

16.323 Lecture 8

Constrained Optimal Control - 2

- Can repeat the analysis in Lecture 7 for minimum time and energy problems using the PMP
 - Issue is that the process of developing a solution by analytic construction is laborious and very hard to extend to anything nonlinear and/or linear with more than 2 states
- Need to revisit the problem statement and develop a new approach.
- **Goal:** develop the control input sequence

$$M_i^- \leq u_i(t) \leq M_i^+$$

that drives the system (nonlinear, but linear control inputs)

$$\dot{\mathbf{x}} = A(\mathbf{x}, t) + B(\mathbf{x}, t)\mathbf{u}$$

from an arbitrary state \mathbf{x}_0 to the origin to minimize maneuver time

$$\min J = \int_{t_0}^{t_f} dt$$

- **Solution:** form the Hamiltonian

$$\begin{aligned} H &= 1 + \mathbf{p}^T(t) \{A(\mathbf{x}, t) + B(\mathbf{x}, t)\mathbf{u}\} \\ &= 1 + \mathbf{p}^T(t) \{A(\mathbf{x}, t) + [\mathbf{b}_1(\mathbf{x}, t) \ \mathbf{b}_2(\mathbf{x}, t) \ \cdots \ \mathbf{b}_m(\mathbf{x}, t)] \mathbf{u}\} \\ &= 1 + \mathbf{p}^T(t)A(\mathbf{x}, t) + \sum_{i=1}^m \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t)u_i(t) \end{aligned}$$

- Now use the PMP: select $u_i(t)$ to minimize H , which gives

$$u_i(t) = \begin{cases} M_i^+ & \text{if } \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t) < 0 \\ M_i^- & \text{if } \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t) > 0 \end{cases}$$

which gives us the expected **Bang-Bang** control

- Then solve for the costate

$$\dot{\mathbf{p}} = -H_{\mathbf{x}}^T = - \left(\frac{\partial A}{\partial \mathbf{x}} + \frac{\partial B}{\partial \mathbf{x}} u \right)^T \mathbf{p}$$

– Could be very complicated for a nonlinear system.

- Note: shown how to pick $u(t)$ given that $\mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t) \neq 0$
 - Not obvious what to do if $\mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t) = 0$ for some finite time interval.
 - In this case the coefficient of $u_i(t)$ is zero, and PMP provides no information on how to pick the control inputs.
 - Will analyze this **singular condition** in more detail later.

- To develop further insights, restrict the system model further to LTI, so that

$$A(\mathbf{x}, t) \rightarrow A\mathbf{x} \quad B(\mathbf{x}, t) \rightarrow B$$

- Assume that $[A, B]$ controllable
 - Set $M_i^+ = -M_i^- = u_{m_i}$
 - Just showed that if a solution exists, it is Bang-Bang
 - **Existence:** if $\mathbb{R}(\lambda_i(A)) \leq 0$, then an optimal control exists that transfers any initial state \mathbf{x}_0 to the origin.
 - ◇ Must eliminate unstable plants from this statement because the control is bounded.
 - **Uniqueness:** If an extremal control exists (i.e. solves the necessary condition and satisfies the boundary conditions), then it is unique.
 - ◇ Satisfaction of the PMP is both necessary and sufficient for time-optimal control of a LTI system.
 - If the eigenvalues of A are all real, and a unique optimal control exists, **then each control input can switch at most $n - 1$ times.**
 - Still need to find the costates to determine the switching times – but much easier in the linear case.
-

- **Goal:** develop the control input sequence

$$M_i^- \leq u_i(t) \leq M_i^+$$

that drives the system

$$\dot{\mathbf{x}} = A(\mathbf{x}, t) + B(\mathbf{x}, t)\mathbf{u}$$

from an arbitrary state \mathbf{x}_0 to the origin in a fixed time t_f and optimizes the cost

$$\min J = \int_{t_0}^{t_f} \sum_{i=1}^m c_i |u_i(t)| dt$$

- **Solution:** form the Hamiltonian

$$\begin{aligned} H &= \sum_{i=1}^m c_i |u_i(t)| + \mathbf{p}^T(t) \{A(\mathbf{x}, t) + B(\mathbf{x}, t)\mathbf{u}\} \\ &= \sum_{i=1}^m c_i |u_i(t)| + \mathbf{p}^T(t)A(\mathbf{x}, t) + \sum_{i=1}^m \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t)u_i(t) \\ &= \sum_{i=1}^m [c_i |u_i(t)| + \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t)u_i(t)] + \mathbf{p}^T(t)A(\mathbf{x}, t) \end{aligned}$$

- Use the PMP, which requires that we select $u_i(t)$ to ensure that for all admissible $u_i(t)$

$$\sum_{i=1}^m [c_i |u_i^*(t)| + \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t)u_i^*(t)] \leq \sum_{i=1}^m [c_i |u_i(t)| + \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t)u_i(t)]$$

- If the components of \mathbf{u} are independent, then can just look at

$$c_i |u_i^*(t)| + \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t)u_i^*(t) \leq c_i |u_i(t)| + \mathbf{p}^T(t)\mathbf{b}_i(\mathbf{x}, t)u_i(t)$$

– As before, this boils down to a comparison of c_i and $\mathbf{p}^T(t)\mathbf{b}_i$

– Resulting control law is:

$$u_i^*(t) = \begin{cases} M_i^- & \text{if } c_i < \mathbf{p}^T(t)\mathbf{b}_i \\ 0 & \text{if } -c_i < \mathbf{p}^T(t)\mathbf{b}_i < c_i \\ M_i^+ & \text{if } \mathbf{p}^T(t)\mathbf{b}_i < -c_i \end{cases}$$

- Consider $G(s) = 1/s^2 \Rightarrow$

$$A = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$\min J = \int_{t_0}^{t_f} c|u(t)|dt$$

– Drive state to the origin with t_f fixed.

$$H = |u| + p_1x_2 + p_2u$$

- Consider case with $c = 1$, final control $u(t_f) = u_m \Rightarrow p_2(t_f) < -1$

$$p_2(t) = c_2 - c_1t$$

- As before, integrate EOM forward from 0 to t_2 using $-u_m$, then from t_2 to t_1 using $u = 0$, and from t_1 to t_f using u_m
 - Apply terminal conditions and solve for c_1 and c_2

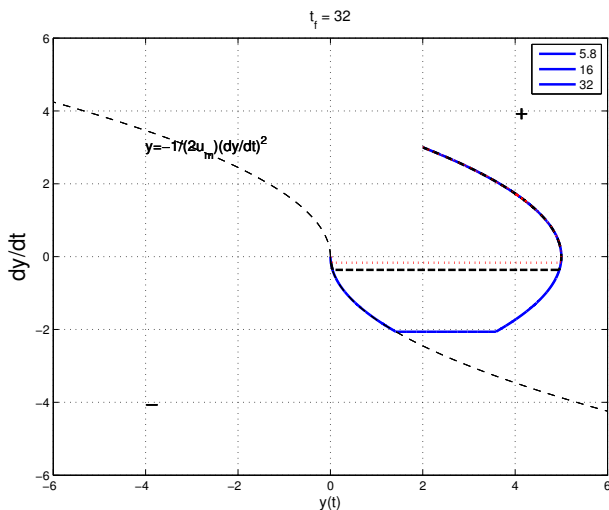


Figure 1: Min Fuel for varying final times

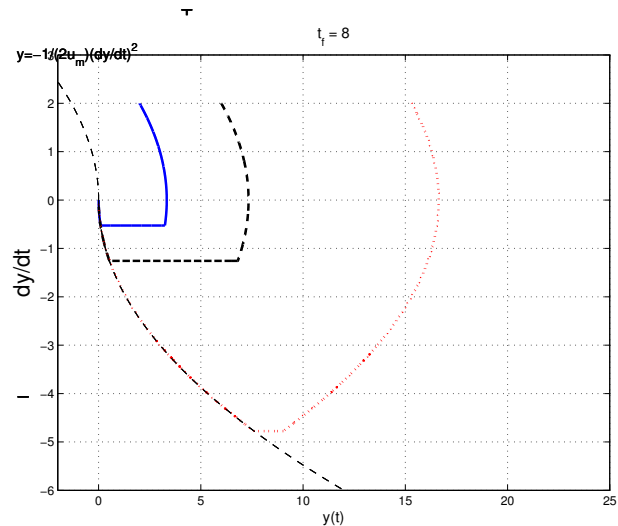


Figure 2: Min fuel for fixed final time, varying IC's

- First switch depends on IC, t_f , and $c \Rightarrow$ no clean closed-form solution
 - Larger c results in longer coast (deadband)
 - Larger t_f leads to longer coast.
 - For given t_f , limit to the IC from which we can reach the origin.

- Goal: for a fixed final time and terminal constraints

$$\min J = \frac{1}{2} \int_0^{t_f} \mathbf{u}^T R \mathbf{u} dt \quad R > 0$$

- Again use special dynamics:

$$\begin{aligned} \dot{\mathbf{x}} &= A(\mathbf{x}, t) + B(\mathbf{x}, t)\mathbf{u} \\ H &= \frac{1}{2} \mathbf{u}^T R \mathbf{u} + \mathbf{p}^T \{ A(\mathbf{x}, t) + B(\mathbf{x}, t)\mathbf{u} \} \end{aligned}$$

- Obviously with no constraints on \mathbf{u} , solve $H_{\mathbf{u}} = 0$, to get

$$\mathbf{u} = -R^{-1} B^T \mathbf{p}(t)$$

- But with bounded controls, must solve:

$$\mathbf{u}^*(t) = \arg \min_{\mathbf{u}(t) \in \mathcal{U}} \left[\frac{1}{2} \mathbf{u}^T R \mathbf{u} + \mathbf{p}^T B(\mathbf{x}, t) \mathbf{u} \right]$$

which is a constrained quadratic program in general

– However, for diagonal R , the effects of the controls are independent

$$\mathbf{u}^*(t) = \arg \min_{\mathbf{u}(t) \in \mathcal{U}} \left[\sum_{i=1}^m \frac{1}{2} R_{ii} u_i^2 + \mathbf{p}^T \mathbf{b}_i u_i \right]$$

– In the unconstrained case, each $u_i(t)$ can easily be determined by minimizing

$$\frac{1}{2} R_{ii} u_i^2 + \mathbf{p}^T \mathbf{b}_i u_i \quad \rightarrow \quad \tilde{u}_i = R_{ii}^{-1} \mathbf{p}^T \mathbf{b}_i$$

- The resulting controller inputs are $u_i(t) = \text{sat}(\tilde{u}_i(t))$

$$u_i(t) = \begin{cases} M_i^- & \text{if } \tilde{u}_i < M_i^- \\ \tilde{u}_i & \text{if } M_i^- < \tilde{u}_i < M_i^+ \\ M_i^+ & \text{if } M_i^+ < \tilde{u}_i \end{cases}$$

Min Fuel

```

1  %
2  % Min fuel for double integrator
3  % 16.323 Spring 2006
4  % Jonathan How
5  %
6  c=1;
7  t=[0:.01:t_f];
8  alp=(1/2/u_m) % switching line
9  T_2=roots([-u_m/2 yd0 y0] + conv([-u_m yd0],[-2 t_f+yd0/u_m])-alp*conv([-u_m yd0],[-u_m yd0]));%
10 t_2=min(T_2);
11 yd2=-u_m*t_2+yd0;yd1=yd2;
12 t_1=t_f+yd1/u_m;
13 c_1=2/(t_1-t_2);c_2=c_1*t_1-1;
14
15 G=ss([0 1;0 0],[0 1]',eye(2),zeros(2,1));
16 arc1=[0:.001:t_2]'; arc2=[t_2:.001:t_1]';arc3=[t_1:.001:t_f]'; %
17 [Y1,T1,X1]=lsim(G,-u_m*ones(length(arc1),1),arc1,[y0 yd0]'); %
18 [Y2,T2,X2]=lsim(G,0*ones(length(arc2),1),arc2,Y1(end,:)''); %
19 [Y3,T3,X3]=lsim(G,u_m*ones(length(arc3),1),arc3,Y2(end,:)''); %
20 plot(Y1(:,1),Y1(:,2),zzz,'Linewidth',2); hold on%
21 plot(Y2(:,1),Y2(:,2),zzz,'Linewidth',2); plot(Y3(:,1),Y3(:,2),zzz,'Linewidth',2);%
22 ylabel('dy/dt','FontSize',18); xlabel('y(t)','FontSize',12);%
23 text(-4,3,'y=-1/(2u_m)(dy/dt)^2','FontSize',12)%
24 text(4,4,'+', 'FontSize',18);text(-4,-4,'-', 'FontSize',18);grid on;hold off
25 title(['t_f = ',mat2str(t_f)], 'FontSize',12)%
26
27 hold on;% plot the switching curves
28 kk=[0:1:8]'; plot(-alp*kk.^2, kk, 'k--');plot(alp*kk.^2, -kk, 'k--');
29 hold off;axis([-4 4 -4 4]/4*6);
30
31 figure(2);%
32 p2=c_2-c_1*t;%
33 plot(t,p2,'Linewidth',4);%
34 hold on; plot([0 t_f],[c c], 'k--', 'Linewidth',2);hold off; %
35 hold on; plot([0 t_f],[-c c], 'k--', 'Linewidth',2);hold off; %
36 hold on; plot([t_1 t_1],[-2 2], 'k:', 'Linewidth',3);hold off; %
37 text(t_1+1,1.5, 't_1', 'FontSize',12)%
38 hold on; plot([t_2 t_2],[-2 2], 'k:', 'Linewidth',3);hold off; %
39 text(t_2+1,-1.5, 't_2', 'FontSize',12)%
40 title(['c = ',mat2str(c), ' u_m = ',mat2str(u_m)], 'FontSize',12);%
41 ylabel('p_2(t)', 'FontSize',12); xlabel('t', 'FontSize',12);%
42 text(1,c+1, 'c', 'FontSize',12);text(1,-c+1, '-c', 'FontSize',12)%
43 axis([0 t_f -3 3]);grid on; %
44
45 return
46
47 figure(1);clf
48 y0=2;yd0=3;t_f=5.8;u_m=1.5;zzz='-';minu;
49 figure(1);hold on
50 y0=2;yd0=3;t_f=16;u_m=1.5;zzz='k--';minu;
51 figure(1);hold on
52 y0=2;yd0=3;t_f=32;u_m=1.5;zzz='r: ';minu;
53 figure(1);
54 legend('5.8', '16', '32')
55 print -f1 -depsc uopt1.eps;jpdf('uopt1');
56
57
58 figure(1);clf
59 y0=2;yd0=2;t_f=8;u_m=1.5;zzz='-';minu
60 figure(1);hold on
61 y0=6;yd0=2;t_f=8;u_m=1.5;zzz='k--';minu
62 figure(1);hold on
63 y0=15.3;yd0=2;t_f=8;u_m=1.5;zzz='r: ';minu
64 figure(1);axis([-2 25 -6 3])
65 print -f1 -depsc uopt2.eps;jpdf('uopt2');

```
