 133160000 1.0 q 133170000 1.0 q 133180000 1.0 q 133190000
20503306 1.0 q 133200000
*
$=====
*control variables to calculate total power transfered in inter-cooler
*
20503400 ic_hQ1 sum 1.0 -128865440.1
20503401 0.0 1.0 q 570010000 1.0 q 570020000 1.0 q 570030000
20503402 1.0 q 570040000 1.0 q 570050000 1.0 q 570060000 1.0 q 570070000
20503403 1.0 q 570080000 1.0 q 570090000 1.0 q 570100000 1.0 q 570110000
20503404 1.0 q 570120000 1.0 q 570130000 1.0 q 570140000 1.0 q 570150000
20503405 1.0 q 570160000 1.0 q 570170000 1.0 q 570180000 1.0 q 570190000
20503406 1.0 q 570200000
*
20503500 ic_cQ1 sum 1.0 128865440.1
20503501 0.0 1.0 q 143010000 1.0 q 143020000 1.0 q 143030000
20503502 1.0 q 143040000 1.0 q 143050000 1.0 q 143060000 1.0 q 143070000
20503503 1.0 q 143080000 1.0 q 143090000 1.0 q 143100000 1.0 q 143110000
20503504 1.0 q 143120000 1.0 q 143130000 1.0 q 143140000 1.0 q 143150000
20503505 1.0 q 143160000 1.0 q 143170000 1.0 q 143180000 1.0 q 143190000
20503506 1.0 q 143200000
*
*
$=====
*control variables to calculate total power to compressor
*
*ctlvar name type factor init f c min max
20503600 qrcl_1 mult -1.0 130462160.1
*
*ctlvar v1 p1 v2 p2
20503601 cprtrq 550 cprvel 550
*
*ctlvar name type factor init f c min max
20503700 qrch_1 mult -1.0 126931640.1
*

```



```
*ctrlvar v1 p1 v2 p2
20503701 cprtrq 580 cprvel 580
*
20503800 cpr1 sum 1.0 2.57394+8 1
20503801 0.0 1.0 cntrlvar 036 1.0 cntrlvar 037
*
20503900 cpr1pf sum 1.0 2.4e6 1
20503901 0.0 1.0 p 550010000 -1.0 cprhead 550
*
20504000 Rp1 div 1.0 1.8 1
20504001 cntrlvar 039 p 550010000
*
20504100 cpr2pf sum 1.0 4.5e6 1
20504101 0.0 1.0 p 580010000 -1.0 cprhead 580
*
20504200 Rp2 div 1.0 1.56 1
20504201 cntrlvar 039 p 580010000
```