#### SPHEROIDAL SOLUTION FOR UNBOUNDED ORBITS

#### ABOUT AN OBLATE PLANET

by

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S.B., Massachusetts Institute of Technology

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Thomas J. Lang

Submitted to the Department of Aeronautics and Astronautics on

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#### ABSTRACT

This paper derives the equations of motion for a satellite in an unbounded orbit about an oblate planet. The only force assumed present is the one due to Vinti's spheroidal gravitational potential, which can be fitted to the Earth so as to account exactly for the even zonal harmonics through the second and for most of the fourth. The equations of motion in integral form are obtained as a result of the separability of the Hamilton-Jacobi equation. Two sets of orbital elements are used for the solution. The first set can be obtained directly from a set of initial conditions. The second set, which allows analytical evaluation of the integrals, can be obtained from the first through numerical factoring of a quartic polynomial. The final solution, which is summarized in Chapter 10, is given in terms of this second set of orbital elements and certain uniformizing variables, whose periodic terms are correct to the second order in  $J_2$ .

The solution is valid for all inclinations, has no troublesome poles and reduces to Keplerian hyperbolic motion for a perfectly spherical planet. In order that certain series converge, however, we find it necessary to restrict out attention to trajectories whose extensions do not pass through a small spheroid in the center of the planet. A computer program is also presented which calculates the trajectory about both an oblate planet and a perfectly spherical planet for the same initial conditions.

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#### CHAPTER I

#### INTRODUCTION

If we let  $\underline{r}$  be the position vector of a satellite relative to the center of mass of an oblate planet and if forces other than the gravitational forces between the two bodies can be neglected, then the motion of the satellite is determined by the equation

$$\mathbf{r} = -\nabla \mathbf{V} \tag{1.1}$$

The gravitational potential V of the planet can be expressed in terms of spherical harmonics as

$$V = -\frac{\mu}{r} \left[ 1 - \sum_{n=2}^{\infty} \left( \frac{r_e}{r} \right)^n J_n P_n(\sin\theta) \right] + \text{tesseral harmonics}$$
(1.2)

where  $\mu$  is the product of the gravitational constant and the mass of the planet, r is the magnitude of the position vector,  $r_e$  is the equatorial radius,  $\theta$  is the declination,  $P_n$  is the nth Legendre polynomial, and the  $J_n$  are constants which characterize the planet's potential. For the Earth  $J_2 \simeq 1.08 \times 10^{-3}$  and all other  $J_n$ 's are of the order  $10^{-6}$  or smaller.

Most methods of solving the equations of motion involve determining a reference trajectory using the potential  $V_0 = -\frac{\mu}{r}$  and then determining the pertubations of this reference trajectory caused by the higher harmonics of the true potential. Vinti [1], however, derived a form for the potential of an oblate planet as the solution of Laplace's equation in oblate spheroidal coordinates which leads to separability of the Hamilton-Jacobi equation. As used in this paper Vinti's spheroidal potential accounts for the second zonal harmonic  $J_2$  and most of the fourth. Using his spheroidal potential Vinti [2,3] then solved the resulting equations of motion for the case of a bounded orbit, that is for total energies  $\alpha_1 < 0$ . The solution has an exact secular part and a periodic part correct to the second order in  $J_2$ .

The main object of the present paper is to provide a solution using Vinti's spheroidal potential for the case of an unbounded trajectory, that is for total energy  $\alpha_1 > 0$ . The approach will be to introduce certain uniformizing variables and then to evaluate the integrals of the equations of motion in terms of these variables in a manner analagous to that of Vinti for the bounded case. The equations of motion are then inverted so as to obtain the position and velocity vectors as functions of time. In order that the similarities between the bounded case and the unbounded case to be derived may be apparent, Vinti's notation has been preserved as far as possible in the present treatment. In addition we shall show that the solution for the unbounded case reduces to simple Keplerian hyperbolic motion for a perfectly spherical planet and that the solutions for bounded and unbounded spheroidal trajectories reduce to the same "parabolic" trajectory for  $\alpha_1 = 0$ .

A computer program is also developed which calculates the trajectory about both an oblate planet and a spherical planet for the same initial conditions. A numerical comparison then enables us to determine the effect of the oblateness and how it varies with the energy, inclination, and perigee distance of the trajectory.

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#### CHAPTER 2

#### THE KINETIC EQUATIONS

#### 2.1 The Oblate Spheroidal Coordinates

Of the eleven Staeckel coordinate systems, the oblate spheroidal system has the most appropriate symmetry for an oblate planet such as the Earth. If X, Y, Z are the rectangular coordinates and r,  $\theta$ ,  $\phi$  are the spherical coordinates, then the oblate spheroidal coordinates,  $\rho$ ,  $\eta$ ,  $\phi$ , are defined by

$$X + iY = r \cos\theta \exp i\phi = \left[ (\rho^2 + c^2)(1 - \eta^2) \right]^{\frac{1}{2}} \exp i\phi \qquad (2.1)$$

$$Z = r \sin \theta = \rho \eta \qquad (-1 \le \eta \le 1) \quad (\rho \ge 0) \qquad (2.2)$$

Here r and  $\theta$  are the geocentric distance and declination, and  $\phi$  is the right ascension. For the spheroidal coordinates, the surfaces of constant  $\rho$  are oblate spheroids, the surfaces of constant  $\eta$  are hyperboloids of one sheet, and the surfaces of constant  $\phi$  are planes through the polar axis. The constant, c, is the radius of the focal circle in the equatorial plane. The portion of the equatorial plane inside the focal circle is the surface  $\rho = 0$ , while the portion outside is the surface  $\eta = 0$ . Note that for large r,  $\rho = r$  and  $\eta = \sin\theta$ .

#### 2.2 The Gravitational Potential

According to Vinti [1] the potential field of an oblate body may be closely represented by



FIGURE 2.1 The Oblate Spheroidal Coordinates

$$V = -\mu \rho \left(\rho^2 + c^2 \eta^2\right)^{-1}$$
(2.3)

where  $\mu$  is the product of the gravitational constant and the planetary mass, and

$$c^2 = r_{e}^2 J_2$$
 (2.4)

where  $r_e$  is the planet's equatorial radius and  $J_2$  is the coefficient of the second zonal harmonic in the expansion of the potential in spherical harmonics. For the Earth  $J_2$  is approximately  $1.082 \times 10^{-3}$  and  $c \approx 210$  km. In the equation for the potential, (2.3), we have taken the center of mass at the origin of the coordinate system.

The above potential leads to separability of the Hamilton-Jacobi equation in spheroidal coordinates. From Vinti [1], the resulting kinetic equations with the separation constants  $\alpha_1$ , k,  $\alpha_3$  and the Hamilton-Jacobi function  $S(\rho, \eta, \phi)$  are

$$\frac{\partial S}{\partial \alpha_{1}} = t + \beta_{1} = \int_{\rho_{1}}^{\rho} t \rho^{2} \frac{1}{F}(\rho) d\rho + c^{2} \int_{\eta_{1}}^{\eta} t \eta^{2} \frac{1}{G}(\eta) d\eta$$

$$\frac{\partial S}{\partial k} = \beta_{2}^{2} = \frac{1}{2} \int_{\rho_{1}}^{\rho} t \frac{-1}{F}(\rho) d\rho + \frac{1}{2} \int_{\eta_{1}}^{\eta} t \frac{-1}{G}(\eta) d\eta \qquad (2.5)$$

$$\frac{\partial S}{\partial \alpha_{3}} = \beta_{3} = \phi + c^{2} \alpha_{3} \int_{\rho_{1}}^{\rho} t (\rho^{2} + c^{2}) F^{-\frac{1}{2}}(\rho) d\rho + \alpha_{3} \int_{\eta_{1}}^{\eta} t (1 - \eta^{2})^{-1} G^{-\frac{1}{2}}(\eta) d\eta$$

where

$$F(\rho) = c^2 \alpha_3^2 + (\tilde{k} + 2\mu\rho + 2\alpha_1\rho^2)(\rho^2 + c^2)$$
(2.6)

and

$$G(\eta) = -\alpha_3^2 + (1-\eta^2)(-\tilde{k}+2\alpha^1c^2\eta^2)$$
(2.7)

and the betas are Jacobi constants. For bounded motion,  $\alpha_1$  is negative. For such motion Vinti [1] has shown that the constant  $\tilde{k}$  is negative, a fact which leads to considerable simplification of the integrals.

#### 2.3 The Separation Constant k

We should now like to investigate the separation constant  $\tilde{k}$ , for unbounded motion  $\alpha_1 > 0$ . According to Vinti [1] the final separation of the Hamilton-Jacobi equation becomes (for the CM at the origin)

$$(\xi^{2}+1)(\frac{\partial S}{\partial \xi})^{2} - (\xi^{2}+1)^{-1}\alpha_{3}^{2} - 2\mu c\xi - 2\alpha_{1}c^{2}\xi^{2} = -(1-\eta^{2})(\frac{\partial S}{\partial \eta})^{2} - (1-\eta^{2})^{-1}\alpha_{3}^{2} + 2\alpha_{1}c^{2}\eta^{2} = \tilde{k}$$
(2.8)

where  $\rho = c\xi$ .

Since we have taken the center of mass of the earth to be at the origin of the coordinate system we can assume that the trajectory (or its extension) will pass through the equatorial plane. Furthermore, we will require this passage to occur on or outside the focal circle which is shown in Figure 2.2. Thus  $\eta = 0$  will be reached by the trajectory and according to (2.8)

$$\tilde{k} + \alpha_3^2 = -\left(\frac{\partial S}{\partial \eta}\right)^2 \leq 0$$
(2.9)

For physically realizable motion the Kinetic equations (2.5) require that  $F(\rho)$  and  $G(\eta)$  be positive and our coordinate system requires that  $\eta^2 \leq 1$  and  $\rho \geq 0$ . Rewriting  $F(\rho)$  in the form

$$F(\rho) = c^2 \alpha_3^2 + 2\alpha_1(\rho^2 + c^2) \left[ \left( \dot{\rho} + \frac{\mu}{2\alpha_1} \right) + \frac{\tilde{k}}{2\alpha_1} - \frac{\mu^2}{4\alpha_1^2} \right]$$
(2.10)

and setting  $a_3 = 0$ , we find for the two real zeroes of  $F(\rho)$ 

$$\rho = -\frac{\mu}{2\alpha_1} \pm \left[\frac{\mu^2}{4\alpha_1^2} - \frac{\tilde{k}}{2\alpha_1}\right]^{\frac{1}{2}}$$
(2.11)



FIGURE 2.2 The Equatorial Plane

The more positive of the two roots will be labeled  $\rho_1$ , the other  $\rho_2$ . Equation (2.9) can be rewritten as

$$\tilde{k} \leq -a_3^2 \tag{2.12}$$

A consideration of the derivatives of  $F(\rho)$  and the values of  $F(\rho)$  for  $\rho = \pm \infty$  enables us to sketch  $F(\rho)$  for  $\alpha_3 = 0$  as in Figure 2.3. Realizable motion then takes place in the shaded region of the sketch from  $\rho = \rho_1$  to  $\rho = \infty$ . Clearly  $\rho_1$  is the  $\rho$ -perigee of the trajectory.

For the case  $\alpha_3 \neq 0$  we put  $F(\rho)$  in the form

$$F(\rho) = 2\alpha_1 \rho^4 + 2\mu \rho^3 + (\tilde{k} + 2\alpha_1 c^2) \rho^2 + 2\mu c^2 \rho + c^2 (\tilde{k} + \alpha_3^2)$$
(2.13)

At  $\rho = 0$  we then have

$$F(0) = c^{2}(\tilde{k} + \alpha_{3}^{2})$$
(2.14)

F(0) will then be non-positive if (2.12) is imposed. For convergence of certain series we will later find it necessary to restrict our attention to trajectories with

$$2\alpha_1 c^2 << -\tilde{k}$$
 (2.15)

Thus the third and fifth terms of (2.13) are negative for  $\rho > 0$  so that, by Descarte's rule of sign, there are no more than three positive real zeroes of  $F(\rho)$ . A similar consideration for  $\rho < 0$  reveals that  $F(\rho)$  has no more than one negative real zero.  $F(\rho)$  might then appear as in Figure 2.4 for  $\alpha_3 \neq 0$ . Again realizable motion occurs only for  $\rho$  and  $F(\rho)$  nonnegative. We shall later see that case (b) of Figure 2.4 occurs only for equatorial or very nearly equatorial orbits.



FIGURE 2.3 Sketch of  $F(\rho)$  for  $\aleph_3 = 0$ 



FIGURE 2.4 Sketch of  $F(\boldsymbol{\rho})$  for  $\boldsymbol{\alpha}_3 \neq 0$ 

According to (2.12) we can then set

$$\tilde{k} = -\alpha_2^2 \tag{2.16}$$

where

$$\alpha_2^2 \ge \alpha_3^2 \tag{2.17}$$

Having done this we can take  $\alpha_2$  as our new Jacobi constant. The equations (2.5), (2.6), and (2.7) then become

$$\frac{\partial S}{\partial \alpha_1} = t + \beta_1 = \int_{\rho_1}^{\rho} t \rho^2 F^{-\frac{1}{2}}(\rho) d\rho + c^2 \int_{0}^{\eta} t \eta^2 G^{-\frac{1}{2}}(\eta) d\eta \qquad (2.18a)$$

$$\frac{\partial S}{\partial \alpha_2} = \beta_2 = \alpha_2 \int_{\rho_1}^{\rho} F^{-\frac{1}{2}}(\rho) d\rho + \alpha_2 \int_{0}^{\eta} G^{-\frac{1}{2}}(\eta) d\eta$$
(2.18b)

$$\frac{\partial S}{\partial \alpha_3} = \phi - \beta_3 = c^2 \alpha_3 \int_{\rho_1}^{\rho_{\pm}} (\rho^2 + c^2)^{-1} F^{-\frac{1}{2}}(\rho) d\rho + \alpha_3 \int_{\rho_1}^{\eta_{\pm}} (1 - \eta^2)^{-1} G^{-\frac{1}{2}}(\eta) d\eta$$
(2.18c)

where

$$F(\rho) = c^2 \alpha_3^2 + (\rho^2 + c^2)(-\alpha_2^2 + 2\mu\rho + 2\alpha_1\rho^2)$$
(2.19)

and

$$G(n) = -\alpha_3^2 + (1-n^2)(\alpha_2^2 + 2\alpha_1 c^2 n^2)$$
(2.20)

The  $\alpha$ 's and  $\beta$ 's are the Jacobi constants, with  $\alpha_1$ , the energy, greater than zero for hyperbolic motion and  $\alpha_3$ , the polar component of angular momentum, greater than or less than zero for direct or retrograde trajectories respectively. As  $c \rightarrow 0$  and we approach Keplerian motion the separation constant  $\alpha_2$  reduces to the total angular momentum, -  $\beta_1$  to the time of perigee passage,  $\beta_2$  to the argument of perigee  $\omega$ , and  $\beta_3$  to the longitude of the node  $\Omega$ . (These claims will be justified in Section 7)

Since terms with  $c^2$  in them represent the deviations from a conic trajectory (which we expect to be small) the appropriate zeroes,  $\rho_1$  and  $\rho_2$ , of F( $\rho$ ) will approximately be equal to the zeroes of

$$f(\rho) = (-\alpha_2^2 + 2\mu\rho + 2\alpha_1\rho^2)$$
(2.21)

Since  $\alpha_1 \ge 0$ , this tells us that one zero will be positive, the other negative (approaching  $-\infty$  as  $\alpha_1$  approaches zero); which is just what we found in our investigation of  $F(\rho)$ . The positive zero has been labeled  $\rho_1$ ; the negative zero,  $\rho_2$ . We will discover shortly that the other two roots of  $F(\rho)$  are imaginary, except for nearly equatorial orbits.

Our ultimate objective is to solve (2.18), (2.19), and (2.20) for  $\rho$ ,  $\eta$ ,  $\phi$  as functions of time. To do this we must first solve (2.18a) and (2.18b) for  $\rho(t)$  and  $\eta(t)$  and substitute into (2.18c) to find  $\phi(t)$ . This requires evaluating the six integrals which we shall find possible through the introduction of certain uniformizing variables, and the ability to factor the quartic polynomials  $F(\rho)$  and  $G(\eta)$ .

#### CHAPTER 3

# THE ORBITAL ELEMENTS $a_0$ , $e_0$ , $i_0$ , $\beta_1$ , $\beta_2$ , $\beta_3$

For Keplerian hyperbolic motion (c = 0) the two roots of  $f(\rho)$  would be

$$\rho_1 = r_1 = a_0(e_0 - 1) \tag{3.1}$$

$$\rho_2 = \mathbf{r}_2 = -\mathbf{a}_0(\mathbf{e}_0 + 1) \tag{3.2}$$

where  $r_1$  would be the perigee radius and  $r_2$  an unphysical quantity. For future reference we solve for  $a_0$  and  $e_0$  from the above. Thus

$$a_0 = -\frac{(r_1 + r_2)}{2}$$
(3.1a)

$$e_0 = -\frac{(r_1 - r_2)}{r_1 + r_2}$$
(3.2a)

Here we have taken

$$a_0 = \frac{1}{2} \mu \alpha_1^{-1}$$
 (3.3)

and

$$e_0^2 \equiv 1 + 2\alpha_1 \alpha_2^2 \mu^{-2}$$
 (3.4)

For our spheroidal solution with  $c \neq 0$  we can still define the constants  $a_0$  and  $e_0$  as above as well as another constant

$$i_0 \equiv \cos^{-1}(\alpha_3/\alpha_2) \tag{3.5}$$

Thus the constants  $a_0$ ,  $e_0$ ,  $i_0$ ,  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$  would be one possible set of orbital elements. The corresponding semi-latus rectum  $p_0$  would then be

$$p_0 = a_0(e_0^2 - 1) \tag{3.6}$$

so that

$$\alpha_2^2 = \mu p_0 \tag{3.7}$$

To find  $a_0$ ,  $e_0$ , and  $i_0$  we first need  $\alpha_1$ ,  $\alpha_2$ , and  $\alpha_3$ . These constants may be determined from the initial conditions. From Vinti [2]

$$\alpha_{1} = \frac{1}{2}u_{1}^{2} - \mu\rho_{1}(\rho_{1}^{2} + c^{2}\eta_{1}^{2})^{-1}$$
(3.8)

$$\alpha_{2}^{2} = (1 - \eta_{1}^{2})^{-1} [(\rho_{1}^{2} + c^{2} \eta_{1}^{2})^{2} \eta_{1}^{2} + \alpha_{3}^{2} - 2\alpha_{1}c^{2} \eta_{1}^{2}(1 - \eta_{1}^{2})]$$
(3.9)

$$\alpha_{3} = r_{i}^{2} \cos^{2} \theta_{i} \phi_{i} = X_{i} Y_{i} - Y_{i} X_{i}$$
(3.10)

where the subscript i denotes initial values and u is the speed. So from the initial coordinates and their derivatives we can determine the  $\alpha$ 's and thus find  $a_0$ ,  $e_0$ , and  $i_0$ . Numerical values for the  $\alpha$ 's would allow numerical factoring of  $F(\rho)$  in the form

$$F(\rho) = 2\alpha_1(\rho - \rho_1)(\rho - \rho_2)(\rho^2 + A\rho + B)$$
(3.11)

We can, however get an analytical solution for  $\rho_1 + \rho_2$ ,  $\rho_1 \rho_2$ , A, and B by following the procedure of Vinti [2] and equating corresponding powers of  $\rho$  in (3.11) and (2.19). Thus we find

$$\rho^{3}: \quad \rho_{1}+\rho_{2}-A = -\mu\alpha_{1}^{-1} = -2a_{0} \qquad (3.12)$$

$$\rho^{2}: \quad B+\rho_{1}\rho_{2}-(\rho_{1}+\rho_{2})A = c^{2}-\frac{1}{2}\alpha_{2}^{2}\alpha_{1}^{-1} = c^{2}-a_{0}p_{0}$$
(3.13)

$$\rho^{1}: \quad (\rho_{1}+\rho_{2})B-\rho_{1}\rho_{2}A = -\mu c^{2}\alpha_{1}^{-1} = -2a_{0}c^{2} \qquad (3.14)$$

$$\rho^{0}: \quad \rho_{1}\rho_{2}B = -\frac{1}{2}c^{2}(\alpha_{2}^{2}-\alpha_{3}^{2})\alpha_{1}^{-1} = -a_{0}p_{0}c^{2}\sin^{2}i_{0} \qquad (3.15)$$

We can define

$$k_0 \equiv c^2/p_0^2 \equiv \left(\frac{r_e}{p_0}\right)^2 J_2$$
 (3.16)

$$x \equiv (e_0^2 - 1)^{\frac{1}{2}}$$
 (3.17)

$$y \equiv \alpha_3/\alpha_2 = \cos i_0 \tag{3.18}$$

and then solve (3.12) through (3.15) for  $\rho_1\rho_2$ ,  $\rho_1 + \rho_2$ , A, and B by assuming that each is a power series in  $k_0$ 

$$\rho_1 + \rho_2 \equiv \sum_{n=0}^{\infty} b_{1n} k_0^n$$
 (3.19)

$$\rho_1 \rho_2 \equiv \sum_{n=0}^{\infty} b_{2n} k_0^n$$
 (3.20)

$$A \equiv \sum_{n=0}^{\infty} b_{3n} k_0^{n}$$
 (3.21)

$$B \equiv \sum_{n=0}^{\infty} b_{4n} k_0^n \qquad (3.22)$$

and solving for the coefficients. For sufficiently small  $k_0$  the series will converge rapidly (the range of validity of this assumption will be investigated at the end of this section) and the solution to  $O(k_0^2)$  will be sufficiently accurate. The series solution, which is carried out in Appendix A, results in:

$$\rho_1 + \rho_2 = \frac{-2p_0}{x^2} \left[ 1 + x^2 y^2 k_0 + x^2 y^2 k_0^2 (8y^2 + 3x^2 y^2 - 2x^2 - 4) + \cdots \right] \quad (3.23)$$

$$\rho_1 \rho_2 = \frac{-p_0^2}{x^2} \left[ 1 - y^2 k_0 (4 + x^2) + k_0^2 y^2 (12x^2 - 20x^2 y^2 - 32y^2 + 16) + x^4 - x^4 y^2 \right]$$
(3.24)

$$A = -2k_0 p_0 y^2 \left[ 1 + k_0 (8y^2 + 3x^2 y^2 - 2x^2 - 4) + \cdots \right]$$
(3.25)

$$B = k_0 p_0^2 (1-y^2) \left[ 1 + k_0 (4y^2 + x^2y^2) + \cdots \right]$$
(3.26)

Note that

$$A^{2} - 4B \approx -4k_{0}p_{0}^{2} \left[ 1 - y^{2} + k_{0}(4y^{2} - 5y^{4} + x^{2}y^{2} - x^{2}y^{4}) \right]$$
(3.27)

which is positive for  $\sin^2 i_0 < k_0/[1+k_0(6+x^2)]$  so that for equatorial or very nearly equatorial orbits we have case (b) of Figure 2.4.

We can define the constants a and e in terms of the two real roots of  $F(\rho)$ . By analogy to Keplerian motion, equations (3.1), (3.2), (3.1a), and (3.2a) we define

$$\rho_1 \equiv \mathbf{a}(\mathbf{e}-\mathbf{1}) \tag{3.28}$$

$$\rho_2 \equiv -a(e+1)$$
 (3.29)

so that

$$a = -\frac{(\rho_1 + \rho_2)}{2}$$
 (3.30)

and

$$e \equiv -\frac{\rho_1 - \rho_2}{\rho_1 + \rho_2}$$
 (3.31)

the corresponding semi-latus rectum is

$$p \equiv a(e^2-1) = -\frac{\rho_1 \rho_2}{a}$$
 (3.32)

The constants a, e, and p will occur in the evaluation of the  $\rho$ -integrals. We can calculate them in terms of  $a_0$ ,  $e_0$ ,  $p_0$ , and  $i_0$  to the second order in  $k_0$  as follows: From (3.30)

$$\frac{a}{a_0} = -\frac{(\rho_1 + \rho_2)}{2a}$$

Substituting for  $\rho_1 + \rho_2$  from (3.23) yields

$$\frac{a}{a_0} = 1 + k_0 x^2 y^2 + k_0^2 x^2 y^2 (8y^2 + 3x^2 y^2 - 2x^2 - 4) + \cdots$$
(3.33)

Then from (3.32) and (3.30)

$$\frac{p}{p_0} = -\frac{\rho_1 \rho_2}{a p_0} = \frac{2\rho_1 \rho_2}{p_0 (\rho_1 + \rho_2)}$$

Substituting for  $\rho_1\rho_2$  and  $\rho_1+\rho_2$  from (3.24) and (3.23) and using the binomial expansion theorem we find

$$\frac{p}{p_0} = 1 - 2k_0 y^2 (2 + x^2) + k_0^2 y^2 (16x^2 - 24x^2 y^2 - 32y^2 + 16) + 3x^4 - 2x^4 y^2) + \cdots$$
(3.34)

or equivalently

$$\frac{p_0}{p} = 1 + 2k_0y^2(2+x^2) + k_0^2y^2(-3x^4+6x^4y^2-16x^2) + 40x^2y^2-16+48y^2) + \cdots$$
(3.35)

Then since

$$\frac{e^2 - 1}{e_0^2 - 1} = \frac{p}{p_0} \frac{a_0}{a}$$

we find

$$\frac{e^{2}-1}{e_{0}^{2}-1} = 1 + k_{0}y^{2}(-3x^{2}-4) + k_{0}^{2}y^{2}(5x^{4}-2x^{4}y^{2} + 20x^{2}-28x^{2}y^{2}+16-32y^{2}) + \cdots$$
(3.36)

and thus

$$\left(\frac{e^{2}-1}{e_{0}^{2}-1}\right)^{2} = 1 + \frac{1}{2} k_{0}y^{2}(-3x^{2}-4) + \frac{1}{8} k_{0}^{2}y^{2}(20x^{4}) - 17x^{4}y^{2} + 80x^{2} - 136x^{2}y^{2} + 64 - 144y^{2}) + \cdots$$
(3.37)

We can calculate e in terms of  $e_0$  by noting

$$e \equiv \left[ (e^2 - 1) + 1 \right]^{\frac{1}{2}}$$
 (3.38)

substituting for (e<sup>2</sup>-1) from (3.36) and taking the square root we find that, to first order in  $k_0$ 

$$e = \left[ (e_0^2 - 1) [1 + k_0 y^2 (-3x^2 - 4) + \cdots ] + 1 \right]^{\frac{1}{2}}$$

so that

$$e = \left[ e_0^2 - x^2 y^2 k_0 (3x^2 + 4) + \cdots \right]^{\frac{1}{2}}$$
(3.39)

We shall later regard a and e as two of the final orbital elements, since they are part of a set from which the orbit can be calculated immediately. The above equations show how to find a, e, and related quantities, without iteration, from those quantities  $a_0$ ,  $e_0$ , and  $i_0$  which are obtainable immediately from the initial conditions.

The quartic G(n) may be put in the factored form

$$G(\eta) \equiv (\alpha_2^2 - \alpha_3^2) \eta^4 (\eta^{-2} - \eta_0^{-2}) (\eta^{-2} - \eta_2^{-2})$$
(3.40)

On comparing this with (2.20) we find that  $n_0^{-2}$  and  $n_2^{-2}$  are the roots of

$$(\alpha_2^2 - \alpha_3^2)\eta^{-4} + (2\alpha_1 c^2 - \alpha_2^2)\eta^{-2} - 2\alpha_1 c^2 = 0$$
 (3.41)

Solving this for  $\eta^{-2}$  we get two roots and label them as follows:

$$\eta_0^{-2} = \frac{1}{2} \left( \alpha_2^2 - 2\alpha_1 c^2 \right) \left( \alpha_2^2 - \alpha_3^2 \right)^{-1} \left( 1 + W^2 \right)$$
(3.42)

and

$$n_2^{-2} = \frac{1}{2} (\alpha_2^2 - 2\alpha_1 c^2) (\alpha_2^2 - \alpha_3^2)^{-1} (1 - W^2)$$
(3.43)

where

$$W = 1 + 8\alpha_1 c^2 (\alpha_2^2 - \alpha_3^2) (\alpha_2^2 - 2\alpha_1 c^2)^{-2}$$
(3.44)

In order to find  $n_0^2$  and  $n_2^2$  in terms of  $a_0$ ,  $e_0$ ,  $p_0$ , and  $i_0$  we substitute for the a's in the above equations according to (3.3) through (3.7). Thus

$$W = 1 + \frac{\frac{4k_0 x^2 (1-y^2)}{(1-k_0 x^2)^2}}{(3.45)}$$

$$n_0^2 = \frac{2(1-y^2)}{(1-k_0x^2)(1+W^2)}$$
(3.46)

and

.

$$n_2^2 = \frac{2(1-y^2)}{(1-k_0x^2)(1-W^2)}$$
(3.47)

Substituting W from (3.45) into (3.46) and (3.47) and performing the required binomial expansions we find

$$n_0 = \sin i_0 \left[ 1 + \frac{1}{2} k_0 x^2 y^2 + \frac{1}{8} k_0^2 x^4 y^2 (7y^2 - 4) \cdots \right]$$
(3.48)

$$(1-n_0^2)^{-\frac{1}{2}} = |\sec i_0| \left[ 1 + \frac{1}{2} k_0 x^2 (1-y^2) + \frac{1}{8} k_0 x^4 (1-y^2) (5y^2-1) + \cdots \right]$$
(3.49)

$$n_2^{-2} = -k_0 x^2 (1 + k_0 x^2 y^2 + \cdots)$$
 (3.50)

$$(n_0/n_2)^2 = -k_0 x^2 (\sin^2 i_0) (1 + 2k_0 x^2 y^2 + \cdots)$$
(3.51)

Note that  $n_2^{-2} \simeq -k_0 x^2$ , so that  $n_2^2$  is negative and  $n_2$  is imaginary. We

shall retain the notation  $n_2^2$  for the present, recalling that it is actually a negative quantity, since we shall have no occasion to deal with the quantity  $n_2$  alone.

For the above series expansions in powers of  $k_0$  to be valid we must have

$$k_0 x^2 = \frac{c^2}{a_0 p_0} = \frac{2\alpha_1 c^2}{\alpha_2^2} << 1$$
(3.52)

which justifies our earlier restriction in (2.15) and implies that we must have

$$\frac{c^2}{ap} = \frac{c^2}{-\rho_1 \rho_2} << 1$$
(3.53)

Or, since  $|\rho_2| > |\rho_1|$ , we should like to keep

$$\frac{c^2}{\rho_1^2} << 1 \tag{3.54}$$

Since  $\rho_1$  is the value of  $\rho$ -perigee, if our trajectory or its continuation through the planet does not pass too near the surface

$$\rho^2 = c^2$$
 (3.55)

then (3.52) will be valid. In x, y, z coordinates this surface is an oblate spheroid as in Figure 3.1. This small forbidden zone (recall  $c \approx 210 \text{ km}$ ) in the center of the Earth should not appreciably limit the scope of problems to which this spheroidal method may be applied. Few space vehicles are fired directly from Earth into hyperbolic orbit and even fewer of these on paths whose extensions would have passed through this zone. The only practical case which readily comes to mind of a



FIGURE 3.1 Forbidden Zone for Convergence of Series Solutions

trajectory which might pass through this zone is a meteor on a collision course with the Earth. Certainly any trajectory which does not intersect the Earth will cause no trouble.

#### CHAPTER 4

# THE ORBITAL ELEMENTS a, e, I, $\beta_1$ , $\beta_2$ , $\beta_3$

If we put  $G(\eta)$  in the factored form

$$G(n) = -2\alpha_1 c^2 (n_0^2 - n^2) (n_2^2 - n^2)$$
(4.1)

then on comparing this to (3.40) and equating coefficients of equal powers of n we find

$$n_0^2 + n_2^2 = 1 - \frac{\alpha_2^2}{2\alpha_1 c^2} = 1 - \frac{a_0 p_0}{c^2}$$
 (4.2)

$$n_0^2 n_2^2 = -\frac{(\alpha_2^2 - \alpha_3^2)}{2\alpha_1 c^2} = -\frac{a_0 p_0 \sin^2 i_0}{c^2}$$
(4.3)

We now define I by

Such a definition is allowed since rationalizing the denominator of (3.46) yields

$$n_0^2 = -\left(\frac{1-k_0 x^2}{2k_0 x^2}\right) + \frac{1}{2k_0 x^2} \left[(1+k_0 x^2)^2 - 4k_0 x^2 y^2\right]^{\frac{1}{2}}$$

It then follows that  $n_0^2 \leq 1$ , with the equality occuring for polar trajectories.

If we now substitute equations (3.30), (3.31), and (3.32) into equations (3.12) through (3.15) we find

$$-2a - A = -2a_0$$
 (4.5)

$$B - ap + 2aA = c^2 - a_0 p_0 \tag{4.6}$$

$$-2aB + apA = -2a_0c^2$$
 (4.7)

$$-apB = -a_0 p_0 c^2 \sin^2 i_0 \tag{4.8}$$

If we now assume a, e, and  $n_0$  are known (i.e. regard a, e, I,  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$  as orbital elements), then we have six equations in the six unknowns a , e , i , A, B, and  $n_2^2$ . With the orbital elements a, e, I,  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$  it turns out that the system can be solved exactly. This fact was first pointed out by Izsac (1960) and later utilized by Vinti (1961) in his spheroidal solution for bounded motion.

To proceed with the solution we first solve for  $n_2^2$  from (4.2) and (4.3)

$$n_2^2 = -\frac{a_0 p_0}{c^2} \frac{\sin^2 i_0}{n_0^2} = 1 - \frac{a_0 p_0}{c^2} - n_0^2$$
(4.9)

solving now for  $\sin^2 i_0$  we find

$$\frac{\alpha_2^2 - \alpha_3^2}{\alpha_2^2} = \sin^2 i_0 = n_0^2 - \frac{c^2 n_0^2 (1 - n_0^2)}{a_0 p_0}$$
(4.10)

Inserting this into (4.8)

$$-apB = c^2 \eta_0^2 (-a_0 p_0 + c^2) - c^4 \eta_0^4$$
(4.11)

If we now use (4.6) to eliminate  $c^2-a_0p_0$  from (4.11) we find

$$\frac{c^4 n_0^4 - apB}{c^2 n_0^2} = B - ap + 2aA$$
(4.12)

Eliminating  $a_0$  between equations (4.5) and (4.7) yields

$$-2a - A = \frac{-2aB}{c^2} + \frac{apA}{c^2}$$
(4.13)

Equations (4.12) and (4.13) are now in terms of A and B only. Their simultaneous solution results in

$$A = \frac{-2ac^{2}(1-n_{0}^{2})(ap + c^{2}n_{0}^{2})}{(ap+c^{2})(ap + c^{2}n_{0}^{2}) + 4a^{2}c^{2}n_{0}^{2}}$$
(4.14)

$$B = c^{2}n_{0}^{2} \left[ \frac{4a^{2}c^{2} + (ap+c^{2}n_{0}^{2})(c^{2}+ap)}{(ap+c^{2})(ap+c^{2}n_{0}^{2}) + 4a^{2}c^{2}n_{0}^{2}} \right]$$
(4.15)

Then from (4.14) and (4.5)

$$\frac{\mu}{2a\alpha_1} \equiv \frac{a_0}{a} = 1 + \frac{A}{2a} = 1 - \frac{c^2(1-n_0^2)(ap+c^2n_0^2)}{(ap+c^2)(ap+c^2n_0^2) + 4a^2c^2n_0^2}$$
(4.16)

From (3.3), (3.7), (4.15) and (4.11)

$$\frac{\alpha_2^2}{2\alpha_1} \equiv a_0 p_0 = c^2 (1 - n_0^2) + a_p \left[ \frac{(a_p + c^2)(a_p + c^2 n_0^2) + 4a^2 c^2}{(a_p + c^2)(a_p + c^2 n_0^2) + 4a^2 c^2 n_0^2} \right]$$
(4.17)

These last two equations allow the determination of  $\alpha_2$  from the set of orbital elements a, e, and I. Putting  $\eta_0 = \sin I$  into (4.10) yields

$$\alpha_3 = \alpha_2 \cos I \left[ 1 + \frac{c^2 \eta_0^2}{a_0 p_0} \right]^{\frac{1}{2}}$$
 (4.18)

So that (4.16), (4.17) and (4.18) determine the  $\alpha$ 's, or equivalently, the elements  $a_0$ ,  $e_0$ ,  $i_0$ . Finally to find  $n_2^2$  we combine (4.3) and (4.8) to get

$$n_2^2 = -\frac{Bap}{c^4 n_0^2} \tag{4.19}$$

and then substitute for B from (4.15) to get

$$n_2^2 = -\frac{ap}{c^2} \left[ \frac{(ap+c^2)(ap+c^2n_0^2) + 4a^2c^2}{(ap+c^2)(ap+c^2n_0^2) + 4a^2c^2n_0^2} \right]$$
(4.20)

Thus equations (4.14) through (4.20) yield the required unknowns when the orbital elements are taken to be a, e, and I. Use of these orbital elements allows factoring the quartic polynomials  $F(\rho)$  and G(n) and facilitates evaluating the  $\rho$  and n integrals.

If we define a new oblateness parameter

$$k \equiv \frac{c^2}{p^2} = \frac{re^2}{p^2} J_2$$
 (4.21)

corresponding to the orbital elements a, e, and I, then we can easily show that, at least to first order, the results obtained in this section agree with those of section 3.

Taking first order terms of (3.25), (3.26), (4.14), and (4.15), we find

$$A \simeq -2k_0 p_0 \cos^2 i_0 \simeq -2k p \cos^2 I \tag{4.22}$$

$$B \approx k_0 p_0^2 \sin^2 i_0 \approx k p^2 \sin^2 I \tag{4.23}$$

To first order (3.33) and (4.16) become

$$\frac{a_0}{a} \approx 1 - k_0 \cos^2 i_0 (e_0^2 - 1) \approx 1 - k \cos^2 I(e^2 - 1)$$
(4.24)

Solving (4.17) for  $p_0/p$  to first order and using (4.24) to eliminate  $a_0$ and then comparing results with the first order portion of (3.35), we find

$$\frac{p_0}{p} \approx 1 + 2k_0 \cos^2 i_0 (e_0^2 + 1) \approx 1 + 2k \cos^2 I(e^2 + 1)$$
(4.25)

Then, since  $\frac{e_0^2-1}{e^2-1} = \frac{p_0}{p} \frac{a}{a_0}$  we find to first order

$$\frac{e_0^2 - 1}{e^2 - 1} \approx 1 + k_0 \cos^2 i_0 (3e_0^2 + 1) \approx 1 + k \cos^2 I (3e^2 + 1)$$
(4.26)

From (4.10)

$$\frac{\sin^2 i_0}{\sin^2 I} = 1 - \frac{c^2 \cos^2 I}{a_0 p_0} \approx 1 - k(e^2 - 1) \cos^2 I$$
(4.27)

to first order. Taking the square root of (4.27) and comparing with the first order inverse of (3.48) gives

$$\frac{\sin i_0}{\sin I} \approx 1 - \frac{1}{2} k_0 (e_0^2 - 1) \cos^2 i_0 \approx 1 - \frac{1}{2} k (e^2 - 1) \cos^2 I \qquad (4.28)$$

Comparing the first order portions of (3.50) and (4.20) gives

$$n_2^{-2} \simeq -k_0(e_0^2 - 1) \simeq -k(e^2 - 1)$$
 (4.29)

Then from (3.51) and the previous equation, we find

$$(n_0/n_2)^2 \approx -k_0(e_0^2 - 1)\sin^2 i_0 \approx -k(e^2 - 1)\sin^2 I$$
 (4.30)

Thus the results of Sections 3 and 4 agree to first order.

We have seen that, of G(n)'s four roots, two are real,  $n = \pm \sqrt{n_0^2}$ , while two are imaginary,  $n = \pm \sqrt{n_2^2}$  (recalling that  $n_2^2 < 0$ ). With G(n) in the form of (4.1) we can see that for  $\alpha_1 > 0$  G(n) will approach  $-\infty$  for n approaching either  $+\infty$  or  $-\infty$ . Furthermore at n = 0, G(n) =  $-2\alpha_1c^2n_0^2n_2^2$ =  $\alpha_2^2 - \alpha_3^2$ , so that a sketch of G(n) can be drawn as in Figure 4.1.

Again, according to the Kinetic equation, only the portion of the curve  $G(n) \ge 0$  represents allowable motion. Thus, the real motion must occur in the interval between the two hyperboloids

$$-n_0 \leq n \leq +n_0 \tag{4.31}$$
 where  $n_0^2 \leq 1$ 

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FIGURE 4.1 Sketch of G(n)

The following two sections will be devoted to evaluating the  $\rho$  and  $\eta$  integrals in terms of the orbital elements a, e, I, and certain uniformizing variables H, f, and  $\psi$ , corresponding to the hyperbolic anomaly, the true anomaly, and the argument of latitude respectively in Keplerian hyperbolic motion.

As opposed to elliptic motion, where the quantities a, e, and I might be determined by following the orbit for many revolutions and applying some sort of least-squares process, the "one-shot" nature of hyperbolic motion will probably require the use of  $a_0$ ,  $e_0$ , and  $i_0$ , which can be determined from a set of initial conditions, as orbital elements. To find a, e, and I, one must then numerically factor  $F(\rho)$ . This is accomplished through order  $J_2^2$  by means of equations (3.23) through (3.26) and equations (3.42) and (3.43). Once a, e, and I are thus known, we can insert observations into the formulae resulting from equations (2.18) to find the  $\beta$ 's. (see Section 7.5) Thus we can always find the orbital elements a, e, I,  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$ . From this point on, in the evaluation of the integrals, we shall assume that a, e,  $\eta_0 \equiv \sin I$ ,  $\beta_1$ ,  $\beta_2$ , and  $\beta_3$  are known and give the solution in terms of these quantities.

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## CHAPTER 5

### THE *p*-INTEGRALS

In the Kinetic equations (2.18) we define

$$R_{1} \equiv \int_{\rho_{1}}^{\rho} * \rho^{2} F(\rho)^{-\frac{1}{2}} d\rho$$
 (5.1)

$$R_{2} \equiv \int_{\rho_{1}}^{\rho} t F(\rho)^{-\frac{1}{2}} d\rho$$
 (5.2)

$$R_{3} \equiv \int_{\rho_{1}}^{\rho} t (\rho^{2} + c^{2})^{-1} F(\rho)^{-\frac{1}{2}} d\rho$$
 (5.3)

where the + sign is to be used for positive dp and the - sign for negative dp. With F(p) given by (3.11), A and B by (4.14) and (4.15), and  $\rho_1$  by (3.28), we then write  $F^{-\frac{1}{2}}(p)$  as

$$F(\rho)^{-\frac{1}{2}} = (2\alpha_1)^{-\frac{1}{2}} (\rho - \rho_1)^{-\frac{1}{2}} (\rho - \rho_2)^{-\frac{1}{2}} \rho^{-1} (1 + A\rho^{-1} + B\rho^{-2})^{-\frac{1}{2}}$$
(5.4)

If we define

$$b_1 \equiv -\frac{A}{2} \tag{5.5}$$

$$b_2 \equiv \sqrt{B}$$
 (5.6)

$$\lambda \equiv \frac{b_1}{b_2} \tag{5.7}$$

$$h \equiv \frac{b_2}{\rho} \tag{5.8}$$

then

$$(1+A\rho^{-1}+B\rho^{-2})^{-\frac{1}{2}} = (1-2\lambda h+h^2)^{-\frac{1}{2}}$$
(5.9)

In this form we recognize the generating function for the Legendre polynomials. Thus we can write

$$(1+A\rho^{-1}+B\rho^{-2})^{-\frac{1}{2}} = \sum_{n=0}^{\infty} h^n P_n(\lambda)$$
 (5.10)

where the  $P_n(\lambda)$  are the Legendre polynomials. According to Hobson [4] such replacement is valid as long as

$$h < 1 \quad \text{for } \lambda < 1 \tag{5.11}$$

$$h < \lambda - (\lambda^2 - 1)^{\frac{1}{2}} \text{ for } \lambda > 1$$
 (5.12)

The conditions under which (5.11) is satisfied are investigated in Appendix B. The resulting limiting surface, within which we require the extension of the trajectory not to pass, is somewhat less restrictive than the limiting surface discussed previously in Section 3.

Putting (5.8) and (5.10) into (5.4) we find

.

$$F(\rho)^{-\frac{1}{2}} = (2\alpha_1)^{-\frac{1}{2}} \sum_{n=0}^{\infty} b_2^n P_n(\lambda) \rho^{-1-n} [(\rho-\rho_1)(\rho-\rho_2)]^{-\frac{1}{2}}$$
(5.13)

On putting this into (5.1) and evaluating the first two terms of the summation, we find

$$(2\alpha_{1})^{\frac{1}{2}}R_{1} = \int_{\rho_{1}}^{\rho} \rho^{2} (\rho^{-1} + b_{2}\lambda\rho^{-2}) [(\rho - \rho_{1})(\rho - \rho_{2})]^{-\frac{1}{2}} (\pm d\rho)$$
  
+  $\sum_{n=2}^{\infty} b_{2}^{n} P_{n}(\lambda) \int_{\rho_{1}}^{\rho} \rho^{1-n} [(\rho - \rho_{1})(\rho - \rho_{2})]^{-\frac{1}{2}} (\pm d\rho)$  (5.14)
or equivalently

$$(2\alpha_{1})^{\frac{1}{2}}R_{1} = \int_{\rho_{1}}^{\rho} (\rho + b_{1})[(\rho - \rho_{1})(\rho - \rho_{2})]^{-\frac{1}{2}} (td\rho) + \sum_{n=2}^{\infty} b_{2}^{n} P_{n}(\lambda) \int_{\rho_{1}}^{\rho} \rho^{1-n} [(\rho - \rho_{1})(\rho - \rho_{2})]^{-\frac{1}{2}} (td\rho)$$
(5.15)

We can eliminate the plus or minus signs in the above integrals by introducing the uniformizing variables H and f, analagous respectively to the hyperbolic anomaly and true anomaly in Keplerian hyperbolic motion. We thus define H and f by

$$\rho = a(e \cosh H-1) = \frac{p}{1+ecosf}$$
(5.16)

and the requirement that they always increase with time. Here H goes from  $-\infty$  on the inbound assymptote ( $\rho = \infty$ ,  $t = -\infty$ ) to  $+\infty$  on the outbound assymptote ( $\rho = \infty$ ,  $t = \infty$ ). From (5.16) we find

$$d\rho = ae \sinh H dh$$
 (5.17)

Using (5.16), (5.17),  $\rho_1 = a(e-1)$ , and  $\rho_2 = -a(e+1)$  we find that

$$[(\rho - \rho_1)(\rho - \rho_2)]^{-\frac{1}{2}} (td\rho) = t\frac{\sinh H}{|\sinh H|} dH = dH$$
(5.18)

Again from (5.16)

$$d\rho = \frac{\text{pe sinf df}}{(1+e \cos f)^2}$$
(5.19)

Using (5.19) and (5.16) we find

$$[(\rho-\rho_1)(\rho-\rho_2)]^{-\frac{1}{2}}(\pm d\rho) = (e^2-1)^{\frac{1}{2}}(1+e\cos f)^{-1} df$$
 (5.20)

## 5.1 The R<sub>1</sub> Integral

If we substitute (5.18) into the first term of (5.15) and substitute (5.20) into the remaining terms of the series we find

$$(2\alpha_{1})^{\frac{1}{2}}R_{1} = \int_{0}^{H} (ae \cosh H - a + b_{1})dH + \sum_{n=2}^{\infty} b_{2}^{n} P_{n}(\lambda) \int_{0}^{f} (\frac{p}{1 + e\cos f})^{1-n} (e^{2} - 1)^{\frac{1}{2}} (1 + e\cos f)^{-1} df$$
(5.21)

which becomes

$$(2\alpha_{1})^{\frac{1}{2}}R_{1} = a(esinh-H-H)+ b_{1}H + p(e^{2}-1)^{\frac{1}{2}}\sum_{n=2}^{\infty} (\frac{b_{2}}{p})^{n} P_{n}(\lambda) \int_{0}^{f} (1+ecosf)^{n-2} df \qquad (5.22)$$

where we have replaced the lower limits of the integrals by zero, since at  $\rho_1$ , H = f = 0. If we define

$$S_{1} = \sum_{n=2}^{\infty} \left(\frac{b_{2}}{p}\right)^{n} P_{n}(\lambda) \int_{0}^{f} (1 + e \cos f)^{n-2} df$$
 (5.23)

or equivalently

$$S_{1} = \left(\frac{b_{2}}{p}\right)^{2} \sum_{m=0}^{\infty} \left(\frac{b_{2}}{p}\right)^{m} P_{m+2}(\lambda) \int_{0}^{f} (1 + e\cos f)^{m} df$$
(5.24)

then we should like to investigate the convergence of this series. This is done in Appendix C for both of the cases  $\lambda \leq 1$  and  $\lambda > 1$ . The resulting limiting surface, within which we require the extension of the trajectory not to pass, is found to be the same as the limiting surface for allowing the replacement of  $(1 + A\rho^{-1} + B\rho^{-2})^{-\frac{1}{2}}$  by the Legendre series. Thus we are certain S<sub>1</sub> will converge as long as the trajectory does not pass within the surface of Figure 3.1.

To evaluate  $R_1$  we need to evaluate  $S_1$  and to do this we first separate it into a part proportional to f and a periodic part. Using the method of Vinti [2] in his treatment of the bounded case we define

$$f_{m}(f) \equiv \int_{0}^{f} (1 + \cos f)^{m} df \qquad (5.25)$$

In Appendix D we notice that  $f_m(f) - (\frac{f}{2\pi})f_m(2\pi)$  is an odd function of f of period  $2\pi$ . Then, from (D.9)  $f_m(2\pi) = 2f_m(\pi)$ , so that from (D.12)

$$f_{m} \equiv \int_{0}^{f} (1 + \cos f)^{m} df = \frac{1}{\pi} f \int_{0}^{\pi} (1 + \cos f)^{m} df \qquad (5.26)$$
$$+ \int_{j=1}^{m} c_{mj} \sin j f$$

We have thus separated  $f_m$  into periodic and proportional parts. We will later observe that to evaluate the periodic portions of the  $\rho$ -integrals to order  $k^2$  it will only be necessary to consider values of m up to 4 in the summation of (5.26). The proportional term of (5.26), however, requires more analysis.

We can obtain a more convenient expression for the proportional term of (5.26) by noting that

$$\int_{0}^{\pi} (z + \sqrt{z^{2} - 1} \cos f)^{m} df = \pi P_{m}(z)$$
(5.27)

a relation which, according to Madelung [5] is valid for all z including imaginary values. Here the  $P_m(z)$  are again the Legendre polynomials

$$P_{m}(z) \equiv \frac{2^{-m}}{m!} \frac{d^{m}}{dz^{m}} (z^{2}-1)^{m}$$
(5.28)

If in (5.27) we substitute

$$z = -\frac{i}{\sqrt{e^2 - 1}}$$
 (5.29)

we obtain

$$\pi P_{m}[-i(e^{2}-1)^{-\frac{1}{2}}] = \int_{0}^{\pi} \left[ -\frac{i}{\sqrt{e^{2}-1}} - i(\frac{e^{2}}{e^{2}-1})^{\frac{1}{2}} \cos f \right]^{m} df$$
$$= \left( -\frac{i}{\sqrt{e^{2}-1}} \right)^{m} \int_{0}^{\pi} (1+e \cos f)^{m} df \qquad (5.30)$$

so that

$$\int_{0}^{\pi} (1 + e \cos f)^{m} df = \pi (i \sqrt{e^{2} - 1})^{m} P_{m} \left( - \frac{i}{\sqrt{e^{2} - 1}} \right)$$
(5.31)

$$= \pi T_{m} (\sqrt{e^{2}-1})$$
 (5.32)

where we have defined

$$T_{m}(\sqrt{e^{2}-1}) \equiv (i\sqrt{e^{2}-1})^{m} P_{m}(-\frac{i}{\sqrt{e^{2}-1}})$$
 (5.33)

The first few of these polynomials  $T_m(x)$  are given in Table 5.1 along with the corresponding Legendre functions.

The polynomials  $T_n(x)$  can easily be calculated from  $T_0(x) = 1$ ,  $T_1(x) = 1$ , and the recursion formula

$$T_{m}(x) = [(2m-1) T_{m-1}(x) + (m-1)x^{2}T_{m-2}(x)]/m$$
 (5.34)

Now, substituting (5.32) into (5.26), we have in terms of  $T_n(\sqrt{e^2-1})$ 

$$\int_{0}^{f} (1 + e \cos f)^{m} df = f T_{m}(\sqrt{e^{2} - 1}) + \sum_{j=1}^{m} c_{mj} sinjf$$
(5.35)

We then find the coefficients  $c_{mj}$  by choosing an m, expanding (l+e cos f)<sup>m</sup>, integrating, and comparing to the right hand side of (5.35). Thus for m = 1

$$\int_{0}^{f} (1 + e \cos f) df = f + e \sin f$$
 (5.36)

Then since  $T_1(x) = 1$  we must have  $c_{11} = e$  and all the other  $c_{1j} = 0$ .

THE	POLYNOMIALS	$T_m(x)$
		111

TABLE 5.1

 $P_{m}(-\frac{i}{x})$  $T_{m}(x)$ m 0 1 1  $-\frac{i}{x}$ 1 1  $\frac{1}{2}(-\frac{3}{x^2}-1)$  $\frac{1}{2}(\frac{51}{x^3}+\frac{31}{x})$  $\frac{1}{2}(3 + x^2)$ 2  $\frac{1}{2}(5 + 3x^2)$ 3  $\frac{1}{8}(\frac{35}{x^4} + \frac{30}{x^2} + 3)$  $\frac{1}{8}(35 + 30x^2 + 3x^4)$ 4  $\frac{1}{8}\left(-\frac{63i}{x^5} - \frac{70i}{x^3} - \frac{15i}{x}\right)$  $\frac{1}{16}\left(-\frac{231}{x^6} - \frac{315}{x^4} - \frac{105}{x^2} - 5\right)$  $\frac{1}{8}(63 + 70x^2 + 15x^4)$ 5 6  $\frac{1}{16}(231 + 315x^2 + 105x^4 + 5x^6)$ 

Applying this method for m = 0 to m = 4 we compile Table 5.2. Substituting (5.35) into (5.23) would then give us S<sub>1</sub>. Let us consider first the portion of S<sub>1</sub> proportional to f. Thus from (5.35) and (5.23) we write

$$p(e^{2}-1)^{\frac{1}{2}}(S_{1})_{prop.} = p(e^{2}-1)^{\frac{1}{2}} f \sum_{n=2}^{\infty} (\frac{b_{2}}{p})^{n} P_{n}(\lambda) T_{n-2}[(e^{2}-1)^{\frac{1}{2}}]$$
 (5.37)

 $\equiv A_1 f$  (5.38)

where we have defined

$$A_{1} \equiv p(e^{2}-1)^{\frac{1}{2}} \sum_{n=2}^{\infty} (\frac{b_{2}}{p})^{n} P_{n}(\lambda) T_{n-2}(\sqrt{e^{2}-1})$$
(5.39)

then since  $T_m (\sqrt{e^2-1}) \leq (1+e)^m$  our previous investigation of the convergence of  $S_1$  shows the rapid convergence of  $A_1$ .

If we now consider the periodic part of  $S_1$ , we find from (5.35) and (5.24)

$$p(e^{2}-1)^{\frac{1}{2}}(S_{1})_{per.} = (\frac{b_{2}}{p})^{2} \sum_{m=1}^{\infty} (\frac{b_{2}}{p})^{m} P_{m+2}(\lambda) \sum_{j=1}^{m} c_{mj} \text{ sinjf}$$
(5.40)

$$\equiv \sum_{j=1}^{\infty} A_{l_j} \text{ sinjf}$$
 (5.41)

where we have defined by (5.41)

$$A_{1j} = p(e^{2}-1)^{\frac{1}{2}} \left[ \left( \frac{b_{2}}{p} \right)^{3} P_{3}(\lambda) c_{1j} + \left( \frac{b_{2}}{p} \right)^{4} P_{4}(\lambda) c_{2j} + \left( \frac{b_{2}}{p} \right)^{5} P_{5}(\lambda) c_{3j} + \cdots \right]$$

If in (5.42) we substitute the values of the  $P_n(b_1/b_2)$  and the  $c_{mj}$ and retain only those terms through order  $k^2$  [recalling from (B.3) and (B.4) that  $b_1 = O(k)$ ,  $b_2 = O(k^2)$ ] we find



THE COEFFICIENTS cmj

TABLE 5.2

$$A_{11} = \frac{3(e^2 - 1)^2}{4p^3} \left[ -2b_1 b_2^2 p + b_2^4 \right] e$$
 (5.43)

$$A_{12} = \frac{3(e^2 - 1)^2 b_2^4 e^2}{32p^3}$$
(5.44)

The other  $A_{1j}$  are of order  $k^3$  or higher. Finally, substituting (5.41) and (5.38) back into (5.22) there results

$$(2\alpha_1)^{\frac{1}{2}}R_1 = a(e \sinh H - H) + b_1H + A_1f + \sum_{j=1}^{2} A_{1,j} \sinh f$$
 (5.45)

with  $A_1$ ,  $A_{11}$ , and  $A_{12}$  given by (5.39), (5.43) and (5.44) respectively.

## 5.2 The R<sub>2</sub> Integral

From (5.2) the R<sub>2</sub> integral is

$$R_2 = \int_{\rho_1}^{\rho} t F(\rho)^{-\frac{1}{2}} d\rho$$
 (5.2)

If into this we insert (5.13) for  $F(\rho)^{-\frac{1}{2}}$  and then use (5.20) to put the result in terms of the uniformizing variable f we find

$$(2\alpha_1)^{\frac{1}{2}}R_2 = \frac{(e^2-1)^{\frac{1}{2}}}{p} \sum_{n=0}^{\infty} (\frac{b_2}{p})^n P_n(\lambda) \int_0^f (1+e\cos f)^n df$$
(5.46)

We then define

$$S_2 \equiv \sum_{n=0}^{\infty} \left(\frac{b_2}{p}\right)^n P_n(\lambda) \int_0^f (1 + e \cos f)^n df$$
 (5.47)

We should like to investigate the convergence of  $S_2$ . Since cos f cannot exceed 1, we may write

$$|S_2| \leq f \sum_{n=0}^{\infty} (\frac{b_2}{p})^n P_n(\lambda) (1+e)^n$$
 (5.48)

Evaluating the first two terms of the series we find

$$|S_2| \leq f + \frac{b_1(1+e)f}{p} + \left[\frac{b_2(1+e)}{p}\right]^2 f \sum_{m=0}^{\infty} \left(\frac{b_2}{p}\right)^m P_{m+2}(\lambda)(1+e)^m$$
 (5.49)

On comparing the third term of (5.49) with equation (C.1) of Appendix C, we see that S<sub>2</sub> will converge whenever S<sub>1</sub> converges. We saw in Appendix C that we were assured of S<sub>1</sub> (and thus S<sub>2</sub>) converging as long as the conditions derived in Appendix B, for the replacement of  $(1+A\rho^{-1}+B\rho^{-2})^{-\frac{1}{2}}$  by the Legendre series, were met.

To evaluate  $R_2$  we proceed as we did with  $R_1$  and separate it into parts proportional to f and periodic in f. We substitute (5.35) into (5.46) to get

$$(2\alpha_1)^{\frac{1}{2}} R_2 = A_2 f + \sum_{j=1}^{\infty} A_{2j} sinjf$$
 (5.50)

where we have defined

.

$$A_{2} \equiv \frac{(e^{2}-1)^{\frac{1}{2}}}{p} \sum_{n=0}^{\infty} (\frac{b_{2}}{p})^{n} P_{n}(\lambda) T_{n}(\sqrt{e^{2}-1})$$
(5.51)

and

$$A_{2j} \equiv \frac{(e^2 - 1)^2}{p} \left[ \frac{b_2}{p} P(\lambda) c_{1j} + (\frac{b_2}{p})^2 P_2(\lambda) c_{2j} + \cdots \right]$$
(5.52)

Evaluating the  $A_{2\,\mathbf{j}}$  as before and keeping only the terms through order  $k^2$  we find

$$A_{21} = \frac{(e^2 - 1)^{\frac{1}{2}}e}{p} \left[ \frac{b_1}{p} + \frac{3b_1^2 - b_2^2}{p^2} - \frac{9b_1b_2^2}{2p^3} (1 + \frac{e^2}{4}) + \frac{3b_2^4}{8p^4} (4 + 3e^2) \right] (5.53)$$

$$A_{22} = \frac{(e^2 - 1)^2 e^2}{p} \left[ \frac{3b_1^2 - b_2^2}{8p^2} - \frac{9b_1 b_2^2}{8p^3} + \frac{3b_2^4}{16p^4} \left(3 + \frac{e^2}{2}\right) \right]$$
(5.54)

$$A_{23} = \frac{(e^2 - 1)^{\frac{1}{2}}e^3}{8p} \left[ -\frac{b_1 b_2^2}{p^3} + \frac{b_2^4}{p^4} \right]$$
(5.55)

$$A_{24} = \frac{3(e^2 - 1)^{\frac{1}{2}}b_2^{4}e^4}{256p^5}$$
(5.56)

The remaining  $A_{2j}$ 's are of order  $k^3$  or higher. Thus we can rewrite (5.50) as

$$(2\alpha_1)^{\frac{1}{2}} R_2 = A_2 f + \sum_{j=1}^{4} A_{2j} sinjf$$
 (5.57)

where  $A_2$ ,  $A_{21}$ ,  $A_{22}$ ,  $A_{23}$ , and  $A_{24}$  are given by (5.51) and (5.53) through (5.56). Note that the convergence of  $A_2$  is assured by the convergence of  $S_2$ .

## 5.3 The R<sub>3</sub> Integral

We should now like to evaluate

$$R_{3} \equiv \int_{\rho_{1}}^{\rho} \pm (\rho^{2} + c^{2})^{-1} F(\rho)^{-\frac{1}{2}} d\rho$$
 (5.3)

Applying the binomial expansion theorem to  $(\rho^2+c^2)^{-1}$  results in

$$(\rho^{2}+c^{2})^{-1} = \rho^{-2} \sum_{j=0}^{\infty} (-1)^{j} c^{2j} \rho^{-2j}$$
$$= \left(\frac{1+e\cos f}{p}\right)^{2} \sum_{j=0}^{\infty} (-1)^{j} \left(\frac{c}{p}\right)^{2j} (1+e\cos f)^{2j}$$
(5.58)

since  $\rho \equiv \frac{p}{1+ecosf}$ . Substituting (5.58), (5.13), and (5.20) into (5.3) yields

$$(2\alpha_1)^{\frac{1}{2}}R_3 = \frac{(e^2 - 1)^{\frac{1}{2}}}{p} \int_{0}^{f} \sum_{j=0}^{\infty} (-1)^{j} (\frac{c}{p})^{2j} (1 + e\cos f)^{2j} \sum_{n=0}^{\infty} (\frac{b_2}{p})^{n} P_n(\lambda) (1 + e\cos f)^{n+2} df$$
(5.59)

Let us consider the two series within the integrand separately. We define

$$S_{31} \equiv \sum_{j=0}^{\infty} (-1)^{j} \left(\frac{c}{p}\right)^{2j} (1 + cosf)^{2j}$$
(5.60)

The series  $S_{31}$  is a geometric series with first term = 1 and a ratio between successive terms of

$$r_{31} \equiv -\left(\frac{c}{p}\right)^2 \left(1 + e\cos f\right)^2 = -\frac{c^2}{\rho^2}$$
 (5.61)

Clearly S<sub>31</sub> will converge as long as  $|r_{31}| < 1$  which requires

$$\rho > c$$
 (5.62)

Thus  $\rho = c$  is the limiting surface within which actual motion must not take place if S<sub>31</sub> is to converge. Since the substance of the Earth effectively prohibits all actual motion in this region, S<sub>31</sub> will always converge.

We next define the series

$$S_{32} \equiv \sum_{n=0}^{\infty} \left(\frac{b_2}{p}\right)^n P_n(\lambda) (1 + ecosf)^{n+2}$$
 (5.63)

If  $\lambda \leq 1$  then  $|P_n(\lambda)| \leq 1$  and so

$$|S_{32}| \leq (1 + cosf)^2 \sum_{n=0}^{\infty} (\frac{b_2}{\rho})^n$$
 (5.64)

We can consider (5.64) to be a geometric series and thus require the ratio between successive terms to be less than one.

$$\mathbf{r}_{32} \equiv \frac{b_2}{\rho} < 1$$
 (5.65)

or equivalently we require

$$\rho > b_2 \simeq c \sin I \tag{5.66}$$

The condition  $\rho > c$  sin I will always be satisfied since actual motion cannot occur within the Earth. The approximation  $b_2 \simeq c$  sin I, however, is only valid under the restrictions discussed at the end of Section 3.

For  $\lambda > 1$  our restriction on the ratio between successive terms becomes

$$\mathbf{r}_{32} = \frac{2\mathbf{b}_1}{\rho} < 1 \tag{5.67}$$

This restriction will certainly be satisfied if  $\rho_1 > 2b_1$ , a condition which we imposed in Appendix B in order that  $(1+A\rho^{-1}+B\rho^{-2})^{-\frac{1}{2}}$  be the Legendre polynomial generating function. Thus no additional restrictions have been required in order that  $S_{32}$  converge. We have now established the integrand of (5.59) as a product of two absolutely convergent series (assuming our trajectory meets the conditions previously imposed) and, consequently, [2] it is equal to the absolutely convergent series formed by summing the products of the individual terms. Since this resulting series is uniformly convergent we may integrate it term by term.

Accordingly we can rewrite (5.59) as

$$2(\alpha_1)^{\frac{1}{2}} R_3 = \frac{(e^2 - 1)^{\frac{1}{2}}}{p^3} \int_0^f \sum_{m=0}^{\infty} D_m (1 + e\cos f)^{m+2} df$$
(5.68)

where

$$D_{\rm m} = \sum d_{\rm j} \delta_{\rm n} \,. \tag{5.69}$$

and the summation takes place over all the integers j and n' such that

$$m = 2j + n^{\prime}$$
 (5.70)

In (5.69) we have defined

$$d_{j} \equiv (-1)^{j} \left(\frac{c}{p}\right)^{2j}$$
 (5.71)

and

$$\delta_{n} \equiv \left(\frac{b_2}{p}\right)^n P_{n}(\lambda) \tag{5.72}$$

Then, since we can integrate (5.68) term by term we rewrite it as

$$(2\alpha_1)^{\frac{1}{2}} R_3 = \frac{(e^2 - 1)^{\frac{1}{2}}}{p^3} \sum_{m=0}^{\infty} D_m \int_0^f (1 + e\cos f)^{m+2} df$$
(5.73)

Before proceeding with the evaluation of  $R_3$  let us investigate the convergence of our new series

$$S_{33} \equiv \sum_{m=0}^{\infty} D_m \int_0^f (1 + e \cos f)^{m+2} df$$
 (5.74)

We first take the case  $\lambda \leq 1$ , which excludes only near-equatorial trajectories. If m is even, then n' must also be even, so we set m = 2i, n' = 2n, and j = i-n. Thus

$$D_{2_{i}} = \sum_{n=0}^{i} d_{i-n} \delta_{2_{n}} = \sum_{n=0}^{i} (-1)^{i-n} (\frac{c}{p})^{2i-2n} (\frac{b_{2}}{p})^{2n} P_{2_{n}}(\lambda)$$
(5.75)

Then since  $|P_{2_n}(\lambda)| \leq 1$  for  $\lambda \leq 1$ 

$$|D_{2_{i}}| \leq \left(\frac{c}{p}\right)^{2_{i}} \sum_{n=0}^{i} \left(\frac{b_{2}}{c}\right)^{2_{n}}$$
 (5.76)

If the extension of the trajectory does not pass through the region defined in Section 3, then  $b_2 \simeq c \sin I$  and

$$|D_{2i}| \leq k^{i} \sum_{n=0}^{i} (\sin^{2}I)^{n} \leq k^{i}(i+1)$$
 (5.77)

If, on the other hand, m is odd, then m = 2i+1, n' = 2n+1, and j = i-n. Thus

$$D_{2_{i+1}} = \sum_{n=0}^{i} d_{j} \delta_{2_{n+1}} = \sum_{n=0}^{i} (-1)^{i-n} (\frac{c}{p})^{2i-2n} (\frac{b_{2}}{p})^{2n+1} P_{2_{n+1}}(\lambda)$$
(5.78)

and

$$|D_{2_{i+1}}| \leq (\frac{c}{p})^{2_{i}} \frac{b_{2}}{p} \sum_{n=0}^{i} (\frac{b_{2}}{c})^{2_{n}}$$
 (5.79)

If we again take  $b_2 \simeq c \sin I$ 

$$|D_{2_{i+1}}| \leq k^{i+\frac{1}{2}} \sin I \sum_{n=0}^{i} (\sin^{2}I)^{n} \leq k^{i+\frac{1}{2}} (i+1) \sin I$$
 (5.80)

If we now consider  $\lambda > 1$ , the equatorial and near-equatorial trajectories, then by (C.10)  $\left|\left(\frac{b_2}{p}\right)^n P_n(\lambda)\right| \le \left(\frac{2b_1}{p}\right)^n$ . If m is even, we then find

$$|D_{2_{i}}| \leq (\frac{c}{p})^{2_{i}} \sum_{n=0}^{i} (\frac{2b_{1}}{c})^{2_{n}}$$
 (5.81)

Again assuming the trajectory's extension does not pass through the region defined in Section 3, we can set  $b_1 \simeq kpcos^2I$ , so that

$$|D_{2i}| \leq k^{i} \sum_{n=0}^{i} (4k\cos^{4}I)^{n} \leq k^{i} \sum_{n=0}^{i} (4k)^{n}$$
(5.82)

Then by finding the sum of this infinite geometric progression we must have

$$|D_{2_{i}}| \leq k^{i} \left[ \frac{1 - (4k)^{i}}{1 - 4k} \right]$$
 (5.83)

Finally, if m is odd, we find

$$|D_{2i+1}| \leq (\frac{c}{p})^{2i} \frac{2b_1}{p} \sum_{n=0}^{i} (\frac{2b_1}{c})^{2n} \leq 2k^{i+1} \cos^{2} I \sum_{n=0}^{i} (4k)^n$$
(5.84)

Again evaluating the sum of the infinite geometric progression and setting  $\cos^2 I \approx 1$  for near-equatorial trajectories

$$|D_{2_{i+1}}| \leq 2k^{i+1} \left[ \frac{1 - (4k)^{i}}{1 - 4k} \right]$$
 (5.85)

We now separate S<sub>33</sub> into an even series and an odd series, S<sub>e</sub> and S<sub>o</sub> respectively. Thus for  $\lambda \leq 1$ 

$$|s_{e}| \leq f(e+1)^{2} \sum_{i=0}^{\infty} k^{i} (i+1)(1+2e)^{2i}$$
 (5.86)

and

$$|S_0| \le k^2 \sin I \ (1+e)^3 \ f \sum_{i=0}^{\infty} (i+i) \ [(k(e+i)^2]^i \ (5.87)$$

Then since  $\sum_{0}^{\infty} x^{i} = \frac{1}{1-x}$  and  $\sum_{0}^{\infty} ix^{i} = \frac{x}{(1-x)^{2}}$  we can see that  $\sum_{0}^{\infty} (i+1)x^{i} = \frac{1}{(1-x)^{2}}$ . Applying this to (5.86) and (5.87) yields

$$|S_{e}| \leq \frac{f(e+1)^{2}}{[1-k(e+1)^{2}]^{2}}$$
(5.88)

and

$$|S_{0}| \leq \frac{k^{2} \sin I(1+e)^{3} f}{[1-k(e+1)^{2}]^{2}}$$
(5.89)

so that

$$|S_{33}| \leq \frac{(e+1)^2 f[1 + k^2 \sin I(e+1)]}{[1 - k(e+1)^2]^2}$$
(5.90)

For  $\lambda > 1 S_e$  and S<sub>o</sub> become

$$|S_{e}| \leq \frac{(e+1)^{2}f}{1-4k} \sum_{i=0}^{\infty} [k(e+1)^{2}]^{i} - [4k^{2}(e+1)^{2}]^{i} = \frac{(e+1)^{2}f}{1-4k} \left[\frac{1}{1-k(e+1)^{2}} - \frac{1}{1-4k^{2}(e+1)^{2}}\right]$$
(5.91)

and

$$|S_{0}| \leq \frac{2k(e+1)^{3}f}{1-4k} \sum_{i=0}^{\infty} [k(e+1)^{2}]^{i} - [4k^{2}(e+1)^{2}]^{i} = \frac{2k(e+1)^{3}f}{1-4k} \left[ \frac{1}{1-k(e+1)^{2}} - \frac{1}{1-4k^{2}(e+1)^{2}} \right]$$
(5.92)

Adding these even and odd series together yields

$$|S_{33}| \leq \frac{k(e+1)^4 f}{[1 - k(e+1)^2][1 - 2k(e+1)]}$$
(5.93)

From (5.90) and (5.93) it is clear that  $S_{33}$  will converge as long as  $k(e+1)^2 < 1$  or equivalently  $\frac{c^2}{\rho_1^2} < 1$ . This requirement for the convergence of  $S_{33}$  is exactly the same as that discussed in Section 3.

The values of D<sub>m</sub> can be found from equations (5.69) through (5.72), and are shown in Table 5.3 to order  $k^2$ .

These  $\mathrm{D}_{\mathrm{m}}$  can easily be calculated from the first two values and the recursion formula

$$D_{j} = -\left(\frac{c}{p}\right)^{2} D_{j-2} + \left(\frac{b_{2}}{p}\right)^{j} P_{j}(b_{1}/b_{2})$$
(5.94)

To evaluate  $R_3$  we separate it into a part proportional to f and a part periodic in f. Thus we rewrite (5.73) as

$$(2\alpha_1)^{\frac{1}{2}} R_3 = A_3 f + \sum_{j=1}^{\infty} A_{3j} sinjf$$
 (5.95)

where according to (5.35) we must have

$$A_{3} = \frac{(e^{2}-1)^{\frac{1}{2}}}{p^{3}} \sum_{m=0}^{\infty} D_{m} T_{m+2} (\sqrt{e^{2}-1})$$
(5.96)

and

$$A_{3j} = \frac{(e^2 - 1)^{\frac{1}{2}}}{p^3} \sum_{m=0}^{\infty} D_m c_{m+2,j}$$
(5.97)

TABLE 5.3

VALUES OF D TO ORDER  $k^2$ 

m	Order	D
0	k <sup>0</sup>	l
l	k	b <sub>1</sub> /p
2	k	$(b_2/p)^2 P_2(b_1/b_2) - (c/p)^2$
3	k <sup>2</sup>	$(b_2/p)^3 P_3(b_1/b_2) - (c/p)^2(b_1/p)$
14	k <sup>2</sup>	$(b_2/p)^4 P_4(b_1/b_2) - (c/p)^2(b_2/p)^2 P_2(b_1/b_2)$ + $(\frac{c}{p})^4$

Since R<sub>3</sub> is multiplied by  $c^2 = kp^2$  in the Kinetic equation (2.18c) we need only to find the periodic terms through order k in order to have the final solution correct to order  $k^2$ . Thus from (5.97) we find

$$A_{31} = \frac{(e^2 - 1)^2 e}{p^3} \left[ 2 + \frac{b_1}{p} \left( 3 + \frac{3e^2}{4} \right) - \left( \frac{b_2^2}{2p^2} + \frac{c^2}{p^2} \right) 4 + 3e^2 \right]$$
(5.98)

$$A_{32} = \frac{(e^2 - 1)^2}{p^3} \left[ \frac{e^2}{4} + \frac{3b_1 e^2}{4p} - \left( \frac{b_2^2}{2p^2} + \frac{c^2}{p^2} \right) \left( \frac{3e^2}{2} + \frac{e^4}{4} \right) \right]$$
(5.99)

$$A_{33} = \frac{(e^2 - 1)^2}{p^3} \left[ \frac{b_1 e^3}{12p} - \left( \frac{b_2^2}{2} + c^2 \right) \frac{e^3}{3p^2} \right]$$
(5.100)

and

$$A_{34} = \frac{(e^2 - 1)^{\frac{1}{2}}}{p^3} \left[ -\frac{e^4}{32p^2} (\frac{b_2^2}{2} + c^2) \right]$$
(5.101)

Since the other  $A_{3j}$  are of order  $k^2$  or higher we can rewrite (5.95) as

$$(2\alpha_1)^{\frac{1}{2}} R_3 = A_3 f + \sum_{j=1}^{l_4} A_{3j} sinjf$$
 (5.102)

with  $A_3$  and  $A_{3,j}$  as given previously.

#### CHAPTER 6

#### THE n-INTEGRALS

In the Kinetic equations (2.18) we define the three n integrals

$$N_{1} \equiv \int_{0}^{\eta} t \eta^{2} G^{-\frac{1}{2}}(\eta) d\eta$$
 (6.1)

$$N_{2} \equiv \int_{0}^{n} t G^{-\frac{1}{2}}(n) dn$$
 (6.2)

$$N_{3} \equiv \int_{0}^{n} t(1-n^{2})^{-1} G^{-\frac{1}{2}}(n) dn$$
 (6.3)

where the upper sign is to be used for positive  $d\eta$  and the lower sign for negative  $d\eta$ , and with  $G(\eta)$  given by (3.40),  $\eta_2^2$  by (4.20),  $\alpha_2^2$  by (4.16) and (4.17), and  $(\alpha_2^2 - \alpha_3^2)$  by (4.10). Following Vinti's example for bounded motion we introduce the uniformizing variable  $\psi$  defined by

$$\psi = \sin^{-1}(n/n_0)$$
 (6.4)

and the requirement that  $\psi$  always increase with time. For the case of Keplerian motion c = 0 and (6.4) becomes

$$\sin \psi = \frac{\eta}{\eta_0} \div \frac{\sin \theta}{\sin i}$$
(6.5)

so that  $\psi$  reduces to the angle between the line of nodes and the radius vector to the satellite, commonly referred to as the argument of latitude.

Inserting (6.4) into (3.40) yields

$$G(n) = (\alpha_2^2 - \alpha_3^2) \cos^2 \psi (1 + n^2 \sin^2 \psi)$$
(6.6)

where we have defined

$$n^2 = -\frac{n_0^2}{n_2^2} = O(k)$$
 (6.7)

Notice that n is a real positive number whose magnitude is less than one, since  $|n_2^2| > 1 > n_0^2$ . Thus we find

$${}^{\pm}G(n)^{-\frac{1}{2}}dn = (\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}}n_0(1 + n^2 \sin^2 \psi)^{-\frac{1}{2}}d\psi$$
(6.8)

## 6.1 The N1 Integral

Inserting (6.8) and (6.4) into (6.1) results in

$$N_{1} = (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0}^{3} \int_{0}^{\psi} (1 + n^{2} \sin^{2} \psi)^{-\frac{1}{2}} \sin^{2} \psi \, d\psi$$
(6.9)

To have the final result correct to  $O(k^2)$  we shall only need to evaluate  $N_l$  to O(k) since it is multiplied by  $c^2$  in the Kinetic equations. Use of the relation

$$-n^{2}(1+n^{2}\sin^{2}\psi)^{-\frac{1}{2}}\sin^{2}\psi \equiv (1+n^{2}\sin^{2}\psi)^{-\frac{1}{2}} - (1+n^{2}\sin^{2}\psi)^{\frac{1}{2}}$$
(6.10)

enables us to separate (6.9) into parts which can be more easily integrated.

$$N_{1} = - (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} \frac{n_{0}^{3}}{n^{2}} \left[ \int_{0}^{\psi} \frac{d\psi}{\sqrt{1 + n^{2} \sin^{2}\psi}} - \int_{0}^{\psi} \sqrt{1 + n^{2} \sin^{2}\psi} d\psi \right]$$
(6.11)

The integrals are now in the form of Elliptic integrals of the first and second kinds, with imaginary moduli. To avoid using imaginary moduli, we employ variable transformations. If in the first integral of (6.11) we set  $\psi = \gamma - \frac{\pi}{2}$ ,  $d\psi = d\gamma$ ,  $\cos \psi = \sin \gamma$ , we find

$$\int_{0}^{\psi} \frac{d\psi}{\sqrt{1+n^{2}\sin^{2}\psi}} = \frac{1}{\sqrt{n^{2}+1}} \int_{\pi/2}^{\gamma} \frac{d\gamma}{\sqrt{1-k_{1}^{2}\sin^{2}\gamma}}$$
(6.12)

where

$$k_1^2 = \frac{n^2}{n^2 + 1} \tag{6.12a}$$

so that

$$\int_{0}^{\psi} \frac{d\psi}{\sqrt{1+n^{2}\sin^{2}\psi}} = \frac{1}{\sqrt{n^{2}+1}} \left[ \int_{0}^{\gamma} \frac{d\gamma}{\sqrt{1-k_{1}^{2}\sin^{2}\gamma}} - \int_{0}^{\pi/2} \frac{d\gamma}{\sqrt{1-k_{1}^{2}\sin^{2}\gamma}} \right] \quad (6.13)$$
$$= \frac{1}{\sqrt{n^{2}+1}} \left[ F(\gamma,k_{1}) - K(k_{1}) \right] \quad (6.14)$$

where  $F(\gamma, k_1)$  is the elliptic integral of the first kind of amplitude  $\gamma$ and modulus  $k_1$ , and  $K(k_1)$  is the complete elliptic integral of the first kind of modulus  $k_1$ .

Applying the same transformation to the second integral of (6.11) yields

$$\int_{0}^{\psi} \sqrt{1 + n^{2} \sin^{2} \psi} \, d\psi = \sqrt{1 + n^{2}} \int_{\pi/2}^{\gamma} \sqrt{1 - k_{1}^{2} \sin^{2} \gamma} \, d\gamma$$
(6.15)

$$= \sqrt{1 + n^{2}} \left[ \int_{0}^{\gamma} \sqrt{1 - k_{1}^{2} \sin^{2} \gamma} \, d\gamma - \int_{0}^{\pi/2} \sqrt{1 - k_{1}^{2} \sin^{2} \gamma} \, d\gamma \right]$$
(6.16)

$$= \sqrt{1 + n^2} \left[ E(\gamma, k_1) - E(k_1) \right]$$
 (6.17)

where  $E(\gamma, k_1)$  and  $E(k_1)$  are the elliptic integral of the second kind and the complete elliptic integral of the second kind, respectively.

We now seek to express each elliptic integral as a part proportional to  $\gamma$  and a Fourier series of the form  $\sum_{l=1}^{\infty} B_n \sin 2n\gamma$ . We first note [6] that

$$F(\gamma + m\pi, k_1) = 2m K(k_1) + F(\gamma, k_1)$$
 (6.18)

so that the function  $F(\gamma, k_1) - \frac{2}{\pi} K(k_1)\gamma$  is periodic in  $\gamma$  with period  $\pi$ . Furthermore, since it is an odd function of  $\gamma$ , we can expand it in a Fourier series using only the sines of even multiples of  $\gamma$ . Thus we write

$$F(\gamma, k_1) = \frac{2}{\pi} \gamma K(k_1) + \sum_{m=1}^{\infty} F_{k_1 m} \sin 2m\gamma$$
 (6.19)

To calculate the Fourier coefficients we note the definition of  $F(\gamma, k_1)$ 

$$F(\gamma, k_1) \equiv \int_0^{\gamma} (1 - k_1^2 \sin^2 \gamma)^{-\frac{1}{2}} d\gamma$$
 (6.20)

and then differentiate both (6.19) and (6.20) with respect to  $\gamma$  to get

$$(1 - k_1^2 \sin^2 \gamma)^{-\frac{1}{2}} = \frac{2}{\pi} K(k_1) + 2 \sum_{m=1}^{\infty} m F_{k_1 m} \cos 2m\gamma$$
(6.21)

which is in the form  $f(x) = A_0 + \sum_{l=1}^{\infty} A_n \cos \frac{n\pi x}{L}$ . Thus by Hildebrand [7]  $A_n = \frac{2}{L} \int_0^L f(x) \cos \frac{n\pi x}{L} dx$  or solving for the  $F_{k_1m}$ , we find

$$\mathbf{F}_{k_{1}m} = \frac{2}{m\pi} \int_{0}^{\pi/2} (1 - k_{1}^{2} \sin^{2} \gamma)^{-\frac{1}{2}} \cos 2m\gamma \, d\gamma$$
(6.22)

To evaluate these Fourier coefficients we follow Vinti's example [2] and expand the radical using the relation

$$(1 - k_1^2 \sin^2 \gamma)^{-\frac{1}{2}} = 1 + \sum_{\ell=1}^{\infty} \frac{(2\ell)! k_1^{2\ell} \sin^2 \ell \gamma}{2^{2\ell} (\ell!)^2}$$
(6.23)

which can easily be proved by noting that the right hand side generates the binomial expansion of the left hand side. Substituting (6.23) into (6.22) yields

$$F_{k_{1}m} = \frac{2}{\pi m} \sum_{\ell=1}^{\infty} \frac{(2\ell)! k_{1}^{2\ell}}{2^{2\ell} (\ell!)^{2}} \int_{0}^{\pi/2} \sin^{2\ell}\gamma \cos 2m\gamma \, d\gamma \qquad (6.24)$$

However, for  $l \ge 1$ 

$$\sin^{2\ell} \gamma = \frac{(2\ell)!}{(\ell!)^{2} 2^{2\ell}} + (-1)^{\ell} 2^{1-2\ell} \sum_{j=0}^{\ell-1} (-1)^{j} \frac{(2\ell)!}{(2\ell-j)!j!} \cos(2\ell-2j) \gamma$$
(6.25)

This relation can be proved by expanding  $\left[\frac{1}{2i}(e^{i\gamma}-e^{-i\gamma})\right]^{2\ell}$  binomially and rearranging terms so as to form the summation of (6.25). We also have the identity

$$\cos[(2l-2j)\gamma] \cos 2m\gamma = \frac{1}{2} \cos[(2l+2m-2j)\gamma] + \frac{1}{2} \cos[(2l-2m-2j)\gamma]$$
(6.26)

With (6.25) and (6.26) substituted into (6.24) we see that the integral of the first term of (6.25) is zero for the limits  $0 \neq \frac{\pi}{2}$  and the terms of (6.26) will yield a zero integral unless either j = l + m or j = l - m. However, (6.26) tells us that j < l so that only the term corresponding to j = l - m contributes to the integral. Thus

$$\int_{0}^{\pi} \sin^{2\ell} \gamma \, \cos 2m\gamma \, d\gamma = \frac{(-1)^{m} \, (2\ell)!}{2^{2\ell} \, (\ell+m)! \, (\ell-m)!} \tag{6.27}$$

for  $m \leq \ell$ . Substituting this into (6.24) yields

$$F_{k_{1}m} = \frac{(-1)^{m}}{m} \sum_{\ell=m}^{\infty} \frac{(2\ell)!^{2} k_{1}^{2\ell}}{2^{4\ell} (\ell!)^{2} (\ell+m)! (\ell-m)!}$$
(6.28)

from which we can see that  $F_{k_1m} = O(k_1^{2m}) = O(n^{2m}) = O(k^m)$ . Consequently for accuracy up to  $O(k^2)$  in the periodic part we need only take  $F_{k_1l}$  and  $F_{k_12}$ . To  $O(k^2)$  these are found to be

$$F_{k_1 l} = -\frac{1}{8} k_1^2 - \frac{3}{32} k_1^4$$
(6.29)

$$F_{k_1 2} = \frac{3 k_1^4}{256}$$
(6.30)

Substituting these back into (6.19) yields

$$F(\gamma, k_1) = \frac{2\gamma}{\pi} \quad K(k_1) - \frac{k_1^2}{8} (1 + \frac{3}{4} k_1^2) \sin 2\gamma + \frac{3k_1^4}{256} \sin^4\gamma + \cdots$$
(6.31)

We now transform back to our original variable  $\psi$  using  $\gamma = \psi + \frac{\pi}{2}$ , sin2 $\gamma = -\sin 2\psi$ , and sin $4\gamma = \sin 4\psi$ , so that

$$F(\psi, k_1) - K(k_1) = \frac{2}{\pi} \psi K(k_1) + \frac{k_1^2}{8} (1 + \frac{3}{4} k_1^2) \sin 2\psi + \frac{3k_1^4}{256} \sin^4\psi + \cdots$$
(6.32)

We can now use the same method to handle the elliptic integral  $E(\gamma, k_1)$ . Thus  $E(\gamma, k_1) - \frac{2}{\pi} \gamma E(k_1)$  is odd in  $\gamma$  and periodic in  $\gamma$  with period  $\pi$ , so that

$$E(\gamma, k_{1}) \equiv \int_{0}^{\gamma} (1 - k_{1}^{2} \sin^{2} \gamma)^{\frac{1}{2}} d\gamma = \frac{2}{\pi} E(k_{1})\gamma + \sum_{\ell=1}^{\infty} E_{k_{1}m} \sin^{2} m\gamma \qquad (6.33)$$

As before we differentiate (6.33) with respect to  $\gamma$  to get

$$(1 - k_1^2 \sin^2 \gamma)^{\frac{1}{2}} = \frac{2}{\pi} \gamma E(k_1) + 2 \sum_{m=1}^{\infty} m E_{k_1 m} \cos 2m\gamma$$
(6.34)

and evaluate the Fourier coefficients as

$$E_{k_{1}m} = \frac{2}{m\pi} \int_{0}^{\pi/2} (1 - k_{1}^{2} \sin^{2} \gamma)^{\frac{1}{2}} \cos 2m\gamma \, d\gamma \qquad (6.35)$$

Binomial expansion then yields

$$(1 - k_1^2 \sin^2 \gamma)^{\frac{1}{2}} = 1 - \sum_{\ell=1}^{\infty} \frac{(2\ell-2)! k_1^{2\ell} \sin\gamma}{2^{2\ell-1} \ell! (\ell-1)!}$$
(6.36)

and insertion of (6.36) into (6.35) thus gives

$$E_{k_{1}m} = -\frac{2}{m\pi} \sum_{\ell=1}^{\infty} \frac{(2\ell-2)! k_{1}^{2\ell}}{2^{2\ell-1} \ell! (\ell-1)!} \int_{0}^{\pi/2} \sin^{2\ell}\gamma \cos 2m\gamma \, d\gamma \qquad (6.37)$$

since the integral of the first term of (6.36) is zero. Then by equation (6.27)

$$E_{k_{1}m} = \frac{(-1)^{m+1}}{m} \sum_{\ell=m}^{\infty} \frac{(2\ell-2)! (2\ell)! k_{1}^{2\ell}}{2^{4\ell-1} \ell! (\ell-1)! (\ell+m)! (\ell-m)!}$$
(6.38)

so that  $E_{k_1m} = O(k_1^{2m}) = O(n^{2m}) = O(k^m)$ . For accuracy to  $O(k^2)$  we need use only the first two Fourier coefficients. They are

$$E_{k_1 l} = \frac{k_1^2}{8} + \frac{k_1^4}{32} + \cdots$$
 (6.39)

and

$$E_{k_1 2} = -\frac{k_1^4}{256} + \cdots$$
 (6.40)

On substituting (6.39) and (6.40) into (6.33), we find

$$E(\gamma,k_1) = \frac{2}{\pi} \gamma E(k_1) + (\frac{k_1^2}{8} + \frac{k_1^4}{32}) \sin 2\gamma - \frac{k_1^4}{256} \sin 4\gamma + \cdots$$
 (6.41)

Transformation back to our original variable  $\psi$  then shows that

$$E(\psi, k_1) - E(k_1) = \frac{2}{\pi} \psi E(k_1) - (\frac{k_1^2}{8} + \frac{k_1^4}{32}) \sin 2\psi - \frac{k_1^4}{256} \sin^4\psi + \cdots$$
(6.42)

If we now substitute (6.14), (6.17), (6.32), and (6.41) back into (6.11), we find, after some manipulation, to O(k)

$$N_{1} = -(\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0}^{3} [B_{1}\psi + \frac{1}{8}(2 - n^{2})\sin 2\psi + \frac{n^{2}}{64}\sin 4\psi]$$
(6.43)

where

$$B_{1} \equiv \frac{k_{1}}{n^{3}} \left[ \frac{2}{\pi} \left[ \kappa(k_{1}) - E(k_{1}) \right] - n^{2} \left( \frac{2}{\pi} \right) E(k_{1}) \right]$$

$$= \frac{k_{1}^{3}}{n^{3}} \left[ \frac{1}{2} + \frac{3}{16} k_{1}^{2} + \frac{15}{128} k_{1}^{4} + \cdots \right] - \frac{k_{1}}{n} \left[ 1 - \frac{1}{4} k_{1}^{2} - \frac{3}{64} k_{1}^{4} + \cdots \right]$$

$$(6.44)$$

$$(6.44)$$

We then transform  $B_1$  back to our original variable n by using

$$\frac{k_1^3}{n^3} = (1+n^2)^{-\frac{3}{2}} = 1 - \frac{3}{2}n^2 + \frac{15}{8}n^4 - \cdots$$
(6.46)

and

$$\frac{k_1}{n} = (1+n^2)^{-\frac{1}{2}} = 1 - \frac{1}{2}n^2 + \frac{3}{8}n^4 - \cdots$$
(6.47)

Substituting (6.47) and (6.46) into  $B_1$  yields to  $O(k^2)$ 

$$B_1 = -\frac{1}{2} + \frac{3}{16} n^2 - \frac{15}{128} n^4 + \cdots$$
 (6.48)

 $N_1$  is now given by (6.43) and (6.48).

# 6.2 The N<sub>2</sub> Integral

The  $N_2$  integral is given by

$$N_2 \equiv \int_0^n \pm G^{-\frac{1}{2}}(n) \, dn \tag{6.2}$$

or by (6.8)

$$N_{2} = (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0} \int_{0}^{\psi} (1 + n^{2} \sin^{2} \psi)^{-\frac{1}{2}} d\psi$$
 (6.49)

With use of (6.14) and (6.32), this becomes

$$N_{2} = (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} \frac{n_{0}}{\sqrt{1 + n^{2}}} \left[ \frac{2}{\pi} \psi K(k_{1}) + \frac{k_{1}^{2}}{8} (1 + \frac{3}{4}k_{1}^{2}) \sin 2\psi + \frac{3k_{1}^{4}}{256} \sin^{4}\psi + \cdots \right]$$
(6.50)

or, with  $k_1^2 = n^2 - n^4 + \cdots$  in the periodic terms,

$$N_{2} = (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0} [B_{2}\psi + \frac{1}{8}(n^{2} - \frac{3}{4}n^{4})\sin 2\psi + \frac{3n^{4}}{256}\sin 4\psi + \cdots]$$
(6.51)

where

$$B_2 \equiv \frac{1}{\sqrt{1+n^2}} \frac{2}{\pi} K(k_1) = \frac{k_1}{n} [1 + \frac{1}{4}k_1^2 + \frac{9}{64}k_1^4 + \cdots]$$
(6.52)

Transforming  $B_2$  back to the parameter n by means of (6.47) yields

$$B_2 = 1 - \frac{1}{4}n^2 + \frac{9n^4}{64} - \dots$$
 (6.53)

Thus  $N_2$  is given by (6.51) and (6.53).

# 6.3 The N<sub>3</sub> Integral

Inserting (3.40) into (6.3) yields N<sub>3</sub> in the form

$$(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}} N_3 = \int_0^{n} (1 - n^2)^{-1} (1 - n^2/n_0^2)^{-\frac{1}{2}} (1 - n^2/n_2^2)^{-\frac{1}{2}} dn \qquad (6.54)$$

Since  $|n^2/n_2^2| \le |n_0^2/n_2^2| = n^2 = O(k)$  we can expand  $(1-n^2/n_2^2)^{-\frac{1}{2}}$ by the binomial theorem. Thus

$$(1-n^2/n_2^2)^{-\frac{1}{2}} = \sum_{m=0}^{\infty} \frac{(2m)!}{2^{2^m}(m!)^2} (n^2/n_2^2)^m$$
(6.55)

where  $n^2/n_2^2$  is negative. Substituting (6.55) into (6.54), we find

$$(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}} N_3 = \sum_{m=0}^{\infty} \frac{(2m)! n_2^{-2^m}}{2^{2^m} (m!)^2} L_m$$
(6.56)

where

$$L_{m} = \int_{0}^{n} t (1-n^{2})^{-1} (1-n^{2}/n_{0}^{2})^{-\frac{1}{2}} n^{2^{m}} dn \qquad (6.57)$$

for m=0

$$L_0 \equiv \int_0^n t(1-n^2)^{-1}(1-n^2/n_0^2)^{-\frac{1}{2}} dn \qquad (6.58)$$

We then notice that  $n^2/(1-n^2) = 1/(1-n^2) -1$ ,  $n^4/(1-n^2) = n^2/(1-n^2) - n^2$ ,  $n^6/(1-n^2) = n^4/(1-n^2) - n^4$ , etc., so that we can write

$$\frac{\eta^{2^{m}}}{1-\eta^{2}} = \frac{1}{1-\eta^{2}} - \sum_{n=0}^{m-1} \eta^{2^{n}}$$
(6.59)

for  $m \ge 1$ . Use of this relation in (6.57) yields

$$L_{m} = \int_{0}^{n} (1-n^{2})^{-1} (1-n^{2}/n_{0}^{2})^{-\frac{1}{2}} dn - \int_{0}^{n} \int_{n=0}^{m-1} n^{2n} (1-n^{2}/n_{0}^{2})^{-\frac{1}{2}} dn \qquad (6.60)$$

$$= L_0 - \sum_{n=0}^{m-1} L_{1_n}$$
 (6.61)

where

$$L_{1_n} = \int_{0}^{n} t n^{2n} (1 - n^2 / n_0^2)^{-\frac{1}{2}} dn$$
 (6.62)

To evaluate  $L_0$  we first rewrite it as

$$L_{0} = \int_{0}^{n} t \eta^{-3} (\eta^{-2} - 1)^{-1} (\eta^{-2} - \eta_{0}^{-2})^{-\frac{1}{2}} d\eta$$
 (6.63)

and then introduce the new variable  $\boldsymbol{\chi},$  defined by

$$\tan \chi \equiv (1-\eta_0^2)^{\frac{1}{2}} \tan \psi = |\cos I| \tan \psi$$
 (6.64)

We also require that  $\chi$  and  $\psi$  keep in step; that is, whenever  $\psi$  is a multiple of  $\pi/2$ ,  $\chi$  and  $\psi$  are equal. Using this new variable we find

$$\csc^2 \psi = 1 + \cos^2 I \, \cot^2 \chi \tag{6.65}$$

so that

$$n^{-2} = n_0^{-2} \csc^2 \psi = 1 + \cot^2 I \csc^2 \chi$$
 (6.66)

Differentiating (6.66) yields

$$\eta^{-3}d\eta = \cot^2 I \csc^2 \chi \cot \chi d\chi$$
(6.67)

We note that

$$\cot \chi \ d\chi > 0 \quad \text{for } d\eta > 0 \tag{6.68}$$

$$\cot \chi \ d\chi < 0 \quad \text{for } d\eta < 0$$

Then, substituting (6.67) and  $\eta=\eta_0\sin\psi$  into (6.63), we find

$$L_0 = \int_0^{\chi} t |\tan I| \cot \chi |\tan \chi| d\chi = \int_0^{\chi} |\tan I| d\chi$$
 (6.69)

by (6.68). Thus  $L_0$  is given by

$$L_0 = |\tan I|_{\chi} = n_0 (1 - n_0^2)^{-\frac{1}{2}}_{\chi}$$
(6.70)

For Keplerian hyperbolic motion (i.e. c=0) we see from (6.66)

$$\eta^{-2} \div \csc^2 \theta = 1 \div \cot^2 I \csc^2 \chi \tag{6.71}$$

which becomes

$$\sin\chi \rightarrow \tan\theta/|\tan I|$$
 (6.72)

 $\mathbf{or}$ 

 $\chi \neq \phi - \Omega \tag{6.73}$ 

for direct orbits. (For retrograde orbits  $\phi < 0$  and since  $\chi > 0$  always, one must then reverse the sign.) Thus, for c=0,  $\chi$  becomes the projection of the argument of latitude on the equator.

We then evaluate the  $L_{l_n}$  integrals by substituting  $\eta=\eta_0\sin\psi$  in (6.62). Thus

$$L_{l_n} = n_0^{2n+1} \int_{0}^{\psi} \sin^{2n} \psi \, d\psi \tag{6.74}$$

For n=0, we can easily integrate (6.74) to get

$$L_{10} = n_0 \psi$$
 (6.75)

To facilitate evaluating the  $L_{l_n}$  for n>0 we note that

$$\sin^{2n} \psi = \frac{(2n)!}{2^{2n}(n!)^2} + 2^{1-2n} \sum_{j=1}^{n} \frac{(-1)^j (2n)!}{(n+j)! (n-j)!} \cos 2j\psi$$
(6.76)

a relation which can easily be proved by applying the binomial expansion theorem to  $[(e^{i\psi}-e^{-i\psi})/2i]^{2n}$  and noting that the resulting series generates the right hand side of (6.76). Inserting (6.76) into (6.74) and performing the integration yields

$$L_{1n} = \frac{n_0^{2^{n+1}}(2n)!\psi}{2^{2^n}(n!)^2} + \frac{n_0^{2^{n+1}}}{2^{2^n}} \sum_{j=1}^n \frac{(-1)^j(2n)!\sin 2j\psi}{(n+j)!(n-j)!j}$$
(6.77)

for n>0. If we now substitute (6.61), (6.70), (6.75), and (6.77) back into (6.56), our expression for  $N_3$ , we find

$$(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}} N_3 = n_0(1 - n_0^2)^{-\frac{1}{2}} \chi \sum_{m=0}^{\infty} \frac{(2m)! n_2^{-2m}}{2^{2m}(m!)^2} - n_0 \psi \sum_{m=1}^{\infty} \frac{(2m)! n_2^{-2m}}{2^{2m}(m!)^2}$$

$$-\psi \sum_{m=2}^{\infty} \frac{(2m)! n_2^{-2m}}{2^{2^m} (m!)^2} \sum_{n=1}^{m-1} \frac{n_0^{2^{n+1}} (2n)!}{2^{2^n} (n!)^2}$$
(6.78)

$$-\sum_{m=2}^{\infty} \frac{(2m)! n_2^{-2^m}}{2^{2^m} (m!)^2} \sum_{n=1}^{m-1} \frac{n_0^{2^{n+1}}}{2^{2^n}} \sum_{j=1}^{n} \frac{(-1)^j (2n)! \sin 2j\psi}{(n+j)! (n-j)! j}$$

Letting  $\eta^2=1$  in (6.55) results in

4

$$(1-\eta_2^{-2})^{-\frac{1}{2}} = \sum_{m=0}^{\infty} \frac{(2m)!\eta_2^{-2m}}{2^{2m}(m!)^2} = 1 + \sum_{m=1}^{\infty} \frac{(2m)!\eta_2^{-2m}}{2^{2m}(m!)^2}$$
(6.79)

so that we can rewrite (6.78) as

$$(\alpha_{2}^{2} - \alpha_{3}^{2})^{\frac{1}{2}} N_{3} = n_{0}(1 - n_{0}^{2})^{-\frac{1}{2}}(1 - n_{2}^{-2})^{-\frac{1}{2}}\chi - \chi \left[n_{0}\left[(1 - n_{2}^{-2})^{-\frac{1}{2}}\right]^{-\frac{1}{2}}$$
  
-1] +  $n_{0}\sum_{m=2}^{\infty} \frac{(2m)!}{2^{2m}(m!)^{2}} \sum_{n=1}^{m-1} \frac{n_{0}^{2n}(2n)!}{2^{2n}(n!)^{2}} n_{2}^{-2m}\right]$  (6.80)  
-  $n_{0}\sum_{m=2}^{\infty} \frac{(2m)!n_{2}^{-2m}}{2^{2m}(m!)^{2}} \sum_{n=1}^{m-1} \frac{n_{0}^{2n}}{2^{2n}} \sum_{j=1}^{n} \frac{(-1)^{j}(2n)!\sin 2j\psi}{(n+j)!(n-j)!j}$ 

or in abbreviated form

$$(\alpha_{2}^{2} - \alpha_{3}^{2})^{\frac{1}{2}} N_{3} = n_{0}[(1 - n_{0}^{2})^{-\frac{1}{2}}(1 - n_{2}^{-2})^{-\frac{1}{2}}X + B_{3}\psi$$
  
+ 
$$\sum_{s=1}^{\infty} B_{3s} \sin 2s\psi]$$
(6.81)

where we have defined

$$B_{3} \equiv 1 - (1 - \eta_{2}^{-2})^{-\frac{1}{2}} - \sum_{m=2}^{\infty} \gamma_{m} \eta_{2}^{-2m}$$
(6.82)

$$\gamma_{\rm m} = \frac{(2m)!}{2^{2m}(m!)^2} \sum_{n=1}^{m-1} \frac{\eta_0^{2n}(2n)!}{2^{2n}(n!)^2}$$
(6.83)

and

$$\sum_{s=1}^{\infty} B_{3s} \sin 2s\psi = -\sum_{m=2}^{\infty} \frac{(2m)! n_2^{-2m}}{2^{2m} (m!)^2} \sum_{n=1}^{m-1} \frac{n_0^{2n}}{2^{2n}} \sum_{j=1}^{n} \frac{(-1)^j (2n)! \sin 2j\psi}{(n+j)! (n-j)! j}$$
(6.84)

To solve for  $B_{3s}$  we note that the functions  $\sin 2j\psi$  are orthogonal. Suppose we multiply (6.84) by  $\sin 2s'\psi$  and integrate from 0 to  $\frac{\pi}{2}$ . We can then do away with the summation over j and set j = s' for the coefficient  $B_{3s}'$ . Since j must be less than or equal to n, our lower bound on n becomes s'. Similarly, n must be less than m, so the lower bound on m

$$B_{3_{s}} = -\sum_{m=s+1}^{\infty} \frac{(2m)! n_{2}^{-2m}}{2^{2m}(m!)^{2}} \sum_{n=s}^{m-1} \frac{n_{0}^{2n} 2^{-2n} (-1)^{s} (2n)!}{(n+s)! (n-s)! s}$$
(6.85)

where we have dropped the prime from the s. Since  $B_{3_s} = O(n_2^{-2(s+1)})$ =  $O(k^{s+1})$  we need only the  $B_{31}$  terms in order to have the sine terms of N<sub>3</sub> accurate to order k<sup>2</sup>. Setting s = 1 in (6.85) yields to  $O(k^2)$ 

$$B_{31} = \frac{3}{32} n_0^2 n_2^{-4} + \cdots$$
 (6.86)

Thus for our purposes (6.81) becomes

$$(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}} N_3 = n_0 [(1 - n_0^2)^{-\frac{1}{2}} (1 - n_2^{-2})^{-\frac{1}{2}} + B_3 \psi$$
  
+  $B_{31} \sin 2\psi + \cdots]$  (6.87)

with  $B_3$  and  $B_{31}$  given by (6.82), (6.83), and (6.86).

Let us now investigate the convergence of the series  $\sum_{m=2}^{\infty} \gamma_m \eta_2^{-2m}$ . Since

$$\frac{(2n)!}{2^{2n}(n!)^2} = \frac{1}{2} \cdot \frac{3}{4} \cdot \frac{5}{6} \cdots \frac{(2n-1)}{2n} \leq \frac{1}{2}$$
(6.88)

for  $n \ge 1$ , then if we sum m-l of such terms we must have

$$\sum_{n=1}^{m-1} \frac{(2n)! n_0^{2n+1}}{2^{2n}(n!)^2} \leq \sum_{n=1}^{m-1} \frac{(2n)!}{2^{2n}(n!)^2} \leq \frac{m-1}{2}$$
(6.89)

Also, for  $m \geq 2$ 

$$\frac{(2m)!}{2^{2m}(m!)^2} \leq \frac{3}{8} \tag{6.90}$$

Thus by (6.89) and (6.90) .

$$\gamma_{\rm m} = \frac{(2m)!}{2^{2m}(m!)^2} \sum_{n=1}^{\rm m-1} \frac{(2n)! \eta_0^{2n}}{2^{2n}(n!)^2} \le \frac{3}{8} \left(\frac{\rm m-1}{2}\right) = \frac{3}{16} (\rm m-1)$$
(6.91)

for  $m \ge 2$ . Thus

$$\sum_{m=2}^{\infty} \gamma_m \eta_2^{-2m} \leq \sum_{m=2}^{\infty} \frac{3}{16} (m-1) \eta_2^{-2m}$$
(6.92)

The ratio of two successive terms is

$$\mathbf{r}_{4} = \frac{m}{m-1} \, n_{2}^{-2} \leq 2n_{2}^{-2} \tag{6.93}$$

Since  $n_2^{-2} = O(k)$ , the series  $\sum_{m=2}^{\infty} \gamma_m n_2^{-2m}$  converges rapidly. Consider now the convergence of the Fourier series

$$\left|\sum_{s=1}^{\infty} B_{3_{s}} \sin 2s\psi\right| \leq \sum_{s=1}^{\infty} |B_{3_{s}}| \leq \sum_{m=2}^{\infty} \frac{(2m)! |\eta_{2}^{-2m}|}{2^{2m}(m!)^{2}} \sum_{n=1}^{m-1} \sum_{j=1}^{n} \frac{2^{-2n}(2n)!}{(n+j)!(n-j)!}$$
(6.94)

But, for  $n \ge 0$ 

$$\frac{(2n)!}{2^{2n}(n+s)!(n-s)!} \leq \frac{(2n)!}{2^{2n}(n!)} \leq 1$$
(6.95)

so that

$$\sum_{n=1}^{m-1} \sum_{j=1}^{n} \frac{(2n)!}{2^{2n}(n+s)!(n-s)!} < \sum_{n=1}^{m-1} n < m^2$$
(6.96)

and

$$\left|\sum_{s=1}^{\infty} B_{3s} \sin 2s\psi\right| < \sum_{m=2}^{\infty} \frac{m^2(2m)! |n_2^{-2m}|}{2^{2m} (m!)^2} < \sum_{m=2}^{\infty} m^2 |n_2^{-2m}|$$
(6.97)

by (6.95). Then the ratio between successive terms must be less than

$$\mathbf{r}_{5} = \frac{(m+1)^{2}}{m^{2}} |\mathbf{n}_{2}^{-2}| \leq \frac{9}{4} |\mathbf{n}_{2}^{-2}|$$
(6.98)

for  $m \ge 2$ . Again since  $n_2^{-2} = O(k)$  the series converges rapidly.

Referring back to our equation for N<sub>3</sub> (6.87), it is now clear that all the terms are well-behaved, except for the  $\chi$  term which seems to become infinite for  $\eta_0 = \pm 1$  (ie I =  $\frac{\pi}{2}$ ,  $\frac{3\pi}{2}$ , etc.) These apparent singular points represent polar trajectories. N<sub>3</sub>, however, occurs only in the third Kinetic equation (2.18c) where it is multiplied by  $\alpha_3$ , the polar component of angular momentum, which reduces to zero for a polar orbit.

Let us investigate  $\alpha_3 N_3$  as  $\eta_0^2 \rightarrow 1$ . For this case the  $\chi$  term of N<sub>3</sub> will be by far the largest, so for a polar trajectory we can write

$$\alpha_{3}N_{3} = \frac{\alpha_{3}}{(\alpha_{2}^{2} - \alpha_{3}^{2})^{2}} \eta_{0}(1 - \eta_{0}^{2})^{-\frac{1}{2}}(1 - \eta_{2}^{-2})^{-\frac{1}{2}}\chi + \text{higher order terms}$$
(6.99)

or since  $\alpha_2^2 - \alpha_3^2 \rightarrow \alpha_2^2$ 

$$\alpha_{3}N_{3} \simeq \frac{\alpha_{3}}{|\alpha_{2}|} n_{0}(1-n_{0}^{2})^{-\frac{1}{2}}(1-n_{2}^{-2})^{-\frac{1}{2}}\chi$$
(6.100)

But from (4.9) and (4.10) we find

$$\frac{\alpha_2^2 - \alpha_3^2}{\alpha_2^2} = n_0^2 + \sin^2 i_0 n_2^{-2} (1 - n_0^2)$$
(6.101)

so that

$$\frac{\alpha_3^2}{\alpha_2^2} = 1 - n_0^2 - \sin^2 i_0 n_2^{-2} (1 - n_0^2)$$
(6.102)

or since  $\sin^2 i_0 \approx 1$  for polar trajectories

$$\frac{|\alpha_3|}{\alpha_2} \simeq (1 - \eta_2^{-2})^{\frac{1}{2}} (1 - \eta_0^{-2})^{\frac{1}{2}}$$
(6.103)

Inserting (6.103) into (6.100) we find

$$a_3N_3 = (sgna_3)\chi + higher order terms$$
 (6.104)

Thus  $\alpha_3N_3$  is well-behaved for a polar trajectory as long as  $\chi$  is wellbehaved. We can plot  $\chi$  versus  $\psi$  from equation (6.64) and the requirement that  $\chi$  equal  $\psi$  at every multiple of  $\frac{\pi}{2}$ .

1. For  $n_0^2 = 0$  (equatorial trajectory),  $tan\chi = tan\psi$ 

2. For 
$$n_0^2 = \frac{3}{4}$$
,  $\tan \chi = \frac{1}{2} \tan \psi$ 

3. For 
$$\eta_0^2 = 1$$
,  $\tan \chi = 0$ 

Thus  $\chi$  as a function of  $\psi$  can be plotted as in Figure 6.1. Whenever the trajectory passes over a pole,  $\psi = \frac{\pi}{2}, \frac{3\pi}{2}$ , etc., with  $\dot{\psi} > 0$ , then  $\chi$  jumps by  $\pi$ . If the trajectory passes over a pole with  $\dot{\psi} < 0$  then  $\chi$  drops by  $\pi$ . Since for a polar orbit  $\alpha_3N_3$  is given by (6.104), it clear from (2.18c) that the right ascension, $\phi$ , also jumps or drops by  $\pi$ , in accord with the jump or drop in  $\chi$ .




# CHAPTER 7

# SOLUTION OF THE KINETIC EQUATIONS

# 7.1 Summary of Integrals

Before proceeding to the solution of the Kinetic equations, let us assemble the results of the two preceeding sections

$$(2\alpha_1)^{\frac{1}{2}}R_1 = a(e \sinh H - H) + b_1H + A_1f + A_{11}sinf + A_{12}sin2f$$
 (5.45)

$$(2\alpha_1)^{\frac{1}{2}}R_2 = A_2f + A_{21}sinf + A_{22}sin2f + A_{23}sin3f + A_{24}sin4f$$
 (5.57)

$$(2\alpha_1)^2 R_3 = A_3 f + A_{31} sinf + A_{32} sin2f + A_{33} sin3f + A_{34} sin^4 f$$
 (5.102)

$$N_{1} = -(\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0}^{3} \left[ B_{1} \psi + \frac{1}{8} (2 - n^{2}) \sin 2\psi + \frac{n^{2}}{64} \sin^{4} \psi \right]$$
(6.43)

$$N_{2} = (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0} \left[ B_{2} \psi + \frac{1}{8} (n^{2} - \frac{3}{4}n^{4}) \sin 2\psi + \frac{3n^{4}}{256} \sin 4\psi \right]$$
(6.51)

$$N_{3} = (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0} \left[ (1 - n_{0}^{2})^{-\frac{1}{2}} (1 - n_{2}^{-2})^{-\frac{1}{2}} \chi + B_{3}\psi + B_{31}\sin 2\psi \right]$$
(6.87)

where

$$A_{1} = p(e^{2}-1)^{\frac{1}{2}} \sum_{n=2}^{\infty} (\frac{b_{2}}{p})^{n} P_{n}(\lambda) T_{n-2}(\sqrt{e^{2}-1})$$
(5.39)

$$A_{11} = \frac{3(e^2 - 1)^2}{4p^3} \left[ -2b_1 b_2^2 p + b_2^4 \right] e$$
 (5.43)

$$A_{12} = \frac{3(e^2 - 1)^{\frac{1}{2}}b_2^4 e^2}{32p^3}$$
(5.44)

$$A_{2} = \frac{(e^{2}-1)^{\frac{1}{2}}}{p} \sum_{n=0}^{\infty} (\frac{b_{2}}{p})^{n} P_{n}(\lambda) T_{n}(\sqrt{e^{2}-1})$$
(5.51)

$$A_{21} = \frac{(e^2 - 1)^2 e}{p} \left[ \frac{b_1}{p} + \frac{3b_1^2 - b_2^2}{p^2} - \frac{9b_1 b_2^2}{2p^3} (1 + \frac{e^2}{4}) + \frac{3b_2^4}{8p^4} (4 + 3e^2) \right]$$
(5.53)

$$A_{22} = \frac{(e^2 - 1)^{\frac{1}{2}}e^2}{p} \left[ \frac{3b_1^2 - b_2^2}{8p^2} - \frac{9b_1b_2^2}{8p^3} + \frac{3b_2^4}{16p^4} (3 + \frac{e^2}{2}) \right]$$
(5.54)

$$A_{23} = \frac{(e^2 - 1)^2 e^3}{8p} \left[ \frac{b_1 b_2^2}{p^3} + \frac{b_2^4}{p^4} \right]$$
(5.55)

$$A_{24} = \frac{3(e^2 - 1)^{\frac{1}{2}} b_2^4 e^4}{256p^5}$$
(5.56)

$$A_{3} = \frac{(e^{2}-1)^{\frac{1}{2}}}{p} \sum_{m=0}^{\infty} D_{m} T_{m+2}(\sqrt{e^{2}-1})$$
(5.96)

$$A_{31} = \frac{(e^2 - 1)^{\frac{1}{2}}e}{p^3} \left[ 2 + \frac{b_1}{p} (3 + \frac{3e^2}{4}) - (\frac{b_2^2}{2p^2} + \frac{c^2}{p^2})(4 + 3e^2) \right]$$
(5.98)

$$A_{32} = \frac{(e^2 - 1)^2}{p^3} \left[ \frac{e^2}{4} + \frac{3b_1 e^2}{4p} - \left( \frac{b_2^2}{2p^2} + \frac{c^2}{p^2} \right) \left( \frac{3e^2}{2} + \frac{e^4}{4} \right) \right]$$
(5.99)

$$A_{33} = \frac{(e^2 - 1)^2}{p^3} \left[ \frac{b_1 e^3}{12p} - \left( \frac{b_2^2}{2} + c^2 \right) \frac{e^3}{3p^2} \right]$$
(5.100)

$$A_{34} = \frac{(e^2 - 1)^2}{p^3} \left[ -\frac{e^4}{32p^2} \left( \frac{b_2^2}{2} + c^2 \right) \right]$$
(5.101)

$$B_1 = -\frac{1}{2} + \frac{3}{16}n^2 - \frac{15}{128}n^4 \tag{6.48}$$

$$B_2 = 1 - \frac{1}{4}n^2 + \frac{9}{64}n^4 \tag{6.53}$$

$$B_{3} = 1 - (1 - \eta_{\overline{2}}^{2})^{-\frac{1}{2}} - \sum_{m=2}^{\infty} \gamma_{m} \eta_{2}^{-2m}$$
(6.82)

$$\gamma_{\rm m} = \frac{(2m)!}{2^{2m}(m!)^2} \sum_{\rm n=1}^{\rm m-1} \frac{\eta_0^{2n}(2n)!}{2^{2n}(n!)^2}$$
(6.83)

$$B_{31} = \frac{3}{32} n_0^2 n_2^{-4} \tag{6.86}$$

$$n^2 = -\frac{n_0^2}{n_2^2} \tag{6.7}$$

### 7.2 The p and n Kinetic Equations

Our method of solving the Kinetic equations will be to solve for  $\rho$ and  $\eta$  from the first two Kinetic equations and then use these results to solve the third Kinetic equation for  $\phi$ . Before doing this it is desirable to obtain some relationships between f and H. From  $\rho = a(e \cosh H-1) =$  $a(e^2-1)/(1+e \cosh)$  we find

$$\cos f = \frac{e - \cosh H}{e \cosh H - 1}$$
(7.1)

$$\sin f = \frac{\sqrt{e^2 - 1} \sinh H}{e \cosh H - 1}$$
(7.2)

$$\cosh H = \frac{e + \cos f}{1 + e \cos f}$$
(7.3)

$$\sinh H = \frac{\sqrt{e^2 - 1} \sin f}{1 + e \cos f}$$
(7.4)

$$\tan \frac{f}{2} = \left(\frac{e+1}{e-1}\right)^{\frac{1}{2}} \tanh \frac{H}{2}$$
(7.5)

so that one anomaly is uniquely determined by the value of the other. The plus sign occurs in (7.2) and (7.4) because both  $\dot{f}$  and  $\ddot{H}$  are positive for all t. Substituting the appropriate  $\rho$  and  $\eta$  integrals into the first two Kinetic equations, (2.18a) and (2.18b), results in

$$t + \beta_{1} = (2\alpha_{1})^{-\frac{1}{2}} [b_{1}H + a(esinhH-H) + A_{1}f + A_{11}sinf + A_{12}sin2f] - c^{2}(\alpha_{2}^{2}-\alpha_{3}^{2})^{-\frac{1}{2}} n_{0}^{3}[B_{1}\psi + \frac{1}{8}(2-n^{2})sin2\psi + \frac{n^{2}}{64}sin^{4}\psi] + periodic terms O(k^{3})$$
(7.6)

$$\beta_{2}/\alpha_{2} = -(2\alpha_{1})^{-\frac{1}{2}} [A_{2}f + A_{21}sinf + A_{22}sin2f + A_{23}sin3f + A_{24}sin^{4}f] + (\alpha_{2}^{2}-\alpha_{3}^{2})^{-\frac{1}{2}} n_{0}[B_{2}\psi + \frac{1}{8}(n^{2}-\frac{3}{4}n^{4})sin2\psi + \frac{3n^{4}}{256}sin^{4}\psi] + periodic terms O(k^{3})$$
(7.7)

Our aim is to solve the above two equations for f, H, and  $\psi$  using the relations between f and H derived previously. With f, H, and  $\psi$  we can then find  $\rho = a(ecoshH-1) = \frac{a(e^2-1)}{1+ecosf}$  and  $n = n_0 \sin\psi$ .

To solve for f, H, and  $\psi$  we first set

$$f = f_0 + f_1 + f_2 \tag{7.8}$$

$$H = H_0 + H_1 + H_2$$
(7.9)

$$\psi = \psi_0 + \psi_1 + \psi_2 \tag{7.10}$$

where  $f_0$ ,  $H_0$ , and  $\psi_0$  are the solutions to the zeroth order portion of (7.6) and (7.7) (ie the part of the equations remaining after all terms of order  $J_2$  or higher have been dropped.) Similarly,  $f_0 + f_1$ ,  $H_0 + H_1$ , and  $\psi_0 + \psi_1$  are solutions to the equations after the terms of order  $J_2^2$ or higher have been dropped. Finally,  $f_2$ ,  $H_2$ , and  $\psi_2$  complete the solution to an accuracy of  $J_2^2$ . Thus  $f_0$ ,  $H_0$ ,  $\psi_0$  are of order  $J_2^0$ ;  $f_1$ ,  $H_1$ ,  $\psi_1$  of order  $J_2^1$ ; and  $f_2$ ,  $H_2$ ,  $\psi_2$  of order  $J_2^2$ . We are essentially solving for f, H, and  $\psi$  as series solutions in powers of  $J_2$ . Listing the coefficients of (7.6) and (7.7) according to their order in J<sub>2</sub> we find

$$J_2^{0}: a, (2\alpha_1)^{-\frac{1}{2}}, (\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}}, e, n_0, B_1, B_2, A_2$$
$$J_2^{1}: A_1, A_{21}, n^2, b_1, c^2, A_{22}, b_2^2$$
$$J_2^{2}: A_{11}, A_{12}, A_{23}, A_{24}$$

For the zeroth order solution we set  $H = H_0$ ,  $f = f_0$ ,  $\psi = \psi_0$  and drop all terms of  $O(J_2)$  or higher. Equations (7.6) and (7.7) become

$$(t+B_1) = (2\alpha_1)^{-\frac{1}{2}} [a(e\sinh H_0-H_0)]$$
 (7.11)

and

$$\beta_2/\alpha_2 = -(2\alpha_1)^{-\frac{1}{2}} A_2 f_0 + n_0(\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}} B_2 \psi_0$$
 (7.12)

Equation (7.11) is just Kepler's equation in hyperbolic form. We can assume that it has been solved by some convenient method to yield the value of H<sub>0</sub>. We then find  $f_0$  from our previously derived anomaly relations, e.g.

$$\tan \frac{f_0}{2} = \left(\frac{e+1}{e-1}\right)^{\frac{1}{2}} \tanh \frac{H_0}{2}$$
(7.13)

Using this value of  $f_0$  we can solve for  $\psi_0$  from (7.12) in the form

$$\psi_0 = (\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}} \eta_0^{-1} B_2^{-1} [\beta_2/\alpha_2 + (2\alpha_1)^{-\frac{1}{2}} A_2 f_0]$$
(7.14)

Proceeding to the first order solution we set  $f = f_0 + f_1$ ,  $H = H_0 + H_1$ ,  $\psi = \psi_0 + \psi_1$  and drop all terms of  $O(J_2^2)$  or higher in (7.6) and (7.7). Thus we find

t + 
$$\beta_1 = (2\alpha_1)^{-\frac{1}{2}} [b_1H_0 + \operatorname{aesinh}(H_0+H_1) - a(H_0+H_1) + A_1f_0] - c^2\eta_0^3(\alpha_2^2-\alpha_3^2)^{-\frac{1}{2}} [B_1\psi_0 + \frac{1}{4}\sin 2\psi_0]$$
 (7.15)

$$\beta_{2}/\alpha_{2} = -(2\alpha_{1})^{-\frac{1}{2}} [A_{2}(f_{0}+f_{1}) + A_{21}\sin f_{0}+A_{22}\sin 2f_{0}] + \eta_{0}(\alpha_{2}^{2}-\alpha_{3}^{2})^{-\frac{1}{2}} [B_{2}(\psi_{0}+\psi_{1}) + \frac{n^{2}}{8}\sin 2\psi_{0}]$$
(7.16)

 $\mathtt{But}$ 

 $\sinh(H_0+H_1) = \sinh H_0 + \sinh H_0(\cosh H_1-1) + \cosh H_0 \sinh H_1$  (7.17)

= 
$$\sinh H_0 + \frac{H_1^2}{2} \sinh H_0 + H_1 \cosh H_0$$
 (7.18)

to order  $J_2^2$ . Substituting (7.18) into (7.15) and subtracting (7.11), we find

$$0 = (2\alpha_1)^{-\frac{1}{2}} [b_1H_0 + ae \frac{H_1^2}{2} \sinh H_0 + aeH_1 \cosh H_0 - aH_1 + A_1f_0] - c^2n_0^3(\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}} [B_1\psi_0 + \frac{1}{4}\sin 2\psi_0]$$
(7.19)

which can be put in the form

$$H_{1}^{2}\left(\frac{\operatorname{aesinh} H_{0}}{2}\right) + H_{1}\left(\operatorname{ae} \cosh H_{0}-a\right) + b_{1}H_{0} + A_{1}f_{0}$$
$$- c^{2}n_{0}^{3}(2\alpha_{1})^{\frac{1}{2}}(\alpha_{2}^{2}-\alpha_{3}^{2})^{-\frac{1}{2}}(B_{1}\psi_{0}+\frac{1}{4}\sin 2\psi_{0}) = 0 \qquad (7.20)$$

Equation (7.20) is a quadratic in  $H_1$ , and thus yields two solutions for  $H_1$ . Since  $H_1$  is small we seek that solution of (7.20) which is closest to the solution of (7.20) with the first term set to zero. That solution is

$$H_{1} = H_{1} (1 - \frac{\operatorname{esinh} H_{0}}{2(\operatorname{ecosh} H_{0} - 1)} H_{1})$$
(7.21)

where

$$h_{1}^{\prime} = \frac{c^{2} \eta_{0}^{3} (2\alpha_{1})^{\frac{1}{2}} (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} [B_{1}\psi_{0} + \frac{1}{4} \sin 2\psi_{0}] - b_{1}H_{0} - A_{1}f_{0}}{a(e \cosh H_{0} - 1)}$$
(7.22)

we then find  $f_1$  from our anomaly relations, e.g.

$$\tan \frac{(f_0+f_1)}{2} = \left(\frac{e+1}{e-1}\right)^{\frac{1}{2}} \tanh \frac{(H_0+H_1)}{2}$$
(7.23)

Subtracting (7.12) from (7.16) and solving for  $\psi_1$  results in

$$\psi_{1} = -B_{2}^{-1} \frac{n^{2}}{8} \sin 2\psi_{0} + B_{2}^{-1} (2\alpha_{1})^{-\frac{1}{2}} (\alpha_{2}^{2} - \alpha_{3}^{2})^{\frac{1}{2}} n_{0}^{-1} [A_{2}f_{1} + A_{21} \sin f_{0} + A_{22} \sin 2f_{0}]$$
(7.24)

Finally, for the second order solution we set  $f = f_0 + f_1 + f_2$ ,  $H = H_0 + H_1 + H_2$ ,  $\psi = \psi_0 + \psi_1 + \psi_2$  and drop only those terms of order  $J_2^3$  or higher in (7.6) and (7.7). There results

$$t + \beta_{1} = (2\alpha_{1})^{-\frac{1}{2}} [b_{1}(H_{0}+H_{1}) + \operatorname{aesinh}(H_{0}+H_{1}+H_{2}) - a(H_{0}+H_{1}+H_{2}) + A_{1}(f_{0}+f_{1}) + A_{11} \operatorname{sinf}_{0} + A_{12} \operatorname{sin2} f_{0}] - c^{2} n_{0}^{3} (\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} [B_{1}(\psi_{0}+\psi_{1}) + \frac{1}{4} (\operatorname{sin2} \psi_{0}+2\psi_{1} \cos 2\psi_{0}) - \frac{n^{2}}{8} \operatorname{sin2} \psi_{0} + \frac{n^{2}}{64} \operatorname{sin4} \psi_{0}]$$
(7.25)

and

$$\beta_{2}/\alpha_{2} = -(2\alpha_{1})^{-\frac{1}{2}} [A_{2}(f_{0}+f_{1}+f_{2}) + A_{21}(\sin f_{0} + f_{1}\cos f_{0}) + A_{22}(\sin 2f_{0} + 2f_{1}\cos 2f_{0}) + A_{23}\sin 3f_{0} + A_{24}\sin 4f_{0}] + n_{0}(\alpha_{2}^{2}-\alpha_{3}^{2})^{-\frac{1}{2}} [B_{2}(\psi_{0}+\psi_{1}+\psi_{2}) + \frac{n^{2}}{8}(\sin 2\psi_{0} + 2\psi_{1}\cos 2\psi_{0}) - \frac{3n^{4}}{32}\sin 2\psi_{0} + \frac{3n^{4}}{256}\sin 4\psi_{0}]$$
(7.26)

But to order  $J_2^2$ 

$$sinh(H_0+H_1+H_2) = sinh(H_0+H_1) + H_2coshH_0$$
 (7.27)

If we substitute this into (7.25), and subtract (7.15) from the result, we find

$$0 = (2\alpha_1)^{-\frac{1}{2}} [b_1H_1 + aeH_2 \cosh H_0 - aH_2 + A_1f_1 + A_{11} \sin f_0 + A_{12} \sin 2f_0] - c^2 n_0^3 (\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}} [B_1\psi_1 + \frac{\psi_1}{2} \cos 2\psi_0 - \frac{n^2}{8} \sin 2\psi_0 + \frac{n^2}{64} \sin 4\psi_0]$$
(7.28)

or solving for  ${\rm H}_2$ 

$$H_{2} = (\operatorname{aecoshH}_{0}-a)^{-1} \left[ -b_{1}H_{1}-A_{1}f_{1}-A_{11}\operatorname{sinf}_{0} -A_{12}\operatorname{sin2}f_{0} + c^{2}n_{0}^{3}(2\alpha_{1})^{\frac{1}{2}}(\alpha_{2}^{2}-\alpha_{3}^{2})^{-\frac{1}{2}}[B_{1}\psi_{1} + \frac{\psi_{1}}{2}\cos2\psi_{0} - \frac{n^{2}}{8}\sin2\psi_{0} + \frac{n^{2}}{64}\sin4\psi_{0}] \right]$$
(7.29)

We then solve for  $f_2$  from the anomaly relations, e.g.

$$\tan \frac{(f_0 + f_1 + f_2)}{2} = \left(\frac{e+1}{e-1}\right)^{\frac{1}{2}} \tanh \frac{(H_0 + H_1 + H_2)}{2}$$
(7.30)

To find  $\psi_2$  we subtract (7.16) from (7.26) leaving

$$0 = -(2\alpha_1)^{-\frac{1}{2}} [A_2 f_2 + A_{21} f_1 \cos f_0 + A_{22} 2 f_1 \cos 2 f_0 + A_{23} \sin 3 f_0 + A_{24} \sin^4 f_0] + n_0 (\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}} [B_2 \psi_2 + \frac{n^2}{8} 2 \psi_1 \cos 2 \psi_0 - \frac{3n^4}{32} \sin 2 \psi_0 + \frac{3n^4}{256} \sin^4 \psi_0]$$
(7.31)

Solving for  $\psi_2$  we find

$$\psi_{2} = B_{2}^{-1} \left(-\frac{n^{2}}{4} \psi_{1} \cos 2\psi_{0} + \frac{3n^{4}}{32} \sin 2\psi_{0} - \frac{3n^{4}}{256} \sin^{4}\psi_{0}\right) + B_{2}^{-1} \eta_{0}^{-1} \left(\alpha_{2}^{2} - \alpha_{3}^{2}\right)^{\frac{1}{2}} (2\alpha_{1})^{-\frac{1}{2}} \left[A_{2}f_{2} + A_{21}f_{1} \cos f_{0} + A_{22}2f_{1} \cos 2f_{0} + A_{23} \sin 3f_{0} + A_{24} \sin^{4}f_{0}\right]$$
(7.32)

This completes the solution, through order  $J_2^2$ , for f, H, and  $\psi$ , and thus for the spheroidal coordinates  $\rho$  and  $\eta$ .

# 7.3 The Right Ascension $\phi$

According to the final Kinetic equation (2.18c) and the definitions of  $R_3$  and  $N_3$  we have

$$\phi = \beta_3 - c^2 \alpha_3 R_3 + \alpha_3 N_3 \tag{7.33}$$

Substituting above for R<sub>3</sub> and N<sub>3</sub> from (5.102) and (6.87) respectively we find

$$\phi = \beta_3 + \alpha_3(\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}} n_0[(1 - n_0^2)^{-\frac{1}{2}}(1 - n_2^{-2})^{-\frac{1}{2}}\chi + B_3\psi + \frac{3}{32} n_0^2 n_2^{-4} \sin 2\psi] - c^2 \alpha_3(2\alpha_1)^{-\frac{1}{2}} [A_3f + A_{31} \sin f + A_{32} \sin 2f + A_{33} \sin 3f + A_{34} \sin^4 f]$$
(7.34)

where  $\psi$  and f are now known and  $\chi$  can be found from  $\tan \chi = (1-\eta_0^2)^2 \tan \psi$ . Thus the final spheroidal coordinate  $\phi$  can be found from (7.34)

From Figure 6.1 it is clear that  $\chi$  may vary quite rapidly as the satellite passes over or near a pole. We can avoid such difficult calculations, however, by expressing the position of the satellite in rectangular coordinates. The relations between rectangular and spheroidal coordinates are given by (2.1) and (2.2). From (7.34) it is clear that  $\phi$ may be expressed as

$$\phi = \Omega' + \kappa \chi \tag{7.35}$$

where

$$\Omega^{\prime} \equiv \beta_{3} + \alpha_{3}(\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0}[B_{3}\psi + \frac{3}{32} n_{0}^{2} n_{2}^{-4} \sin 2\psi] - c^{2}\alpha_{3}(2\alpha_{1})^{-\frac{1}{2}}[A_{3}f + \sum_{j=1}^{4} A_{3j} \sin jf]$$
(7.36)

which is well-behaved near the poles and  $\kappa \chi$  is that part of  $\phi$  which varies rapidly near the poles. By definition  $n_0$  is positive so that we may write

$$\kappa = |\kappa| \operatorname{sgn} \alpha_3 \tag{7.37}$$

and thus find

$$\kappa^{2} = \alpha_{3}^{2} (\alpha_{2}^{2} - \alpha_{3}^{2})^{-1} n_{0}^{2} (1 - n_{0}^{2})^{-1} (1 - n_{2}^{-2})^{-1}$$
(7.38)

$$= \frac{\alpha_3^2 n_0^2 n_2^2}{(\alpha_2^2 - \alpha_3^2)(n_0^2 + n_2^2 - 1 - n_0^2 n_2^2)}$$
(7.39)

Substituting for  $n_0^2 n_2^2$  and  $n_0^2 + n_2^2$  from (4.3) and (4.2) respectively we find

$$\kappa^2 = 1 \tag{7.40}$$

so that

$$\kappa = \operatorname{sgn}\alpha_3 = \pm 1 \tag{7.41}$$

for direct or retrograde motion, respectively, so that  $\phi$  will either always increase or always decrease. Thus

$$\phi = \Omega' + \chi \text{sgn } \alpha_3 \tag{7.42}$$

From the relation  $\tan \chi = (1-n_0^2)^{\frac{1}{2}} \tan \psi$  and the requirement that  $\dot{\chi}$  and  $\dot{\psi}$  are always positive, we find

.

$$\sin \chi = \frac{(1-n_0^2)^{\frac{1}{2}} \sin \psi}{\sqrt{1-n_0^2 \sin^2 \psi}}$$
(7.43)

and

$$\cos\chi = \frac{\cos\psi}{\sqrt{1 - \eta_0^2 \sin^2\psi}} \tag{7.44}$$

so that

$$\exp i\chi = \frac{\cos\psi + i\sqrt{1 - n_0^2} \sin\psi}{\sqrt{1 - n_0^2 \sin^2\psi}}$$
(7.45)

If we insert (7.45) and (7.42) into (2.1) using the relation  $sgna_3(1-n_0^2)^2 = sgna_3|cosI| = cosI$  we find

$$X + iY = (\rho^2 + c^2)^{\frac{1}{2}} [\cos \psi + i\cos I \sin \psi] \exp i\Omega^{2}$$
(7.46)

or separately

$$X = (\rho^2 + c^2)^2 [\cos\psi \, \cos\Omega' - \cos I \, \sin\psi \, \sin\Omega']$$
(7.47)

and

$$Y = (\rho^2 + c^2)^{\frac{1}{2}} [\cos I \sin \psi \cos \Omega^2 + \sin \Omega^2 \cos \psi]$$
(7.48)

also from (2.2)

$$Z = \rho \eta \tag{7.49}$$

These expressions for X, Y, and Z cover all cases and do not involve calculating  $\phi$ . Thus they contain no singularities or rapidly varying quantities, causing no trouble for polar or nearly polar trajectories. For a strictly polar trajectory cos I  $\rightarrow$  0,  $\alpha_3 \rightarrow$  0, so that  $\Omega' = \beta_3$  and

$$X + iY = (\rho^{2} + c^{2})^{\frac{1}{2}} \cos \psi \exp i\beta_{3}$$
 (7.50)

If we did want to calculate  $\phi$  for a nearly polar trajectory, it would be best calculated by

$$\exp i\chi = \frac{\cos\psi + i|\cos I| \sin\psi}{\sqrt{\cos^2\psi + \cos^2 I \sin^2\psi}}$$
(7.51)

and (7.36). Using (7.51) for  $\chi$  avoids the difference of two nearly equal terms in the denominator.

# 7.4 The Velocity Components

Differentiating (7.46) with respect to time yields

$$\dot{\mathbf{X}} + \mathbf{i}\dot{\mathbf{Y}} = \left[\frac{\rho\dot{\rho}}{\rho^{2} + \mathbf{c}^{2}} + \mathbf{i}\dot{\Omega}^{2}\right](\mathbf{X} + \mathbf{i}\mathbf{Y}) + (\rho^{2} + \mathbf{c}^{2})^{\frac{1}{2}}(-\sin\psi + \mathbf{i}\cos\mathbf{I}\,\cos\psi)\dot{\psi}\,\exp\,\mathbf{i}\Omega^{2}$$
(7.52)

or separately

$$\dot{\mathbf{X}} = \frac{\rho \dot{\rho}}{\rho^2 + c^2} \mathbf{X} - \mathbf{Y} \dot{\Omega}^{\prime} + (\rho^2 + c^2)^{\frac{1}{2}} (-\sin\psi \ cos\Omega^{\prime} - \cosI \ \cos\psi \ sin\Omega^{\prime}) \dot{\psi}$$
(7.53)

$$\dot{\mathbf{Y}} = \frac{\rho \ \dot{\rho}}{\rho^2 + c^2} \ \mathbf{Y} + \mathbf{X} \hat{\Omega}^2 + (\rho^2 + c^2)^2 (-\sin\psi \ \sin\Omega^2 + \cos \mathbf{I} \ \cos\psi \ \cos\Omega^2) \dot{\psi}$$
(7.54)

Then from (7.49) we obtain

$$\dot{Z} = \dot{\rho}n + \rho\dot{n} = \dot{\rho}n + n_0\rho \cos\psi\dot{\psi}$$
 (7.55)

Clearly, the three velocity components are well-behaved for all trajectories. To find  $\hat{\rho}$  we first combine equations (10.1) and (13.1) of Vinti [1] to get

$$\frac{\partial S}{\partial \xi} = c^2 \frac{(\rho^2 + c^2 \eta^2)}{(\rho^2 + c^2)} \dot{\xi}$$
(7.56)

where S is the Hamilton-Jacobi function and

$$\xi = \frac{\rho}{c} \tag{(7.57)}$$

Then from equation (53.1) of Vinti [1] we find

$$\frac{\partial S}{\partial \xi} = \frac{\pm \sqrt{F(\rho)}}{c(\xi^2 + 1)}$$
(7.58)

Combining (7.56), (7.57), and (7.58) yields

$$\dot{\rho} = \frac{\pm \sqrt{F(\rho)}}{(\rho^2 + c^2 \eta^2)}$$
(7.59)

If we take  $F(\rho)$  in the form of (3.11) and insert  $\rho_1 = a(e-1)$ ,  $\rho_2 = -a(e+1)$ , and  $\rho = a(e \cosh H-1)$  we find

$$F(\rho) = 2\alpha_1 (\operatorname{aesinh} H)^2 (\rho^2 + A\rho + B)$$
(7.60)

Since  $\dot{\rho}$  = ae sinhH H and H > 0 for all t, sinhH  $\gtrless$  0 accordingly as  $\dot{\rho} \gtrless$  0, respectively. The  $\ddagger$ |sinhH| resulting from (7.59) and (7.60) thus reduces to sinhH and thus

$$\dot{\rho} = \frac{(2\alpha_1)^{\frac{1}{2}}}{(\rho^2 + c^2 \eta^2)} \frac{\operatorname{aesinh} H(\rho^2 + A\rho + B)^{\frac{1}{2}}}{(\rho^2 + c^2 \eta^2)}$$
(7.61)

We then proceed to find n by a similar method.

Combining equations (13.2) and (10.2) of Vinti [1] yields

$$\frac{\partial S}{\partial \eta} = \frac{\rho^2 + c^2 \eta^2}{1 - \eta^2} \dot{\eta}$$
(7.62)

But from (53.2) of the same paper

$$\frac{\partial S}{\partial \eta} = \pm \frac{\sqrt{G(\eta)}}{(1-\eta^2)} \tag{7.63}$$

so that

$$n = \pm \frac{\sqrt{G(n)}}{\rho^2 + c^2 n^2}$$
 (7.64)

If we use G(n) in the form of (3.40) and insert  $n = n_0 \sin \psi$  and

$$n^2 = -\frac{n_0^2}{n_2^2}$$
, there results

$$G(n) = (\alpha_2^2 - \alpha_3^2)(1 + n^2 \sin^2 \psi) \cos^2 \psi$$
 (7.65)

Substituting (7.65) for G(n) in (7.64) results in

$$\dot{n} = \frac{(\alpha_2^2 - \alpha_3^2)^2 (1 + n^2 \sin^2 \psi)^2 \cos \psi}{\rho^2 + c^2 \eta^2}$$
(7.66)

The  $\pm |\cos\psi|$  resulting from (7.64) becomes  $\cos\psi$ , since  $\cos\psi \gtrless 0$ accordingly as  $\eta \gtrless 0$ , respectively. Then, since  $\dot{\eta} = \eta_0 \cos\psi \dot{\psi}$  we can solve for  $\dot{\psi}$  as

$$\dot{\psi} = \frac{\dot{n}}{n_0 \cos\psi} = \frac{(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}} (1 + n^2 \sin^2 \psi)^{\frac{1}{2}}}{n_0 (\rho^2 + c^2 \eta^2)}$$
(7.67)

To find  $\hat{\Omega}'$  we differentiate (7.36). Thus

$$\hat{\Omega}^{\prime} = \alpha_{3}(\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} n_{0}[B_{3} + \frac{3}{16} n_{0}^{2} n_{2}^{-4} \cos 2\psi]\dot{\psi} - c^{2}\alpha_{3}(2\alpha_{1})^{-\frac{1}{2}} [A_{3} + \sum_{j=1}^{4} jA_{3j} \cos jf]\dot{f}$$
(7.68)

To solve for f we differentiate the relation  $\rho = p(1+e\cos f)^{-1}$ . Solving for f we find

$$f = \frac{p\rho}{\rho^2 esinf}$$
(7.69)

Using the anomaly connection (7.2) to substitute for sinf yields

$$\dot{f} = \frac{\dot{\rho}}{\rho \sinh H} \frac{\sqrt{e^2 - 1}}{e}$$
(7.70)

Finally substituting for  $\rho$  from (7.61)

$$\mathbf{\dot{f}} = \frac{a\sqrt{e^2 - 1} (2\alpha_1)^{\frac{1}{2}} (\rho^2 + A\rho + B)^{\frac{1}{2}}}{\rho(\rho^2 + c^2 \eta^2)}$$
(7.71)

Thus equations (7.53), (7.54), (7.55), (7.61), (7.66), (7.67), (7.68), and (7.71) form a complete algorithm for the velocity vector in X, Y, Z, space.

#### 7.5 Determining the $\beta$ 's From an Initial State Vector

Up to this point we have merely assumed the  $\beta$ 's to be known constants without specifying how they might be calculated. In this section, therefore, we consider determining the values of the  $\beta$ 's given an initial state vector of the satellite. We have seen previously that from this initial state vector the a's can be calculated according to equations (3.8), (3.9), and (3.10). Using these values of the a's we can then calculate the orbital elements  $a_0$ ,  $e_0$ , and  $i_0$  from equations (3.3), (3.4), and (3.5). This allows us to calculate values for the set of orbital elements a, e, and  $n_0 = \sin I$ from equations (3.33), (3.36), and (3.48). We can determine the initial values of the anomalies H and f from the equation,  $\rho_i = a(e^2-1)/(1+e\cos f_i)$ , and the anomaly connections (viz. equation (7.5)). The initial values of  $\psi$  and  $\chi$  can be calculated from  $n_i = n_0 \sin \psi_i$  and  $\tan \chi_i = (1-n_0^2)^{\frac{1}{2}} \tan \psi_i$ . We now have sufficient information to evaluate all the terms in the Kinetic equations (7.6), (7.7), and (7.34), excluding the  $\beta$ 's. Thus we can solve for the  $\beta$ 's numerically from these three Kinetic equations. Note that for nearly polar orbits, where our calculation of  $\chi_i$  depends on the difference of two nearly equal numbers,  $\chi_i$  would be better calculated by (7.5.)

In summary, we have seen that the  $\beta$ 's like the  $\alpha$ 's, can be determined from an initial state vector.

# 7.6 Solution of the Kinetic Equations as c Approaches Zero

Setting c = 0 in the Kinetic equations (7.6), (7.7), and (7.34) should reduce them to the case of simple Keplerian hyperbolic motion. In this manner we can not only provide a rough check on our results, but also obtain some insight into what the constants  $\beta_1$ ,  $\beta_2$ , and  $\beta_3$  represent.

Dropping all terms of order k or higher in (7.6), (7.7), and (7.34) results in

$$t + \beta_1 = \frac{a}{\sqrt{2\alpha_1}} (esinhH-1)$$
(7.72)

$$\beta_2/\alpha_2 = -(2\alpha_1)^{-\frac{1}{2}} \frac{\sqrt{e^2-1}}{p} f + n_0(\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}} \psi$$
 (7.73)

$$\phi = \beta_3 + \alpha_3 (\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}} \frac{\eta_0}{\sqrt{1 - \eta_0^2}} \chi$$
 (7.74)

But for c = 0 we know  $a = a_0$ ,  $e = e_0$ , and  $I = i_0$  so that

$$2\alpha_1 \rightarrow \frac{\mu}{a}$$
 (7.75)

$$\eta = \sin I \sin \psi \rightarrow \sin \theta \tag{7.76}$$

$$(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}} \rightarrow \alpha_2 \text{ sinI}$$
 (7.77)

Using these relations in (7.72), (7.73), and (7.74) we reduce the Kinetic equations to

t + 
$$\beta_1 = (\frac{a^3}{\mu})^{\frac{1}{2}} (\text{esinhH-H})$$
 (7.78)

$$\beta_2 = \psi - f = \sin^{-1}(\frac{\sin\theta}{\sin I}) - f \qquad (7.79)$$

$$\phi = \beta_3 + \chi = \beta_3 + \sin^{-1}(\frac{\tan\theta}{\tan I})$$
(7.80)

The corresponding Keplerian relations are

$$t - \tau = \left(\frac{a^3}{\mu}\right)^{\frac{1}{2}} (esinhH-H)$$
 (7.81)

$$\omega = \psi - f = \sin^{-1} \left( \frac{\sin \theta}{\sin I} \right) - f \tag{7.82}$$

$$\phi = \Omega + \chi = \Omega + \sin^{-1} \left(\frac{\tan\theta}{\tan I}\right) \tag{7.83}$$

These angles are defined in Figure 7.1.

Upon comparing the reduced Kinetic equations (7.78), (7.79), and (7.80), to the corresponding Keplerian relations, it is apparent that to agree identically we must have

$$-\beta_1 \rightarrow \tau$$
 = time of perigee passage (7.84)





$$\beta_2 \rightarrow \omega = \text{argument of perigee}$$
 (7.85)

 $\beta_3 \rightarrow \Omega = \text{longitude of the node}$  (7.86)

as c goes to zero. We have also seen that f, I, and  $\chi$  reduce to the true anomaly, inclination, and projection of the argument of latitude onto the equator, respectively, as c goes to zero.

#### CHAPTER 8

#### ASYMPTOTIC MOTION

In this section we consider the analytic determination of one of the asymptotes of the spheroidal "hyperbola," either incoming or outgoing, given the other asymptote. Such a solution would find application in calculating swingby maneuvers about an oblate body. Thus given a desired outgoing asymptote, for example, we could determine the necessary incoming conditions.

The incoming asymptote is defined by  $\rho \rightarrow r \rightarrow \infty$ ,  $t \rightarrow -\infty$ , while the outgoing asymptote is defined by  $\rho \rightarrow r \rightarrow \infty$ ,  $t \rightarrow \infty$ . From (2.2), these conditions imply  $\eta \rightarrow \sin\theta$  on the asymptotes. Setting  $\rho \rightarrow \infty$  in (7.61), (7.66), (7.67), (7.68), and (7.71) results in

$$\dot{\rho} \rightarrow \dot{r} \rightarrow (2\alpha_1)^{\frac{1}{2}} \tag{8.1}$$

- $n \to 0$  (8.2)
- $\dot{\psi} \rightarrow 0$  (8.3)
- $\mathbf{\dot{f}} \neq 0$  (8.4)

$$\hat{\Omega}^* \neq 0 \tag{8.5}$$

Note that these equations are true on both asymptotes. Inserting (8.1) through (8.5) into (7.53), (7.54), and (7.55) we find

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$$\dot{X} \rightarrow \frac{X\dot{r}}{r}$$
 (8.6)

$$\dot{Y} \rightarrow \frac{Y\dot{r}}{r}$$
 (8.7)

$$\dot{z} \rightarrow \dot{r}\eta$$
 (8.8)

But by (7.47) and (7.48)  

$$X \rightarrow r(\cos\psi \cos\Omega' - \cos I \sin\psi \sin\Omega')$$
 (8.9)  
 $Y \rightarrow r(\cos I \sin\psi \cos\Omega' + \sin\Omega' \cos\psi)$  (8.10)

Substituting (8.9) and (8.10) into (8.6) and (8.7) and using  $\eta = \sin I \sin \psi$  in (8.8) yields

$$\dot{X} \rightarrow \dot{r}(\cos\psi \, \cos\Omega' - \cos I \, \sin\psi \, \sin\Omega')$$
 (8.11)

$$\dot{\mathbf{Y}} \rightarrow \dot{\mathbf{r}}(\cos\mathbf{I} \sin\psi \cos\Omega' + \sin\Omega' \cos\psi)$$
 (8.12)

$$\dot{Z} \rightarrow \dot{r} \sin I \sin \psi$$
 (8.13)

Given a state vector on an asymptote we can most easily calculate  $\cdot$  the  $\alpha$ 's using the modified forms of (3.8), (3.9), and (3.10)

$$\alpha_{1} = \frac{1}{2} \dot{r}_{1}^{2} = \frac{1}{2} (\dot{x}^{2} + \dot{y}^{2} + \dot{z}^{2})$$
(8.14)

$$\alpha_{3} = X_{i}\dot{Y}_{i} - Y_{i}\dot{X}_{i} = [(r_{ax}^{2} + r_{ay}^{2})(\dot{X}^{2} + \dot{Y}^{2})]^{\frac{1}{2}}$$
(8.15)

$$\alpha_{2}^{2} = \frac{\left[r_{i}(\dot{z}_{i} - \dot{r}_{i}n_{i})\right]^{2} + \alpha_{3}^{2} - 2\alpha_{1}c^{2}n_{i}^{2}(1 - n_{i}^{2})}{(1 - n_{i}^{2})}$$

$$= (\dot{x}^{2} + \dot{y}^{2} + \dot{z}^{2})(r_{ax}^{2} + r_{ay}^{2} + r_{az}^{2}) - c^{2}\dot{z}^{2}$$
(8.16)

where  $\dot{X}\underline{i} + \dot{Y}\underline{j} + \dot{Z}\underline{k}$  is now the hyperbolic excess velocity vector and  $\underline{r}_{a} = r_{ax}\underline{i} + r_{ay}\underline{j} + r_{az}\underline{k}$  is the vector from the origin to the aiming point, i.e. the point on the extension of the asymptote closest to the origin. With these values of the  $\alpha$ 's we can then determine the orbital elements  $a_0$ ,  $e_0$ ,  $i_0$ , and the elements a, e, I using the method of the previous section. Then equations (8.11), (8.12), and (8.13) allow us to find  $\psi_i$  and  $\Omega'_i$ . Since  $\dot{r}$  and I will be the same for both asymptotes, the problem of determining one asymptote given the other reduces to the problem of determining the  $\Delta\Omega'$  and  $\Delta\psi$  caused by a swingby of the oblate body. Here we have defined

$$\psi_{\text{out}} = \psi_{\text{in}} + \Delta \psi \tag{8.17}$$

$$\Omega_{\text{out}}^{*} = \Omega_{\text{in}}^{*} + \Delta \Omega^{*}$$
(8.18)

To solve for  $\Delta\Omega^{\prime}$  and  $\Delta\psi$  we first consider the outgoing asymptote. Setting  $t \rightarrow \infty$  in (7.11) yields

$$H_{0}_{out} = \infty \tag{8.19}$$

and thus by (7.13)

$$f_{0_{out}} = \cos^{-1}(-\frac{1}{e}) \equiv f_a$$
 (8.20)

Inserting this value of fo into (7.14) results in

$$\psi_{0}_{\text{out}} = \frac{(\alpha_{2}^{2} - \alpha_{3}^{2})^{\frac{1}{2}}}{n_{0}B_{2}} \left[\frac{\beta_{2}}{\alpha_{2}} + (2\alpha_{1})^{-\frac{1}{2}} A_{2}f_{a}\right]$$
(8.21)

Then by (7.22)

$$H'_{1_{out}} = \frac{-2b_1H_0}{ae} = \frac{-2b_1}{ae} \frac{1}{1+\frac{H_0}{2!}+\frac{H_0^2}{3!}} = 0$$
(8.22)

so that by (7.21)

$$H_{1_{out}} = 0$$
 (8.23)

Proceeding similarly with the remaining equations of Section 7.2 we find

$$f_{1_{out}} = 0$$
 (8.24)

$$\psi_{1_{out}} = -B_2^{-1} \frac{n^2}{8} \sin 2\psi_{0_{out}} + B_2^{-1} (2\alpha_1)^{-\frac{1}{2}}$$

$$\frac{(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}}}{\eta_0} [A_{21} \sin f_a + A_{22} \sin 2f_a] \qquad (8.26)$$

$$H_{2}_{out} = 0$$
 (8.27)

$$f_{2_{out}} = 0$$
 (8.28)

$$\psi_{2_{out}} = B_{2}^{-1} \left(-\frac{n^{2}}{4} \psi_{1_{out}} \cos 2\psi_{0_{out}} + \frac{3n^{4}}{32} \sin 2\psi_{0_{out}} - \frac{3n^{4}}{256} \sin^{4}\psi_{0_{out}}\right) + B_{2}^{-1} \eta_{0}^{-1} (\alpha_{2}^{2} - \alpha_{3}^{2})^{\frac{1}{2}} (2\alpha_{1})^{-\frac{1}{2}}$$

$$\left[A_{23} \sin 3f_{0_{out}} + A_{24} \sin^{4}f_{0_{out}}\right] \qquad (8.29)$$

Thus

$$\Psi_{\text{out}} = \Psi_{0}_{\text{out}} + \Psi_{1}_{\text{out}} + \Psi_{2}_{\text{out}} = \frac{\left(\alpha_{2}^{2} - \alpha_{3}^{2}\right)^{\frac{1}{2}}}{B_{2}n_{0}} \left[\beta_{2}/\alpha_{2} + (2\alpha_{1})^{-\frac{1}{2}}(A_{2}f_{a} + A_{2})\sin f_{a} + A_{22}\sin 2f_{a} + A_{23}\sin 3f_{a} + A_{24}\sin 4f_{a}\right] + B_{2}^{-1}\left[-\frac{n^{2}}{8}\sin 2\Psi_{0}_{\text{out}} - \frac{n^{2}}{4}\Psi_{1}_{\text{out}}\cos 2\Psi_{0}_{\text{out}} + \frac{3n^{4}}{32}\sin 2\Psi_{0}_{\text{out}} - \frac{3n^{4}}{256}\sin 4\Psi_{0}_{\text{out}}\right]$$
(8.30)

$$\Omega_{\text{out}}^{*} = \beta_{3} + \alpha_{3}(\alpha_{2}^{2} - \alpha_{3}^{2})^{-\frac{1}{2}} \eta_{0}[B_{3}\psi_{\text{out}} + \frac{3}{32}\eta_{0}^{2}\eta_{2}^{-4} \sin^{2}\psi_{\text{out}}] - c^{2}\alpha_{3}(2\alpha_{1})^{-\frac{1}{2}}[A_{3}f_{a} + A_{31}\sin f_{a} + A_{32}\sin^{2}f_{a} + A_{33}\sin^{3}f_{a} + A_{34}\sin^{4}f_{a}]$$
(8.31)

Proceeding now to the incoming asymptote we set t  $\rightarrow -\infty$  in (7.11), resulting in

$$H_{0_{in}} = -\infty \tag{8.32}$$

so that by (7.13)

$$f_{0_{in}} = \cos^{-1}\left(-\frac{1}{e}\right)$$
(8.33)

Since  $f_{0_{in}}$  cannot equal  $f_{0_{out}}$  we must have

$$f_{0_{in}} = -f_{0_{out}} = -f_{a}$$
 (8.34)

Clearly equations (8.21) through (8.31) can be applied just as well to the incoming asymptote if we replace all "out" subscripts by "in" subscripts and substitute  $-f_a$  for  $f_a$ . Performing the above replacements in (8.30) and then subtracting the result from (8.30) yields

$$\Delta \Psi \equiv \Psi_{\text{out}} - \Psi_{\text{in}} = \frac{2(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}}(2\alpha_1)^{-\frac{1}{2}}}{n_0 B_2} [A_2 f_a + A_{21} \sin f_a + A_{22} \sin 2f_a + A_{23} \sin 3f_a + A_{24} \sin 4f_a] + B_2^{-1} [-\frac{n^2}{8} \sin(2\psi_0 + 2\Delta\psi_0) + \frac{n^2}{8} \sin(2\psi_0 - \frac{n^2}{4}(\psi_1 + \Delta\psi_1)\cos(2\psi_0 + 2\Delta\psi_0)) + \frac{n^2}{8} \sin(2\psi_0 + 2\Delta\psi_0) - \frac{3n^4}{32} \sin(2\psi_0 + 2\Delta\psi_0) - \frac{3n^4}{32} \sin(2\psi_0 + 2\Delta\psi_0) - \frac{3n^4}{32} \sin(2\psi_0 + 2\Delta\psi_0) + \frac{3n^4}{32} \sin(2\psi_0 + 2\Delta\psi_0) + \frac{3n^4}{32} \sin(2\psi_0 + 2\Delta\psi_0) + \frac{3n^4}{32} \sin(2\psi_0 + 2\Delta\psi_0)]$$

$$(8.35)$$

where we have dropped the in-out subscripts in favor of letting the incoming conditions be represented by  $\psi_0$ ,  $\psi_1$ , and the outgoing conditions by  $\psi_0 + \Delta \psi_0$ ,  $\psi_1 + \Delta \psi_1$ . If in (8.35) we expand the sin(a+b) and cos(a+b) terms and substitute sin  $n\psi_0 = \sin n\psi_{in} - n\psi_1 \cos n\psi_{in}$  and  $\cos n\psi_0 = \cos n\psi_{in}$ +  $n\psi_1 \sin n\psi_{in}$  we find that, to order  $J_2^2$ , (8.35) becomes

$$\Delta \Psi = 2(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}}(2\alpha_1)^{-\frac{1}{2}} n_0^{-1} B_2^{-1} [A_2 f_a + A_{21} \sin f_a + A_{22} \sin 2f_a + A_{23} \sin 3f_a + A_{24} \sin 4f_a] + A_{22} \sin 2f_a + A_{23} \sin 3f_a + A_{24} \sin 4f_a] + B_2^{-1}[-\frac{n^2}{8}(\sin 2(\Psi_{in} + \Delta \Psi_0) - \sin 2\Psi_{in}) - \frac{n^2}{4} \Delta \Psi_1 \cos 2(\Psi_{in} + \Delta \Psi_0) + \frac{3n^4}{32}(\sin 2(\Psi_{in} + \Delta \Psi_0) - \sin 2\Psi_{in}) - \frac{3n^4}{256}(\sin 4(\Psi_{in} + \Delta \Psi_0) - \sin 4\Psi_{in})]$$

$$(8.36)$$

where  $\psi_{in}$  can be determined from the incoming asymptote as discussed earlier in this section. If in (8.21) we replace  $f_a$  by  $-f_a$ , change the subscripts to "in", and subtract the result from the original equation, we find

$$\Delta \psi_0 = \frac{2A_2(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}}(2\alpha_1)^{-\frac{1}{2}} f_a}{n_0 B_2}$$
(8.37)

Performing the same operations on (8.26) and keeping only first order terms results in

$$\Delta \psi_{1} = -B_{2}^{-1} \frac{n^{2}}{8} [\sin^{2}(\psi_{in} + \Delta \psi_{0}) - \sin^{2}\psi_{in}] + 2B_{2}^{-1} \eta_{0}^{-1} (2\alpha_{1})^{-\frac{1}{2}} (\alpha_{2}^{2} - \alpha_{3}^{2})^{\frac{1}{2}} [A_{21} \sin^{2} f_{a} + A_{22} \sin^{2} f_{a}]$$
(8.38)

Thus since  $f_a$  and  $\psi_{in}$  can be found for the incoming asymptote, we can then calculate  $\Delta\psi_0$ ,  $\Delta\psi_1$ , and finally  $\Delta\psi$  from (8.37), (8.38), and (8.36) respectively. Then, by (8.31),  $\Delta\Omega'$  can be determined from

$$\Delta \Omega' = \alpha_3 (\alpha_2^2 - \alpha_3^2)^{-\frac{1}{2}} n_0 [B_3 \Delta \psi + \frac{3}{32} n_0^2 n_2^{-4} (\sin 2(\psi_{in} + \Delta \psi) - \sin 2\psi_{in})] - c^2 \alpha_3 (2\alpha_1)^{-\frac{1}{2}} 2[A_3 f_a + A_{31} \sin f_a + A_{32} \sin 2f_a + A_{33} \sin 3f_a + A_{34} \sin 4f_a]$$

$$(8.39)$$

Having then determined  $\psi_{out} = \psi_{in} + \Delta \psi$  and  $\Omega'_{out} = \Omega'_{in} + \Delta \Omega'$  we can then proceed to calculate the outgoing velocity component and thus the outgoing asymptote, from (8.11), (8.12), and (8.13). Notice that equations (8.36), (8.37), (8.38), and (8.39) can be used equally well to find the incoming asymptote if given the outgoing asymptote. In this case we merely replace  $f_a$  by  $-f_a$  and  $\psi_{in}$  by  $\psi_{out}$  $-\Delta\psi_0$ . The resulting  $\Delta\psi$  and  $\Delta\Omega'$  will be such that  $\psi_{in} = \psi_{out} + \Delta\psi$  and  $\Omega'_{in} = \Omega'_{out} + \Delta\Omega'$ .

#### CHAPTER 9

### THE "PARABOLIC" TRAJECTORY

#### 9.1 Definition and Problem Formulation

In this section we consider the special case of trajectories which have  $\alpha_1 = 0$ . These trajectories are the analog of parabolic motion in the Keplerian formulation. Setting  $\alpha_1 = 0$  in (2.6) we find

$$F(\rho) = c^2 \alpha_3^2 + (\rho^2 + c^2)(\tilde{k} + 2\mu\rho)$$
(9.1)

to have  $F(\rho) = 0$  we must have  $\tilde{k} + 2\mu\rho = -c^2\alpha_3^2(\rho^2+c^2)^{-1}$ , or for  $\tilde{k} = 0$ 

$$\rho^3 + \rho c^2 + \frac{c^2 \alpha_3^2}{2\mu} = 0 \tag{9.2}$$

which will have one negative real root, which we will label  $\rho_1$ , and two imaginary roots. For  $\tilde{k} = 0$  we can see from (9.1) that the slope of  $F(\rho)$ will always be positive. Also from (9.1) it is clear that increasing  $\tilde{k}$ from zero allows  $\rho_1$  to be even more negative, while decreasing  $\tilde{k}$  from zero forces  $\rho_1$  to increase, finally becoming positive. The critical value of  $\tilde{k}$  at which this transition occurs is seen to be

$$\tilde{k}_{crit} = -\alpha_3^2 \qquad (9.3)$$

From the above information we can sketch  $F(\rho)$  as in Figure 9.1. For physically realizable motion we must have  $F(\rho) > 0$ , so that for perigee,  $\rho_1$ , to be positive  $\tilde{k}$  must be negative and greater in magnitude



FIGURE 9.1  $F(\varphi)$  Versus  $\varphi$  for  $\alpha_1=0$ 

than  $\alpha_3^2$ . Thus, as before, we can define

$$\tilde{k} \equiv -\alpha_3^2 \tag{9.4}$$

where

$$\alpha_2^2 \ge \alpha_3^2 \tag{9.5}$$

Setting  $a_1 = 0$  in (2.20) results in

$$G(n) = -\alpha_3^2 + (1-n^2)\alpha_2^2$$
(9.6)

If  $\pm n_0$  are the roots of G(n) = 0 then

$$n_0 = \frac{(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}}}{\alpha_2}$$
(9.7)

According to (9.5) both roots are real. Then, since  $G(n) = -\infty$  for  $n = \infty$  or  $n = -\infty$  we can sketch G(n) as in Figure 9.2. The motion again takes place between  $-n_0$  and  $+n_0$ .

### 9.2 The Orbital Elements

According to (3.3), (3.4), and (3.5) the orbital elements  $a_0$ ,  $e_0$ , and  $i_0$  become

 $a_0 \rightarrow \infty$  (9.8)

$$e_0 \neq 1 \tag{9.9}$$

$$i_0 \equiv \cos^{-1}(\alpha_3/\alpha_2) \tag{9.10}$$

and by (3.7)

$$p_0 = \frac{\alpha_2^2}{\mu} \tag{9.11}$$

Note that these are the same values we would obtain from setting  $\alpha_1 = -0$ 



FIGURE 9.2 G(n) Versus  $\mathcal{N}$  for  $\ll_1=0$ 

in the corresponding orbital element definitions for the bounded case. (Vinti [2] equations (3.3), (3.4), and (3.5).) Inserting (9.4) in (9.1) results in

$$F(\rho) = c^2 \alpha_3^2 + (\rho^2 + c^2)(-\alpha_2^2 + 2\mu\rho)$$
(9.12)

If we put  $F(\rho)$  in the form

$$F(\rho) = 2\mu(\rho - \rho_1)(\rho^2 + A\rho + B)$$
(9.13)

we find, upon comparing coefficients of  $\rho$  in (9.12) and (9.13)

$$\alpha_2^2 = 2\mu(\rho_1 - A) = \mu p_0$$
 (9.14)

$$c^2 = B - \rho_1 A$$
 (9.15)

$$c^{2}(\alpha_{2}^{2}-\alpha_{3}^{2}) = 2\mu\rho_{1}B$$
(9.16)

With  $k_0$  and y defined as before we then seek a series solution of the form

$$\rho_1 = \sum_{n=0}^{\infty} b_{1_n} k_0^n$$
 (9.17)

$$A = \sum_{n=0}^{\infty} b_{2n} k_0^{n}$$
(9.18)

$$B = \sum_{n=0}^{\infty} b_{3_n} k_0^n$$
 (9.19)

Inserting (9.17), (9.18), and (9.19) into (9.14), (9.15), and (9.16) and solving for the  $b_{i,j}$  we find to order  $k_0^2$ 

$$\rho_1 = \frac{p_0}{2} \left[ 1 - 4y^2 k_0 + 16y^2 k_0^2 (1 - 2y^2) \right]$$
(9.20)

$$A = -2p_0 y^2 k_0 [1 - 4k_0 (1 - 2y^2)]$$
(9.21)

$$B = p_0^2(1-y^2) k_0[1 + 4y^2k_0]$$
(9.22)

For nearly equatorial trajectories (9.13) will have three positive real roots. Note that (9.21) and (9.22) correspond exactly to the A and B equations for the bounded case (Vinti [2] equations (3.19) and (3.20)) with  $x = (1-e_0^2)^{\frac{1}{2}} = 0$ . They also correspond exactly to (3.25) and (3.26) of the present paper with  $x = (e_0^2-1) = 0$ .

Since  $a_0 \rightarrow \infty$  for "parabolic" motion we find it more convenient to choose as orbital elements  $p_0$ ,  $e_0$ , and  $i_0$ . The elements p, e, and I are then defined by

$$p \equiv 2\rho_1 \tag{9.23}$$

$$\eta_0 \equiv \sin I \tag{9.24}$$

$$e \equiv e_0 = 1 \tag{9.25}$$

Combining (9.20) with (9.23) results in

$$p/p_0 = 1 - 4y^2 k_0 + 16y^2 k_0^2 (1 - 2y^2) + \cdots$$
(9.26)

and from (9.7) and (9.10)

$$n_0 = \sin I = \frac{(\alpha_2^2 - \alpha_3^2)^{\frac{1}{2}}}{\alpha_2} = \sin i_0$$
 (9.27)

Thus the elements I and  $i_0$  are identical for this case. Equations (9.25), (9.26), and (9.27), which define the relationship between the two sets of orbital elements, can be obtained alternately from the corresponding bounded (Vinti [2]: (3.32), (3.26), and (3.40)) or unbounded (present paper: (3.39), (3.34), and (3.48)) relations by considering the limiting case  $e_0 = 1$ . Having shown that the "parabolic" orbital elements  $p_0$ ,  $e_0$ ,  $i_0$ , or p, e, I can be derived as the limiting case of either the bounded or unbounded equations, we can now proceed to obtain the values of the  $\rho$  and  $\eta$  integrals for the case  $\alpha_1 = 0$  from those previously derived for the cases  $\alpha_1 < 0$  or  $\alpha_1 > 0$ . The next two subsections are devoted to showing that the two sets of "parabolic" equations of motion so derived are identical.

### 9.3 The "Parabolic" Solution as Derived From the Unbounded Solution

In this subsection we seek to determine the "parabolic"  $\rho$  and  $\eta$  integrals, and thus the Kinetic equations, as the limiting case,  $\alpha_1 \neq 0$ , of our results for unbounded motion. From (5.45) and the definition of  $a_0$  we find

$$R_{1} = \left(\frac{a_{0}}{\mu}\right)^{\frac{1}{2}} [b_{1}H - aH + aesinhH + A_{1}f + A_{11}sinf + A_{12}sin2f] \quad (9.28)$$

However, substituting  $x^2 \equiv e_0^2 - 1 = 0$  into (3.33) we find that  $a = a_0$  so that (9.28) can be rewritten as

$$R_{1} = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left[\frac{1}{\sqrt{e^{2}-1}} \left[b_{1}H - aH + aesinhH\right]_{1} + \frac{1}{\sqrt{e^{2}-1}} \left[A_{1}f + A_{11}sinf + A_{12}sin2f\right]\right]$$
(9.29)

Consider first the term in brackets with the subscript 1. From the anomaly relation (7.4) we have

$$\sinh H = \frac{\sqrt{e^2 - 1} \sin f}{1 + \cos f}$$
(7.4)

and so

$$H = \sinh^{-1} \frac{\sqrt{e^2 - 1} \sinh}{1 + \cos f}$$
(9.30)

However, the series expansion of  $\sinh^{-1}$  is

$$\sinh^{-1}u = u - \frac{u^3}{6} + \frac{3u^5}{40} + \cdots$$
 (9.31)

so that (9.30) may be rewritten as

$$H = (e^{2}-1)^{\frac{1}{2}} \left[ \frac{\sin f}{1+\cos f} - \frac{1}{6} \frac{(e^{2}-1)\sin^{3}f}{(1+\cos f)^{3}} + \cdots \right]$$
(9.32)

If we then write the subscripted bracket term in the form

$$\left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left(e^{2}-1\right)^{-\frac{1}{2}} \left[\cdots\right]_{1} = \left(\frac{p^{3}}{\mu}\right)^{\frac{1}{2}} \left(e^{2}-1\right)^{-\frac{1}{2}} \left[\frac{b_{1}}{p}H - \frac{H}{(e^{2}-1)} + \frac{esinnH}{(e^{2}-1)}\right]$$
(9.33)

and insert into it (9.3) and (7.4) for H and sinhH, respectively, we find

$$\frac{(p_{\mu})^{\frac{1}{2}}(e^{2}-1)^{-\frac{1}{2}}[\cdots]_{1}}{(e^{2}-1)^{\frac{1}{2}}[\cdots]_{1}} = \frac{(p^{3})^{\frac{1}{2}}}{(p^{3})^{\frac{1}{2}}} \left[ \frac{b_{1}}{p} \left[ \frac{\sinh f}{1+\cosh f} - \frac{1}{6} \frac{(e^{2}-1)\sin^{3}f}{(1+\cosh f)^{3}} + \cdots \right] \right]$$

$$+ \frac{\sinh f}{(e+1)(1+\cosh f)} + \frac{1}{6} \frac{\sin^{3}f}{(1+\cosh f)^{3}} + \cdots \right]$$

$$(9.34)$$

$$= \left(\frac{p^{3}}{\mu}\right)^{\frac{1}{2}} \left[\frac{b_{1}}{p} \tan \frac{f}{2} + \frac{1}{2} \tan \frac{f}{2} + \frac{1}{6} \tan^{3} \frac{f}{2}\right]$$
(9.35)

in the limit as  $e \rightarrow 1$ . With this result we can rewrite (9.29) as

$$R_{1} = \left(\frac{p^{3}}{\mu}\right)^{\frac{1}{2}} \left[\left(\frac{b_{1}}{p} + \frac{1}{2}\right) \tan \frac{f}{2} + \frac{1}{6} \tan^{3} \frac{f}{2} + A_{1} f + A_{11} \sinh f + A_{12} \sin 2f\right]$$
(9.36)

where by the use of (5.39), (5.43), and (5.44) we have defined

$$A_{1} = \sum_{n=2}^{\infty} \left(\frac{b_{2}}{p}\right)^{n} P_{n}(\lambda) T_{n-2}(0)$$
(9.37)

$$A_{11} = \frac{3}{4p^4} \left(-2b_1 b_2^2 p + b_2^4\right)$$
(9.38)

$$A_{12}^{\prime} = \frac{3b_2^{4}}{32p^4} \tag{9.39}$$

Again using the fact that  $a = a_0$  in the limit, we can write (5.57) in the form

$$R_{2} = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \frac{1}{\sqrt{e^{2}-1}} \left[A_{2}f + \sum_{j=1}^{4} A_{2j} \sin jf\right]$$
(9.40)

or, dividing the coefficients by  $\sqrt{e^2-1}$  and taking the limit as  $e \rightarrow 1$ 

$$R_{2} = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left[A_{2}^{f} + \sum_{j=1}^{4} A_{2}^{j} \sin j f\right]$$
(9.41)

where, with the use of (5.51) and (5.53) through (5.56)

$$A_{2}^{\prime} = p^{-1} \sum_{n=0}^{\infty} \left(\frac{b_{2}}{p}\right)^{n} P_{n}(\lambda) T_{n}(0)$$
(9.42)

$$A_{21} = \frac{b_1}{p^2} + \frac{3b_1^2 - b_2^2}{p^3} - \frac{45}{8} \frac{b_1 b_2^2}{p^4} + \frac{21}{8} \frac{b_2^4}{p^5}$$
(9.43)

$$A_{22}^{\prime} = \frac{3b_1^2 - b_2^2}{8p^3} - \frac{9}{8} \frac{b_1 b_2^2}{p^4} + \frac{21}{32} \frac{b_2^4}{p^4}$$
(9.44)

$$A_{23}^{\prime} = -\frac{b_1 b_2^2}{8 p^4} + \frac{b_2^4}{8 p^5}$$
(9.45)

$$A_{24}^{-} = \frac{3b_2^{-4}}{256p^5} \tag{9.46}$$

In a similar fashion the  $R_3$  integral (5.102) becomes

$$R_{3} = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} [A_{3}f + \sum_{j=1}^{4} A_{3j} \sin j f]$$
(9.47)

where from (5.96) through (5.101)

$$A_3 = p^{-3} \sum_{m=0}^{\infty} D_m T_{m+2}(0)$$
 (9.48)

$$A_{31} = p^{-3} \left[2 + \frac{15}{4} \frac{b_1}{p} - 7\left(\frac{b_2^2}{2p^2} + \frac{c^2}{p^2}\right)\right]$$
(9.49)

$$A_{32}^{-} = p^{-3} \left[ \frac{1}{4} + \frac{3}{4} \frac{b_1}{p} - \frac{7}{4} \left( \frac{b_2^2}{2p^2} + \frac{c^2}{p^2} \right) \right]$$
(9.50)

$$A_{33} = \frac{b_1}{12p^4} - \frac{1}{3p^5} \left(\frac{b_2^2}{2} + c^2\right)$$
(9.51)

$$A_{34}^{\prime} = -\frac{1}{32p^5} \left(\frac{b_2^2}{2} + c^2\right)$$
(9.52)

In evaluating the n integrals we first note that setting  $x^2 \equiv e_0^2 - 1$ = 0 in (3.51) results in

$$n^2 = -n_0^2 / n_2^2 = 0 \tag{9.53}$$

for the "parabola." Inserting (9.53) and (9.7) into (6.43) and (6.48) results in

$$N_{1} = \frac{\alpha_{2}^{2} - \alpha_{3}^{2}}{\alpha_{2}^{3}} \left( \frac{\psi}{2} - \frac{1}{4} \sin 2\psi \right) \quad \text{exact} \quad (9.54)$$

Similarly (6.51) and (6.53) become

1

$$N_2 = \frac{\psi}{\alpha_2} \qquad \text{exact} \qquad (9.55)$$

To calculate N<sub>3</sub> we note, in addition, that from (3.50)  ${n_2}^{-2} = 0$  for the "parabola," so that (6.87) becomes

$$N_3 = \frac{\chi}{\alpha_3} \qquad \text{exact} \qquad (9.56)$$

It is interesting to notice that all the  $\eta$  integrals are exact. Substituting these integrals into the Kinetic equations (2.18) results in

$$t + \beta_{1} = \left(\frac{p^{3}}{\mu}\right)^{\frac{1}{2}} \left[ \left(\frac{b_{1}}{p} + \frac{1}{2}\right) \tan \frac{f}{2} + \frac{1}{6} \tan^{3} \frac{f}{2} + A_{1} f + \sum_{j=1}^{2} A_{1,j} \sin j f + \text{periodic terms } O(k^{3}) \right] + c^{2} \frac{(\alpha_{2}^{2} - \alpha_{3}^{2})}{\alpha_{2}^{3}} \left[ \frac{\psi}{2} - \frac{1}{4} \sin 2\psi \right]$$
(9.57)

$$\beta_2 = -\alpha_2 \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left[A_2 f + \sum_{j=1}^{\mu} A_{2j} sinjf + periodic terms O(k^3)\right] + \psi$$
(9.58)

$$\phi - \beta_3 = -c^2 \alpha_3 \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left[A_3 f + \sum_{j=1}^{4} A_{3j} \sin j f + \text{periodic terms } O(k^3)\right] + \chi$$
(9.59)

Setting  $c \rightarrow 0$  in the above Kinetic equations and comparing to the corresponding Keplerian equations provides one method of checking our solution. Thus dropping all terms of O(k) or higher from (9.57), (9.58), and (9.59) we find

$$t + \beta_1 = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left(\frac{1}{2} \tan \frac{f}{2} + \frac{1}{6} \tan \frac{3f}{2}\right)$$
(9.60)

$$\beta_2 = \psi - f = \sin^{-1} \left( \frac{\sin \theta}{\sin i} \right) - f \qquad (9.61)$$

$$\phi - \beta_3 = \chi = \sin^{-1} \left( \frac{\tan \theta}{\tan i} \right) \tag{9.62}$$

which are indeed the Keplerian equations of motion for the parabolic trajectory.

# 9.4 The "Parabolic" Solution as Derived From the Bounded Solution

In this subsection we will show that the "parabolic" solution obtained as the limiting case of Vinti's [2] bounded spheroidal solution is identical to the "parabolic" solution derived in the previous subsection. This, of course, must be the case if both the solutions for the bounded and unbounded cases are to be correct. Since we have previously shown that the orbital elements p, e, i and  $p_0$ ,  $e_0$ ,  $i_0$  have the same value in the limit of "parabolic" motion whether derived from the bounded or unbounded case, we can retain the notation found in Vinti's equations without ambiguity. Furthermore, since Vinti's variable v is defined exactly the same as f in the present paper, we may make the substitution  $v \rightarrow f$  in Vinti's equations.
From V(5.30)\* and V(3.3) the R<sub>1</sub> integral becomes

$$R_{1} = \left(\frac{a_{0}}{\mu}\right)^{\frac{1}{2}} [b_{1}E + aE - aesinE + A_{1}f + A_{11}sinf + A_{12}sin2f] \qquad (9.63)$$

Dividing V(3.26) by V(3.28) yields

$$\frac{a}{a_0} = \frac{p/p_0}{(1-e^2)/(1-e_0^2)}$$

$$= \frac{1 + 2k_0y^2(x^2-2) + k_0^2y^2(3x^4-2x^4y^2-16x^2+24x^2y^2+16-32y^2)}{1 + k_0y^2(3x^2-4) + k_0^2y^2(5x^4-2x^4y^2-20x^2+28x^2y^2+16-32y^2)}$$
(9.64)

Setting  $x^2 \equiv 1-e_0^2 = 0$  in the above relation yields

$$a = a_0$$
 (9.65)

for the "parabola." Using this fact we can rewrite (9.63) as

$$R_{1} = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} (1-e^{2})^{-\frac{1}{2}} [b_{1}E + aE - aesinE + A_{1}f + A_{11}sinf + A_{12}sin2f]$$
(9.66)

If we then solve V(8.1a) and V(8.16) for sinE we find

$$\sin E = \frac{(1-e^2)^2 \sin f}{1+e\cos f}$$
(9.67)

or, equivalently

$$E = \sin^{-1} \left[ \frac{(1 - e^2)^2 \sin f}{1 + \cos f} \right]$$
(9.68)

where  $\sin^{-1}u$  may be written as the series expansion

$$\sin^{-1}u = u + \frac{u^3}{6} + \frac{3u^5}{40} + \cdots$$
 (9.69)

If we insert (9.67) and (9.68) into (9.66), using the above series

<sup>\*</sup> Equations preceeded by a V indicate their origin in Vinti [2].

expansion for  $\sin^{-1}$ , perform the indicated division by  $(1-e^2)^{\frac{1}{2}}$ , and then take the limit as  $e \rightarrow 1$  we find that  $R_1$  reduces to

$$R_{1} = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left[\left(\frac{b_{1}}{p} + \frac{1}{2}\right) \tan \frac{f}{2} + \frac{1}{6} \tan^{3} \frac{f}{2} + A_{1} f + A_{11} \sinh f + A_{12} \sin 2f\right]$$
(9.70)

where

$$A_{1} = \sum_{n=2}^{\infty} \left(\frac{b_{2}}{p}\right)^{n} P_{n}(\lambda) R_{n-2}(0)$$
(9.71)

and  $A_{11}$  and  $A_{12}$  are identical to the coefficients derived previously and given in (9.38) and (9.39). Further investigation reveals the fact that  $R_n(0) = T_n(0)$ , so that (9.70) and (9.37) are identical. A comparison of (9.36) and (9.70) then shows the  $R_1$  derived from Vinti's equations to be the same as the  $R_1$  derived previously from the unbounded case.

From V(5.35) the R<sub>2</sub> integral may be expressed as

$$R_{2} = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left(1 - e^{2}\right)^{-\frac{1}{2}} \left[A_{2}f + \sum_{j=1}^{\mu} A_{2j} \operatorname{sinjf}\right]$$
(9.72)

which, upon dividing the coefficients by  $(1-e^2)^{\frac{1}{2}}$  and then setting  $e \rightarrow 1$ , reduces immediately to equations (9.41) through (9.46) of the previous subsection. Thus the R<sub>2</sub> integrals as obtained from the limiting cases of the two solutions are identical.

The R<sub>3</sub> may be written from V(5.60) as

$$R_{3} = \left(\frac{p}{\mu}\right)^{\frac{1}{2}} \left(1 - e^{2}\right)^{-\frac{1}{2}} \left[A_{3}f + \sum_{j=1}^{4} A_{3j} \operatorname{sinjf}\right]$$
(9.73)

The same manipulations used in reducing  $R_2$  allow us to reduce  $R_3$  to equations (9.48) through (9.52) of the previous subsection. Thus, in the limit of "parabolic" motion, the  $R_3$  integrals are identical.

In finding the limiting values of the n integrals we first note that for  $x^2 \equiv (1-e^2) = 0$  (3.42) and (3.43) become

$$q^2 \equiv (n_0/n_2)^2 = 0 = n_2^{-2}$$
 (9.74)

Using the above relation along with (9.7) in Vinti's N<sub>1</sub>, N<sub>2</sub>, and N<sub>3</sub> integrals (V(6.38) through V(6.41) and V(6.64), V(6.65), and V(6.70)) permits us to reduce them to the same n integrals obtained previously ((9.54), (9.55), and (9.56)) from the unbounded case.

We have thus shown that, for the spheroidal problem, the solutions for bounded motion proposed by Vinti [2] and the unbounded motion given in the present paper reduce to the same "parabolic" solution, as given by (9.57), (9.58), and (9.59), in the limiting case  $\alpha_1 = 0$ .

### CHAPTER 10

### SUMMARY: ALGORITHM FOR SATELLITE POSITION AND VELOCITY

In this section we summarize the results of previous chapters by presenting an algorithm for calculating the position and velocity vectors of a satellite on an unbounded trajectory using the spheroidal method of solution. We assume that the constants  $\mu$ ,  $r_e$ , and  $J_2$ , which characterize the gravitating body, are given and, in addition, the spheroidal orbital elements a, e, I,  $\beta_1$ ,  $\beta_2$ , and  $\beta_3$  are known. This case is entirely general since we have seen in section 7.5 how one could calculate these elements from a set of initial conditions. Thus with  $\mu$ ,  $r_e$ ,  $J_2$ , a, e, I,  $\beta_1$ ,  $\beta_2$ , and  $\beta_3$  known we compute once for each trajectory

$$c^2 = r_e^2 J_2$$
 (2.4)

 $n_0 = \sin I \tag{4.4}$ 

$$p = a(e^2 - 1) > 0$$
 (3.32)

$$D = (ap+c^2)(ap+c^2n_0^2) + 4a^2c^2n_0^2$$
(10.1)

$$N = (ap+c^2)(ap+c^2n_0^2) + 4a^2c^2$$
(10.2)

$$A = -2ac^{2}(1-n_{0}^{2})(ap+c^{2}n_{0}^{2})/D < 0$$
 (4.14)

 $B = c^2 \eta_0^2 N/D > 0$  (4.15)

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$$n_{\overline{2}}^2 = -\frac{c^2 D}{a p N} < 0$$
 (4.20)

,

$$b_1 = -A/2$$
 (5.5)

$$b_2 = B^2 > 0$$
 (5.6)

$$a_0 = a + A/2 = a - b_1 < a$$
 (4.5)

$$p_0 = [c^2(1-n_0^2) + a_0 N/D]/a_0$$
(4.17)

$$\alpha_2 = (p_0 \mu)^{\frac{1}{2}}$$
 (3.7)

$$\alpha_3 = \alpha_2 \cos[(1 + \frac{c^2 n_0^2}{a_0 p_0})^{\frac{1}{2}}$$
(4.18)

$$n^2 = -n_0^2 n_2^{-2} > 0 \tag{6.7}$$

$$\alpha_{2}^{2} = (\alpha_{2}^{2} - \alpha_{3}^{2})^{\frac{1}{2}} / n_{0} = \alpha_{2} \left[ 1 - \frac{c^{2} (1 - n_{0}^{2})}{a_{0} p_{0}} \right]^{\frac{1}{2}}$$
(10.3)

$$\lambda = b_1/b_2 \tag{5.7}$$

The Legendre Polynomials are found from

$$P_0(\lambda) = 1 \tag{10.4}$$

$$P_1(\lambda) = \lambda \tag{10.5}$$

and for m>1

$$P_{m}(\lambda) = [(2m-1)\lambda P_{m-1}(\lambda) - (m-1)P_{m-2}(\lambda)]/m$$
(10.6)  
$$x^{2} = e^{2} - 1$$

The polynomials  $T_{m}(x)$  are found from

$$T_0(x) = 1$$
 (10.7)

$$T_1(x) = 1$$
 (10.8)

and for m>1

$$T_{m}(x) = [(2m-1)T_{m-1}(x) + (m-1)x^{2}T_{m-2}(x)]/m$$
 (5.34)

$$A_{1} = px \sum_{n=2}^{\infty} \left(\frac{b_{2}}{p}\right)^{n} P_{n}(\lambda) T_{n-2}(x)$$
(5.39)

$$A_2 = \frac{x}{p} \sum_{n=0}^{\infty} \left(\frac{b_2}{p}\right)^n P_n(\lambda) T_n(x)$$
(5.51)

$$D_0 = 1$$
 (10.9)

$$D_1 = b_1/p$$
 (10.10)

for n>l

$$D_{n} = - \left(\frac{c}{p}\right)^{2} D_{n-2} + \left(\frac{b_{2}}{p}\right)^{n} P_{n}(\lambda)$$
 (5.94)

then

$$A_3 = \frac{x}{p_3} \sum_{m=0}^{\infty} D_m T_{m+2}(x)$$
(5.96)

$$B_1 = -B_1 = 1/2 - 3n^2/16 + 15n^4/128$$
(6.48)

$$B_2 = 1 - n^2/4 + 9n^4/64 \tag{6.53}$$

$$\gamma_{\rm m} = \frac{(2m)!}{2^{2m}(m!)^2} \sum_{n=1}^{m-1} \frac{\eta_0^{2n}(2n)!}{2^{2m}(n!)^2}$$
(6.83)

$$B_{3} = 1 - (1 - n_{2}^{-2})^{-\frac{1}{2}} - \sum_{m=2}^{\infty} \gamma_{m} n_{2}^{-\frac{1}{2}m}$$
(6.82)

$$A_{11} = (3ex/4p^3)(-2b_1b_2p^2 + b_2^4)$$
(5.34)

$$A_{12} = 3xb_2^4 e^2/32p^3$$
 (5.44)

$$A_{21} = \frac{xe}{p} \left[ \frac{b_1}{p} + \frac{3b_1^2 - b_2^2}{p^2} - \frac{9b_1b_2^2}{2p^3} (1 + \frac{e^2}{4}) + \frac{3b_2^4}{8p^4} (4 + 3e^2) \right]$$
(5.53)

$$A_{22} = \frac{xe^2}{p} \left[ \frac{3b_1^2 - b_2^2}{8p^2} - \frac{9b_1b_2^2}{8p^3} + \frac{3b_2^4}{16p^4} (3 + e^2/2) \right]$$
(5.54)

$$A_{23} = \frac{xe^3}{8p} \left[ \frac{-b_1b_2^2}{p^3} + \frac{b_2^4}{p^4} \right]$$
(5.55)

$$A_{24} = \frac{3xb_2^4e^4}{256p^5}$$
(5.56)

$$A_{31} = \frac{xe}{p^3} \left[ 2 + \frac{b_1}{p} \left( 3 + \frac{3e^2}{4} \right) - \left( \frac{b_2^2}{2p^2} + \frac{c^2}{p^2} \right) \left( 4 + 3e^2 \right) \right]$$
(5.98)

$$A_{32} = \frac{x}{p_3} \left[ \frac{e^2}{4} + \frac{3e^2b_1}{4p_1} + \left( \frac{b_2^2}{2p^2} + \frac{c^2}{p^2} \right) \left( \frac{3e^2}{2} + \frac{e^4}{4} \right) \right]$$
 (5.99)

$$A_{33} = \frac{x}{p_3} \left[ \frac{b_1 e^3}{12p} - \frac{e^3}{3p^2} \left( \frac{b_2^2}{2} + c^2 \right) \right]$$
(5.100)

$$A_{34} = -\frac{e^4x}{32p^5} \left( \frac{b^2}{2} + c^2 \right)$$
(5.101)

$$z_1 = (2\alpha_1)^{-\frac{1}{2}} = (\frac{a_0}{\mu})^{\frac{1}{2}}$$
(10.11)

Then for each time t at which the satellite's position and velocity are desired we calculate

solve for  $H_0$ :

$$t + \beta_1 = z_1 a (e \sinh H_0 - H_0)$$
 (7.11)

then

$$f_0 = 2 \tan^{-1} \left[ \left( \frac{e+1}{e-1} \right)^{\frac{1}{2}} \tanh \left( H_0 / 2 \right) \right]$$
(7.13)

$$\psi_0 = \frac{\alpha_2}{B_2} \left[ \beta_2 / \alpha_2 + z_1 A_2 f_0 \right]$$
(7.14)

$$H_{1} = \begin{bmatrix} \frac{(c^{2}n_{0}^{2}/z_{1}\alpha_{2})(-B_{1}\psi_{0} + \frac{1}{4}\sin 2\psi_{0}) - b_{1}H_{0} - A_{1}f_{0}}{a(e \cosh H_{0} - 1)} \end{bmatrix}$$
(7.22)

$$H_1 = H_1 [1 - H_1 e \sinh H_0/2(e \cosh H_0 - 1)]$$
 (7.21)

$$f_1 = 2 \tan^{-1} \left[ \left( \frac{e+1}{e-1} \right)^{\frac{1}{2}} \tanh \left( \frac{H_0 + H_1}{2} \right) \right] - f_0$$
 (7.23)

$$\psi_1 = -\frac{n^2 \sin 2\psi_0}{8B_2} + \frac{z_1 \alpha_2}{B_2} \left[ A_2 f_1 + A_{21} \sin f_0 + A_{22} \sin 2f_0 \right] \quad (7.24)$$

$$H_{2} = \left[-b_{1}H_{1} - A_{1}f_{1} - A_{11}\sin f_{0} - A_{12}\sin 2f_{0} + \frac{c^{2}n_{0}^{2}}{z_{1}\alpha_{2}^{2}}\left(-B_{1}\psi_{1}\right) + \frac{1}{2}\psi_{1}\cos 2\psi_{0} - \frac{n^{2}}{8}\sin 2\psi_{0} + \frac{n^{2}}{64}\sin^{4}\psi_{0}\right]/a(e \cosh H_{0}-1)$$
(7.29)

$$H = H_0 + H_1 + H_2$$
(10.12)

$$f_2 = 2 \tan^{-1} \left[ \left( \frac{e+1}{e-1} \right)^{\frac{1}{2}} \tanh H/2 \right] - f_0 - f_1$$
 (7.30)

$$f = f_0 + f_1 + f_2$$
(10.13)

$$\psi_{2} = B_{2}^{-1} \left( -\frac{n^{2}}{4} \psi_{1} \cos 2\psi_{0} + \frac{3n^{4}}{32} \sin 2\psi_{0} - \frac{3n^{4}}{256} \sin 4\psi_{0} \right)$$
  
+  $\alpha_{2}^{2} z_{1} B_{2}^{-1} \left( A_{2} f_{2} + A_{21} f_{1} \cos f_{0} + A_{22} 2 f_{1} \cos 2f_{0} \right)$   
+  $A_{23} \sin 3f_{0} + A_{24} \sin 4f_{0} \right)$  (7.32)

$$\psi = \psi_0 + \psi_1 + \psi_2 \tag{10.14}$$

 $\rho = a(e \cosh H - 1)$  (5.16)

$$n = n_0 \sin \psi \tag{6.4}$$

$$\Omega^{\prime} = \beta_{3} + \frac{\alpha_{3}}{\alpha_{2}^{2}} \left( B_{3}\psi + \frac{3}{32}n_{0}^{2}n_{2}^{-4}\sin 2\psi \right) - c^{2}\alpha_{3}z_{1} \left( A_{3}f + \sum_{j=1}^{4} A_{3j}\sin jf \right)$$
(7.36)

The components of the position vector are given by

$$X = (\rho^2 + c^2)^{\frac{1}{2}} [\cos\psi\cos\Omega^2 - \cos\mathrm{I}\sin\psi\sin\Omega^2]$$
 (7.47)

$$Y = (\rho^2 + c^2)^{\frac{1}{2}} [\cos I \sin \psi \cos \Omega^2 + \sin \Omega^2 \cos \psi]$$
(7.48)

$$Z = \rho n \tag{7.49}$$

The components of the velocity vector are found from

$$\dot{f} = \frac{ax}{\rho z_1} \frac{\left(\rho^2 + A\rho + B\right)^2}{\left(\rho^2 + c^2 n^2\right)^2}$$
(7.71)

$$\rho = \rho^2 efsinf/p \tag{7.69}$$

$$\dot{\psi} = \alpha_2^2 \left( 1 + n^2 \sin^2 \psi \right)^{\frac{1}{2}} / (\rho^2 + c^2 n^2)$$
(7.67)

$$\hat{\Omega} = \frac{\alpha_3}{\alpha_2^2} (B_3 + \frac{3}{16} n_0^2 n_2^{-4} \cos 2\psi) \dot{\psi} - c^2 \alpha_3 z_1 (A_3 + \sum_{j=1}^{4} jA_{3j} \cos jf) f (7.68)$$

$$X = \frac{\rho \rho}{\rho^2 + c^2} X - Y \Omega' + (\rho^2 + c^2)^2 (-\sin\psi\cos\Omega' - \cos\mathrm{Icos}\psi\sin\Omega')\psi$$
(7.53)

$$Y = \frac{\rho \rho}{\rho^2 + c^2} Y + X\Omega^2 + (\rho^2 + c^2)^{\frac{1}{2}} (-\sin\psi\sin\Omega^2 + \cos\operatorname{Icos}\psi\cos\Omega^2)\psi$$
(7.54)

$$z = \rho n + n_0 \rho \cos \psi \psi$$
 (7.55)

This completes the algorithm for determining, at any time t, the position and velocity vector of a satellite on an unbounded trajectory. The next chapter deals with a computer program which compares the results obtained from this algorithm to ordinary Keplerian hyperbolic motion.

### CHAPTER 11

# NUMERICAL COMPARISON OF THE ORBITS, WITH AND WITHOUT

OBLATENESS, FOR GIVEN INITIAL CONDITIONS

In the previous chapter we summarized the algorithm that one would use to calculate the time history of the position and velocity vectors for a satellite on an unbounded trajectory given the oblateness parameter  $J_2$  of the gravitating body and the spheroidal orbital elements, a, e, I,  $\beta_1$ ,  $\beta_2$ , and  $\beta_3$ . Using the state vector calculated for t = 0, we can then rework the problem for  $J_2 = 0$  by the application of simple conic formulae. We thus calculate the Keplerian orbital elements  $a_s$ ,  $e_s$ ,  $I_s$ ,  $\tau$ ,  $\omega$ ,  $\Omega^*$  and the time history of the trajectory the satellite would traverse if the Earth were a perfect sphere. I will refer to this latter trajectory as the Keplerian or spherical trajectory. A flow chart for the process is shown in Figure 11.1

In this manner we can compare the trajectories for an oblate and a spherical planet for the same initial conditions and determine the magnitude of the deviations as functions of the energy, perigee distance, and inclination of the trajectory. At this point let us derive a set of Keplerian relations suitable for the numerical examples to be considered.

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 $<sup>\</sup>tau$  = time of perigee passage

 $<sup>\</sup>omega$  = argument of perigee

 $<sup>\</sup>Omega$  = longitude of ascending node or, if there is only a descending node, longitude of descending node  $-180^{\circ}$ .

# FIGURE 11.1

### TRAJECTORY COMPARISON FLOW CHART



### 11.1 The Keplerian Trajectory From an Initial State Vector

In this section we assume that  $\underline{r}_0$  and  $\underline{v}_0$ , the initial position and velocity, vectors are given and should like to determine the spherical (i.e.  $J_2 = 0$ ) orbital elements  $a_s$ ,  $e_s$ ,  $I_s$ ,  $\tau$ ,  $\omega$ , and  $\Omega$  as well as the time history of the trajectory. Battin [8] has been used as a reference in the following derivations.

We can find the element  $a_s$  from the energy equation as

$$a_{s} = \left(\frac{v_{0}^{2}}{\mu} - \frac{2}{r_{0}}\right)^{-1}$$
(11.1)

which is greater than zero for hyperbolic motion. We then find the angular momentum from

$$\underline{\mathbf{h}} = \underline{\mathbf{r}}_0 \times \underline{\mathbf{v}}_0 \tag{11.2}$$

which allows us to obtain the eccentricity from

$$e_{s}^{2} = 1 + \frac{h^{2}}{\mu a_{s}}$$
 (11.3)

We then solve for the inclination by dotting a unit vector in the  $\underline{h}$  direction with a unit vector in the z direction.

$$I_{s} = \cos^{-1} \left( \frac{\underline{h}}{h} \cdot \underline{i}_{z} \right)$$
(11.4)

We then calculate the unit vector in the direction of perigee

$$\underline{\mathbf{i}}_{p} = \frac{1}{e_{s}} \left( \frac{1}{a_{s}} + \frac{1}{r_{0}} \right) \underline{\mathbf{r}}_{0} - \frac{1}{\mu e_{s}} (\underline{\mathbf{r}}_{0} \cdot \underline{\mathbf{v}}_{0}) \underline{\mathbf{v}}_{0}$$
(11.5)

and the unit vector along the line of nodes

$$\underline{\mathbf{i}}_{\mathbf{n}} = \frac{\underline{\mathbf{i}}_{\mathbf{z}} \times \underline{\mathbf{h}}}{|\underline{\mathbf{i}}_{\mathbf{z}} \times \underline{\mathbf{h}}|}$$
(11.6)

The longitude of the node and argument of perigee are then

$$\Omega = \cos^{-1}(\underline{i}_{n} \cdot \underline{i}_{x}) \tag{11.7}$$

$$\omega = \cos^{-1}(\underline{i}_{n} \cdot \underline{i}_{p}) \tag{11.8}$$

The initial value of the true anomaly is

$$\frac{\mathbf{f}_{s_0}}{2} = \frac{1}{2} \tan^{-1} \frac{\frac{\mathbf{h}}{\mathbf{r}_0} \cdot \mathbf{v}_0}{\frac{\mathbf{h}^2}{\mathbf{r}_0} - \mu}$$
(11.9)

which allows us to calculate the initial value of the hyperbolic anomaly

$$H_{s_0} = 2 \tanh^{-1} \left[ \left( \frac{e-1}{e+1} \right)^{\frac{1}{2}} \tan \frac{f_{s_0}}{2} \right]$$
(11.10)

Since the initial time is  $t_0 = 0$  we finally solve for the time of perigee passage from Kepler's equation

$$\tau = \left(\frac{a_{s}^{3}}{\mu}\right)\left(H_{s_{0}} - e_{s} \sinh H_{s_{0}}\right)$$
(11.11)

Having thus found the spherical orbital elements we then calculate the position and velocity vectors for each time t from the following set of equations. First, we obtain  $H_s$  as a solution of the Kepler equation

$$\left(\frac{\mu}{a_{s}^{3}}\right)^{\frac{1}{2}}(t-\tau) = e_{s} \sinh H_{s} - H_{s}$$
(11.12)

and then the position and velocity vectors can be found directly from Battin [8] as

$$\underline{\mathbf{r}}_{s}(t) = \left[1 - \frac{\mathbf{a}_{s}}{\mathbf{r}_{0}} \left[\cosh(\mathbf{H}_{s} - \mathbf{H}_{s0}) - 1\right]\right] \underline{\mathbf{r}}_{0} + \left[t - \frac{\sinh(\mathbf{H}_{s} - \mathbf{H}_{s0}) - (\mathbf{H}_{s} - \mathbf{H}_{s0})}{(\frac{\mu}{\mathbf{a}_{s}})^{\frac{1}{2}}}\right] \underline{\mathbf{v}}_{0}$$
(11.13)

$$\underline{\mathbf{v}}_{s}^{(t)} = -\frac{(\mu a)^{\frac{1}{2}}}{\mathbf{r}_{s}\mathbf{r}_{0}} \sinh(\mathbf{H}_{s}-\mathbf{H}_{s0})\underline{\mathbf{r}}_{0} + \left[1 - \frac{\mathbf{a}_{s}}{\mathbf{r}_{s}} \left[\cosh(\mathbf{H}_{s}-\mathbf{H}_{0s}) - 1\right]\right]\underline{\mathbf{v}}_{0}$$
(11.14)

This completes the algorithm for finding the spherical orbital elements and state vector given an initial position and velocity vector. 11.2 The Computer Program

In order to compare results derived from the spheroidal method with results of the ordinary Keplerian equations a computer program, embodying the flow chart of Figure 11.1, was written in Fortran IV computer language for use on the IBM 360 machine. The program, which is shown in Appendix E, accepts values of the oblateness parameter  $J_2$  and the spheroidal orbital elements a, e, I,  $\beta_1$ ,  $\beta_2$ , and  $\beta_3$  as input. Using the spheroidal algorithm summarized in Chapter 10 it then computes the position and velocity vectors and the spheroidal true anomaly and spheroidal hyperbolic anomaly for the desired values of time. The number of time steps required as well as the amount of the time step are specified as inputs to the program. On the basis of the initial position and velocity vectors thus calculated the program then determines the Keplerian orbital elements and the spherical position and velocity vectors for the same values of time using the algorithm derived in the previous section. Notice that the spherical algorithm is invalid for inclinations close to 0 or  $180^{\circ}$  since the orbital elements  $\omega$  and  $\Omega$  lose their meaning. The spheroidal portion of the program, however, is valid for all inclinations.

It is appropriate at this time to explain certain details of the actual numerical computation performed by the program. The physical units utilized are those of the canonical Vanguard system. In this system the unit of length is the equatorial radius of the Earth (taken to be 6378.388 kilometers) and the gravitational constant G is taken to be unity. The value of the Vanguard unit of time is found to be 806.832seconds and  $\mu$ , the product of the gravitational constant and the Earth's mass, is unity.

For the purpose of this thesis arithmetic calculation was performed in the single-precision mode, since higher numerical accuracy was unwarranted to show the effects of oblateness (to be justified in the following section). Only minor program changes are required to utilize the double-precision mode and thus obtain more accurate results.

Both the spheroidal algorithm and the spherical algorithm involved the solution of a Kepler-type equation. The iterative sequence found in statements 141 ff. and 242 ff. of the program in Appendix E was quite sufficient for my purposes. A flow chart of this routine is shown in Figure 11.2. M represents the "mean anomaly" and H the "hyperbolic anomaly."

Using the method depicted in Figure 11.2 and single-precision values for the cosh and sinh functions  $\Delta H$  was found to converge quite rapidly (within ten cycles for all cases tested) to a limiting value well below the required  $10^{-6}$ . Once  $\Delta H$  had reached this limiting value further iterations could not decrease it. Thus the program allows 20 cycles for  $\Delta H$  to become less that  $10^{-6}$ , after which it prints out a warning and proceeds with the calculations using the most recent value for H. The twenty cycle limit was never exceeded in any of the many trajectory calculations performed by the author.

The calculation of the spheroidal coefficients  $A_1$ ,  $A_2$ , and  $A_3$  involving convergent infinite series was also done by an iterative procedure. As soon as the ratio of the nth term of the series to the sum of the

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# FLOW CHART FOR SOLUTION OF KEPLER-TYPE EQUATION

### FIGURE 11.2

previous n-1 terms is less than  $10^{-7}$  we consider the calculation complete. Convergence of the series is normally so rapid that if the criterion has not been met by the 10th term, the program prints out a warning and proceeds with the calculation using the most recent value of the coefficient.

### 11,3 Results of the Computer Comparison

The following six pages are samples of computer output for several unbounded trajectories. The value of  $J_2$  used is that of the Earth and R and V are the magnitudes of the position and velocity vectors, respectively. The subscripts X, Y, and Z indicate components of the vectors along the X, Y, and Z axes. The H and F are the hyperbolic and true anomalies, respectively. An asterisk following an H or F indicates an anomaly is defined by spheroidal coordinates, otherwise the spheroidal and spherical results may be compared directly.

Since the deviations between the spheroidal and spherical trajectories are considerable, it would appear that the single-precision mode of computation is justified for the accuracy required in this analysis. One might well ask, however, just how much of the observed deviation is due to computer roundoff or truncation error in the two different schemes of computation. In order to answer this question the program was run for a number of different trajectories (including the six example trajectories of the text) with the oblateness parameter  $J_2$  set equal to zero. If all calculations were performed perfectly, i.e. no roundoff or truncation error, we would expect the spheroidal and spherical trajectories to be identical. The deviations observed in this case, which can be taken as an indication of roundoff and truncation error, in no case exceeded 3 percent of their value for the  $J_2$  or Earth and were, in fact, of the opposite sign. Thus the deviation of the spheroidal trajectory

GIVEN	J2 = 0.00108	3228	
	A=1.1000	E=2.0000	I=0.3490
8E	TA1=0.0000	BETA2=0.5240	BETA3=0.5240

SPHEROIDAL SOLUTION

TIME	RX	RY	RZ	R	H*
	VX	VY	٧Z	V	F*
0.0	0.566089	0.924758	0.188184	1.100475	-0.000003
	-1.387759	0.749889	0.489112	1.651495	-0.000005
3.0	-3.395325	1.513356	1.094563	3.875118	1.456193
	-1.173351	0.019983	0.219765	1.193920	1.645056
6.0	-6.738613	1.509605	1.701618	7.112193	1.991857
	-1.074125	-0.012813	0.191375	1.091115	1.842113
9.0	-9.895065	1.458208	2.259665	10.254010	2.324736
-	-1.034828	-0.020096	0.181930	1.050890	1.916740
12.0	-12.964940	1.393302	2.797706	13.336350	2.568580
	-1.013591	-0.022801	0.177214	1.029218	1.956570

SPHERICAL SOLUTION

THE SPHERICAL ELEMENTS ARE

-

AS= 0.10988500E 01ES= 0.20014740E 01 IS= 0.34903580E 00 DMGA= 0.52437630E 00 W= 0.52368600E 00TAU= 0.47857000E-04

TIME	R X VX	RY VY	RZ VZ	R V	H F
0.0	0.566089	0.924758	0.188184	1.100475	-0.000041
	-1.387759	0.749889	0.489112	1.651495	-0.000072
3.0	-3.395430	1.514508	1.095820	3.876016	1.456511
	-1.173496	0.020446	0.220269	1.194164	1.644723
6.0	-6.739287	1.512132	1.704369	7.114026	1.992273
	-1.074340	-0.012361	0.191866	1.091407	1.841753
9.0	-9.896434	1.462075	2.263873	10.256800	2.325204
	-1.035069	-0.019653	0.182413	1.051203	1.916367
12.0	-12.967060	1.398487	2,803353	13.340140	2.569081
	-1.013847	-0.022364	0.177692	1.029543	1.956187

-----

GIVEN	J2= 0.00108	3228	
	A=1.1000	E=2.0000	I=0.7850
BE	TA1=0.0000	BETA2=0.5240	BETA3=0.5240

-----

SPHEROIDAL SOLUTION

------

TIME	RX	RY	RZ	R	H*
	VX	VY	VZ	V	F*
0.0	0.630098	0.814009	0.388986	1.100429	-0.000012
	-1.221494	0.462048	1.010767	1.651418	-0.000020
3.0	-3.022916	0.869859	2.262918	3.874980	1.456170
	-1.098582	-0.109111	0.454493	1.193880	1.645044
6.0	-6.159676	0.509516	3.518383	7.111976	1.991831
	-1.009013	-0.125223	0.395792	1.091072	1.842107
9.0	-9.126260	0.130345	4.672523	10.253680	2.324707
	-0.972926	-0.126955	0.376263	1.050845	1.916736
12.0	-12.013070	-0.250594	5.785276	13.335890	2.568548
	-0.953292	-0.126889	0.366510	1.029172	1.956566

SPHERICAL SOLUTION

-----

THE :	SPHERICAL EL	EMENTS ARE			
AS=	= 0.1099250	0E 01ES=	0.20010660E	01 IS= 0.7	8505620E 00
OMGA=	= 0.5242819	0E 00 W=	0.52398870E	00TAU= 0.2	0632300E-03
TIME	RX	RY	RZ	R	н
	VX	٧Y	٧Z	V	F
0.0	0.630098	0.814009	0.388986	1.100429	-0.000179
	-1.221494	0.462048	1.010767	1.651418	-0.000310
3.0	-3.022852	0.869202	2.264124	3.875486	1.456303
	-1.098558	-0.109358	0.454950	1.194055	1.644755
6.0	-6,159600	0.508173	3,520961	7.113091	1.992039
	-1.009025	-0.125444	0.396245	1.091272	1.841820
9.0	-9,126246	0.128342	4.676439	10.255430	2.324953
	-0.972956	-0.127169	0.376709	1.051059	1.916447
12.0	-12.013170	-0.253214	5,790545	13,338310	2.568818
12.00	-0.953333	-0.127097	0.366954	1.029394	1.956275

GIVEN	J2 = 0.00108	3228	
	A=1.1000	E=2.0000	I=1.2220
BE	TA1=0.0000	BETA2=0.5240	BETA3=0.5240

SPHEROIDAL SOLUTION

TIME	RX	RY	RZ	R	H*
	Vx	VY	٧Z	V	F*
0.0	0.730835	0.639702	0.517206	1.100382	-0.000021
	-0.959983	0.009388	1.343605	1.651341	-0.000036
3.0	-2.436705	-0.143623	3.009354	3.874837	1.456146
	-0.980796	-0.312648	0.604602	1.193839	1.645032
6.0	-5.248076	-1.066208	4.679511	7.111744	1.991803
	-0.906431	-0.302474	0•526534	1.091029	1.842099
9.0	-7.915515	-1.962250	6.214892	10.253320	2.324676
	-0.875401	-0.295460	0.500555	1.050798	1.916729
12.0	-10.513910	-2.841522	7.695239	13.335410	2,568515
	-0.858291	-0.291026	0•487581	1.029122	1,956561

SPHERICAL SOLUTION

THE :	SPHERICAL EL	EMENTS ARE			
AS=	= 0.1099651	.0E 01ES=	0.20006610E	01 IS = 0.1	L2220350E 01
OMGA:	= 0.5241361	0E 00 W=	0.52429810E	0.1 = UATO0	36519970E-03
TIME	RX	RY	RZ	R	н
	VX	VY	٧Z	V	F
0.0	0.730835	0.639702	0.517206	1.100382	-0.000316
	-0.959983	0.009388	1.343605	1.651341	-0.000548
3.0	-2.437115	-0.144968	3.009115	3.874960	1.456094
	-0.980871	-0.313140	0.604440	1.193947	1.644787
6.0	-5.248691	-1.068955	4.678831	7.112162	1.991803
	-0.906495	-0.302927	0.526393	1.091140	1.841887
9.0	-7,916330	-1.966333	6,213802	10.254070	2.324700
	-0.875468	-0.295898	0.500424	1.050915	1.916527
12.0	-10-514920	-2-846901	7,693762	13,336500	2,568555
1500	-0.858361	-0.291456	0.487456	1.029243	1.956363

GIVEN	J2= 0.0010	8228	
	A=1.0500	E=2.0000	I=0.7850
BE	TA1=0.0000	BETA2=0.5240	BETA3=0.5240

SPHEROIDAL SOLUTION

TIME	RX	RY	RZ	R	H*
	VX	٧Y	VZ	V	F*
0.0	0.601483	0,777045	0.371301	1.050449	-0.000013
	-1.250238	0.472894	1.034563	1.690279	-0.000022
3.0	-3.111749	0.807484	2.253247	3.925828	1.507944
	-1.113500	-0.114662	0•457108	1.209121	1.669758
6.0	-6.295903	0.434515	3.521371	7.226840	2.048168
	-1.025612	-0.128701	0.401046	1.108728	1.856736
9.0	-9.313935	0.045717	4.692794	10.429460	2.383293
	-0.990537	-0.129982	0.382412	1.069718	1.927282
12.0	-12.254580	-0,344045	5.824722	13.572780	2.628592
	-0.971516	-0.129762	0.373100	1.048754	1.964874

SPHERICAL SOLUTION

AS=	0.1049210	0E 01ES=	0.20011770E	01 IS= 0.	78506150E 00
OMGA=	0.5243093	0E 00 W=	0.52399180E	00TAU= 0.	21146880E-03
TIME	RX	RY	RZ	R	н
	٧X	VY	٧Z	V	F
0.0	0.601483	0.777045	0.371301	1.050449	-0.000197
	-1.250238	0.472894	1.034563	1.690279	-0.000340
3.0	-3.111678	0.806755	2.254622	3.926412	1.508100
	-1.113479	-0.114930	0.457627	1.209324	1.669440
6.0	-6.295843	0.433022	3.524283	7.228118	2.048406
	-1.025631	-0.128944	0.401555	1.108959	1.856420
9.0	-9.313970	0.043499	4.697219	10.431470	2.383573
	-0.990576	-0.130217	0.382916	1.069963	1.926964
12.0 -	12.254740	-0.346939	5.830664	13.575550	2.628898
	-0.971567	-0.129991	0.373602	1.049007	1.964554

	 	مبرو متجد فتنت بجور فتتت بباب

GIVEN	J2= 0.00108		
	A=2.2000	E=1.5000	I=0.7850
BE	TA1=0.0000	BETA2=0.5240	BETA3=0•5240

SPHEROIDAL SOLUTION

		ومحاويري معادلتها والمروا والم	ى الله حاد بليه الله عن خليا عن أمان عن خلك من الله عن الله عن الله عن الله عن الله عن الله عن الله ا		
TIME	RX	RY	R Z	R	H*
	VX	VY	V Z	V	F*
0.0	0.630104	0.814000	0.388996	1.100428	-0.000009
	-1.115030	0.421767	0.922701	1.507500	-0.000020
6.0	-5.343512	-0.025309	2.647197	5.963336	1.555257
	-0.831162	-0.223529	0.221752	0.888802	1.938237
12.0	-10.029419	-1.350449	3.841183	10.824390	2.049596
	-0.746901	-0.217564	0.184822	0.799597	2.091274
18.0	-14.399210	-2.638868	4.909046	15.440190	2.360538
	-0.713591	-0.212266	0.172768	0.764276	2.150681
24.0	-18.621550	-3.901099	5.925914	19.927270	2.590429
	-0.695401	-0.208695	0.166772	0.744949	2.182991

SPHERICAL SOLUTION

THE S	PHERICAL EL	EMENTS ARE	-		
A S=	0.2197410	0E 01ES=	0.15007840E	01 IS = 0.7	78507830E 00
OMGA=	0.5242788	0E 00 W=	0.52402680E	00TAU= 0.3	24921790E-03
TIME	RX	RY	RZ	R	н
	VX	VY	٧Z	V	F
0.0	0.630104	0.814000	0.388996	1.100428	-0.000153
	-1.115030	0.421767	0.922701	1.507500	-0.000341
6.0	-5.343531	-0.026653	2.650151	5.964672	1.555812
	-0.831221	-0.223736	0.222274	0.889040	1.937881
12.0	-10.029990	-1.352983	3.847201	10.827380	2.050305
	-0.747020	-0.217755	0.185325	0.799876	2.090891
18.0	-14.400590	-2.642560	4.918029	15.444970	2.361329
	-0.713737	-0.212454	0.173260	0.764576	2.150282
24.0	-18.623870	-3.905912	5.937845	19.933940	2.591276
	-0.695562	-0.208882	0.167259	0.745261	2.182581

GIVEN	J2 = 0.00100	8228	
	A=0.5500	E=3.0000	I=0.7850
BE	TA1=0.0000	BETA2=0.5240	BETA3=0.5240

SPHEROIDAL SOLUTION

			وی اللہ اللہ کہ ایک ایک کہ ایک کے ایک کی کہ ایک کے ایک کی ایک کے ایک کی کار ایک کے ایک کری ایک کری کے ایک کری ا		
TIME	RX VX	RY VY	R Z VZ	R V	H* F*
0.0	0.630090	0.814021	0.388974	1.100429	-0.000014
	-1.410536	0.533570	1.167149	1.906972	-0.000020
3.0	-3.596646	1.244234	2.873891	4.768986	1.838666
	-1.321800	0.044549	0.699152	1.495978	1.596584
6.0	-7.463285	1.350074	4.897921	9.028451	2.444382
	-1.266719	0.030250	0.659249	1.428320	1.742521
9.0	-11.228040	1.435085	6.853011	13.232240	2.812149
	-1.245694	0.027011	0.645939	1.403466	1.795166
12.0	-14.946950	1.513955	8.779881	17.400840	3.077891
	-1.234573	0.025737	0.639280	1.390507	1.822491

SPHERICAL SOLUTION 

AS=	0.5497317	CE OOES=	0.30017540E	01 IS= 0.7	8502850E 00
OMGA=	0.5242881	0E 00 W=	0.52396020E	00TAU= 0.1	.6015890E-03
TIME	RX	RY	RZ	R	н
	VX	¥٧	٧Z	V	F
0.0	0.630090	0.814021	0.388974	1.100429	-0.000196
	-1.410536	0.533570	1.167149	1.906972	-0.000278
3.0	-3.596594	1.243654	2.874928	4.769419	1.838610
	-1.321776	0.044329	0.699535	1.496130	1.596347
6.0	-7.463190	1.348841	4.900095	9.029368	2.444357
	-1.266719	0.030039	0.659629	1.428483	1.742301
9.0	-11.227930	1.433243	6.856337	13.233670	2.812138
	-1.245693	0.026806	0.646319	1.403637	1.794950
12.0	-14.946850	1.511510	8.784347	17.402800	3.077888
	-1.234576	0.025535	0.639658	1.390679	1.822278

from the Keplerian trajectory as calculated by the program is conservative and can be assumed to be accurate to about 3 parts in 100. For more critical investigations higher accuracy can be obtained, of course, by using higher precision computation.

Let us now turn our attention to the magnitude of the deviation caused by the oblateness as a function of the orbital geometry. Since we have assumed the Earth to be axially symmetric we expect the amount of deviation caused by  $J_2$  to depend most heavily on the inclination, energy, and  $\rho$ -perigee distance of the trajectory. The closer the inclination to 0 or 180° the larger should be the effect of the oblateness. Low energy trajectories, since they spend more time close to the oblate planet, should be affected more than high energy trajectories. Similarly, a trajectory with a low  $\rho$ -perigee (recall ( $\rho_1 \equiv a(e-1)$ ), should be affected more than a trajectory which does not pass so close to the planet (other factors being equal). To test these contentions the twelve trajectories shown in Table 11.1 (six of which were shown earlier as examples) were used as input to the computer program. For all twelve cases  $\beta_1$ ,  $\beta_2$ , and  $\beta_3$  were taken to be 0, 0.542, and 0.542 respectively. Figures 11.3 through 11.6 show the position and velocity deviations from the spherical trajectory as functions of time for these twelve cases. Position deviation was calculated as r spherical r<sub>spheroidal</sub> and velocity deviation as v<sub>spherical</sub> - v<sub>spheroidal</sub>. Note that the velocity deviation curves approach an asymptote as the satellite approaches asymptotic motion.

We first note that within each of the four trajectory classifications increasing the inclination decreases the amount of the deviations. Comparing trajectory 1A to 3A, 1B to 3B, and 1C to 3C it is clear that for the same inclination and  $\rho$ -perigee decreasing the energy of the orbit

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# TABLE 11.1

# TRAJECTORIES USED TO COMPARE THE EFFECTS OF J2

Number	a	е	I	Classification
lA	1.1	2.0	0.349	
1B	89	17	0.785	"standard" trajectory
10	17	11	1.222	
2A	1.05	2.0	0.349	
2B	ŦŦ	**	0.785	lower p-perigee, but higher energy
2 <b>C</b>	11	11	1.222	
3A	2.2	1.5	0.349	
3B	**	11	0.785	lower energy, same $\rho$ -perigee
3C	**	11	1.222	
ЦA	.55	3.0	0.349	
$_{4\mathrm{B}}$	**	11	0.785	higher energy, same $\rho$ -perigee
4C	11	11	1.222	
	1	l	1	1



FIGURE 11.3 Position Deviation from a



FIGURE 11.4 Position Deviation from a



FIGURE 11.5 Velocity Deviation from a



FIGURE 11.6 Velocity Deviation from a

increases the deviations. Conversely comparing 1A to 4A, 1B to 4B, and 1C to 4C, we find that the higher energy orbit has smaller deviations. To determine the effect of  $\rho$ -perigee distance on the amount of deviation we compare 1A to 2A, 1B to 2B, and 1C to 2C. Note that even though the class 2 trajectories have a slightly higher energy, their lower  $\rho$ -perigee distances cause them to have higher deviations than the corresponding "standard" trajectories. We have thus numerically confirmed the follow-ing three points

- 1. Increasing the inclination (toward 90 degrees) decreases the effect of  $J_2$ .
- 2. Increasing the energy of the trajectory decreases the effect of  ${\rm J}_2.$
- 3. Increasing the  $\rho$ -perigee distance decreases the effect of J<sub>2</sub>.

Several trajectories with perigees well within the Earth were put on the computer to test the convergence of the involved series. According to the investigation conducted at the end of Chapter 3 we expect difficulty with the series as  $\rho$ -perigee,  $\rho_1$ , approaches c (c  $\approx 0.0325$  for Earth). Indeed, when  $\rho_1$  was decreased to 0.1 the coefficients  $A_1$  and  $A_3$ failed to converge rapidly enough to satisfy the criterion of the program. As expected, the effect of  $J_2$  on these low-perigee trajectories was quite marked. For  $\rho_1 = 0.3$  (where all the series still converged) differences between the spherical and spheroidal results in the second significant figure were quite common.

### CHAPTER 12

### CONCLUSION

# 12.1 Applications and Advantages of the Spheroidal Solution for Unbounded Orbits

We have seen that the spheroidal method provides a means of calculating accurately the trajectory of an unbounded satellite for cases where the oblateness of the gravitating body is the most important force, other than the normal inverse-square force, acting on the satellite. In cases where forces arising from atmospheric drag, electromagnetic fields, or other bodies must be accounted for, the spheroidal method yields an accurate reference orbit upon which perturbation techniques may be used. Actual computation with the spheroidal method is rapid and no difficulties are encountered with poles or inclinations.

The scope of problems to which the spheroidal method may be applied is, however, limited by the convergence of the series involved. For trajectories whose extensions pass too close to the center of the Earth, i.e. within the small limiting surface derived in Chapter 3, we cannot be certain that the series used in the solution will converge. Because of the rather small size of this zone and the physical rarity of unbounded trajectories whose extensions might pass through it, the applicability of the spheroidal method is not significantly limited.

Cases in which the spheroidal solution for unbounded orbits could be fruitfully applied are quite numerous. Some examples are listed below.

- 1. Calculating escape trajectories for orbiting space vehicles.
- 2. Determining the paths of incoming meteors.
- 3. Finding the required incoming asymptote to achieve a desired outgoing asymptote (or vice-versa) on a swingby of an oblate planet.
- 4. Calculating incoming trajectories to an oblate destination planet.

#### 12.2 Areas for Future Research

There are several areas of spheroidal theory toward which future research effort should be devoted. One of these is the comparison of the effects of  $J_2$  predicted by the present solution for unbounded motion to effects predicted by other methods of analysis. Hori [9] has developed a solution using the Von Ziepel approach which includes the first order perturbation of the oblateness of the Earth on a satellite in hyperbolic motion. Sauer [10] uses the variation of orbital elements approach to obtain expressions for the perturbation of each orbital element in terms of the values of other elements and  $J_2$ . The differences in the forms of the final results as obtained by each of the three methods make analytical comparisons between them difficult. For this reason the application of the three methods to a set of numerical data is perhaps the easiest way to compare them.

The solution for unbounded orbits presented in the present paper is for a gravitational potential which includes all of the second zonal harmonic and more than half of the fourth zonal harmonic. Vinti [11, 12], however, has developed a form for the potential in spheroidal coordinates which allows for the inclusion of the third zonal harmonic  $J_3$  as well and has extended his spheroidal solution for bounded orbits accordingly. A similar extension for the present unbounded case would be valuable to spheroidal theory. In addition to the research indicated above some effort should be applied toward combining Vinti's spheroidal solution for bounded orbits [2] with the present solution for unbounded orbits. The determination of such a universally applicable solution should be facilitated by the many similarities of the two cases and the work done in Chapter 9. Here it was shown that solutions for both the unbounded and bounded cases reduced to the same "parabolic" trajectory.

## APPENDIX A

SERIES SOLUTION FOR A, B,  $\rho_1 + \rho_2, \; \rho_1 \rho_2$ 

From equations 3.12 through 3.18 we have

$$\rho_1 + \rho_2 - A = -2a_0 \tag{A.1}$$

$$B + \rho_1 \rho_2 - (\rho_1 + \rho_2) A = c^2 - a_0 p_0 = k_0 p_0^2 - a_0 p_0$$
(A.2)

$$(\rho_1 + \rho_2)B - \rho_1 \rho_2 A = -2a_0 c^2 = -2a_0 p_0^2 k_0$$
 (A.3)

$$\rho_1 \rho_2 B = -a_0 p_0 c^2 \sin^2 i_0 = -a_0 p_0^3 k_0 (1 - y^2)$$
(A.4)

We then assume series solutions in the form of (3.19) through (3.22)

$$\rho_1 + \rho_2 = \sum_{n=0}^{\infty} b_{1n} k_0^n$$
(3.19)

$$\rho_1 \rho_2 = \sum_{n=0}^{\infty} b_{2n} k_0^n$$
(3.20)

$$A = \sum_{n=0}^{\infty} b_{3_n} k_0^n$$
 (3.21)

$$B = \sum_{n=0}^{\infty} b_{4n} k_{0}^{n}$$
(3.22)

Inserting (3.19) through (3.22) into (A.1) through (A.4) and equating coefficients of like powers of  $k_0$  we find

$$b_{3_0} = b_{1_0} + 2a_0$$

$$b_{1n} = b_{3n} \quad \text{for n>0}$$

$$b_{20}b_{40} = 0$$

$$b_{21}b_{40} + b_{20}b_{4} = -a_{0}p_{0}^{3}(1-y^{2})$$

$$(b_{2}b_{4})_{n} = 0 \quad \text{for n>1} \quad (A.5)$$

$$b_{20} - b_{10}(b_{10}-2a_{0}) = -a_{0}p_{0}$$

$$b_{41} + b_{21} - b_{10}b_{31} - b_{11}b_{30} = p_{0}^{2}$$

$$b_{4n} + b_{2n} - (b_{1}b_{3})_{n} = 0$$

$$(b_{1}b_{4})_{n} - (b_{2}b_{3})_{n} = 0 \quad \text{for n>1}$$

$$b_{10}b_{40} - b_{20}b_{30} = 0$$

$$b_{10}b_{41} + b_{11}b_{40} - b_{20}b_{31} - b_{21}b_{30} = -2a_{0}p_{0}^{2}$$

Since for the Keplerian case (c=0) we know A=B=0, we choose  $b_{3_0}=b_{4_0}=0$  in the present case. Solution of the equations (A.5) is then straight forward and yields (in the order in which they may be determined)

$$b_{3_{0}} = b_{4_{0}} = 0$$
  

$$b_{1_{0}} = -2a_{0}$$
  

$$b_{2_{0}} = -a_{0}p_{0}$$
  

$$b_{41} = p_{0}^{2}(1-y^{2})$$
  

$$b_{31} = -2p_{0}y^{2}$$
  

$$b_{21} = a_{0}p_{0}y^{2}(4+x^{2})$$

(A.6)
$$b_{11} = -2p_0y^2$$

$$b_{42} = x^2(1-y^2)(4+x^2) a_0p_0y^2$$

$$b_{32} = 2p_0(2x^2y^2-3x^2y^4-8y^4+4y^2)$$

$$b_{12} = b_{32}$$

$$b_{22} = -4a_0p_0(3x^2y^2-5x^2y^4-8y^4+4y^2+\frac{1}{4}x^4y^2-\frac{1}{4}x^4y^4)$$

Equations (3.23) through (3.26) of the text then follow.

# APPENDIX B

# RANGE OF VALIDITY OF LEGENDRE EXPANSION

According to Hobson [4] we may use

$$(1 - 2\lambda h + h^2)^{-\frac{1}{2}} = \sum_{h=0}^{\infty} h^2 Pn(\lambda)$$
 (B.1)

as long as  $h \leq 1$  and  $\lambda \leq 1$ , or for  $\lambda > 1$  if

$$h < \lambda - (\lambda^2 - 1)^{\frac{1}{2}}$$
(B.2)

By the definitions of  $b_1$  and  $b_2$  and equations (4.22) and (4.23) we see that to first order

$$b_1 \approx kp \cos^2 I$$
 (B.3)  
 $b_2 \approx k^2 psinI$  (B.4)

<u>Case 1</u>  $\lambda \leq 1$ 

.

To have  $\lambda \ \leq \ l$  we must have

$$\frac{b_1}{b_2} \approx k^{\frac{1}{2}} \cos^2 I \csc I < 1$$

or equivalently

$$\tan^2 I + \tan^4 I > k$$

$$2\tan^2 I > (1+4k)^{\frac{1}{2}} - 1$$

to order k this becomes

$$\tan^{2}I > k$$

from Vinti [2] this occurs provided

$$I_{c} < I < 180^{\circ} - I_{c}$$
 (B.5)

where

$$I_{c} = 1^{\circ} 54'$$
 (B.6)

In this case we require

$$h = \frac{b_2}{\rho} \approx \frac{k^2 p |sinI|}{\rho} < 1$$

this will occur at all points along the trajectory provided it occurs at  $\rho$ -perigee, thus we ask

$$\frac{\frac{1}{k^2 p |\sin I|}}{\rho_1} < 1$$

or

$$\rho_1 > k^{\frac{1}{2}} |sinI|$$

or

$$a(e-1) > k^{\frac{1}{2}} a(e-1)(e+1) |sinI|$$

or

or

$$\frac{c}{p}$$
 (e+1)|sinI| <1

or

$$\rho_1 > c|\sin I| \tag{B.7}$$

Case 2  $\lambda > 1$ 

In this region we require

$$h < \lambda - (\lambda^2 - 1)^{\frac{1}{2}}$$
 (B.2)

but

$$\frac{b_1}{\rho} = \frac{b_1}{b_2} \frac{b_2}{\rho} = \lambda h$$

so that (B.2) is satisfied if and only if

$$\frac{b_1}{\rho} < \lambda^2 - \lambda (\lambda^2 - 1)^{\frac{1}{2}} = g(\lambda)$$
(B.8)

but Vinti [3] shows that for  $\lambda \ge 1$ 

$$\frac{1}{2} < g(\lambda) \le 1 \tag{B.9}$$

so the condition

$$\frac{b_1}{\rho} < \frac{1}{2} \tag{B.10}$$

is sufficient to satisfy (B.2). The above equation will be satisfied at all points in the trajectory provided it is satisfied at  $\rho$ -perigee. Thus we require

$$\frac{b_1}{\rho_1} < \frac{1}{2} \tag{B.11}$$

from (4.14)

$$b_{1} = \frac{ac^{2}(1-n_{0}^{2})(ap+c^{2}n_{0}^{2})}{(ap+c^{2})(ap+c^{2}n_{0}^{2}) + 4a^{2}c^{2}n_{0}^{2}}$$
(B.12)

so that

$$\frac{b_1}{\rho_1} < \frac{ac^2(1-n_0^2)(ap+c^2n_0^2)}{\rho_1(ap+c^2)(ap+c^2n_0^2)} = \frac{ac^2\cos^2 I}{\rho_1(ap+c^2)}$$
(B.13)

so it will be sufficient to have

$$\frac{2ac^2\cos^2 I}{\rho_1} < (ap+c^2)$$
(B.14)

or

$$\frac{2c^2\cos^2 I}{p\rho_1} - \frac{c^2}{ap} < 1$$

or

$$\frac{2c^2\cos^2 I - c^2(e-1)}{p\rho_1} < 1$$

or

$$\rho_1^2(e+1) > 2c^2 \cos^2 I - c^2(e-1)$$
 (B.15)

There will be no trouble satisfying this for  $e \ge 3$ . The worst case occurs for the "parabola" where e = 1. Here (B.15) becomes

$$\rho_1 > c |cosI|$$
, for  $e = 1$  (B.16)

Conditions (B.7) and (B.16) are, at worst, no more restrictive than the limitations discussed at the end of Chapter 3. Thus for all trajectories whose extensions do not pass within the surface of Figure 3.1 we may certainly replace  $(1-2\lambda h+h^2)^{-\frac{1}{2}}$  by the Legendre Polynomial series.

## APPENDIX C

# INVESTIGATION OF THE CONVERGENCE OF S1

We should like to investigate the convergence of the series involved in the evaluation of  $R_{\rm l}$ 

$$S_{1} = \left(\frac{b_{2}}{p}\right)^{2} \sum_{m=0}^{\infty} \left(\frac{b_{2}}{p}\right)^{m} P_{m+2}(\lambda) \int_{0}^{f} (1 + cosf)^{m} df$$
(5.24)

clearly since cosf never exceeds 1 we can say

$$|\mathbf{S}_{1}| \leq \left(\frac{\mathbf{b}_{2}}{\mathbf{p}}\right)^{2} \sum_{\mathbf{m}=0}^{\infty} \left(\frac{\mathbf{b}_{2}}{\mathbf{p}}\right)^{\mathbf{m}} \mathbf{P}_{\mathbf{m}+2}(\lambda) \int_{0}^{\mathbf{f}} (\mathbf{l}+\mathbf{e})^{\mathbf{m}} d\mathbf{f}$$

$$\leq \left(\frac{\mathbf{b}_{2}}{\mathbf{p}}\right)^{2} \sum_{\mathbf{m}=0}^{\infty} \left(\frac{\mathbf{b}_{2}}{\mathbf{p}}\right)^{\mathbf{m}} \mathbf{P}_{\mathbf{m}+2}(\lambda) (\mathbf{l}+\mathbf{e})^{\mathbf{m}} \mathbf{f} \qquad (C.1)$$

<u>Case 1</u>:  $\lambda \leq 1$ 

For this case

$$|P_n(\lambda)| \leq 1 \tag{C.2}$$

so that

$$|\mathbf{S}_1| \leq \left(\frac{\mathbf{b}_2}{\mathbf{p}}\right)^2 \mathbf{f} \sum_{m=0}^{\infty} \left[\frac{\mathbf{b} \ (\mathbf{e+1})}{\mathbf{p}}\right]^m \tag{C.3}$$

If the ratio

$$r_1 = \frac{b_2(e+1)}{p} < 1$$
 (C.4)

then the summation of (C.3) can be considered an infinite geometric progression with first term of 1 and a ratio  $r_1$ . In this case we would have

$$\sum_{m=0}^{\infty} \left[\frac{b_2(1+e)}{p}\right]^m = \frac{1}{1 - \frac{b_2(e+1)}{p}}$$
(C.5)

and so

$$|\mathbf{s}_1| \leq \frac{\left(\frac{\mathbf{b}_2}{\mathbf{p}}\right)^2 \mathbf{f}}{1 - \frac{\mathbf{b}_2(\mathbf{e}+1)}{\mathbf{p}}} \tag{C.6}$$

Consequently we should like to know the conditions under which (C.4) is true. Substituting  $b_2 \approx k^2$  psinI into (C.4) we are thus requiring

$$\left|\frac{k^2 p \sin I (e+1)}{p}\right| < 1$$

or

$$\frac{c|\sin I| (e+1)}{\rho_1(e+1)} < 1$$

$$\rho_1 > c|\sin I| \qquad (C.7)$$

Case 2:  $\lambda > 1$ 

According to Vinti [3] we can write for this case

$$P_{n}(\lambda) = \frac{1}{\pi} \int_{0}^{\pi} \left[\lambda + (\lambda^{2} - 1)^{\frac{1}{2}} \cos x\right]^{n} dx$$
 (C.8)

where x is a dummy variable. Then

$$\left(\frac{b_2}{p}\right)^n P_n(\lambda) = \frac{1}{\pi} \int_0^{\pi} [b_1 p^{-1} + p^{-1} (b_1^2 - b_2^2)^{\frac{1}{2}} \cos x]^n dx$$
 (C.9)

so that

$$\left| \left(\frac{b_2}{p}\right)^n P_n(\lambda) \right| \leq \left[ \frac{b_1}{p} + \frac{b_1}{p} \left( 1 - \lambda^{-2} \right)^{\frac{1}{2}} \right]^n \leq \left(\frac{2b_1}{p}\right)^n$$
(C.10)

since we are now considering  $\lambda > 1$ . Thus S<sub>1</sub> becomes

$$|\mathbf{S}_1| \leq \sum_{n=2}^{\infty} \left(\frac{2\mathbf{b}_1}{p}\right)^n \int_0^f (1 + \mathbf{cosf})^{n-2} df$$

again since cosf cannot exceed 1

$$|S_1| \leq f \left(\frac{2b_1}{p}\right)^2 \sum_{m=0}^{\infty} \left[\frac{2b_1(e+1)}{p}\right]^m$$
 (C.11)

If we now define the ratio

$$\mathbf{r}_2 \equiv \frac{2\mathbf{b}_1(\mathbf{e}+1)}{\mathbf{p}} \tag{C.12}$$

then the summation of (C.11) can be considered an infinite geometric progression of sum

$$\sum_{m=0}^{\infty} r_2^m = \frac{1}{1 - r_2} = \frac{1}{1 - \frac{2b_1(e+1)}{p}}$$
(C.13)

as long as we require that

$$r_2 = \frac{2b_1(1+e)}{p} = \frac{2b_1}{\rho_1} < 1$$
 (C.14)

or

$$\frac{b_1}{\rho_1} < \frac{1}{2}$$
 (C.15)

but this is the same condition we were required to satisfy in order to replace  $(1+A_{\rho}^{-1}+B_{\rho}^{-2})^{-\frac{1}{2}}$  by the Legendre series  $\sum_{n=0}^{\infty} h^{n} P_{n}(\lambda)$ . In Appendix B we saw that this condition reduced to

$$\rho_1^2(e+1) > 2c^2 \cos^2 I - c^2(e-1)$$
 (C.16)

so that for  $e \geq 3$ , the series always converges.

Thus comparing (C.7) and (C.16) to the results of Appendix B we see that the requirements for S<sub>1</sub> to converge are identical to the requirements on  $\rho_1$  in order that  $(1+A\rho^{-1}+B\rho^{-2})^{-\frac{1}{2}}$  be the generating function for the Legendre polynomials.

For a trajectory which does not hit the Earth, the series converges faster than a geometric series of ratio

$$\frac{c}{\rho_1} = \frac{c}{r_e} = \sqrt{J_2} \approx \frac{1}{30}$$
 (C.17)

### APPENDIX D

INVESTIGATION OF 
$$f_m(f) \equiv \int_0^f (1 + e \cos f)^m df$$

In determining the  $\ensuremath{\mathtt{R}}_1$  integral we found it necessary to evaluate

$$f_{m}(f) \equiv \int_{0}^{f} (1 + e\cos x)^{m} dx \qquad (D.1)$$

where x is a dummy variable. We also define

$$g_{m}(f) = \frac{1}{2\pi} f_{m}(2\pi) f$$
 (D.2)

We should first like to prove that  $f_m(f)-g_m(f)$  is an odd function of f. Noting that

$$f_{m}(-f) = \int_{0}^{-f} (1 + e\cos x)^{m} dx$$

if in the above equation we replace x = -y, then dx = -dy, cosx = cosy, and the limits of integration become  $0 \rightarrow f$ . Thus

$$f_{m}(-f) = -\int_{0}^{f} (1 + e \cos y)^{m} dy = -f_{m}(f)$$
 (D.3)

Therefore  $f_m(f)$  is an odd function. By its definition  $g_m$  is an odd function since

$$g_{m}(-f) = \frac{1}{2\pi} f_{m}(2\pi)(-f) = -g_{m}(f)$$
 (D.4)

As a consequence of (D.3) and (D.4) the function  $f_m(f)-g_m(f)$  must be odd. To find the period of  $f_m(f)-g_m(f)$  we first note

$$f_{m}(f+2\pi) = \int_{0}^{2\pi} (1+e\cos x)^{m} dx + \int_{2\pi}^{2\pi+f} (1+e\cos x)^{m} dx$$
(D.5)

If, in the second of these integrals we replace  $x = y+2\pi$ , then dx = dy, cosx = cosy, and the limits of integration become  $0 \rightarrow f$  so that (D.5) becomes

$$f_{m}(f+2\pi) = \int_{0}^{2\pi} (1+e\cos x)^{m} dx + \int_{0}^{f} (1+e\cos y)^{m} dy$$

so that

$$f_{m}(f+2\pi) = f_{m}(2\pi) + f_{m}(f)$$
 (D.6)

we also note that

$$g_{m}(f+2\pi) = \frac{1}{2\pi} f_{m}(2\pi)(f+2\pi) = g_{m}(f) + f_{m}(2\pi)$$
(D.7)

Thus by (D.6) and (D.7)

$$f_{m}(f+2\pi) - g_{m}(f+2\pi) = f_{m}(f) - g_{m}(f)$$
 (D.8)

So that  $f_m(f) - g_m(f)$  has been established to be odd and of period  $2\pi$ . Then we see that

$$f_{m}(2\pi) = \int_{0}^{\pi} (1 + \cos x)^{m} dx + \int_{\pi}^{2\pi} (1 + \cos x)^{m} dx$$

If in the second integral we set  $x = 2\pi - y$ , so that dx = -dy,  $\cos x = -\cos y$ and the limits of integration become  $\pi \rightarrow 0$ 

$$f_{m}(2\pi) = \int_{0}^{\pi} (1 + \cos x)^{m} dx - \int_{\pi}^{0} (1 + \cos y)^{m} dy = 2 f_{m}(\pi)$$
(D.9)

Using (D.9) we can write

$$g_{m}(f) = \frac{f}{\pi} f_{m}(\pi)$$
 (D.10)

Then since  $f_m(f)-g_m(f)$  is odd of period  $2\pi$ 

$$f_{m}(f) - \frac{f}{\pi} f_{m}(\pi) = \sum_{j=1}^{m} c_{mj} sinjf$$
 (D.11)

or equivalently

$$f_{m}(f) \equiv \int_{0}^{f} (1 + \cos f)^{m} df = \frac{f}{\pi} \int_{0}^{\pi} (1 + \cos f)^{m} df + \sum_{j=1}^{m} c_{mj} \sin jf \quad (D.12)$$

.

The fourier series in (D.12) terminates at j = m, because the integrand of (D.1) may be expressed as a trigonometric polynomial in cosjx, with  $j \leq m$ .

#### APPENDIX E

#### THE COMPUTER PROGRAM

The following Fortran IV computer program was run as problem number M6973 at the MIT Computation Center to generate data used in the text on the comparison between the spheroidal solution and a normal Keplerian trajectory. Inputs to the program are the oblateness parameter of the gravitating body  $(J_2)$ , the spheroidal orbital elements (a, e, I,  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$ ), the number of time steps N for which the state vector is desired, the amount DT of each time step, and the number of different trajectories NTRAJ included in the data. Output is as shown in Chapter 11; formatting allows cutting to standard 8  $\frac{1}{2}$  by 11 sheets. Units are assumed to be those of the canonical Vanguard system discussed in the text.

It may be of some value to note that the six example trajectories of Chapter 11 required a total of 4.3 seconds execution time on the IBM 360. The small computation time required for such a large increase in accuracy is one of the main advantages of the spheroidal method. Parameters used in the computer programs are related to the parameters used in the text as follows:

<u>Input Parameters</u>  $C2 = c^2 = J_2$ N = number of time steps DT = amount of each time step NTRAJ = number of different trajectories to be computed A, E, I, BETA1, BETA2, BETA3 = spheroidal orbital elements

Other Parameters

$NUO = n_0$	$PL(N) = P_n$ Legendre polynomials
$NUO2 = n_0^2$	$T(N) = T_n$
$X2 = x^2 = e^2 - 1$	$D(N) = D_n$
$NU22 = n_2^2$	$GN = \gamma_n$
$BS1 = b_1$	TIME = t
$BS2 = b_2$	$HO = H_0$ , etc.
$A0 = a_0$	$FO = f_0$ , etc.
$PO = P_0$	$PSIO = \psi_0, \text{ etc.}$
$N2 = n^2$	$NU = \eta$
$Al = A_l$ , etc	RX = X, etc.
All = $A_{11}$ , etc.	$VX = \dot{X}$ , etc.
$BlP = B_1$	$FDT = \dot{f}$
B2 = $B_2$ , etc.	RHODT = $\dot{\rho}$
$OMGA = \Omega$	$PSIDT = \dot{\psi}$
$W = \omega$	$OMGADT = \hat{\Omega}$
$ROX = r_{0_X}$ , etc.	$OMGAP = \Omega^{\prime}$

<pre>C ************************************</pre>		\$ JOB	HYP,KP=29,TIME=4,PAGES=100
<pre>C THIS PROGRAM ACCEPTS VALUES FOR THE SPHEROIDAL ORBITAL ELEMENTS- C (A,F,T,BETAI,9ETA2,BETA3) AND A VALUE OF J2. FROM THIS IT COMPUTES, USING THE SPHEROIDAL SOLN, THE STATE VECTOR (RX,RY,RY,VY,VZ), C THE MAGNITUDE OF THE POSITION AND VELOCITY VECTORS (R,V), C AND THE VALUES OF THE SPHEROIDAL ANOMALIES (HM,F#), AS FUNCTIONS C DF TIME. THEN, ON THE BASIS OF THE POS AND VEL VECTORS, AN FUNCTIONS C ORBITAL ELEMENTS (AS,ES,IS,OMGA=LONG OF NODE,H=ARG OF PER,TAU), C THE STATE VECTOR, THE MAGN OF THE POS AND VEL VECTORS, AND THE VALUES OF THE SPHERICAL ANOMALIES (H,F), AS FUNCTIOS OF TIME. C LINITATIONSGODO ONLY FOR UNBOUND TRAJECTORIES AND C INCLINATIONSGODO ONLY FOR UNBOUND TRAJECTORIES AND C INCLINATIONS NOT TOO CLOSE TO O DR 180 DEGREES C PHYSICAL UNITS EMPLOYED ARE THOSE OF THE CANONICAL VANGUAR SYSTEM C UNIT OF TIME 806.832 SECONDS C MU= 1 C ***********************************</pre>		С	*******************
<pre>C (A,E,I,BETAL,BETA2,BETA3) AND A VALUE OF J2. FROM THIS IT COMPUTES, C USING THE SPHEROIDAL SOUN. THE STATE VECTOR (RX,RY,RZ,VX,VY,VZ), C THE MAGNITUDE OF THE POSITION AND VELOCITY VECTORS (R,V), C AND THE VALUES OF THE SPHEROIDAL ANOMALIES (H,F*), AS FUNCTIONS OF TIME. THEN, ON THE BASIS OF THE POS AND VEL VECTORS AT C TIME.ZERO, IT COMPUTES, USING THE SPHERICAL SOLN, THE SPHERICAL ORBITAL ELEMENTS (AS,ES,IS,OMGA=LONG OF NODE,W=ARG OF PER,TAU), C THE STATE VECTOR, THE MACN OF THE POS AND VEL VECTORS, AND THE VALUES OF THE SPHERICAL ANOMALIES (H,F), AS FUNCTIOS OF TIME. L IMITATIONSGODO ONLY FOR UNBOUND TRAJECTORS; AND THE VALUES OF THE SPHERICAL ANOMALIES (H,F), AS FUNCTIOS OF TIME. C UNIT OF LENGTH=EQUATORIAL RADIUS= 6378.368 KILOMETERS C UNIT OF TIME= 806.832 SECONDS C UNIT OF TIME= 806.812 NOMALIES C UNIT OF TIME= 806.812 NOMALIES C UNIT OF TIME= 806.812 SECONDS C UNIT OF TIME.800.812 SECONDS C TIME TIME.800.812 SECONDS C UNIT OF TIME.800.812 SECONDS C TIME TIME.800.812 SECONDS C UNIT OF TIME.800.812 SECONDS C UNIT OF TIME.800.812 SECONDS C UNIT OF TIME.800.812 SECONDS C UNIT OF TIME.800.812 SECONDS C</pre>		С	THIS PROGRAM ACCEPTS VALUES FOR THE SPHEROIDAL ORBITAL ELEMENTS-
<pre>G USING THE SPHEROIDAL SOLN, THE STATE VECTOR (R,RA,RA,RA,RA,RA,VA,VY,Z), THE MAGNITUDE OF THE POSITION AND VELOCITY VECTORS (R,V), AND THE VALUES OF THE SPHEROIDAL ANOMALIES (H+,FA, AS FUNCTIONS G DF TIME. THEN, ON THE BASIS OF THE POS AND VEL VECTORS AT TIME=ZERO, IT COMPUTES, USING THE SPHERICAL SOLN, THE SPHERICAL G ORBITAL ELEMENTS (AS,ES,IS,OMGALIONO OF MODE, WAARG OF PER,TAU), C THE STATE VECTOR, THE MAGN OF THE POS AND VEL VECTORS, AND THE VALUES OF THE SPHERICAL NOMALIES (H,F), AS FUNCTIOS OF TIME. C UNITATIONSGOOD ONLY FOR UNBOUND TRAJECTORIES AND C UNIT OF THE BOG.B32 SECONDS C UNIT OF LENGTH=EQUATORIAL RADIUS= 6378.388 KILOMETERS C UNIT OF LENGTH=EQUATORIAL RADIUS= 6378.388 KILOMETERS C UNIT OF THE 806.832 SECONDS C MJ= 1 C ************************************</pre>		C	(A,E,I,BETA1,BETA2,BETA3) AND A VALUE OF J2. FROM THIS IT COMPUTES:
<pre>C THE MAGNITUDE OF THE POSITION AND VELOCITY VECTORS (R,V), AND THE VALUES OF THE SPHERIOLAL ANOMALIES (H+,F+), AS FUNCTIONS OF TIME. THEN, ON THE BASIS OF THE POS AND VEL VECTORS AT TIME.ZERO, IT COMPUTES, USING THE SPHERICAL SOLN, THE SPHERICAL ORBITAL ELEMENTS (AS,ES,IS,OMGA=LONG OF NODE,W=ARG OF PER,TAU), C THE STATE VECTOR, THE MAGN OF THE POS AND VEL VECTORS, AND THE VALUES OF THE SPHERICAL ANOMALIES (H,F), AS FUNCTIOS OF TIME. LIMITATIONSGODD ONLY FOR UNBOUND TRAJECTORIES AND C UNIT OF LENGTH=EQUATORIAL RADIOLSE TO 0 OR 180 DEGRES C UNIT OF TIME SHERICAL ANOMALIES (H,F), AS FUNCTIOS OF TIME. UNIT OF IENGTH=EQUATORIAL RADIOLSE 6378.388 KILOMETERS UNIT OF TIME SHERICAL ANOMALIES (H,F), AS RUCTIOS OF TIME. UNIT OF TIME 806,832 SECONDS C MU= 1 C ***********************************</pre>		C	USING THE SPHEROIDAL SOLN, THE STATE VECTOR (RX;RY;RZ;VX;VY;VZ);
<ul> <li>AND THE VALUES OF THE SPHEROIDAL ANOMALIES (H#,F#, AS FUNCTIONS</li> <li>C OF TIME: THEN, ON THE BASIS OF THE POS AND VEL VECTORS AT</li> <li>TIME: ZERO, IT COMPUTES, USING THE SPHERICAL SOLN, THE SPHERICAL</li> <li>C ORBITAL ELEMENTS (AS,ES,IS,OMGALDNO OF NODE, WEARG OF PERE, TAU),</li> <li>C THE STATE VECTOR, THE MAGN OF THE POS AND VEL VECTORS, AND THE</li> <li>C VALUES OF THE SPHERICAL ANOMALIES (H,F), AS FUNCTIOS OF TIME.</li> <li>LIMITATIONSGODD ONLY FOR UNBOUND TRAJECTORIES AND</li> <li>C INIT OF LENGTH: EQUATORIAL RADIUS = 6376.388 KILOMETERS</li> <li>C UNIT OF LENGTH: EQUATORIAL RADIUS = 6376.388 KILOMETERS</li> <li>C UNIT OF TIME: 806.932 SECONDS</li> <li>MUE 1</li> <li>C THEME: STORY, NUBLY, NUBLY,</li></ul>		C	THE MAGNITUDE OF THE POSITION AND VELOCITY VECTORS (R,V),
<pre>C UP 11ME. IHEN, UN IHE BASIS OF THE POS AND VEL VECTORS AT TIME_ZERO, IT COMPUTES, USING THE SPHERICAL SOLN, THE SPHERICAL ORBITAL ELEMENTS (AS,ES,IS,OMGA=LONG OF NODE,W=ARG OF PER,TAUJ), C THE STATE VECTOR, THE MAGN OF THE POS AND VEL VECTORS, AND THE VALUES OF THE SPHERICAL ANOMALIES (H,F), AS FUNCTIOS OF TIME. LIMITATIONSCODO ONLY FOR UNBOUND TRAJECTORIES AND MILTIONSCODO ONLY FOR UNBOUND TRAJECTORIES AND INCLIVATIONS NOT TOO CLOSE TO 0 OR 180 DEGREES PHYSICAL UNITS EMPLOYED ARE THOSE OF THE CANONICAL VANGUARD SYSTEM UNIT OF LENGTH=EQUATORIAL RADIUS= 6376.386 KILOMETERS UNIT OF TIME= 806,832 SECONDS C UNIT OF TIME= 806,832 SECONDS C UNIT OF TIME= 806,832 SECONDS C UNIT OF TIME= 806,832 SECONDS C MME 1 C ***********************************</pre>		C C	AND THE VALUES OF THE SPHEROIDAL ANOMALIES (H*,F*), AS FUNCTIONS
<pre>C</pre>		C C	UF TIME. THEN, UN THE BASIS OF THE POS AND VEL VECTORS AT
<pre>C UNBIAL ELEMENTS (AS,ES,15,UMGA=LUNG DF NUDE,W=AGG OF PER,TAU), THE STATE VECTOR, THE MAGN OF THE POS AND VEL VECTORS, AND THE VALUES OF THE SPHERICAL ANOMALIES (H,F), AS FUNCTIOS OF TIME. LIMITATIONSGODD ONLY FOR UNBOUND TRAJECTORIES AND INCLINATIONS NOT TOO CLOSE TO 0 OR 180 DEGREES PHYSICAL UNITS EMPLOYED ARE THOSE OF THE CANONICAL VANGUARD SYSTEM UNIT OF LENGTH=EQUATORIAL RADIUS= 6378.388 KILOMETERS UNIT OF TIME= 806,832 SECONDS MU= 1 C ***********************************</pre>		c r	TIME=ZERU, II COMPUTES, USING THE SPHERICAL SOLN, THE SPHERICAL
<pre>C</pre>		r r	URBITAL ELEMENTS (ASJES, ISJUMGA=LUNG UF NUDE, W=ARG ()F PER, TAU),
C LIMITATIONSGOD ONLY FOR UNBOUND TRAJECTORIES AND INCLINATIONS NOT TOO CLOSE TO O OR 180 DEGREES PHYSICAL UNITS EMPLOYED ARE THOSE OF THE CANONICAL VANGUARD SYSTEM UNIT OF LENGTH=EQUATORIAL RADIUS= 6378.388 KILOMETERS MUE 1 C UNIT OF TIME= 806.832 SECONDS MUE 1 C MUE 10 F TIME= 806.832 SECONDS MUE 1 C MUE 10 F TIME= 806.832 SECONDS MUE 1 C REAL 1,NUO,NUO2,NF,NU22,NZ,LAMB,M,MN,H REAL HO,HIP,HI,HZ,NU,GAGA,OMGADT REAL NUM2,HYP,NUM5,NUM6,NUM7,NUM8 6 300 FORMAT (6F10.4) 7 301 FORMAT (16F10.4) 7 301 FORMAT (16F10.4) 7 301 FORMAT (16F10.4) 8 300 FORMAT (16F10.4) 1 300 FORMAT (1 A1 DIO NOT CONVERGE') 9 308 FORMAT (1 A1 DIO NOT CONVERGE') 10 309 FORMAT (1 A1 DIO NOT CONVERGE') 11 310 FORMAT (1/36X,'TRAJECTORY NUMBER ',I2) 12 40 FORMAT (1/36X,'TRAJECTORY NUMBER ',I2) 13 55 FORMAT (1/36X,'TRAJECTORY NUMBER ',I2) 14 551 FORMAT (20X,'BETA1=',F6.4,'3X,'BETA2=',F6.4,'3X,'BETA3=',F6.4/) 15 355 FORMAT (136X,'SPHER)CIDAL SOLUTION') 16 557 FORMAT (136X,'SPHER)CIDAL SOLUTION') 17 356 FORMAT (16X,'SPHER)CIDAL SOLUTION') 18 357 FORMAT (16X,'SPHER)CIDAL SOLUTION') 19 356 FORMAT (16X,'SPHER)CIDAL SOLUTION') 21 366 FORMAT (16X,'SPHER)CIDAL SOLUTION') 23 360 FORMAT (16X,'SPHER)CIAL SOLUTION') 23 360 FORMAT (16X,'SPHER)CIAL SOLUTION') 24 365 FORMAT (16X,'SPHER)CIAL SOLUTION') 25 50 FORMAT (16X,'SPHER)CIAL SOLUTION') 26 365 FORMAT (16X,'SPHER)CIAL SOLUTION') 27 366 FORMAT (16X,'SPHER)CIAL SOLUTION') 28 365 FORMAT (16X,'SPHER)CIAL SOLUTION') 29 365 FORMAT (16X,'SPHER)CIAL SOLUTION') 20 367 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*') 20 999 NTRA=1,NTRAJ C START OF SPHER)CIAL SOLUTION 34 FORMAT (15,301) A,F,I,BETA1=SERA3 35 FORMAT (15,301) A,F,I,BETA1=SERA3 35 MED (5,301) A,F,		r	THE STATE VECTOR, THE MAGN OF THE PUS AND VEL VECTORS, AND THE
<pre>C FINTERIEST TO STRUCT TO CLOSE TO O DRIES AND C INTERIEST TO CLINATIONS NOT TO CLOSE TO O DRIES AND C UNIT OF LINCTHORY DARE THOSE OF THE CANONICAL VANGUARD SYSTEM UNIT OF TIMEE 806.832 SECONDS C UNIT OF TIMEE 806.832 SECONDS C MUE 1 C ***********************************</pre>		ř	VALUES OF THE SCHENICAL ANOMALIES (AFF), AS FUNCTIONS OF TIME.
<pre>PHYSICAL UNITS EMPLOYED ARE THOSE OF THE CANONICAL VANGUARD SYSTEM UNIT OF LENGTH=EQUATORIAL RADIUS= 6376.388 KILOMETEPS UNIT OF THME= 806.832 SECONDS MU= 1 ************************************</pre>		Č	INTERVIEW
<pre>C UNIT OF LENGTH=EQUATORIAL RADIUS = 0378.388 KILOMETEPS UNIT OF TIME 806.832 SECONDS C UNIT OF TIME 806.832 SECONDS C MU= 1 C ***********************************</pre>		Č	PHYSICAL UNITS EMPLOYED ARE THOSE OF THE CANONICAL VANCUARD SYSTEM
C UNIT OF TIME= 806.832 SECONDS C MU= 1 C NUE NOT PL(11), T(11), D(9) R EAL H0, H1P, H1, H2, NU, OMGAP, OMGADT R EAL H0, H1P, H1, H2, NU, OMGAP, OMGADT C REAL H0, H1P, H1, H2, NU, OMGAP, OMGADT C REAL H0, H1P, H1, H2, NU, OMGAP, OMGADT R EAL H0, H1P, H1, H2, NU, OMGAP, OMGADT R EAL H0, H1P, H1, H2, NU, OMGAP, OMGADT C REAL H0, H1P, H1, H2, NU, OMGAP, OMGADT C MEAT (H0, H1P, H1, H2, NU, OMGAP, OMGADT C MEAT (H0, H1P, H1, H2, NU, OMGAP, OMGADT C MEAT (H1), H1P, H1P, H2, NU, H0P, H1P, H1P, H1P, H1P, H1P, H1P, H1P, H1		č	UNIT OF LENGTH=FOUATORIAL RADIUS= 6378-388 KILOMETERS
C MUE 1 C ************************************		C	UNIT OF TIME= 806.832 SECONDS
C ************************************		С	MU = 1
1       DIMENSION PL(11),T(11),D(9)         2       REAL I,NUO,NUO2,NF,NU22,N2,LAMB,M,MN,H         3       REAL HO,HIP,H1,H2,NU,OMGAP,OMGADT         4       REAL HX,HY,HZ,NUMAG,IS,NUMG,POMGADT         5       RFAL LWZ,HYP,NUMS,NUMG,NUMT,NUM8         6       300 FORMAT (6F10.4)         7       301 FORMAT (6F10.4)         7       301 FORMAT (6F10.4)         7       307 FORMAT (1 A1 DID NOT CONVERGE')         9       308 FORMAT (' A2 DID NOT CONVERGE')         10       309 FORMAT (' A3 DID NOT CONVERGE')         11       310 FORMAT (' A3 DID NOT CONVERGE')         12       321 FORMAT ('A4 KEPLER EQUATION TOOK 20 CYCLES***')         13       350 FORMAT ('A5X,'TRAJECTORY NUMBER ',I2)         14       351 FORMAT ('A5X,'CO(1H_))         15       352 FORMAT ('A5X,'GIVEN J2=',F11.8)         16       353 FORMAT ('A5X,'SPHEROIDAL SOLUTION')         354 FORMAT (20X,'BETA1=',F6.4,7X,'E=',F6.4,7X,'BETA2=',F6.4,3X,'BETA3=',F6.4/)         18       355 FORMAT ('A5X,'SPHEROIDAL SOLUTION')         356 FORMAT ('A5X,'SPHEROIDAL SOLUTION')         357 FORMAT ('A5X,'SPHEROIDAL SOLUTION')         358 FORMAT ('A5X,'SPHERICAL SOLUTION')         359 FORMAT ('A5X,'SPHERICAL SOLUTION')         360 FORMAT ('A16X,'TIME',SX,'RX',9X,'Y',9X,'Y',10X,'F*')		С	******
<pre>2 REAL I,NUO,NUO2,NF,NU22,N2,LAMB,M,MN,H 3 REAL H0,HIP,H1,H2,NU,OMGAP,OMGADT 4 REAL H0,HIP,H1,H2,NU,OMGAP,OMGADT 5 REAL NUM2,HYP,NUM5,NUM6,NUM7,NUM8 6 300 FORMAT (E13,5,I3,F6.3) 8 307 FORMAT (E13,5,I3,F6.3) 8 307 FORMAT (* A1 DID NOT CONVERGE') 9 308 FORMAT (* A2 DID NOT CONVERGE') 10 309 FORMAT (* A2 DID NOT CONVERGE') 11 310 FORMAT (* A3 DID NOT CONVERGE') 12 321 FORMAT (* A3 DID NOT CONVERGE') 13 350 FORMAT (* A3 DID NOT CONVERGE *,I2) 14 351 FORMAT (* A3 DID NOT CONVERGE *,I2) 15 352 FORMAT (* A3 DID NOT CONVERGE *,I2) 16 353 FORMAT (* A3 DID NOT CONVERGE *,I2) 17 356 FORMAT (* A3 DID NOT CONVERGE *,I2) 18 350 FORMAT (* A3 DID NOT CONVERGE *,I2) 19 351 FORMAT (*,'STRAJECTORY NUMBER *,I2) 19 355 FORMAT (*,'STRAJECTORY NUMBER *,I2) 10 357 FORMAT (*,'STRAJECTORY NUMBER *,I2) 11 310 FORMAT (*,'STRAJECTORY NUMBER *,I2) 12 358 FORMAT (*,'STRAJECTORY NUMBER *,I2) 13 60 FORMAT (*,'STRAJECTORY NUMBER *,I2) 13 60 FORMAT (*,'STRAJECTORY NUMBER *,I2) 13 60 FORMAT (*,'STRAJECTORY NUMBER *,I2) 14 361 FORMAT (*,'STRAJECTORY NUMBER *,I2) 15 5TORMAT (*,'STRAJECTORY NUMBER *,I2) 16 5TORMAT (*,'STRAJECTORY NUMBER *,I2) 17 364 FORMAT (*,'STRAJECTORY NUMBER *,ETA,'STA,'RY*,9X,'RY*,9X,'RZ*,9X,'R'*,10X,'H*') 18 366 FORMAT (*,'STRAJECTORY NUMP,'Y,'Y,Y,'Y,'Y,'Y,'Y,'Y,'Y,'Y,'Y,'Y,'Y,'</pre>	1		DIMENSION PL(11),T(11),D(9)
<ul> <li>REAL H0, H1P, H1, H2, NU, OMGAP, OMGADT</li> <li>REAL HX, HY, H1Z, NUM4, IS, NUM1, IZX, IZY, IZZ, INX, INY, OMGA, HO</li> <li>REAL NUM2, HYP, NUM5, NUM6, NUM7, NUM8</li> <li>300 FORMAT (6F10.4)</li> <li>301 FORMAT (6F10.4)</li> <li>301 FORMAT (1 A1 DID NOT CONVERGE')</li> <li>308 FORMAT (* A1 DID NOT CONVERGE')</li> <li>309 FORMAT (* A2 DID NOT CONVERGE')</li> <li>309 FORMAT (* A2 DID NOT CONVERGE')</li> <li>309 FORMAT (* A3 DID NOT CONVERGE')</li> <li>310 FORMAT (* ****KEPLER EQUATION TOOK 20 CYCLES***')</li> <li>311 310 FORMAT (/36X, *TRAJECTORY NUMBER ',I2)</li> <li>351 FORMAT (/130X, *TRAJECTORY NUMBER ',I2)</li> <li>352 FORMAT (/16X, 'GIVEN J2=',F11.8)</li> <li>353 FORMAT (24X, *A=',F6.4, TX, *E=',F6.4, TX, *I=',F6.4)</li> <li>354 FORMAT (20X, *BETA1=',F6.4, 3X, *BETA2=',F6.4, 3X, *BETA3=',F6.4/)</li> <li>355 FORMAT (26X, *OFHEROIDAL SOLUTION')</li> <li>356 FORMAT (36X, 19(1H_))</li> <li>357 FORMAT (16X, 'GIVEN J2=',F10.6))</li> <li>358 FORMAT (25X, 'VX',9X, 'VY',9X, 'RY',9X, 'RZ',9X, 'R',10X, 'H*')</li> <li>359 FORMAT (16X, F6.1,5(1X,F10.6))</li> <li>360 FORMAT (16X, 'SPHERICAL SOLUTION')</li> <li>361 FORMAT (37X, 18(1H_))</li> <li>363 FORMAT (16X, 'THE SPHERICAL SOLUTION')</li> <li>364 FORMAT (16X, 'THE SPHERICAL SOLUTION')</li> <li>365 FORMAT (16X, 'THE SPHERICAL SOLUTION')</li> <li>365 FORMAT (16X, 'THE SPHERICAL SOLUTION')</li> <li>366 FORMAT (16X, 'THE SPHERICAL SOLUTION')</li> <li>367 FORMAT (16X, 'TME', 'SX, 'RY', '9X, 'RZ', '9X, 'R',10X, 'H*')</li> <li>368 FORMAT (16X, 'TME', 'SX, 'RY', '9X, 'RZ', '9X, 'R',10X, 'H*')</li> <li>368 FORMAT (16X, 'TME', 'SX, 'RY', '9X, 'RZ', '9X, 'R',10X, 'H*')</li> <li>368 FORMAT (16X, 'TME', 'SX, 'RY', '9X, 'Y', '9X, 'RZ', '9X, 'R', '10X, 'H*')</li> <li>368 FORMAT (16X, 'TME', 'SX, 'RY', '9X, 'Y', '9X, 'RZ', '9X, 'R', '10X, 'H*')</li> <li>368 FORMAT (16X, 'TME 'SX, 'RY', '9X, 'Y', '9X, 'RZ', '9X, 'R', '10X, 'H*')</li>     &lt;</ul>	2		REAL I, NUO, NUO, NUO, NU, NU, NU, NU, NU, NU, NU, NU, NU, NU
<pre>4 REAL HX,HY,HZ,NUM4,IS,NUM1,IZX,IZY,IZZ,INX,INY,OMGA,HO 8 REAL NUM2,HYP,NUM5,NUM6,NUM7,NUM8 6 300 FORMAT (6F10.4) 7 301 FORMAT (14 1 DID NOT CONVERGE') 9 308 FORMAT (' A1 DID NOT CONVERGE') 10 309 FORMAT (' A3 DID NOT CONVERGE') 11 310 FORMAT (' A*KEPLER EQUATION TOOK 20 CYCLES***') 12 321 FORMAT (I3) 13 350 FORMAT (I3) 13 350 FORMAT (I43, VIRAJECTORY NUMBER ',I2) 14 351 FORMAT (I62,'GIVEN J2=',F11.8) 16 353 FORMAT (I62,'GIVEN J2=',F11.8) 16 353 FORMAT (I62,'GIVEN J2=',F11.8) 16 355 FORMAT (35X,'SPHEROIDAL SOLUTION') 19 356 FORMAT (36X,'SPHEROIDAL SOLUTION') 19 356 FORMAT (36X,'SPHEROIDAL SOLUTION') 20 357 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*') 21 358 FORMAT (16X,60(1H_)) 23 360 FORMAT (16X,60(1H_)) 23 360 FORMAT (16X,64.1,5(1X,F10.6)) 24 361 FORMAT (37X,'SPHERICAL SOLUTION') 25 362 FORMAT (37X,'SPHERICAL SOLUTION') 26 363 FORMAT (18X,'AS=',E16.8,'ES=',E16.8,' IS=',E16.8] 27 366 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'R',9X,'R',10X,'H*') 28 365 FORMAT (16X,611H_)) 29 366 FORMAT (16X,*THE SPHERICAL ELEMENTS ARE') 20 367 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'R',9X,'R',10X,'H*') 20 367 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'R',9X,'R',10X,'H*') 28 366 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'R',9X,'R',10X,'H*') 29 366 FORMAT (16X,'TIME',5X,'RX',9X,'Y',9X,'Y',9X,'R',9X,'R',10X,'H*') 20 367 FORMAT (16X,'TIME',5X,'RX',9X,'Y',9X,'R',9X,'R',10X,'H*') 30 367 FORMAT (16X,'TIME',5X,'RX',9X,'Y',9X,'R',9X,'R',10X,'H'') 31 368 FORMAT (16X,'TIME',5X,'RX',9X,'Y',9X,'Y',9X,'R',9X,'R',10X,'H'') 31 368 FORMAT (16X,'TIME',5X,'RX',9X,'Y',9X,'Y',9X,'R',10X,'F') 32 READ (5,301) A,E,I,BETA1,BETA2,BETA3 35 READ (5,3</pre>	3		REAL HO,HIP,H1,H2,NU,OMGAP,OMGADT
<ul> <li>300 FORMAT (6F10.4)</li> <li>301 FORMAT (1 LE13.5,13,F6.3)</li> <li>307 FORMAT (1 A1 DID NOT CONVERGE')</li> <li>308 FORMAT (1 A2 DID NOT CONVERGE')</li> <li>309 FORMAT (1 A2 DID NOT CONVERGE')</li> <li>309 FORMAT (1 A3 DID NOT CONVERGE')</li> <li>310 FORMAT (1 A3 DID NOT CONVERGE')</li> <li>310 FORMAT (1 ****KEPLER EQUATION TOOK 20 CYCLES***')</li> <li>321 FORMAT (13)</li> <li>350 FORMAT (1/36X,'TRAJECTORY NUMBER ',12)</li> <li>351 FORMAT (16X,'GIVEN J2=',F11.8)</li> <li>352 FORMAT (16X,'GIVEN J2=',F6.4,7X,'T=',F6.4)</li> <li>353 FORMAT (24X,'A=',F6.4,7X,'E=',F6.4,7X,'T=',F6.4)</li> <li>354 FORMAT (20X,'SPHEROIDAL SOLUTION')</li> <li>355 FORMAT (36X,19(1H_))</li> <li>356 FORMAT (36X,19(1H_))</li> <li>357 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>358 FORMAT (16X,'SPHEROIDAL SOLUTION')</li> <li>359 FORMAT (16X,'SINERICAL ELEMENTS ARE')</li> <li>360 FORMAT (137X,'SPHERICAL SOLUTION')</li> <li>361 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>363 FORMAT (16X,*GNERICAL ELEMENTS ARE')</li> <li>364 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>365 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>366 FORMAT (16X,*GNERICAL ELEMENTS ARE')</li> <li>367 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'Y',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'Y',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'TIME',5X,'RX',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9X,'Y',9</li></ul>	4		REAL HX, HY, HZ, NUMA, IS, NUMI, IZX, IZY, IZZ, INX, INY, OMGA, HO
<pre>0 300 FORMAT (10F10.+) 7 301 FORMAT (113.5,13,F6.3) 8 307 FORMAT (* A1 DID NOT CONVERGE*) 9 308 FORMAT (* A2 DID NOT CONVERGE*) 10 309 FORMAT (* A3 DID NOT CONVERGE*) 11 310 FORMAT (* A3 DID NOT CONVERGE*) 12 321 FORMAT (136X,*TRAJECTORY NUMBER *,12) 13 350 FORMAT (/16X,*GIVEN J2=*,F11.8) 16 353 FORMAT (/16X,*GIVEN J2=*,F11.8) 16 353 FORMAT (24X,*A=*,F6.4,7X,*E=*,F6.4,7X,*I=*,F6.4) 17 354 FORMAT (20X,*BETA1=*,F6.4,3X,*BETA2=*,F6.4,3X,*BETA3=*,F6.4/) 18 355 FORMAT (26X,*SPHEROIDAL SOLUTION*) 19 356 FORMAT (36X,19(1H_)) 20 357 FORMAT (16X,*GIVEN',9X,*RX',9X,*RY',9X,*RZ',9X,*R*,10X,*H**) 21 358 FORMAT (25X,*VX',9X,*VY',9X,*VZ',9X,*R',10X,*F**) 23 360 FORMAT (16X,60(1H_)) 23 360 FORMAT (16X,F6.1,5(1X,F10.6)) 24 361 FORMAT (20X,51X,F10.6)/ 25 362 FORMAT (16X,*SPHERICAL SOLUTION*) 26 363 FORMAT (16X,*THE SPHERICAL SULUTION*) 26 365 FORMAT (16X,*THE SPHERICAL ELEMENTS ARE*) 28 366 FORMAT (16X,*THE SPHERICAL ELEMENTS ARE*) 29 366 FORMAT (16X,*TIME*,5X,*RX',9X,*RY',9X,*RZ',9X,*R',10X,*H*) 31 368 FORMAT (15,301) A,F,I,BETA1,BETA2,BETA3 35 READ (5,301) A,E,I,BETA1,BETA2,BETA3 35 READ (5,301) C2,N,DT</pre>	5	200	KEAL NUMZ;HTY;NUMD;NUM6;NUM7;NUM8
<ul> <li>307 FORMAT (' A1 DIO NOT CONVERGE')</li> <li>308 FORMAT (' A1 DIO NOT CONVERGE')</li> <li>309 FORMAT (' A3 DID NOT CONVERGE')</li> <li>310 FORMAT (' A3 DID NOT CONVERGE')</li> <li>311 310 FORMAT (' ***KEPLER EQUATION TOOK 20 CYCLES***')</li> <li>321 FORMAT ('/36X,'TRAJECTORY NUMBER ',I2)</li> <li>352 FORMAT (//36X,'TRAJECTORY NUMBER ',I2)</li> <li>353 FORMAT (36X,20(1H_))</li> <li>352 FORMAT (16X,'GIVEN J2=',F11.8)</li> <li>353 FORMAT (24X,'A=',F6.4,7X,'E=',F6.4,7X,'I=',F6.4)</li> <li>354 FORMAT (20X,'BETA1=',F6.4,3X,'BETA2=',F6.4,3X,'BETA3=',F6.4/)</li> <li>355 FORMAT (36X,19(1H_))</li> <li>356 FORMAT (36X,'ITHE',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>358 FORMAT (25X,'VX',9X,'VY',9X,'VZ',9X,'V',10X,'F*')</li> <li>360 FORMAT (16X,F61.1,5(1X,F10.6))</li> <li>361 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>362 FORMAT (16X,F1.1,5(1X,F10.6))</li> <li>363 FORMAT (16X,'THE SPHERICAL ELEMENTS ARE')</li> <li>364 FORMAT (16X,'THE SPHERICAL ELEMENTS ARE')</li> <li>365 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>364 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>365 FORMAT (16X,'THE SPHERICAL ELEMENTS ARE')</li> <li>364 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>365 FORMAT (16X,'OMGA=',E16.8,'B=',E16.8,'IS=',E16.8)</li> <li>367 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'OMGA=',E16.8,'W=',E16.8,'IAU=',E16.8)</li> <li>367 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'NTHE',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'NTHE',5X,'RX',9X,'RY',9X,'Y',10X,'F*')</li> <li>368 FORMAT (16X,'NTHE',5X,'RX',9X,'RY',9X,'Y',10X,'F*')</li> <li>378 FCAD (5,301) A,E,I,BETA1,BETA2,BETA3</li> <li>35 FORMAT (15,301) C2,N,DT</li> </ul>	7	301	- FORMAT (F13.5.13.F6.2)
<ul> <li>308 FORMAT (' A2 DID NOT CONVERGE')</li> <li>309 FORMAT (' A2 DID NOT CONVERGE')</li> <li>310 FORMAT (' ****KEPLER EQUATION TOOK 20 CYCLES***')</li> <li>311 310 FORMAT (' ****KEPLER EQUATION TOOK 20 CYCLES***')</li> <li>312 FORMAT ('30</li> <li>350 FORMAT ('/36X, 'TRAJECTORY NUMBER ',I2)</li> <li>351 FORMAT ('13)</li> <li>352 FORMAT ('13)</li> <li>352 FORMAT ('16X, 'GIVEN J2=',F11.8)</li> <li>353 FORMAT (20X, 'BETA1=',F6.4,7X, 'E=',F6.4, 3X, 'BETA3=',F6.4/)</li> <li>355 FORMAT (36X,'9(IH_))</li> <li>356 FORMAT (36X,'9(IH_))</li> <li>356 FORMAT (36X,'9(IH_))</li> <li>357 FORMAT ('16X,'GIUH_)</li> <li>358 FORMAT (36X,'9(IH_))</li> <li>359 FORMAT ('16X,'GIUH_))</li> <li>359 FORMAT (16X, 'GIVEN J2,'YX',9X,'YY',9X,'RZ',9X,'R',10X,'H*')</li> <li>358 FORMAT (16X, F1,16(IH_))</li> <li>360 FORMAT (16X, F4.1,5(IX,F10.6))</li> <li>361 FORMAT ('16X,'THE SPHERICAL SOLUTION')</li> <li>363 FORMAT (16X,'AS=',E16.8,'LS=',E16.8),'IS=',E16.8)</li> <li>364 FORMAT ('16X,'THE SPHERICAL ELEMENTS ARE')</li> <li>365 FORMAT (16X,'GUNGA=',E16.8,'W=',E16.8,'IAU=',E16.8)</li> <li>367 FORMAT ('16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'OMGA=',E16.8,'W=',E16.8,'IAU=',E16.8)</li> <li>367 FORMAT ('16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'OMGA=',E16.8,'W=',E16.8,'IAU=',E16.8)</li> <li>367 FORMAT ('16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (16X,'OMGA=',E16.8,'W=',E16.8,'IAU=',E16.8)</li> <li>367 FORMAT ('16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT (25X,'YX',9X,'YY',9X,'YZ',9X,'Y',10X,'F*')</li> <li>368 FORMAT ('16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT ('16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')</li> <li>368 FORMAT ('16X,'TIME',5X,'RX',9X,'Y',9X,'Y',10X,'F*')</li> <li>368 FORMAT ('16X,'TIME',5X,'RX',9X,'Y',9X,'Y',10X,'F*')</li> <li>368 FORMAT ('16X,'TIME',5X,'RX',9X,'Y',9X,'Y',10X,'F*')</li> <li>378 FCAD (5,301) A,E,I,BETA1,BETA2,BETA3</li> <li>35 FORMAT ('16X,01) A,E,I</li></ul>	8	307	FORMAT (LIS-S)IS/TO-S/
<pre>10 309 FORMAT (' A3 DID NOT CONVERGE') 11 310 FORMAT (' ***KEPLER EQUATION TOOK 20 CYCLES***') 12 321 FORMAT ('] 13 350 FORMAT ('] 14 351 FORMAT ('] 15 352 FORMAT ('] 16 353 FORMAT ('] 17 354 FORMAT (24X,'A=',F6.4,7X,'E=',F6.4,7X,'I=',F6.4) 17 354 FORMAT (20X,'BETA1=',F6.4,3X,'BETA2=',F6.4,3X,'BETA3=',F6.4/) 18 355 FORMAT (36X,'SPHEROIDAL SOLUTION') 19 356 FORMAT (36X,'SPHEROIDAL SOLUTION') 19 356 FORMAT ('] 16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*') 21 358 FORMAT (25X,'VX',9X,'YY',9X,'RZ',9X,'R',10X,'H*') 22 359 FORMAT (16X,60(1H_)) 23 360 FORMAT (16X,F10.6)) 24 361 FORMAT (20X,511X,F10.6)) 25 362 FORMAT (37X,'SPHERICAL SOLUTION') 26 363 FORMAT ('] 27 364 FORMAT ('] 27 364 FORMAT ('] 28 365 FORMAT ('] 29 366 FORMAT ('] 20 367 FORMAT ('] 20 367 FORMAT ('] 21 358 FORMAT ('] 22 359 23 50 FORMAT ('] 24 361 FORMAT ('] 25 362 FORMAT ('] 26 363 FORMAT ('] 27 364 FORMAT ('] 28 365 FORMAT ('] 29 366 FORMAT ('] 20 367 FORMAT ('] 20 367 FORMAT ('] 21 358 FORMAT ('] 22 359 23 50 FORMAT ('] 24 361 FORMAT ('] 25 362 FORMAT ('] 26 363 FORMAT ('] 27 364 FORMAT ('] 28 365 FORMAT ('] 29 366 FORMAT ('] 20 367 FORMAT ('] 20 360 FORMAT ('] 20 361 FORMA</pre>	ğ	308	FORMAT ( A2 DID NOT CONVERGE)
<pre>11 310 FORMAT (* ***KEPLER EQUATION TOOK 20 CYCLES****) 12 321 FORMAT (13) 13 350 FORMAT (//36X,*TRAJECTORY NUMBER *,12) 14 351 FORMAT (36X,20(1H_)) 15 352 FORMAT (//36X,*GIVEN J2=*,F11.8) 16 353 FORMAT (24X,*A=*,F6.4,7X,*E=*,F6.4,7X,*I=*,F6.4) 17 354 FORMAT (20X,*BETA1=*,F6.4,3X,*BETA2=*,F6.4,3X,*BETA3=*,F6.4/) 18 355 FORMAT (36X,*SPHEROIDAL SOLUTION*) 19 356 FORMAT (36X,*SPHEROIDAL SOLUTION*) 19 356 FORMAT (36X,*GIVEN J2=*,F1.4,8) 20 357 FORMAT (16X,*GIVEN J2=*,F2.4,7X,*R2*,9X,*R2*,9X,*R*,10X,*H**) 21 358 FORMAT (16X,*GIVEN J2=*,F1.4,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7</pre>	10	309	PERMAT ( A3 DID NOT CONVERGE)
<pre>12 321 FORMAT (I3) 13 350 FORMAT (//36X,'TRAJECTORY NUMBER ',I2) 14 351 FORMAT (//36X,'TRAJECTORY NUMBER ',I2) 15 352 FORMAT (36X,20(1H_)) 15 352 FORMAT (16X,'GIVEN J2=',F11.8) 16 353 FORMAT (24X,'A=',F6.4,7X,'E=',F6.4,7X,'I=',F6.4) 17 354 FORMAT (20X,'BETA1=',F6.4,3X,'BETA2=',F6.4,3X,'BETA3=',F6.4/) 18 355 FORMAT (36X,'SPHEROIDAL SOLUTION') 19 356 FORMAT (36X,'SPHEROIDAL SOLUTION') 20 357 FORMAT (/16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*') 21 358 FORMAT (25X,'VX',9X,'VY',9X,'VZ',9X,'V',10X,'F*') 22 359 FORMAT (16X,F6.4,5(1X,F10.6)) 23 360 FORMAT (16X,F4.1,5(1X,F10.6)) 24 361 FORMAT (20X,5(1X,F10.6)/) 25 362 FORMAT (37X,'SPHERICAL SOLUTION') 26 363 FORMAT (37X,'SPHERICAL SOLUTION') 27 364 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H') 386 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H') 393 66 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H') 393 66 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H') 393 67 FORMAT (16X,'TIME',5X,'RX',9X,'YY',9X,'RZ',9X,'R',10X,'H') 394 FORMAT (16X,'TIME',5X,'RX',9X,'YY',9X,'RZ',9X,'R',10X,'H') 395 FORMAT (5,321) NTRAJ 39 00 999 NTRA=1,NTRAJ 39 C START OF SPHEROIDAL SOLUTION 34 READ (5,301) A,E,I,BETA1,BETA2,BETA3 35 READ (5,301) A,E,NDT</pre>	11	310	FORMAT (* ***KEPLER EQUATION TOOK 20 CYCLES****)
<pre>13 350 FORMAT (//36X, 'TRAJECTORY NUMBER ',I2) 14 351 FORMAT (36X, 20(1H_)) 15 352 FORMAT (/16X, 'GIVEN J2=',F11.8) 16 353 FORMAT (24X, 'A=',F6.4, 7X, 'E=',F6.4, 7X, 'I=',F6.4) 17 354 FORMAT (20X, 'BETA1=',F6.4, 3X, 'BETA2=',F6.4, 3X, 'BETA3=',F6.4/) 18 355 FORMAT (36X, 19(1H_)) 19 356 FORMAT (36X, 19(1H_)) 20 357 FORMAT (/16X, 'TIME',5X, 'RX',9X, 'RY',9X, 'RZ',9X, 'R',10X, 'H*') 21 358 FORMAT (16X, 60(1H_)) 23 360 FORMAT (16X, 60(1H_)) 23 360 FORMAT (16X,F4.1,5(1X,F10.6)) 24 361 FORMAT (20X,5(1X,F10.6)/) 25 362 FORMAT (37X, 'SPHERICAL SOLUTION') 26 363 FORMAT (17X, 'SPHERICAL SOLUTION') 27 364 FORMAT (16X, 'TIME SPHERICAL ELEMENTS ARE') 28 365 FORMAT (16X, 'TIME',5X, 'RX',9X, 'RY',9X, 'RZ',9X, 'R',10X, 'H') 31 368 FORMAT (25X, 'VX',9X, 'VZ',9X,'VZ',9X,'RZ',9X, 'R',10X,'H') 32 360 FORMAT (16X, 'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H') 33 60 FORMAT (16X, 'Y, 'Y, 'Y, 'Y, 'Y, 'Y, 'Y, 'Y, 'Y, 'Y</pre>	12	321	FORMAT (13)
<pre>14 351 FORMAT (36X,20(1H_)) 15 352 FORMAT (/16X,'GIVEN J2=',F11.8) 16 353 FORMAT (24X,'A=',F6.4,7X,'E=',F6.4,7X,'I=',F6.4) 17 354 FORMAT (20X,'BETA1=',F6.4,3X,'BETA2=',F6.4,3X,'BETA3=',F6.4/) 18 355 FORMAT (36X,'SPHEROIDAL SOLUTION') 19 356 FORMAT (36X,'I9(1H_)) 20 357 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*') 21 358 FORMAT (25X,'VX',9X,'VY',9X,'VZ',9X,'V',10X,'F*') 22 359 FORMAT (16X,60(1H_)) 23 360 FORMAT (16X,F4.1,5(1X,F10.6)) 24 361 FORMAT (20X,5(1X,F10.6)/) 25 362 FORMAT (37X,18(1H_)) 27 364 FORMAT (37X,18(1H_)) 27 364 FORMAT (16X,'THE SPHERICAL ELEMENTS ARE') 28 365 FORMAT (18X,'AS=',E16.8,'ES=',E16.8,'IS=',E16.8) 29 366 FORMAT (16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H') 31 368 FORMAT (25X,'VX',9X,'VY',9X,'VZ',9X,'RZ',9X,'R',10X,'H') 32 READ (5,321) NTRAJ 33 D0 999 NTRA=1,NTRAJ C START OF SPHEROIDAL SOLUTION 34 READ (5,301) C2,N,DT</pre>	13	350	) FORMAT (//36X, TRAJECTORY NUMBER +,12)
<pre>15 352 FORMAT (/16X, 'GIVEN J2=', F11.8) 16 353 FORMAT (24X, *A=', F6.4, 7X, *E=', F6.4, 7X, *I=', F6.4) 17 354 FORMAT (20X, 'BETA1=', F6.4, 3X, 'BETA2=', F6.4, 3X, 'BETA3=', F6.4/) 18 355 FORMAT (36X, 'SPHEROIDAL SOLUTION') 19 356 FORMAT (36X, 19(1H_)) 20 357 FORMAT (/16X, 'TIME', 5X, *RX', 9X, *RY', 9X, *RZ', 9X, *R', 10X, *H*') 21 358 FORMAT (25X, 'VX', 9X, *VY', 9X, *VZ', 9X, *V', 10X, *F*') 22 359 FORMAT (16X, 60(1H_)) 23 360 FORMAT (16X, F10.6)) 24 361 FORMAT (16X, F10.6)/) 25 362 FORMAT (37X, 'SPHERICAL SOLUTION') 26 363 FORMAT (37X, 'SPHERICAL SOLUTION') 26 363 FORMAT (37X, 18(1H_)) 27 364 FORMAT (/16X, *THE SPHERICAL ELEMENTS ARE') 28 365 FORMAT (16X, *OMGA=', E16.8, 'W=', E16.8, 'TAU=', E16.8) 29 366 FORMAT (16X, *OMGA=', E16.8, 'W=', E16.8, 'TAU=', E16.8) 30 367 FORMAT (/16X, *TIME', 5X, *RX', 9X, *RY', 9X, *RZ', 9X, *R', 10X, *H*') 31 368 FORMAT (25X, 'VX', 9X, 'VY', 9X, *VZ', 9X, *R', 10X, *H*') 32 READ (5, 321) NTRAJ 33 DO 999 NTRA=1, NTRAJ 34 READ (5, 300) A, E, I, BETA1, BETA2, BETA3 35 READ (5, 301) C2, N, DT</pre>	14	351	EFORMAT (36X+20(1H_))
<pre>16 353 FORMAT (24X, 'A=', F6.4, 7X, 'E=', F6.4, 7X, 'I=', F6.4) 17 354 FORMAT (20X, 'BETA1=', F6.4, 7X, 'BETA2=', F6.4, 3X, 'BETA3=', F6.4/) 18 355 FORMAT (36X, 'SPHEROIDAL SOLUTION') 19 356 FORMAT (36X, 'SPHEROIDAL SOLUTION') 20 357 FORMAT (/16X, 'TIME', 5X, 'RX', 9X, 'RY', 9X, 'RZ', 9X, 'R', 10X, 'H*') 21 358 FORMAT (25X, 'VX', 9X, 'VY', 9X, 'VZ', 9X, 'V', 10X, 'F*') 22 359 FORMAT (16X, 60(1H_)) 23 360 FORMAT (16X, F4.1, 5(1X, F10.6)) 24 361 FORMAT (20X, 5(1X, F10.6)/) 25 362 FORMAT (37X, 'SPHERICAL SOLUTION') 26 363 FORMAT (37X, 18(1H_)) 27 364 FORMAT (/16X, 'TIME SPHERICAL ELEMENTS ARE') 28 365 FORMAT (16X, 'TIME SPHERICAL ELEMENTS ARE') 28 365 FORMAT (16X, 'TIME', 5X, 'RX', 9X, 'RY', 9X, 'RZ', 9X, 'R', 10X, 'H') 31 368 FORMAT (/16X, 'TIME', 5X, 'RX', 9X, 'RY', 9X, 'RZ', 9X, 'R', 10X, 'H') 32 READ (5, 321) NTRAJ 33 DO 999 NTRA=1, NTRAJ C START OF SPHEROIDAL SOLUTION 44 READ (5, 300) A, E, I, BETA1, BETA2, BETA3 35 READ (5, 301) C2, N, DT</pre>	15	352	2 FORMAT (/16X, GIVEN J2= , F11.8)
<pre>17 354 FURMAT (20X, "BETA1=",F6.4,3X,"BETA2=",F6.4,3X,"BETA3=",F6.4/) 18 355 FORMAT (36X, 'SPHEROIDAL SOLUTION") 19 356 FORMAT (36X,19(1H_)) 20 357 FORMAT (/I6X,'TIME',5X,'RX",9X,'RY',9X,'RZ',9X,'R',10X,"H*") 21 358 FORMAT (25X,'VX',9X,'VY',9X,'VZ',9X,'V',10X,"F*') 22 359 FORMAT (16X,60(1H_)) 23 360 FORMAT (16X,F4.1,5(1X,F10.6)) 24 361 FORMAT (20X,5(1X,F10.6)/) 25 362 FORMAT (37X, 'SPHERICAL SOLUTION') 26 363 FORMAT (37X,18(1H_)) 27 364 FORMAT (/I6X,'THE SPHERICAL ELEMENTS ARE') 28 365 FORMAT (16X, 'CAL SOLUTION') 29 366 FORMAT (16X, 'TIME',5X,'RX',9X,'RY',9X,'RY',9X,'RZ',9X,'R',10X,'H') 31 368 FORMAT (/16X,'TIME',5X,'RX',9X,'RY',9X,'RY',9X,'RZ',9X,'R',10X,'H') 32 READ (5,321) NTRAJ 26 START OF SPHEROIDAL SOLUTION 26 A READ (5,301) C2,N,DT</pre>	16	353	5 FORMAT (24X, "A=", F6.4, 7X, "E=", F6.4, 7X, "I=", F6.4)
18       355       FORMAT (36X,*SPHEROIDAL SOLUTION*)         19       356       FORMAT (36X,*SPHEROIDAL SOLUTION*)         20       357       FORMAT (/16X,*TIME',5X,*RX*,9X,*RY*,9X,*RZ*,9X,*R*,10X,*H**)         21       358       FORMAT (/16X,*TIME',5X,*RX*,9X,*RY*,9X,*RZ*,9X,*R*,10X,*H**)         22       359       FORMAT (/16X,*TIME',5X,*RX*,9X,*VZ*,9X,*V*,10X,*F**)         23       360       FORMAT (16X,60(1H_))         23       360       FORMAT (16X,60(1H_))         23       360       FORMAT (16X,F10.6)/)         24       361       FORMAT (37X,*SPHERICAL SOLUTION*)         26       363       FORMAT (37X,*SPHERICAL SOLUTION*)         26       363       FORMAT (16X,*THE SPHERICAL ELEMENTS ARE*)         27       364       FORMAT (16X,*THE SPHERICAL ELEMENTS ARE*)         28       365       FORMAT (16X,*OMGA=*,E16.8,*ES=*,E16.8,*IS=*,E16.8)         29       366       FORMAT (16X,*OMGA=*,E16.8,*W=*,E16.8,*TAU=*,E16.8)         30       367       FORMAT (/16X,*TIME',5X,*RX*,9X,*RY*,9X,*RZ*,9X,*R*,10X,*H*)         31       368       FORMAT (25X,*VX*,9X,*VY*,9X,*RZ*,9X,*RZ*,9X,*R*,10X,*H*)         32       READ (5,321) NTRAJ       D0         33       D0       999 NTRA=1,NTRAJ         34       READ (	17	354	FORMAT (20X, 'BETA1=', F6.4, 3X, 'BETA2=', F6.4, 3X, 'BETA3=', F6.4/)
19       356 FURMAT (35X,19(1H_))         20       357 FORMAT (/16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H*')         21       358 FORMAT (25X,'VX',9X,'VY',9X,'VZ',9X,'V',10X,'F*')         22       359 FORMAT (16X,60(1H_))         23       360 FORMAT (16X,F4.1,5(1X,F10.6))         24       361 FORMAT (20X,5(1X,F10.6)/)         25       362 FORMAT (37X,'SPHERICAL SOLUTION')         26       363 FORMAT (37X,18(1H_))         27       364 FORMAT (/16X,'THE SPHERICAL ELEMENTS ARE')         28       365 FORMAT (18X,'AS=',E16.8,'ES=',E16.8,'IS=',E16.8)         29       366 FORMAT (16X,'OMGA=',E16.8,'W=',E16.8,'TAU=',E16.8)         30       367 FORMAT (/16X,'TIME',5X,'RX',9X,'RY',9X,'RZ',9X,'R',10X,'H')         31       368 FORMAT (25X,'VX',9X,'VY',9X,'VZ',9X,'VZ',9X,'RZ',9X,'R',10X,'H')         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         34       READ (5,300) A,E,I,BETA1,BETA2,BETA3         35       READ (5,301) C2,N,DT	18	375	FORMAT (36X, SPHEROIDAL SOLUTION)
20       351 FORMAT (/16X,*TIME*, 3X,*K*, 3X,*K*, 3X,*K*, 3X,*K*, 3X,*K*, 10X,*H*,         21       358 FORMAT (25X,*VX*, 9X,*VY*, 9X,*K*, 3X,*K*, 3X,*K*, 10X,*H*,         22       359 FORMAT (25X,*VX*, 9X,*VY*, 9X,*VZ*, 9X,*V*, 10X,*F**)         22       359 FORMAT (16X,60(1H_))         23       360 FORMAT (16X,F4.1,5(1X,F10.6))         24       361 FORMAT (20X,5(1X,F10.6)/)         25       362 FORMAT (37X,*SPHERICAL SOLUTION*)         26       363 FORMAT (37X,*SPHERICAL SOLUTION*)         26       363 FORMAT (16X,*THE SPHERICAL ELEMENTS ARE*)         28       365 FORMAT (16X,*AS=*,E16.8,*ES=*,E16.8,*IS=*,E16.8)         29       366 FORMAT (16X,*OMGA=*,E16.8,*W=*,E16.8,*TAU=*,E16.8)         30       367 FORMAT (/16X,*TIME*,5X,*RX*,9X,*RY*,9X,*RZ*,9X,*R*,10X,*H*)         31       368 FORMAT (25X,*VX*,9X,*VY*,9X,*RY*,9X,*RY*,9X,*RZ*,9X,*R*,10X,*H*)         31       368 FORMAT (25X,*VX*,9X,*VY*,9X,*VZ*,9X,*V*,9X,*RZ*,9X,*R*,10X,*H*)         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         34       READ (5,300) A,E,I,BETA1,BETA2,BETA3         35       READ (5,301) C2,N,DT	20	267	) FURMAT (/)(V ITTNET EV TOVE OV TOVE OV TOTT OV TOT TOV TOVEL)
22       350 FORMAT (162,40 (A (34,40)))         23       360 FORMAT (16X,60(1H_))         24       361 FORMAT (16X,F4.1,5(1X,F10.6))         25       362 FORMAT (20X,5(1X,F10.6)/)         26       363 FORMAT (37X, 'SPHERICAL SOLUTION')         26       363 FORMAT (37X,18(1H_))         27       364 FORMAT (/16X, 'THE SPHERICAL ELEMENTS ARE')         28       365 FORMAT (18X, 'AS=',E16.8, 'ES=',E16.8, 'IS=',E16.8)         29       366 FORMAT (16X, 'OMGA=',E16.8, 'W=',E16.8, 'TAU=',E16.8)         30       367 FORMAT (/16X, 'TIME',5X, 'RX',9X, 'RY',9X, 'RZ',9X, 'R',10X, 'H')         31       368 FORMAT (/16X, 'TIME',5X, 'RX',9X, 'RY',9X, 'RZ',9X, 'R',10X, 'H')         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         34       READ (5,300) A,E,I,BETA1,BETA2,BETA3         35       READ (5,301) C2,N,DT	20	350	- FORMAT (710A) IIME 10A) KA 97A) KI 97A) KE 10A, K 10A, K 10A, TA*I 8 FORMAT (75%, 1041, 04, 1041, 04, 1041, 04, 1041, 104, 104
23       360       FORMAT (16X,F4.1,5(1X,F10.6))         24       361       FORMAT (20X,5(1X,F10.6)/)         25       362       FORMAT (37X, 'SPHERICAL SOLUTION')         26       363       FORMAT (37X,18(1H_))         27       364       FORMAT (16X, 'THE SPHERICAL ELEMENTS ARE')         28       365       FORMAT (18X, 'AS=',E16.8, 'ES=',E16.8, 'IS=',E16.8)         29       366       FORMAT (16X, 'OMGA=',E16.8, 'W=',E16.8, 'TAU=',E16.8)         30       367       FORMAT (/16X, 'TIME',5X, 'RX',9X, 'RY',9X, 'RZ',9X, 'R',10X,'H')         31       368       FORMAT (/25X,'VX',9X,'VY',9X,'VZ',9X,'V',10X,'F')         32       READ (5,321)       NTRAJ         33       D0       999         34       READ (5,300)       A,E,I,BETA1,BETA2,BETA3         35       READ (5,301)       C2,N,DT	22	350	$= \left[ - \left[ $
24       361 FORMAT (20X,5(1X,F10.6)/)         25       362 FORMAT (37X, 'SPHERICAL SOLUTION')         26       363 FORMAT (37X,18(1H_))         27       364 FORMAT (/16X, 'THE SPHERICAL ELEMENTS ARE')         28       365 FORMAT (18X, 'AS=',E16.8, 'ES=',E16.8, 'IS=',E16.8)         29       366 FORMAT (16X, 'OMGA=',E16.8, 'W=',E16.8, 'TAU=',E16.8)         30       367 FORMAT (/16X, 'TIME',5X, 'RX',9X, 'RY',9X, 'RZ',9X, 'R',10X, 'H')         31       368 FORMAT (25X, 'VX',9X, 'VY',9X, 'VZ',9X, 'V',10X, 'F')         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         34       READ (5,300) A,E,I,BETA1,BETA2,BETA3         35       READ (5,301) C2,N,DT	23	360	FORMAT (16X-F4-1-5(1X-F10-6))
25       362 FORMAT (37X, 'SPHERICAL SOLUTION')         26       363 FORMAT (37X, 18(1H_))         27       364 FORMAT (/16X, 'THE SPHERICAL ELEMENTS ARE')         28       365 FORMAT (18X, 'AS=',E16.8, 'ES=',E16.8, 'IS=',E16.8)         29       366 FORMAT (16X, 'OMGA=',E16.8, 'W=',E16.8, 'TAU=',E16.8)         30       367 FORMAT (/16X, 'TIME',5X, 'RX',9X, 'RY',9X, 'RZ',9X, 'R',10X, 'H')         31       368 FORMAT (/25X, 'VX',9X, 'VY',9X, 'VZ',9X, 'V',10X, 'F')         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         34       READ (5,300) A,E,I,BETA1,BETA2,BETA3         35       READ (5,301) C2,N,DT	24	361	FORMAT (20X,5(1X,F10,6)/)
26       363 FORMAT (37X,18(1H_))         27       364 FORMAT (/16X,*THE SPHERICAL ELEMENTS ARE*)         28       365 FORMAT (18X,*AS=*,E16.8,*ES=*,E16.8,*IS=*,E16.8)         29       366 FORMAT (16X,*OMGA=*,E16.8,*W=*,E16.8,*TAU=*,E16.8)         30       367 FORMAT (/16X,*TIME*,5X,*RX*,9X,*RY*,9X,*RZ*,9X,*R*,10X,*H*)         31       368 FORMAT (/25X,*VX*,9X,*VY*,9X,*VZ*,9X,*V*,10X,*F*)         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         24       READ (5,300) A,E,I,BETA1,BETA2,BETA3         35       READ (5,301) C2,N,DT	25	362	FORMAT (37X, SPHERICAL SOLUTION)
27       364 FORMAT (/16X, *THE SPHERICAL ELEMENTS ARE*)         28       365 FORMAT (18X, *AS=*,E16.8, *ES=*,E16.8, *IS=*,E16.8)         29       366 FORMAT (16X, *OMGA=*,E16.8, *W=*,E16.8, *TAU=*,E16.8)         30       367 FORMAT (/16X, *TIME*,5X, *RX*,9X, *RY*,9X, *RZ*,9X, *R*,10X, *H*)         31       368 FORMAT (/25X, *VX*,9X, *VY*,9X, *VZ*,9X, *V*,10X, *F*)         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         24       READ (5,300) A, E, I, BETA1, BETA2, BETA3         35       READ (5,301) C2,N,DT	26	363	FORMAT (37X,18(1H_))
28       365 FORMAT (18X, *AS= *,E16.8, *ES=*,E16.8, *IS=*,E16.8)         29       366 FORMAT (16X, *OMGA=*,E16.8, *W=*,E16.8, *TAU=*,E16.8)         30       367 FORMAT (/16X, *TIME*,5X, *RX*,9X, *RY*,9X, *RZ*,9X, *R*,10X, *H*)         31       368 FORMAT (25X, *VX*,9X, *VY*,9X, *VZ*,9X, *V*,10X, *F*)         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         C       START OF SPHEROIDAL SOLUTION         34       READ (5,300) A, E, I, BETA1, BETA2, BETA3         35       READ (5,301) C2,N,DT	27	364	FORMAT (/16X, THE SPHERICAL ELEMENTS ARE)
29       366 FORMAT (16X, *OMGA=*,E16.8,*W=*,E16.8,*TAU=*,E16.8)         30       367 FORMAT (/16X,*TIME*,5X,*RX*,9X,*RY*,9X,*RZ*,9X,*R*,10X,*H*)         31       368 FORMAT (25X,*VX*,9X,*VY*,9X,*VZ*,9X,*V*,10X,*F*)         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1,NTRAJ         C       START OF SPHEROIDAL SOLUTION         34       READ (5,300) A,E,I,BETA1,BETA2,BETA3         35       READ (5,301) C2,N,DT	28	365	5 FORMAT (18X, "AS=",E16.8, "ES=",E16.8," IS=",E16.8)
30       367       FURMAT (/16X, *TIME*,5X, *RX*,9X, *RY*,9X, *RZ*,9X, *R*,10X,*H*)         31       368       FORMAT (25X, *VX*,9X, *VY*,9X, *VZ*,9X, *V*,10X,*F*)         32       READ (5,321)       NTRAJ         33       D0       999       NTRA=1,NTRAJ         C       START OF SPHEROIDAL SOLUTION         34       READ (5,300)       A,E,I,BETA1,BETA2,BETA3         35       READ (5,301)       C2,N,DT	29	366	• FORMAT (16X, "OMGA=", E16.8, " W=", E16.8, "TAU=", E16.8)
31       308       FUKMAI (25X, VX, 9X, VY, 9X, VZ, 9X, VV, 10X, F)         32       READ (5,321) NTRAJ         33       D0 999 NTRA=1, NTRAJ         C       START OF SPHEROIDAL SOLUTION         34       READ (5,300) A, E, I, BETA1, BETA2, BETA3         35       READ (5,301) C2, N, DT	30	367	FORMAT (/16x, 'IIME', 5X, 'RX', 9X, 'RY', 9X, 'RZ', 9X, 'R', 10X, 'H')
32       NEAU (2, 521) NEAJ         33       D0 999 NTRA=1,NTRAJ         C       START OF SPHEROIDAL SOLUTION         34       READ (5, 300) A, E, I, BETA1, BETA2, BETA3         35       READ (5, 301) C2, N, DT	.51	308	) FUKMAI 120%9'VX'9Y%9'YYY9Y%9'YZ9YX9'V'910%9'F') DEAD 45 2211 NTDAI
C START OF SPHEROIDAL SOLUTION 34 READ (5,300) A,E,I,BETA1,BETA2,BETA3 35 READ (5,301) C2,N,DT	22		NEAU 1293213 NIKAJ Na 999 NTPA=1.NTPAI
34         READ (5,300) A,E,I,BETA1,BETA2,BETA3           35         READ (5,301) C2,N,DT		с	START OF SPHEROIDAL SOLUTION
35 READ (5, 301) C2, N, DT	34	-	READ (5,300) A.E.I.BETA1.BETA2.BETA3
	35		READ (5,301) C2,N,DT

36		WRITE (6,350) NTRA
37		WRITE (6,351)
38		WRITE (6,352) C2
39		WRITE (6,353) A,E,I
40		WRITE (6,354) BETA1,BETA2,BETA3
41		WRITE (6,355)
47		WRITE (6,356)
43		WRITE (6,357)
44		WRITE (6,358)
47		WRIIE (6,359)
40		NUU=51N(1)
47		NUUZ=NUU##2
40		
50		
51		F= A+A Z RE=1 A + D+C 2 + + ( A + D+C 2 + NUA 2 ) + 4 A + + 2 ) + C 2 + NUA 2
52		
53		$AF = \{-2, 0 \times 1 \times$
54		RF=(2*NIIO2*NE/DE
55		$NU22 = -(C2 \times DE)/(A \times P \times NE)$
56		BS1=-AF/2.0
57		BS2=SORT(BE)
58		AO=A-BS1
59		PC = (C2*(1.0-NUC2)+A*P*NE/DE)/AO
60		ALPHA2=SQRT(PO)
61		ALPHA3=ALPHA2*COS(I)*SQRT(1.0+C2*NU02/(A0*P0))
62		N2=ABS(NU02*NU22)
63		P2=P**2
64		P3=P**3
65		P4=P**4
66		ALPH2=ALPHA2*SQRT(1.0-C2*(1.0-NU02)/(A0*P0))
67		LAMB=BS1/BS2
	C	CALCULATION OF LEGENDRE POLYNOMIALS, PL(N)
68		PL(1) = 1.0
69 70		PL(2)=LAMB
70		UU 401 K=3.11
71		
12	4.01	PL(K]=((2*J-1)*LAMB*PL(K-1)+(J-1)*PL(K-2))/J CONTINUE
15	c 701	
74	C	T(1)=1 0
75		T(2)=1.0
76		$T(3) = (3, 0+x^2)/2, 0$
77		D0 402 K = 4.11
78		J=K-1
79		T(K) = ((2*J-1)*T(K-1)+(J-1)*X2*T(K-2))/J
80	402	CONTINUE
81		22=BS2/P
82		73=C2/(P**2)
	С	CALCULATION OF A1
83		A1=P*X*(Z2**2)*PL(3)
84		DO 403 J=3,10
85		DA1=P*X*(Z2**J)*PL(J+1)*T(J-1)
86		A1=A1+DA1
87		IF (ABS(DA1/A1) .LT0000001) GD TD 404

```
88
         403 CONTINUE
 89
             WRITE (6,307)
 90
         404 CONTINUE
      С
                     CALCULATION OF A2
 91
             A2=X/P
 92
             DO 405 J=1,10
 93
             D42=(X/P)*(Z2**J)*PL(J+1)*T(J+1)
 94
             A2=A2+DA2
 95
             IF (ABS(DA2/A2) .LT. .0000001) GD TO 406
 96
         405 CONTINUE
 97
             WRITE (6,308)
 98
         406 CONTINUE
      С
                     CALCULATION OF D(N)
 99
             D(1) = 1.0
             D(2)=Z2*LAMB
100
101
             FAC=Z2
102
             DO 407 K=3,9
103
             FAC=Z2*FAC
104
             D(K)=-Z3*D(K-2)+PL(K)*FAC
105
        407 CONTINUE
      С
                     CALCULATION OF A3
106
             43=X*T(3)/P3
107
            DO 408 K=2,9
108
             DA3=X*D(K)*T(K+2)/P3
109
             A3=A3+DA3
110
             IF (ABS(DA3/A3) .LT. .0000001) GO TO 409
111
        408 CONTINUE
112
            WRITE (6,309)
113
        409 CONTINUE
      С
                     CALCULATION OF B1 PRIME AND B2
114
            B1P=.5-3.0*N2/16.0+15.0*N2**2/128.0
115
            B2=1.0-N2/4.0+9.0*N2**2/64.0
                     CALCULATION OF THE GAMMAS AND B3
      С
116
            G2=3.0*NU02/16.0
117
            G3=5.0*(3.0*NU02/4.0+1.0)*'\U02/32.0
118
            G4=35.0*((5.0*NU02/8.0+.75)*NU02+1.0)*NU02/256.0
            G5=63.0*(({35.0*NU02/64.0+5.0/8.0}*NU02+.75}*NU02+1.0)*NU02/512.0
119
120
            B3=1.0-1.0/SQRT(1.0-NU22)-G2*NU22**2-G3*NU22**3-G4*NU22**4-G5*
           1NU22**5
      С
                    CALCULATION OF THE A(IJ)
121
            BF2=BF**2
122
            BS12=BS1**2
123
            E2=E**2
124
            A11=(.75*X*E/P3)*(-2.0*BS1*BF*P+BF2)
125
            A12=3.0*X*BF2*E2/(32.0*P3)
            A21=(X*E/P)*(BS1/P+(3.0*BS12-BF)/P2-4.5*BS1*BF*(1.0+E2/4.0)/P3
126
           1+3.0*BF2*(4.0+3.0*E2)/(8.0*P4))
            A22=(X*E2/P)*((3.0*BS12-BF)/(8.0*P2)-9.C*BS1*BF/(8.0*P3)
127
           1+3.0*BF2*(3.0+E2/2.0)/(16.0*P4))
128
            A23=(X*E2*E/(8.0*P4))*(-BS1*BF+BF2/P)
129
            A24=3.0*BF2*E2**2/(256.0*P3*P2)
130
            Z5=(BF/2.0+C2)/P2
            E3=E**3
131
132
            E4=E2**2
            A31=(X*E/P3)*(2.0+BS1*(3.0 _+.75*E2)/P-Z5*(4.0+3.0*E2))
133
```

```
134
             # 32=(X/P3)*(E2/4.0+BS1*.75*E2/P-Z5*(1.5*E2+E4/4.0))
135
             A33=(X/P3)*(BS1*E3/(12.0*P)-Z5*E3/3.0)
136
             A34=(X/P3)*(-Z5*E4/32.0)
137
             Z1=SQRT(A0)
138
             TIME=0.0
      С
                     CALCULATIONS FOR EACH TIME STEP
139
             DO 498 L=1,N
140
             M=(TIME+BETA1)/(Z1*A)
      С
                     SOLVING KEPLERS EQUATION
141
             INDEX=0
142
             IF (ABS(M) .GT. 1.0) GO TO 452
143
             H0=M
144
         453 MN=E*SINH(H0)-H0
145
             INDEX=INDEX+1
146
             DELT=(M-MN)/(E*COSH(HO)-1.0)
147
             IF (ABS(DELT) .LT. .000001) GO TO 454
IF (INDEX .GT. 20) GO TO 457
148
149
             IF (ABS(DELT) .GT. ABS(HO)) GO TO 455
150
         456 H0=H0+DELT
151
             GO TO 453
152
         452 Z=ALOG(ABS(M)*2.0/E)
153
             HO=SIGN(Z,M)
154
             GO TO 453
155
        455 DELT=DELT*ABS(H0)/ABS(DELT)
156
             GO TO 456
157
        457 WRITE (6,310)
158
        454 H0=H0+DELT
159
             F0=2.0*ATAN(SQRT((E+1.0)/(E-1.0))*TANH(H0/2.0))
160
             PSIO=ALPH2*(BETA2/ALPHA2+Z1*A2*F0)/B2
161
            H1P=((C2*NUO2)*(-B1P*PSIO+.25*SIN(2.0*PSIO))/(Z1*ALPH2)
           1-BS1*H0-A1*F0)/(A*(E*COSH(H0)-1.0))
162
             H1=H1P*(1.0-H1P*E*SINH(H0)/(2.0*(E*COSH(H0)-1.0)))
             F1=2.0*ATAN(SQRT((E+1.0)/(E-1.0))*TANH((H0+H1)/2.0))-F0
163
164
            PSI1=-N2*SIN(2.0*PSI0)/(8.0*B2)+(Z1*ALPH2/B2)*(A2*F1+A21*SIN(F0)
            1+A22*SIN(2.0*F0))
            H2=(-BS1*H1-A1*F1-A11*SIN(F0)-A12*SIN(2.0*F0)+(C2*NUC2)/(Z1*ALPH2)
165
           1*(-B1P*PSI1+PSI1*COS(2.0*PSI0)/2.0-N2*SIN(2.0*PSI0)/8.0
           1+N2*SIN(4.0*PSIO)/64.0))/(A*(E*COSH(HO)-1.0))
166
            H=H0+H1+H2
167
            F=2.0*ATAN(SQRT((E+1.0)/(E-1.0))*TANH(H/2.0))
168
            F2=F-F0-F1
            PSI2= (-N2*PSI1*COS(2.0*PSI0)/4.0+3.0*(N2**2)*SIN(2.0*PSI0)/32.0
169
           1-3.0*(N2**2)*SIN(4.0*PSI0)/256.0+ALPH2*Z1*(A2*F2+A21*F1*CDS(F0))
           1+A22*2.0*F1*COS(2.0*F0)+A23*SIN(3.0*F0)+A24*SIN(4.0*F0)))/B2
170
            PSI=PSI0+PSI1+PSI2
171
            RHD=A*(E*COSH(H)-1.0)
172
            NU=NUO*SIN(PSI)
173
            Z6=A31*SIN(F)+A32*SIN(2.0*F)+A33*SIN(3.0*F)+A34*SIN(4.0*F)
174
            OMGAP=BETA3+ALPHA3/ALPH2*(B3*PSI+3.0*NU02*(NU22**2)*SIN(2.0*
           1PSI)/32.0)-C2*ALPHA3*Z1*(A3*F+Z6)
      C
                     THE POSITION AND VELOCITY VECTORS
175
            RX=SQRT(RHD**2+C2)*(COS(PSI)*COS(OMGAP)
           1-COS(I)*SIN(PSI)*SIN(OMGAP))
176
            RY=SQRT(RHO**2+C2)*(COS(I)*SIN(PSI)*COS(OMGAP)
           1+SIN(OMGAP)*COS(PSI))
```

177	RZ=RHO*NU
178	
179	$RHDDT = (RHDx + 2) \times F + STN(F) \times F + F + T + D$
180	
191	77-72-74C+72-34C+11-0+N2+(51N1P51)7**2)/(KHJ**2+(2*(NJ**2))
101	27=A31=CUS(F)+2.0=A32=CUS(2.0=F)+3.0=A33=CUS(3.0=F)
	1+4•0*A34*COS(4•0*F)
182	OMGADT=ALPHA3*PSIDT/ALPH2*(B3+3.0*NUO2*(NU22**2)*
	1COS(2.0*PSI)/16.0)-C2*ALPHA3*Z1*(A3+Z7)*FDT
183	VX = RHO = RHODT = RX / (RHO = 2 + C2) = OMGADT = RY + SORT (RHO = 2 + C2) + (-STN (DST))
	1*COS(OMGAP) = COS(I)*COS(PSI)*SIN(OMCAP))*PSIDT
194	
/	1*SIN(DRCAD)*COS(1)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS(2)*COS
195	
105	
100	K=SQR1 (KX**2+RY**2+RZ**2)
187	V= SQR T ( VX ** 2+VY ** 2+VZ ** 2 )
188	IF (L .GT. 1) GD TO 459
189	ROX=RX
190	ROY=RY
191	ROZ=RZ
192	
193	
194	
105	
104	
190	WRITE (6,360) TIME, RX, RY, RZ, R, H
197	WRITE (6,361) VX,VY,VZ,V,F
198	TIME=TIME+DT
199	498 CONTINUE
	C CALCULATION OF SPHERICAL ELEMENTS
	C BEWARE OF I=O IN CALC OF OMGA AND W
200	WRITE (6.362)
201	WRITE (6.363)
20.2	
203	
204	
204	
205	VII= SQR1 (VI)2)
200	AS=1.07(V02-2.07RO)
207	HX=ROY*VOZ-ROZ*VOY
208	HY=ROZ*VOX-ROX*VOZ
209	HZ=R0X*V0Y-R0Y*V0X
210	H=SQRT(HX**2+HY**2+HZ**2)
211	
212	FS = SORT((H + 2/RO - 1, 0) + 2 + (H + N))M(2/RO ) + 2)
213	
214	
215	
217	
210	
217	
218	
219	I N X= -H Y / SQR T ( H X * 2 + H Y * * 2 )
2 20	INY=HX/SQRT(HX**2+HY**2)
221	OMGA=ARCOS(INX)
222	$Z = INX \star IZ X + INY \star IZY$
223	IE (ABS(7) .GE. 1.0) GD TD 207
224	
225	

•

226		207	W=0_0
220		201	
221		200	
220			X=SQR1(ES##2-1.0)#SIN(F0)/(1.0+ES#C0S(F0))
224			Y=X+SQRI(X**2+1.0)
230			HO=ALCG(Y)
231			TAU=SQRT(AS**3)*(HO-ES*SINH(HO))
232			TIME=0.0
233			WRITE (6,365) AS,ES,IS
234			WRITE (6,366) OMGA,W,TAU
235			WRITE (6,367)
236			WRITE (6.368)
237			WRITE (6.359)
238			WRITE (6.36C) TIME. ROX. ROY. ROZ. RO. HO
239			WRITE (6.361) VOX-VOX-VOZ-VO.ED
2.,,,	c		CALCHATION OF D AND V FOD ANY T
240	0		DO 201 1-2 N
240			DU ZUI JEZYN
241	~		
	L		SULVING KEPLERS EQUATION
242			INDEX=0
243			M = (TIME - TAU) / SQRT(AS * * 3)
244			IF (ABS(M) .GT. 1.0) GO TO 202
245			HYP=M
246		203	MN=ES*SINH(HYP)-HYP
247			INDEX=INDEX+1
248			DELT=(M-MN)/(ES*COSH(HYP)-1.0)
249			IF (ABS(DELT) .LT000001) GD TD 204
250			IF (INDEX .GT. 20) GO TO 217
251			IF (ABS(DELT) .GT. ABS(HYP)) GO TO 205
252		206	HYP=HYP+DF1 T
253		200	60 TO 203
254		202	$7=\Delta I \cap G(\Delta BS(M) * 2 \cdot O/ES)$
255		202	
256			
250		205	
201		205	DELI=DELI#ADS(HTP)/ADS(DELI)
228		~ • • •	
279		211	
260		204	HYP=HYP+DELI
261			NUM5 = 1.0 - AS * (COSH (HYP-HO) - 1.0) / RO
262			NUM6 = TIME - (SINH(HYP-HO) - (HYP-HO)) * SQRT(AS * * 3)
263			RX=NUM5*ROX+NUM6*VOX
264			RY=NUM5*ROY+NUM6*VOY
265			RZ=NUM5*ROZ+NUM6*VOZ
266			R=SQRT(RX**2+RY**2+RZ**2)
267			NUM7=-SQRT(AS)*SINH(HYP-HO)/(R*RO)
268			NUM8=1.0-AS*(COSH(HYP-HO)-1.0)/R
269			VX=NUM7*ROX+NUM8*VOX
270			VY=NUM7*R0Y+NUM8*V0Y
271			V7=NUM7*R07+NUM8*V07
272			V=SQRT(VX**2+VY**2+V7**2)
273			F=2.0*ATAN(SQRT((FS+1.0)/(FS-1.0))*TANH(HYP/2.0))
274			WRITE (6.360) TIME-RX-RY-R7-R-HYP
275			WRITE (6.361) VX.VY.V7.V.E
276		201	
277		C00	CONTINUE
211		777	
210			

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