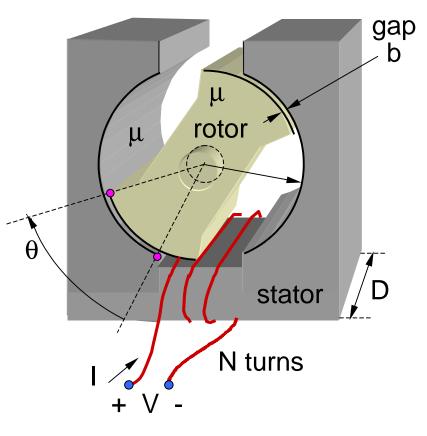
VARIABLE RELUCTANCE MOTORS

Basic 2-Pole Reluctance Motor:

What is the torque on the rotor?

First find B and H:

Since $\nabla \bullet \overline{B} = 0$, then $\overline{B}_{stator} \cong \overline{B}_{gap}$ and $\overline{H}_{stator} \cong (\mu_0/\mu)\overline{H}_{gap} << \overline{H}_{gap}$ $(\mu \cong 10^4 \mu_0)$ $\nabla \times \overline{H} = \overline{J} \Rightarrow$ $NI = \int (\overline{H}_{gap} + \overline{H}_{stator}) \bullet d\overline{s} \cong 2bH_{gap}$ cTherefore $H_{gap} \cong NI/2b$



(independent of rotor cross-sectional area)

VARIABLE RELUCTANCE MOTORS (2)

Find Torque T[Nm] by Differentiating Energy Storage:

Since:
$$W_m \propto \mu |H|^2 / 2 [Jm^{-3}]$$
 and $\overline{H}_{stator} \cong (\mu_0 / \mu) \overline{H}_{gap}$

Therefore: $W_{gap} \cong (\mu/\mu_0) W_{stator} [Jm^{-3}]$

So if: $b/2R \ll \mu_0/\mu$

Then:

 $w_{gap} \gg w_{stator}[J]$ where $w_{gap} \approx 2bR\theta D\mu_0 |H_{gap}|^2/2$

Where: Gap area = $R\theta D[m^2]$ (for $0 < \theta < \pi/2$)

Therefore(?):
$$T = -\partial w_{gap} / \partial \theta = -bRD\mu_0 |H_{gap}|^2$$

WRONG SIGN!

To find force we must always differentiate <u>total</u> energy, including the energy in the power supply!

To Find Torque Correctly:

Can include the changing source energy, but easier to reformulate the energy expression

h

μ rotor

stator

N turns

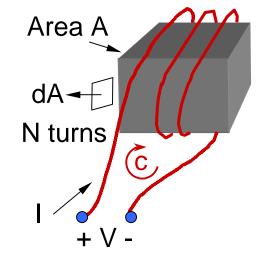
μ

FLUX LINKAGE Λ AND INDUCTANCE L

Definition of Flux Linkage Λ :

Flux Linkage $\Lambda = N \int_A \overline{B} \bullet d\overline{a}$

$$-\nabla \times \overline{E} = \partial \overline{B} / \partial t = N \int_{A} (d\overline{B} / dt) \bullet d\overline{a} = d\Lambda / dt$$
$$-\int \overline{E} \bullet d\overline{s} = V = \frac{d\Lambda}{dt} = L di / dt$$
c coil
Therefore:



Reluctance-Motor Flux Linkage Λ :

- $V = d\Lambda/dt = 0$ if motor short-circuited; therefore
- $\Lambda = \text{constant} \neq f(\theta) \text{ (key step)}$

$$\begin{split} \Lambda &= N\mu_o H_{gap} A_{gap} = N^2 \mu_o I A_{gap}/2b, \text{ where } H_{gap} = NI/2b \text{ [see L22-1]} \\ A_{gap} &= RD\theta \text{ here [L22-2]} \\ L &= \Lambda/I = N^2 \mu_o A_{gap}/2b \end{split}$$

RELUCTANCE MOTOR TORQUE

Energy Storage and Torque with the Source Short-Circuited:

$$\begin{split} & \mathsf{W}_{\mathsf{m}} = \mathsf{L}\mathsf{I}^{2}/2 = \Lambda^{2}/2\mathsf{L} \quad (\mathsf{I} = \Lambda/\mathsf{L}) \\ & \mathsf{T} = -\partial \mathsf{W}_{\mathsf{m}}/\partial\theta = -\Lambda^{2}\partial(1/2\mathsf{L})/\partial\theta = -\Lambda^{2}\partial(\mathsf{b}/\mathsf{N}^{2}\mu_{o}\mathsf{A}_{\mathsf{gap}})/\partial\theta \quad [\mathsf{A}_{\mathsf{gap}} = \mathsf{R}\theta\mathsf{D}] \\ & = -(\Lambda^{2}\mathsf{b}/\mathsf{N}^{2}\mu_{o}\mathsf{R}\mathsf{D})\partial\theta^{-1}/\partial\theta = \Lambda^{2}\mathsf{b}/\mathsf{N}^{2}\mu_{o}\mathsf{R}\mathsf{D}\theta^{2} \\ & \mathsf{Recall} \Lambda = \mathsf{N}^{2}\mu_{o}\mathsf{I}\mathsf{A}_{\mathsf{gap}}/2\mathsf{b} \quad [\mathsf{see} \ \mathsf{L}22\text{-}3] \\ & \mathsf{T} = (\mathsf{N}^{2}\mu_{o}\mathsf{I}\mathsf{R}\theta\mathsf{D}/2\mathsf{b})^{2}\mathsf{b}/\mathsf{N}^{2}\mu_{o}\mathsf{R}\mathsf{D}\theta^{2} \end{split}$$

Therefore:

 $T = N^{2}\mu_{o}I^{2}RD/4b \ [Nm] = (\mu_{o}H_{gap}^{2}/2)(2bRD) \ \neq f(\theta) \quad (e.g. \text{ for } 0 < \theta < \pi/2)$

 $T = W_{mgap}(dV_{olume}/d\theta)$ [Nm]

~Same as for electric motors!

T is limited by maximum energy density

Maximize T: maximize (NI)² and RD (~weight), minimize b (tolerances)

Motor Drive Circuit:

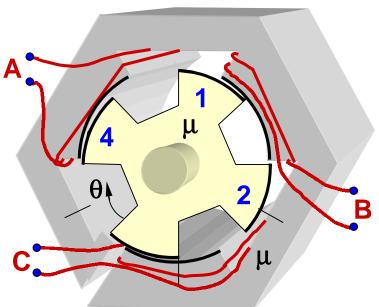
I is turned on when A_{gap} is minimum; torque then increases A_{gap} as the rotor is pulled by the stator. When A_{gap} = maximum, I is set to zero and the rotor coasts until A_{gap} = minimum, and the cycle repeats. (<50% duty cycle here)

¾-POLE VARIABLE RELUCTANCE MOTOR

Winding Excitation Plan:

Start by exciting windings A,B; this pulls pole 1 into pole B; for winding A, the pole area is temporarily constant. When $\Delta \theta = \pi/3$, the currents are switched to B,C; when $\Delta \theta = 2\pi/3$ we excite C,A. Repeating this cycle results in nearly constant clockwise torque.

To go counter-clockwise, excite BC, then AB, then CA.



Torque:

Only one pole is being pulled in; the other winding has either one rotor pole fully in, or one entering and one leaving that cancel. Many pole combinations are used (more poles, more torque).

PERMANENT MAGNET SYSTEMS

Refrigerator Magnets:

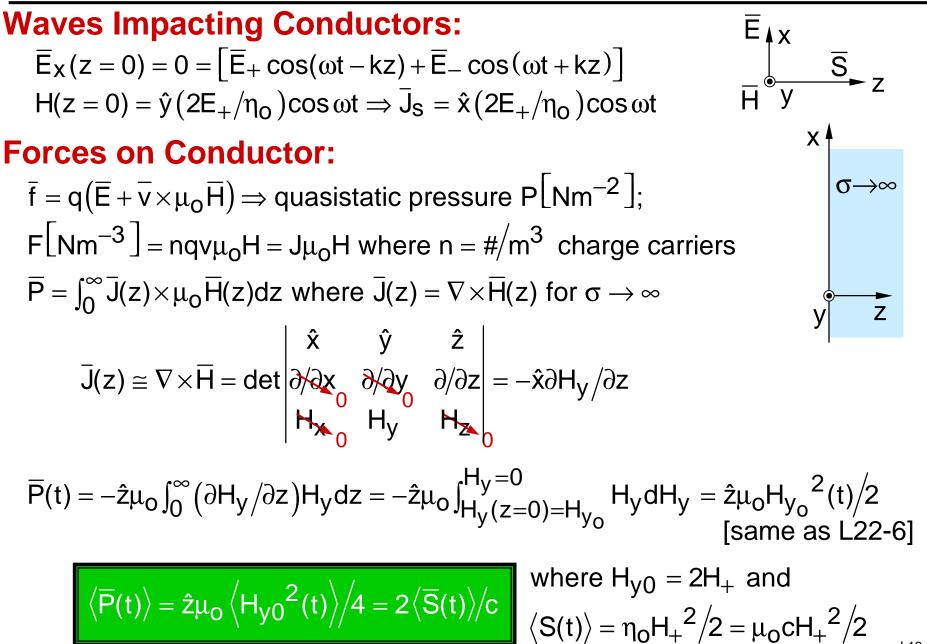
Force: $f = -dw_m/db$ South poleVariable energy: $w_m \cong bA\mu_0H_{gap}^2/2$ [J]Area A $= bAB_{gap}^2/2\mu_0$ $W_m \neq -f(b)$ $W_m \neq -f(b)$ Force density: $f/A = B_{gap}^2/2\mu_0$ [Nm⁻²] W_m^2

Example: Let B = 1 Tesla (10,000 gauss), A = 10 cm² Then f = $0.001 \times 1^2/2 \times 4\pi 10^{-7} \cong 400$ N \cong 100-lb force

Permanent Magnet Properties:

Strength:Typical strong magnets ~0.2T; can \rightarrow 1TeslaTemperature :Above ~200C they fail; some fail at low temperatures

FORCES FROM ELECTROMAGNETIC WAVES



PHOTON PRESSURE

Photon Energy:

hf [J] = "m"
$$c^2$$

h = Planck's constant = 6.625×10^{-34} [Js], f = frequency [Hz]

Photon Momentum:

Transferred to mirror upon reflection: Δ momentum = 2hf/c

Photon Pressure P [Nm⁻²]:

Pressure P is change of momentum $s^{-1}m^{-2}$ [Mechanics: f = d(mv)/dt]

 $\langle P \rangle = n2hf/c = 2\langle S(t) \rangle/c$ [Nm⁻²] where n = # photons reflected s⁻¹m⁻²

If a photon is absorbed, then Δ momentum = hf/c, and P = $\langle S(t) \rangle / c$ In general, if the incident and reflected fluxes are S_1 and S_2 [Wm⁻²],

$$\langle P \rangle = \langle S_1 - S_2 \rangle / c \quad \left[Nm^{-2} \right]$$

Solar Sailing Across Solar System:

Say 1 km² at 1.4 kW/m² \Rightarrow A $\langle P \rangle = A2 \langle S \rangle / c = 10^6 \times 2800 / 3 \times 10^8 = 9N$ (say 10⁻⁶ thick, $\rho = 1g/cm^3$) $v = at = (f/m)t \cong (9/1000)3 \times 10^7 \cong 3 \times 10^5 \text{ ms}^{-1}$ in 1 year = $10^{-3}c$