

RESPONSE OF AN ELASTIC LAYER OVER AN
ELASTIC HALF-SPACE TO A POINT SOURCE

by

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ABSTRACT

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Submitted to the Department of Earth and Planetary
Sciences on June 4, 1970 in partial fulfillment of
the requirements for the degree of Master of Science

Synthetic seismograms are computed for a point source of compressional (P) or poloidal (SV) waves embedded within an elastic layer overlying an elastic half-space. A fast method which utilizes an approximation in Cagniard-de-Hoop technique is used in computation. The results are accurate for short ranges and low frequencies. A computer program evaluates the solution and plots the synthetic seismogram. These results are then compared with solutions to Lamb's problem and the one layer problem computed by the exact method. The comparisons are good.

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Title: Associate Professor of Geophysics

ACKNOWLEDGEMENT

I would like to extend my sincere thanks to Professor Don Helmberger for his assistance and support in formulating and programming this problem. I would also like to thank Professor M. Nafi Toksöz for many fruitful discussions.

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INTRODUCTION

In this paper, a method is presented by which synthetic seismograms for a layer over a half-space can be computed. The method can be easily extended to more complicated models. It has the advantages of requiring little computer time, and being accurate for low as well as high frequencies. In the formulation the generalized ray approach, and the Cagniard-de-Hoop method are utilized to put the solutions into operational form. An improvement is made on the "high frequency approximation" (see Helmberger, 1967) to achieve accurate results for low frequencies. The computations are done for both compressional and shear sources. Plots are shown displaying the effects of combining the two sources.

Low frequency body waves are less affected by inhomogeneities in the crust than are those with high frequencies. They are not as sensitive to irregularities in the vicinity of the receiver. Long period seismograms are thus "cleaner", and give less distorted information about gross properties of the crust, and about the source of the waves. It is therefore important to be able to synthesize long period records quickly.

Many sources of seismic activity produce P and S waves simultaneously. The records obtained from that activity contain the responses to both source types. In order to interpret the records correctly, the effects must be distinguished. It is for this reason that we included both P and SV sources in this study. A source of SH waves could be

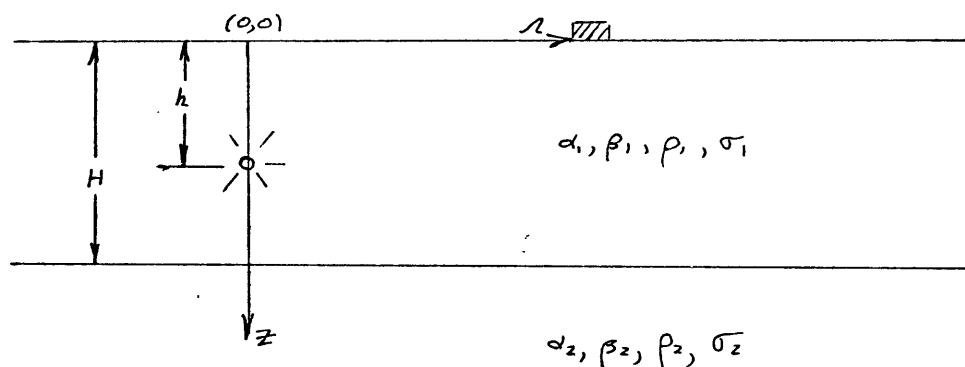
added also, but was not because SH waves do not interact with P and SV waves.

Harkrider (1964) has presented a method to compute surface wave records at long distances. Helmberger (1965) has shown how to compute quickly high frequency records for long ranges. The method presented here is valid for high and low frequencies and short ranges. It can also be used for long ranges, but the surface wave response must be forfeited. However, long period body wave records are calculable at long ranges by this method.

In the next section we introduce the mathematics and the approximation used to bring the solution to operational form. The computer results and their implications are discussed in the third section. We have displayed the computer output following that discussion. A brief description of the program and a printout are included as an appendix.

THEORETICAL FORMULATION

A homogeneous, isotropic, linearly elastic slab of thickness H and infinite horizontal extent overlies a semi-infinite solid with different elastic properties. A point source of compressional (P) and poloidal (SV) waves is embedded within the slab a distance h from its upper surface. The upper surface is stress free. The layer and the half-space are welded together so that pressure and displacement are continuous across the interface. The problem will be formulated in circular cylindrical coordinates with the origin at the upper surface directly above the source. All variables are independent of the azimuthal coordinate.



We wish to compute the response at the surface. This is done by solving the linearized elastic wave equation by Laplace transform methods. The solution is then represented as an infinite sum of contributions from ray paths across

the layer. Inversion is accomplished by Cagniard-de-Hoop techniques. The details of this approach have been displayed by several authors (Helmberger, 1967, and Phinney, 1965), as well as in Appendix I and will not be included in this section.

The once-transformed (in time) displacement for the n^{th} generalized ray from a step function source can be written

$$(1) \quad \bar{u}_{z,n}(r, \theta, z) = \alpha \, c \, \ln \int_0^{\infty} p F_{z,n}(p) K_0(\alpha p r) e^{-\alpha g_n(p)} dp$$

$$(2) \quad \bar{u}_{r,n}(r, \theta, z) = \alpha \, c \, \ln \int_0^{\infty} p F_{r,n}(p) K_1(\alpha p r) e^{-\alpha g_n(p)} dp$$

The subscript z refers to the vertical component, r refers to the radial component. $K_0(\alpha p r)$ and $K_1(\alpha p r)$ are modified Bessel functions. The functions $F_{z,n}$, $F_{r,n}$, and g_n are defined as follows:

$$F_{n,z}(p) = S R_z(p) C_n(p)$$

$$F_{n,r}(p) = S R_r(p) C_n(p)$$

where

$$S = [2\pi^2 \gamma_1 (\lambda_1 + 2\mu_1)]^{-1} \quad \text{for P source}$$

$$S = [2\pi^2 \gamma_1' \mu_1]^{-1} \quad \text{for SV source}$$

with

$$\eta_1 = \left(\frac{1}{\alpha_1^2} - p^2 \right)^{1/2}$$

$$\eta_1' = \left(\frac{1}{\beta_1^2} - p^2 \right)^{1/2}$$

α_1 and β_1 are the P and S wave speeds in the slab, respectively. $Q_2(p)$ and $Q_n(p)$ are the receiver directivity functions which contain the response of the free surface due to an impinging P or SV wave. They are written out explicitly in the appendix. $L_n(p)$ is the reflection function for the n^{th} generalized ray. It is formed from the product of the reflection coefficients due to internal reflections within the layer. The reflection coefficients are also written out in the appendix. Finally, the function $g_n(p)$ is a measure of the time required to traverse vertically the n^{th} ray path.

$$g_n(p) = (1 - HK_{ud}) \left[(1 - K_{sp}) \eta_1' + K_{sp} \eta_1 \right] + l_s^{(n)} \eta_1' H + l_p^{(n)} \eta_1 H$$

$$Q_n \cdot g_n(p) = (1 - HK_{ud} - h) \left[(1 - K_{sp}) \eta_1' + K_{sp} \eta_1 \right] + l_s^{(n)} \eta_1' H + l_p^{(n)} \eta_1 H$$

where

$$K_{ud} = \begin{cases} 1 & \text{if, at the source, the ray is directed upward.} \\ 0 & \text{if, at the source, the ray is directed downward.} \end{cases}$$

$$K_{sp} = \begin{cases} 1 & \text{if the source emits P waves.} \\ 0 & \text{if the source emits S waves.} \end{cases}$$

and $l_s^{(n)}$ is the number of times the n^{th} ray path traverses the layer as an SV wave, and $l_p^{(n)}$ is the number of traverses as a P wave.

We have two approaches from which to choose in evaluating equations (1) and (2). The first is to invert the

expressions analytically and evaluate the result. This is done with the Laplace inversion formulas

$$\mathcal{L}^{-1}\{K_0(\rho r) e^{-\rho g_n}\} = \frac{\mathcal{H}(t - pr - g_n)}{[(t - g_n)^2 - p^2 r^2]^{1/2}}$$

and

$$\mathcal{L}^{-1}\{K_1(\rho r) e^{-\rho g_n}\} = \frac{t - g_n}{pr} \cdot \frac{\mathcal{H}(t - pr - g_n)}{[(t - g_n)^2 - p^2 r^2]^{1/2}}$$

where \mathcal{H} is the Heaviside step function. The displacements then become

$$(3) \quad u_{z,n}(r, 0, t) = \frac{\partial}{\partial t} \operatorname{Re} \int_{t_0}^{t_1} \frac{\mathcal{H}(t - \tau)}{[(t - \tau)(t - \tau + pr)]^{1/2}} p F_{z,n}(p) dp$$

$$(4) \quad u_{r,n}(r, 0, t) = \frac{\partial}{\partial t} \operatorname{Re} \int_{t_0}^t \frac{(t - g_n) \mathcal{H}(t - \tau)}{r [(t - \tau)(t - \tau + pr)]^{1/2}} F_{r,n}(p) dp$$

where we have set $\tau = pr + g_n$ and t_0 is the time at the beginning of the signal.

Equations (3) and (4) can now be evaluated by numerical quadrature. $p(\tau)$ is computed from the requirement that the argument of the Heaviside function be real (thus giving the contour of integration). The author has done this for Lamb's problem (elastic half-space with a free surface), and Pekeris, et al (1965) has used this method for a layer over a half-space. This method is time consuming, however. Since the upper limit of integration is included in the integrand, an integration from t_0 must be performed for every value of the upper limit. In addition to its time requirements, this method has the disadvantage of requiring repeated integrations past a strong pole in the complex plane. This is a source of numerical instabilities.

↳ BRANCH POINT!
Repeated arrivals

Our second choice is to approximate the modified Bessel functions with their asymptotic expansions, and then invert the results. Expressions for the Bessel functions valid for large values of their argument (spr) are (Dwight, 1961):

$$(5) \quad K_0(spr) \approx \left(\frac{\pi}{2spr}\right)^{1/2} e^{-spr} \left[1 - \frac{1}{8}(spr)^{-1} + \frac{9}{128}(spr)^{-2} + \dots\right]$$

$$(6) \quad K_1(spr) \approx \left(\frac{\pi}{2spr}\right)^{1/2} e^{-spr} \left[1 + \frac{3}{8}(spr)^{-1} + \frac{3}{128}(spr)^{-2} + \dots\right]$$

Substituting these expressions into (1) and (2), we have

$$(7) \quad \bar{u}_{2,n}(r, 0, z) \approx \alpha \sqrt{\frac{\pi}{2}} \operatorname{clm} \int_0^{+\infty} p F_{2,n}(p) \frac{e^{-az}}{\sqrt{spr}} \left\{1 - \frac{1}{8}(spr)^{-1} + \frac{9}{128}(spr)^{-2} + \dots\right\} dp$$

$$(8) \quad \bar{u}_{1,n}(r, 0, z) \approx \alpha \sqrt{\frac{\pi}{2}} \operatorname{clm} \int_0^{+\infty} p F_{1,n}(p) \frac{e^{-az}}{\sqrt{spr}} \left\{1 + \frac{3}{8}(spr)^{-1} + \frac{3}{128}(spr)^{-2} + \dots\right\} dp$$

By making use of the following inversion formulas

$$\mathcal{L}^{-1} \left[s^{1/2} e^{-az} \bar{f}(s) \right] = \frac{\partial}{\partial t} \left[\frac{1}{\sqrt{\pi t}} * f(t) \right]$$

$$\mathcal{L}^{-1} \left[s^{-1/2} e^{-az} \bar{f}(s) \right] = \frac{\partial}{\partial t} \left\{ \frac{1}{\sqrt{\pi t}} * [\mathcal{H}(t) * f(t)] \right\}$$

$$\mathcal{L}^{-1} \left[s^{-3/2} e^{-az} \bar{f}(s) \right] = \frac{\partial}{\partial t} \left\{ \frac{1}{\sqrt{\pi t}} * [t * f(t)] \right\}$$

where $*$ denotes convolution, equations (7) and (8) are

$$(9) \quad u_{2,n}(r, 0, t) = \frac{1}{\sqrt{2}} \operatorname{clm} \frac{\partial}{\partial t} \left\{ \frac{1}{\sqrt{t}} * \left[\sqrt{\frac{p}{r}} F_{n,2}(p) \frac{dp}{dt} - \frac{1}{8} \mathcal{H}(t) * \left(\frac{1}{\sqrt{pr^3}} F_{n,2}(p) \frac{dp}{dt} \right) + \frac{9}{128} t * \left(p^{-3/2} r^{-3/2} F_{n,2}(p) \frac{dp}{dt} \right) \right] \right\}$$

$$\begin{aligned}
 u_{\eta, \alpha}(\alpha, \phi, t) = & \frac{1}{\sqrt{2}} \operatorname{ctn} \frac{\alpha}{2} \left\{ \frac{1}{\sqrt{t}} * \left[-\sqrt{\frac{t}{2}} F_{\eta, \alpha}(p) \frac{d\phi}{dt} - \frac{3}{8} \gamma(t) * \left(\frac{1}{\sqrt{p^3}} F_{\eta, \alpha}(p) \frac{d\phi}{dt} \right) + \right. \right. \\
 (10) \quad & \left. \left. + \frac{3}{128} t * \left(p^{-7/2} t^{-5/2} F_{\eta, \alpha}(p) \frac{d\phi}{dt} \right) \right] \right\}
 \end{aligned}$$

If we consider the lowest order term and do the inversion, we get the so-called high frequency approximation. As the name implies, this approximation is poor for low frequencies. It is also poor for short ranges. An improvement can be made by including terms that are higher order in $1/(\text{spr})$ in (9) and (10). Again, the contour of integration is computed by requiring that α be real, but now only one integration--a convolution--need be performed. This is considerably faster than the first alternative. We have done calculations employing this improved approximation, and present the results in the next section.

DISCUSSION OF RESULTS

The primary purpose of this investigation is to compute synthetic seismograms which have good low frequency response. Since surface waves have lower frequencies than body waves, they provide a means for testing. A program was already in existence which would compute exactly (i.e., by the first method of inversion described earlier) the response of a half-space to a buried compressional point source. A Rayleigh wave is produced at the surface by the impinging P wave. The approximate method was also used for this problem by allowing the program to consider only the ray which travels directly to the receiver with no internal reflections. The impulse response was convolved with a triangle whose base is 0.2 sec., and whose area is one (this applies to all the plots presented here). The results are shown in Figures 1-8 and the comparison appears good. In these calculations, the first two terms in the sums in equations (7) and (8) were used. It thus appears that two terms are sufficient. The displacement due to an SV source is also shown (Figures 9-12). The response begins with that part of the energy which has been refracted along the free surface as a P wave. The direct S arrives later and is followed soon by the Rayleigh wave.

The remaining models are layered. As a further test of our method, a comparison was made with the results of Pekeris, et al (1965), where they used the first inversion technique. The comparison is shown for two ranges and is seen to be

good (Figures 13-15, 21). The reader will notice that the record for the approximate program is shorter than the other. This is because ray theory characteristically diverges rapidly from the actual values at some time from the beginning of the record, and the plot was terminated where a strong drift began. The divergence normally occurs near the time of arrival of the interfacial trapped wave, and there is a pole on the real p axis which is responsible for the contribution of the interface wave. Since more reflection coefficients are involved in the calculation of the interface wave than for the Rayleigh wave, the effect of the pole is multiplied. If a sufficient number of rays are not evaluated in the vicinity of that value of p , the result will not converge on the true value. Pekeris, et al, (1965) used about five times the number of rays that we used, and although this many rays could have easily been included in our computations, the extra expense would not have enhanced our goal of showing the accuracy of our results. It is also interesting to note that the ratio $\frac{H-h}{r}$, the contour comes closer to the pole, and the seismogram diverges more rapidly.

This model (labeled Model I in Table 1) was embedded with an SV source also. The plots (Figures 17, 18, 23, 24) show a prominent Rayleigh wave following the direct S wave closely. For $r = 10$, the vertical displacement has a long quiet period preceding several large signals due to S-multiples and the Rayleigh wave.

Model I was used again with the source moved to within 0.05 km. of the surface. The expected growth of the Rayleigh wave with respect to the body waves for smaller values of $\frac{h}{r}$ occurred. These plots (Figures 29-34) were not labeled with the ray arrival times because the behaviour of the Rayleigh wave was the predominant feature.

The shear wave velocity in the layer was then lowered to 0.756. This raised Poisson's ratio to 0.3, making the layer less rigid. This is Model II. The P source record shows a much stronger P_3 arrival than Model I (Figure 35). For the S source, there is an additional peak near the direct S arrival due to the beginnings of the interface wave (Figure 37). The arrival times are marked on the plots so that the reader may make further comparisons.

Model III was constructed by changing Poisson's ratio to 0.35 in both the layer and the half-space (Figures 41-48). The response to the S source is changed little. For the P source, the amplitude of the Rayleigh wave is diminished. The effect of P_3 and P_4 is increased and the downward spike due to P_2S is enlarged by the changes in Poisson's ratio.

In Figures 27, 28, 47, and 48 the amplitude of the shear source is multiplied by 0.2 to show the effect of changing the ratio of P to S source strengths. Compare these with Figures 25, 26, 45, and 46 respectively (where there has been no multiplication).

In all the calculations done here, the Rayleigh wave amplitude is greater for an S source than for a P source.

It would seem that an SV source is a more efficient generator of Rayleigh waves. Mathematically, this occurs because the contour path lies closer to the real axis for the direct S wave than for the P wave.

TABLE 1

Models used for computation

The models referred to in the text are the following (velocities in km/sec, and densities in gm/cc). The parameters were not chosen to represent real earth values, but to use in comparing with existing calculations.

Model I

$$\alpha_1 = 1.73, \quad \beta_1 = 1.00, \quad \rho_1 = 1.00, \quad \sigma_1 = 0.25$$

$$\alpha_2 = 1.90, \quad \beta_2 = 1.10, \quad \rho_2 = 1.65, \quad \sigma_2 = 0.25$$

Model II

$$\alpha_1 = 1.73, \quad \beta_1 = 0.76, \quad \rho_1 = 1.17, \quad \sigma_1 = 0.30$$

$$\alpha_2 = 1.90, \quad \beta_2 = 1.10, \quad \rho_2 = 1.65, \quad \sigma_2 = 0.25$$

Model III

$$\alpha_1 = 2.16, \quad \beta_1 = 1.00, \quad \rho_1 = 1.00, \quad \sigma_1 = 0.35$$

$$\alpha_2 = 2.29, \quad \beta_2 = 1.10, \quad \rho_2 = 1.65, \quad \sigma_2 = 0.35$$

In all these cases, the thickness H of the layer is one (1.) km. Unless otherwise noted, the source depth is 0.5 km.

COMPUTER PLOTS

In the figure captions, the first entry refers to the component (r or z), the second to the range, the third to the model (I, II, or III), and the fourth to the source type (P, S or C for the combination of P and S). The P and S source strengths are equal unless otherwise noted. The source depth is 0.5 km unless otherwise noted. The letters P, S, PS, etc. refer to the arrival times of rays with specified number of multiple reflections in the layer.

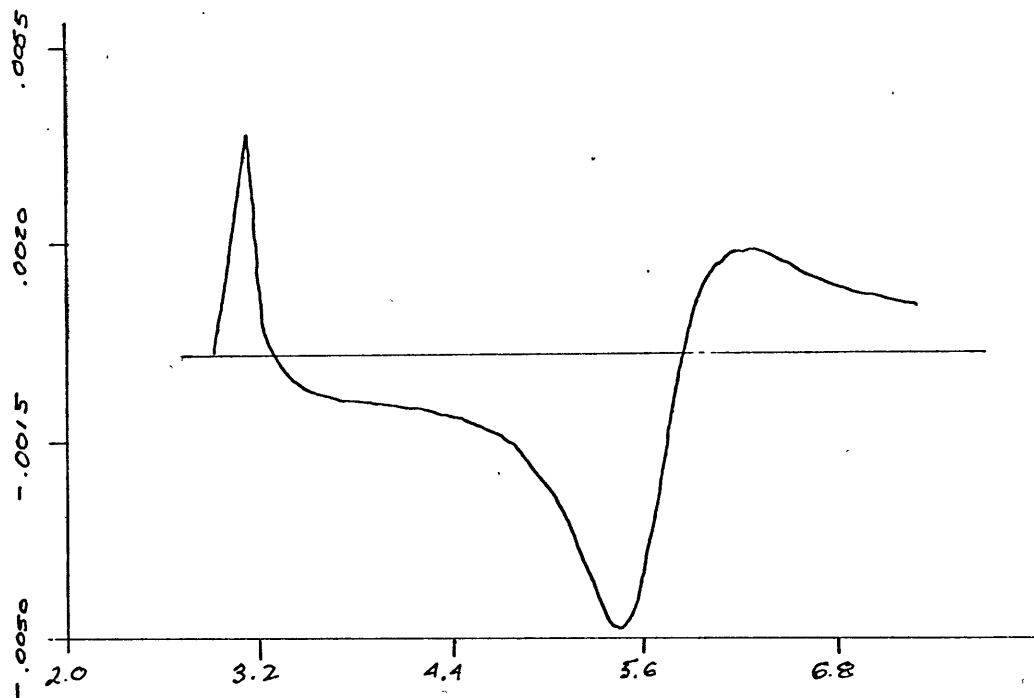


Fig. 1: $z, 5, I, P$ Lamb's problem by approximate program.

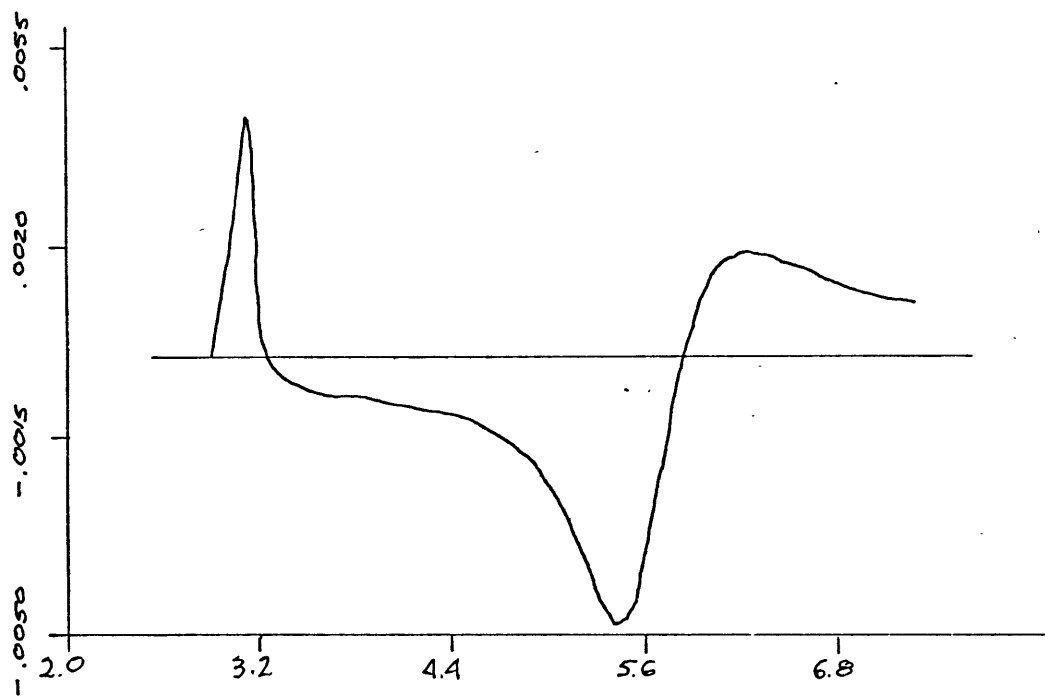


Fig. 2: $z, 5, I, P$ Lamb's problem by exact program.

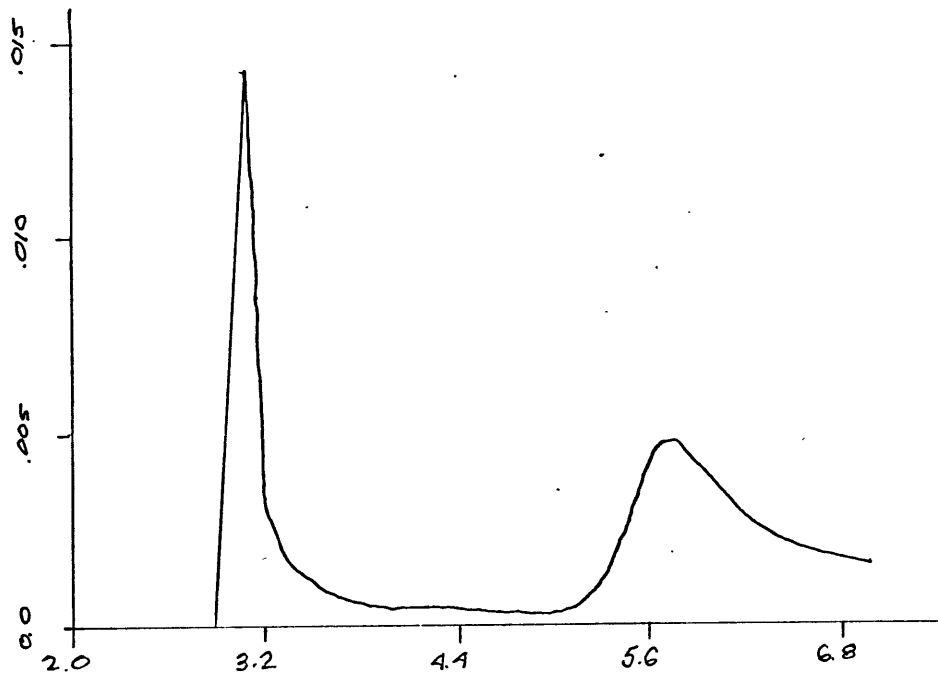


Fig. 3: $r, 5, I, P$ Lamb's problem by approximate program.

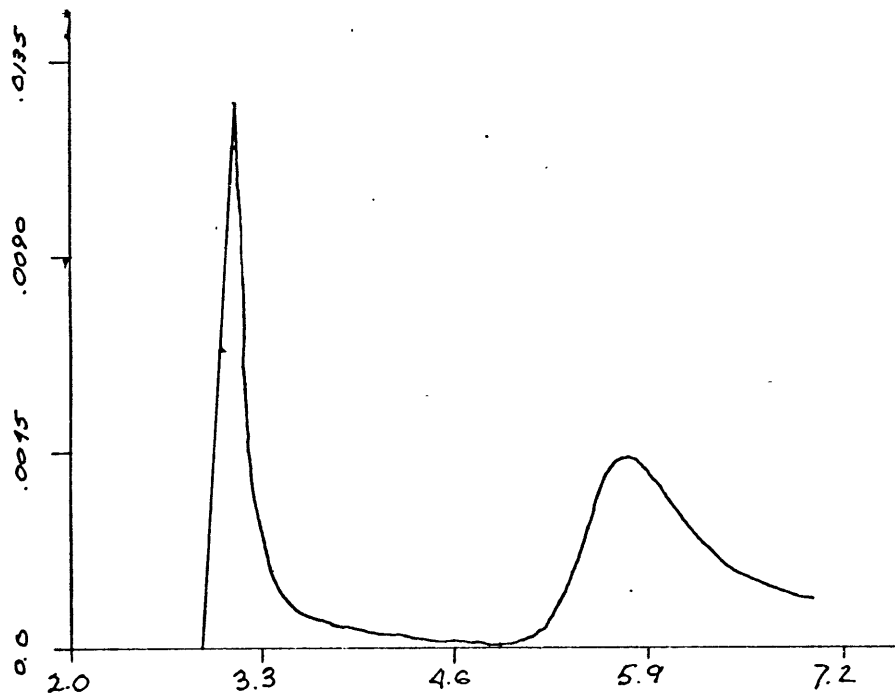


Fig. 4: $r, 5, I, P$ Lamb's problem by exact program.

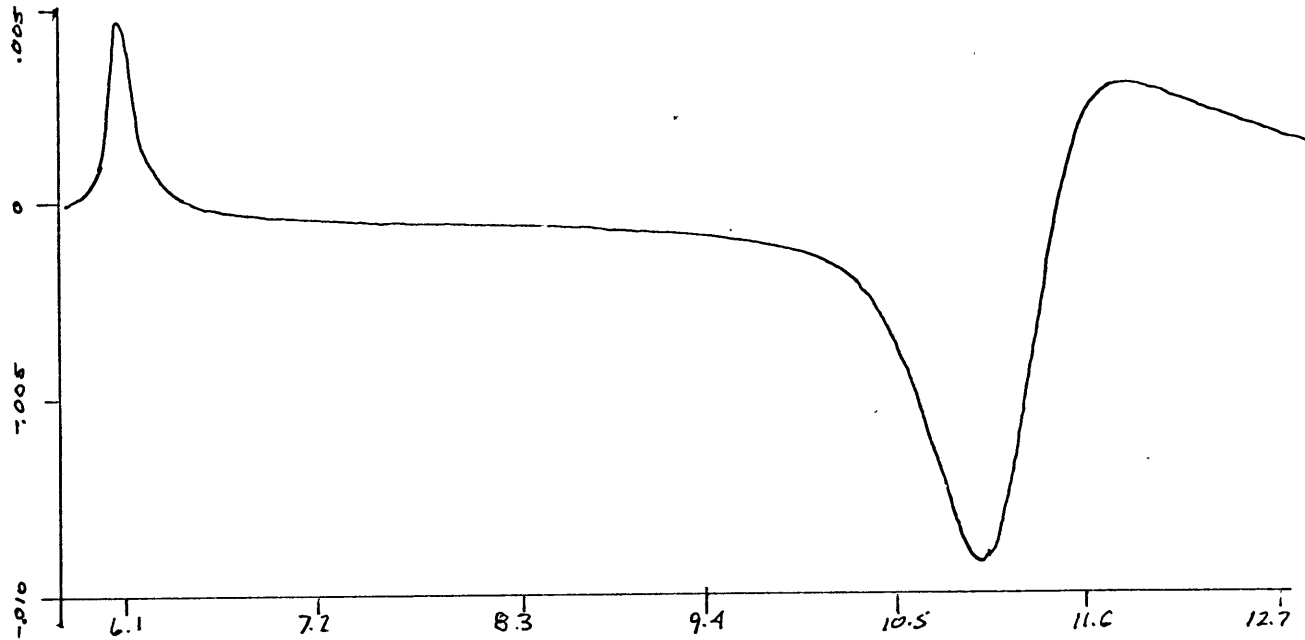


Fig. 5: z, l_0, I, P Lamb's problem by approximate program.

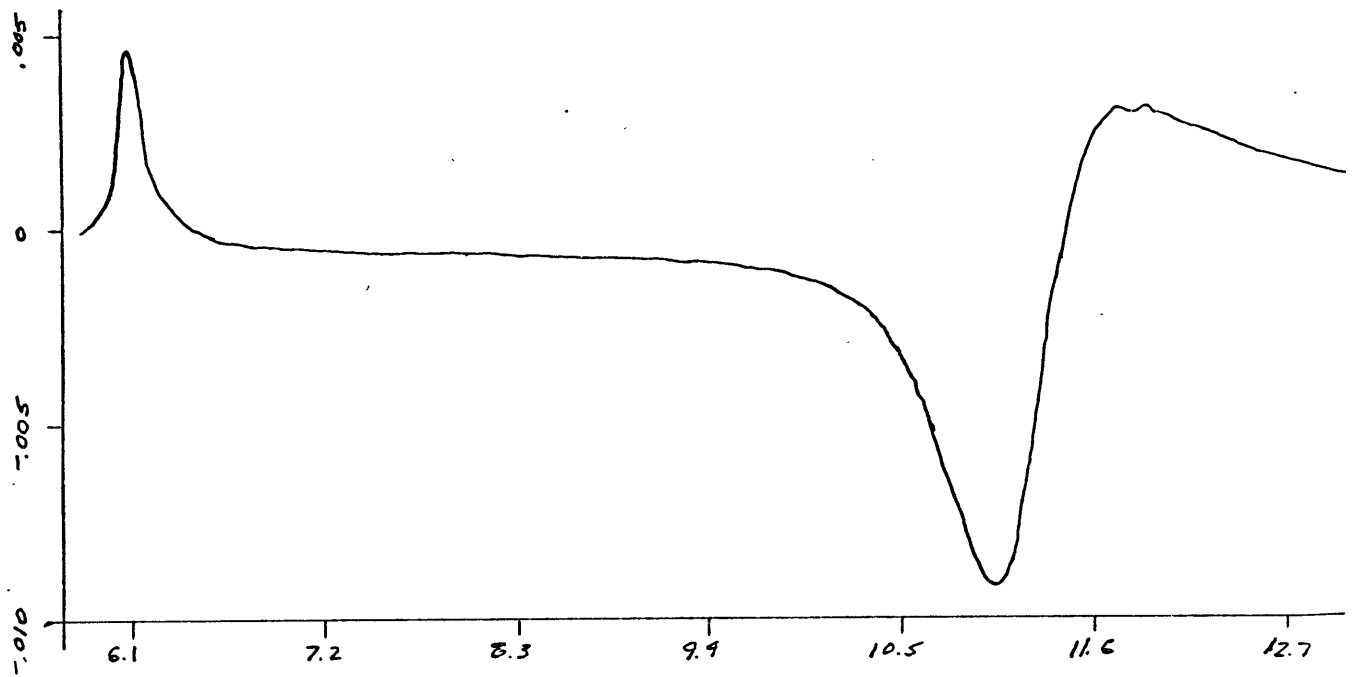


Fig. 6: z, l_0, I, P Lamb's problem by exact program.

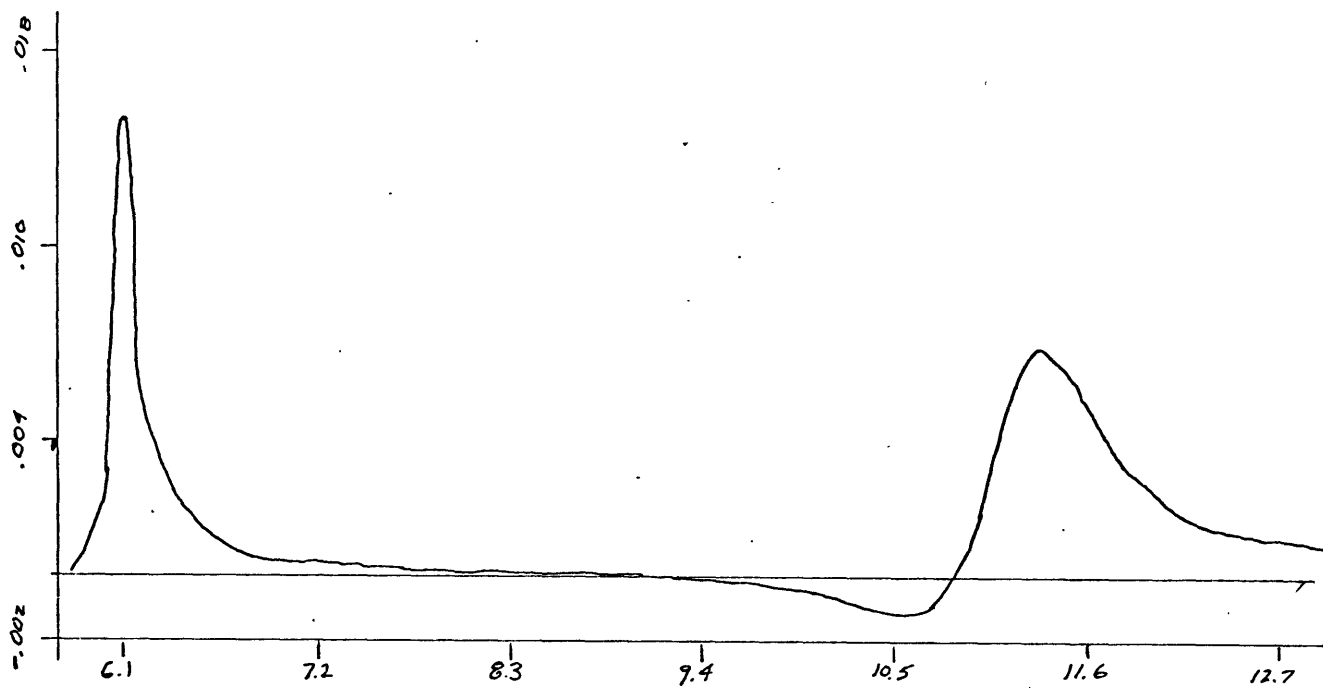


Fig. 7: r, l_0, I, P Lamb's problem by approximate program.

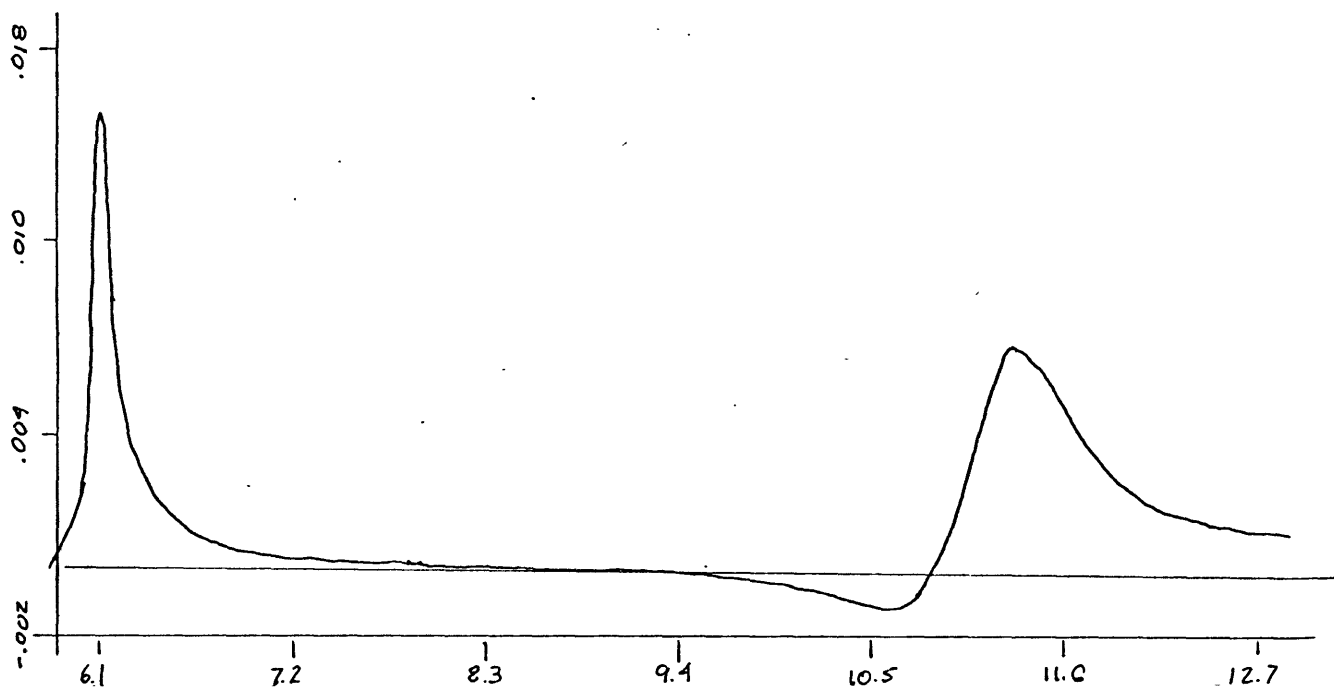


Fig. 8: r, l_0, I, P Lamb's problem by exact program.

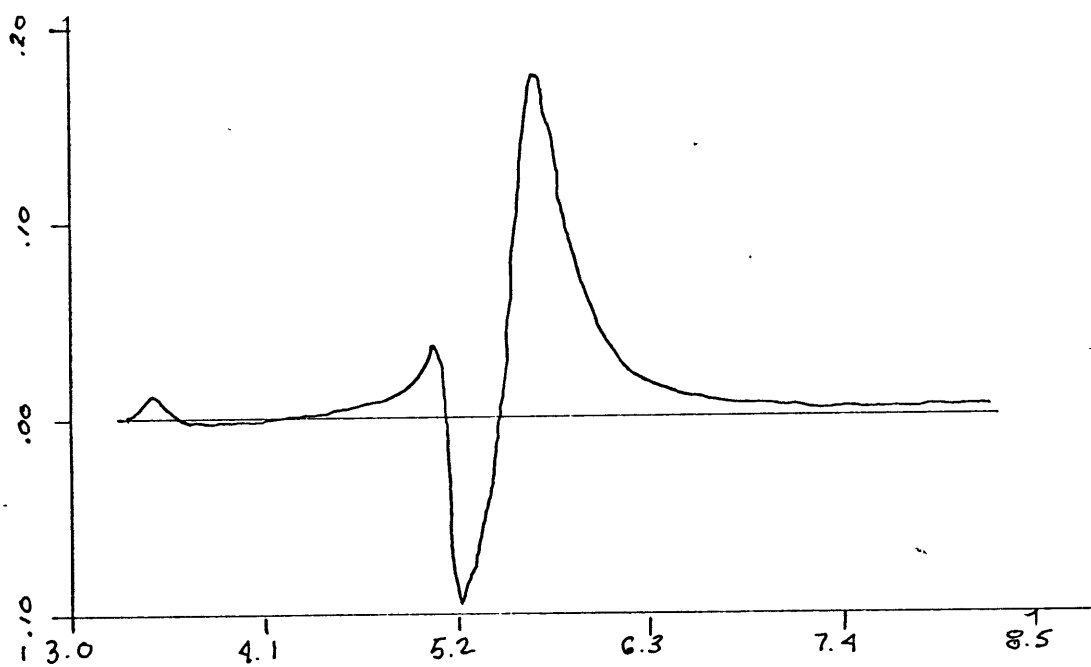


Fig. 19: $z, 5, I, S$ Lamb's problem

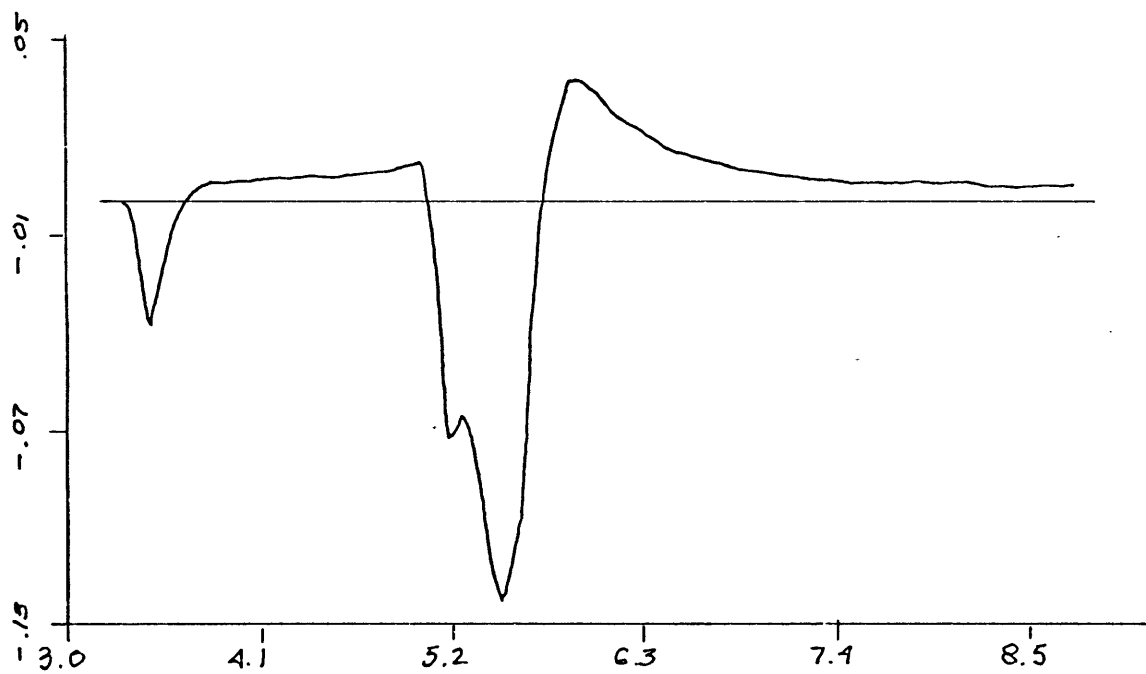
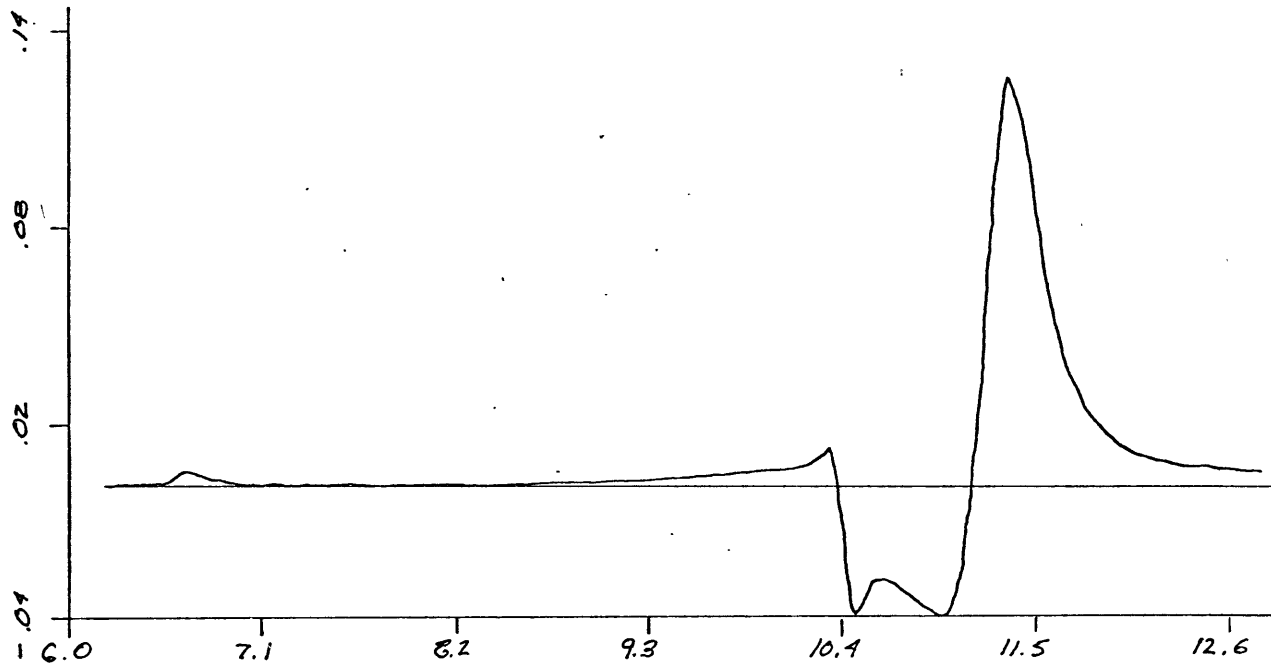
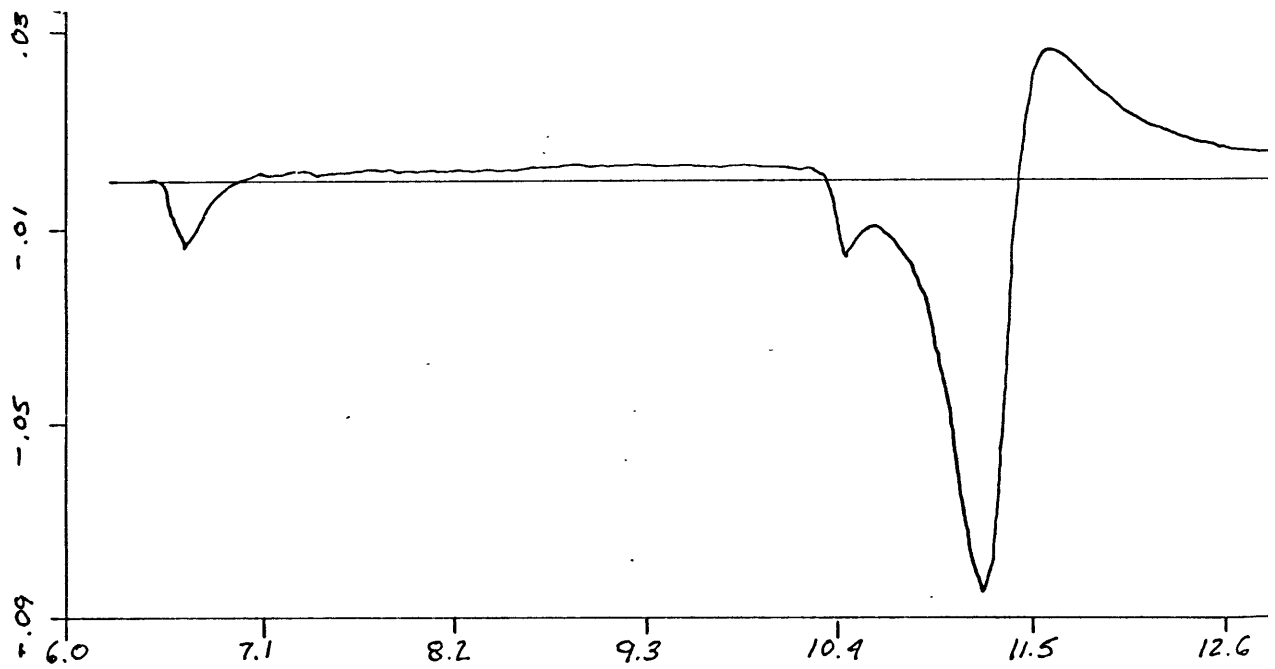


Fig. 10: $r, 5, I, S$

Fig. 11: $z, 10, I, S$

Lamb's problem

Fig. 12: $r, 10, I, S$

Lamb's problem

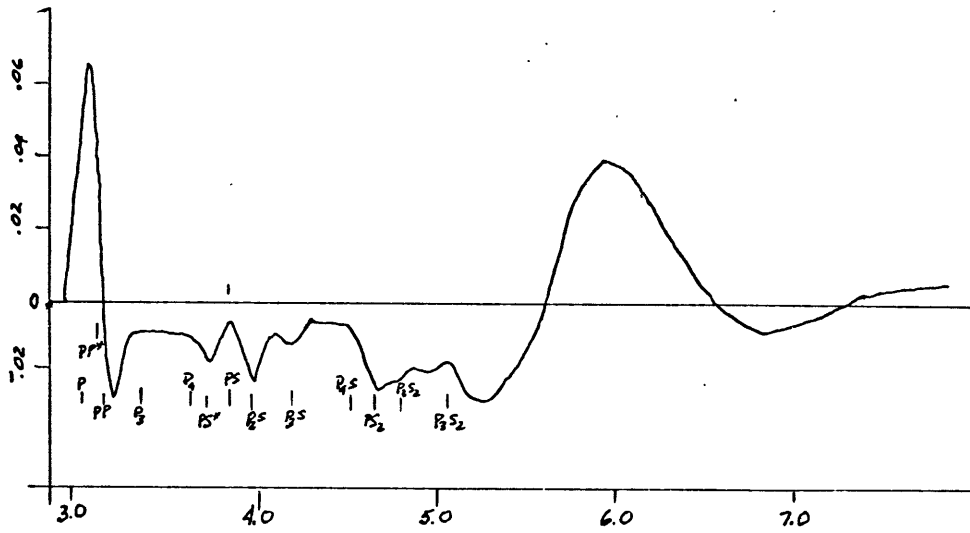


Fig. 13: $z, 5, I, P$ Exact solution
according to Pekeris, et, al.

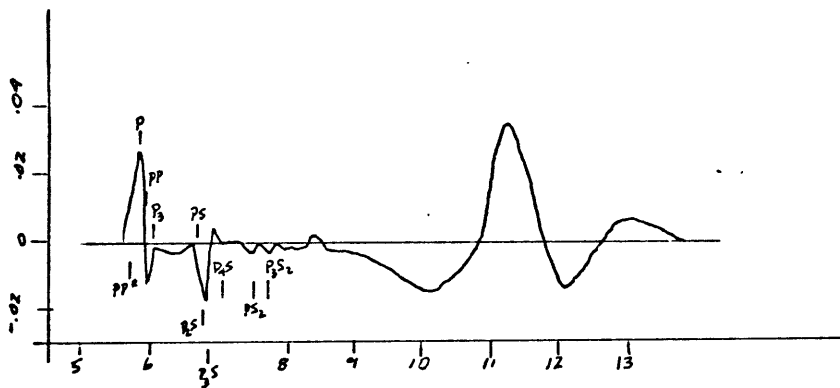


Fig. 14: $z, 10, I, P$ Exact solution
according to Pekeris, et, al.

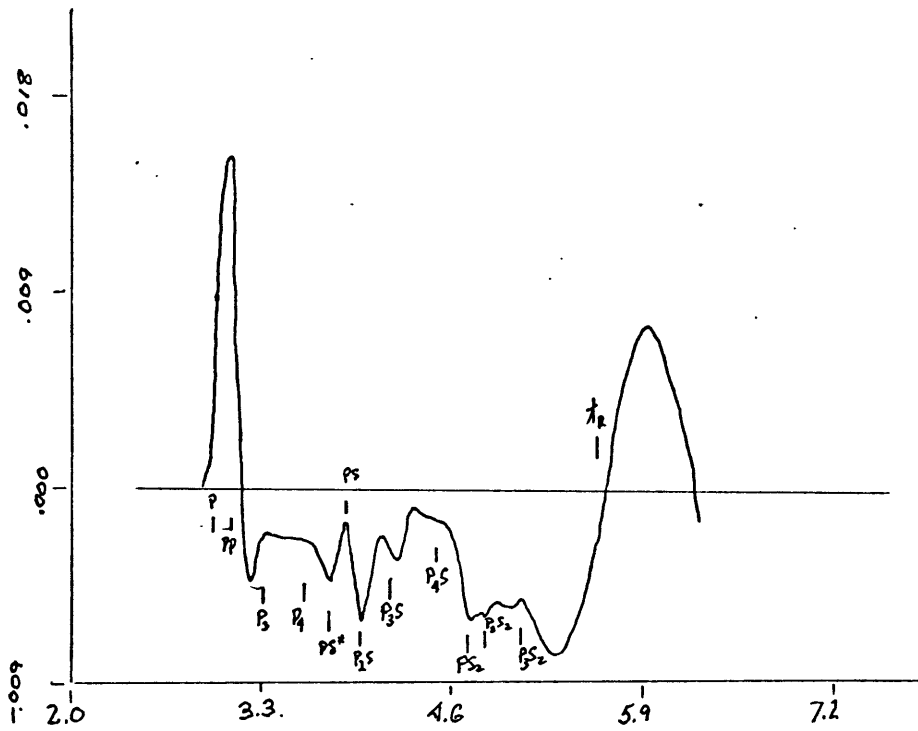


Fig. 15: z, 5, I, P

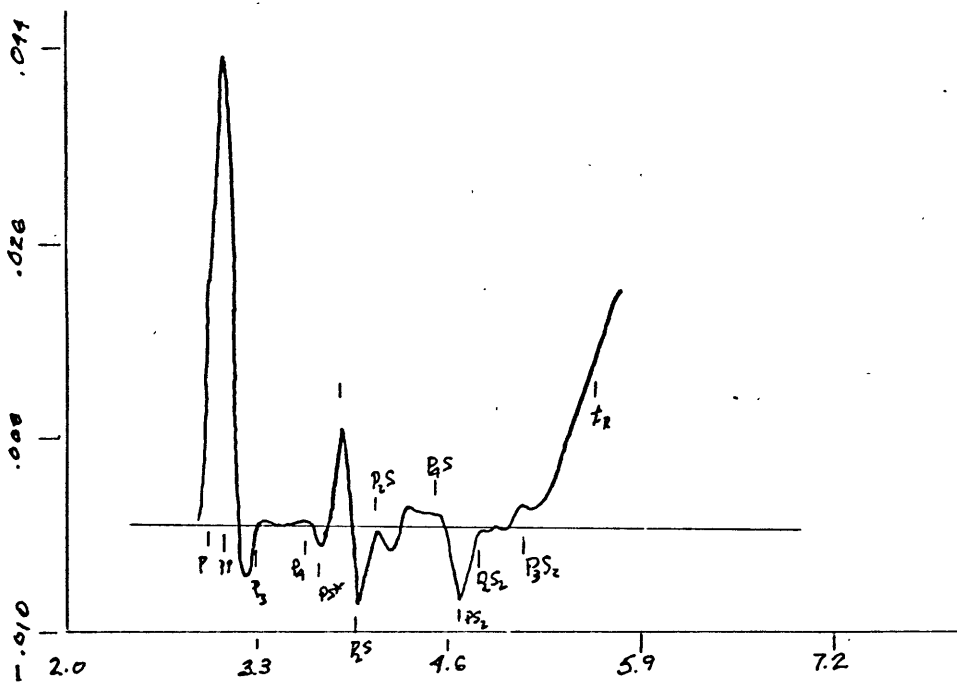


Fig. 16: r, 5, I, P

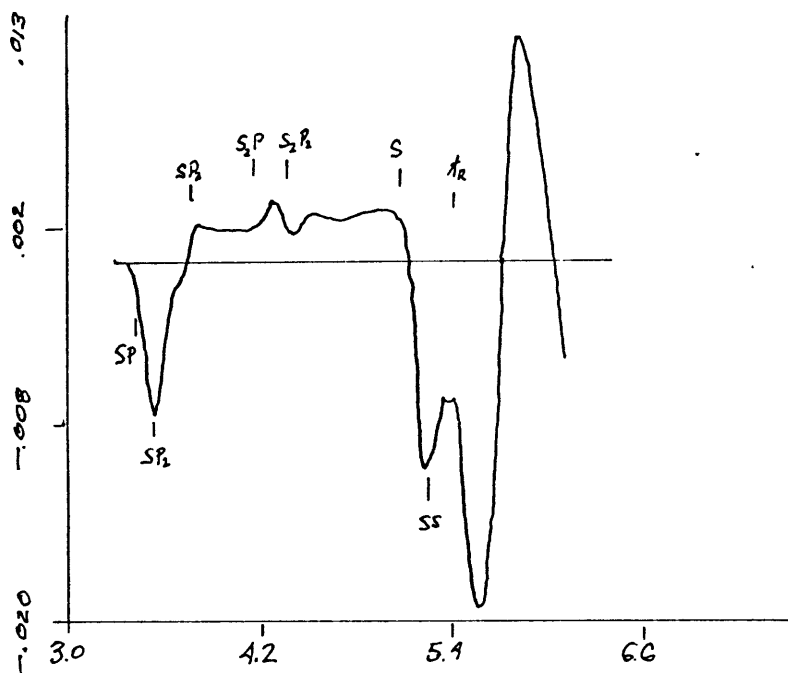


Fig. 17: r,5,I,S

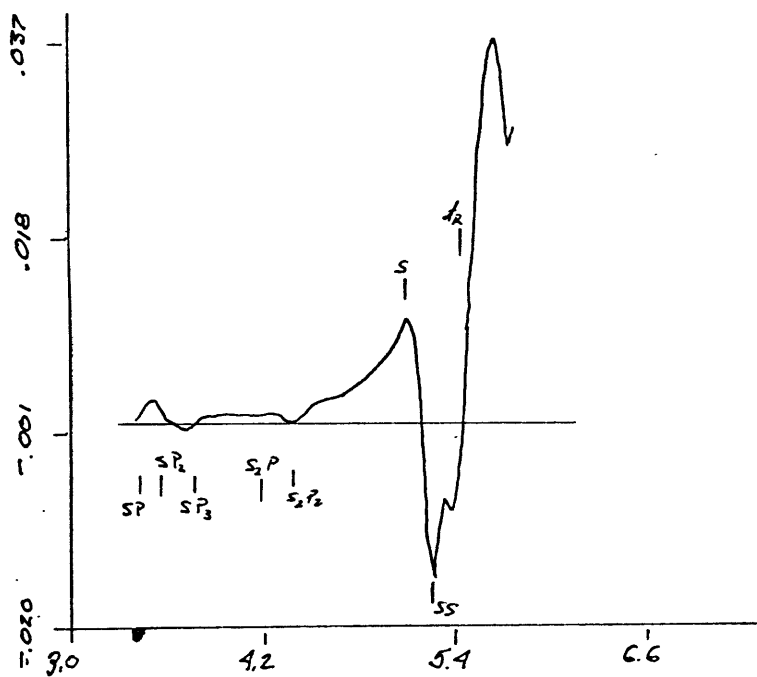


Fig. 18: z,5,I,S

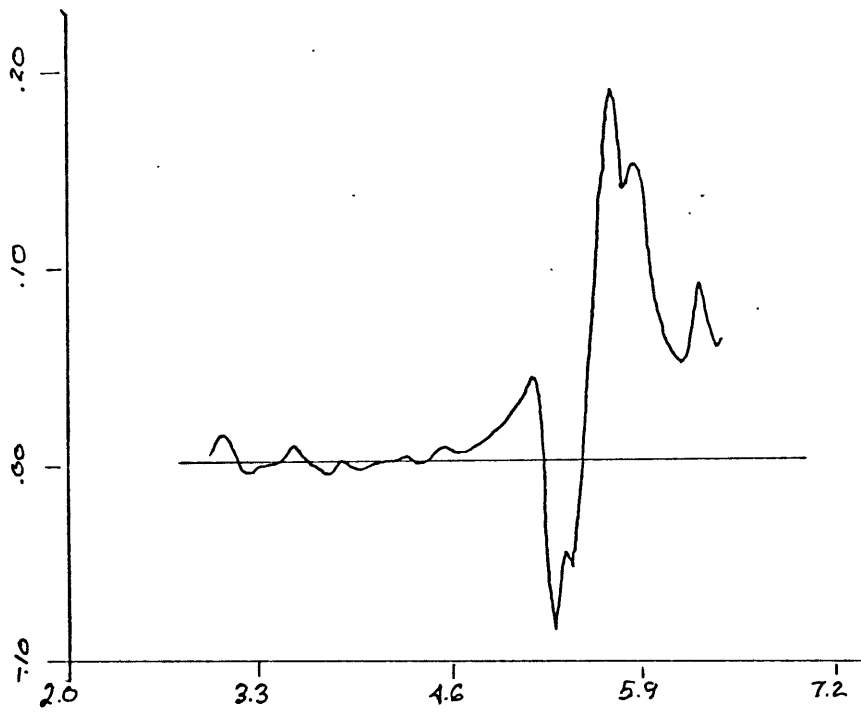


Fig. 19: z,5,I,c

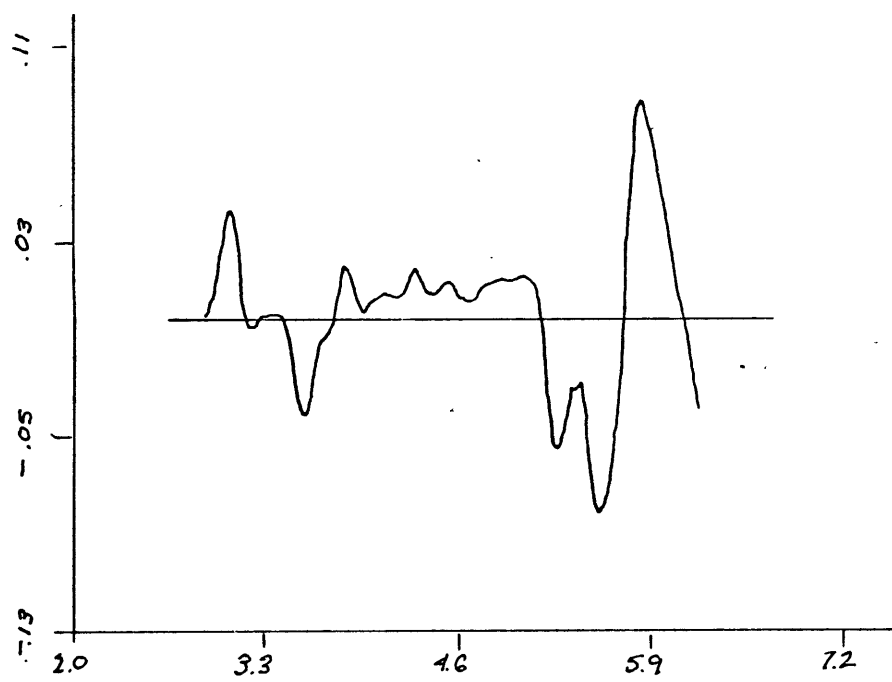


Fig. 20: r,5,I,C

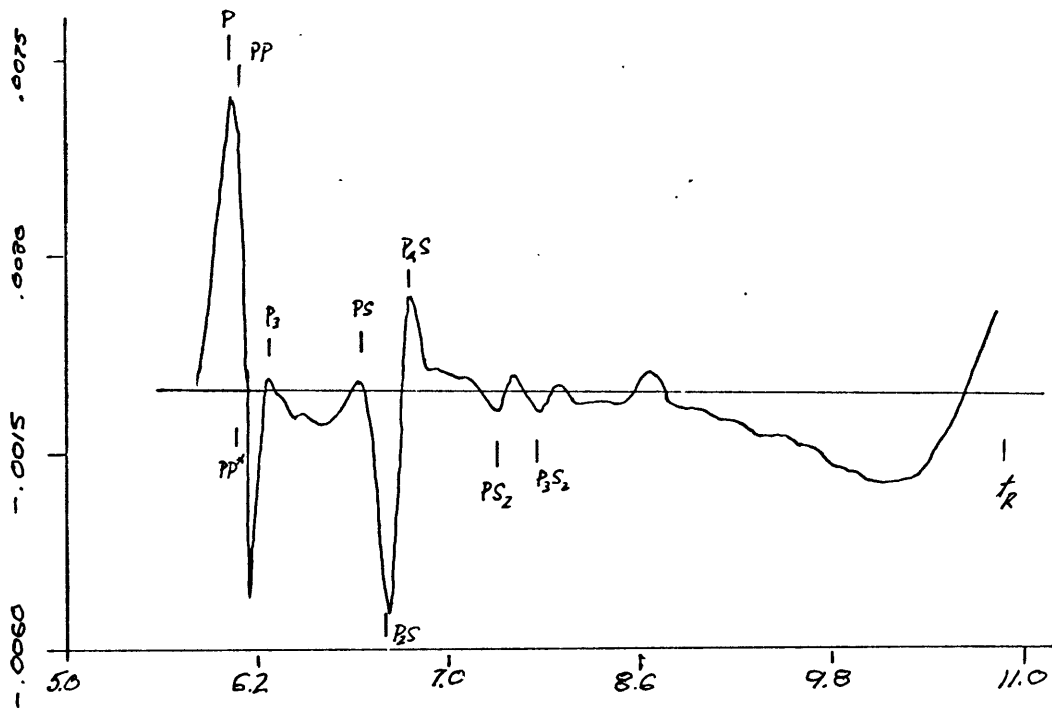


Fig. 21: z, 10, I, P

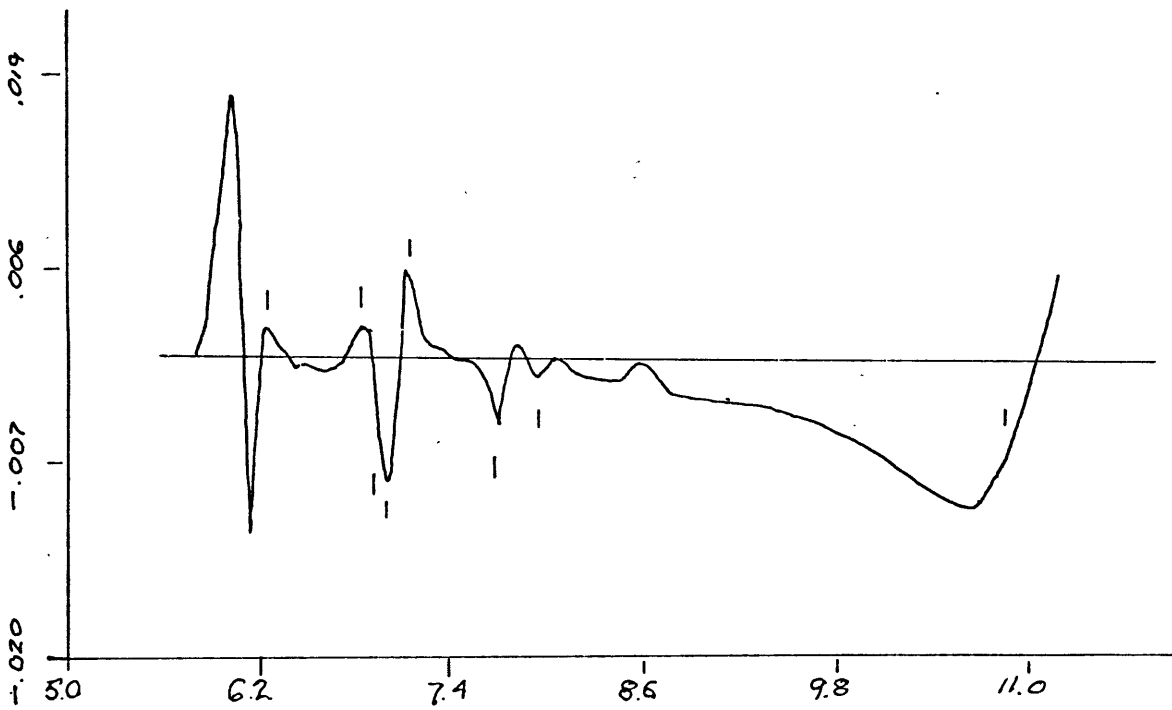


Fig. 22: r, 10, I, P

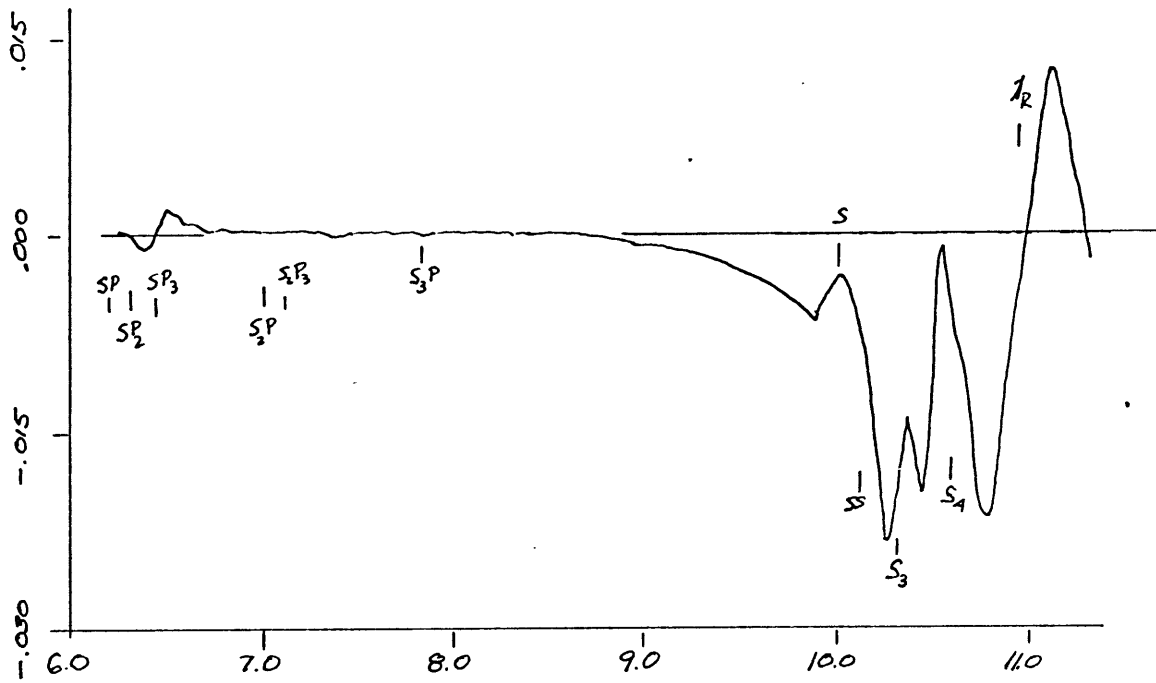


Fig. 23: z,10,I,S

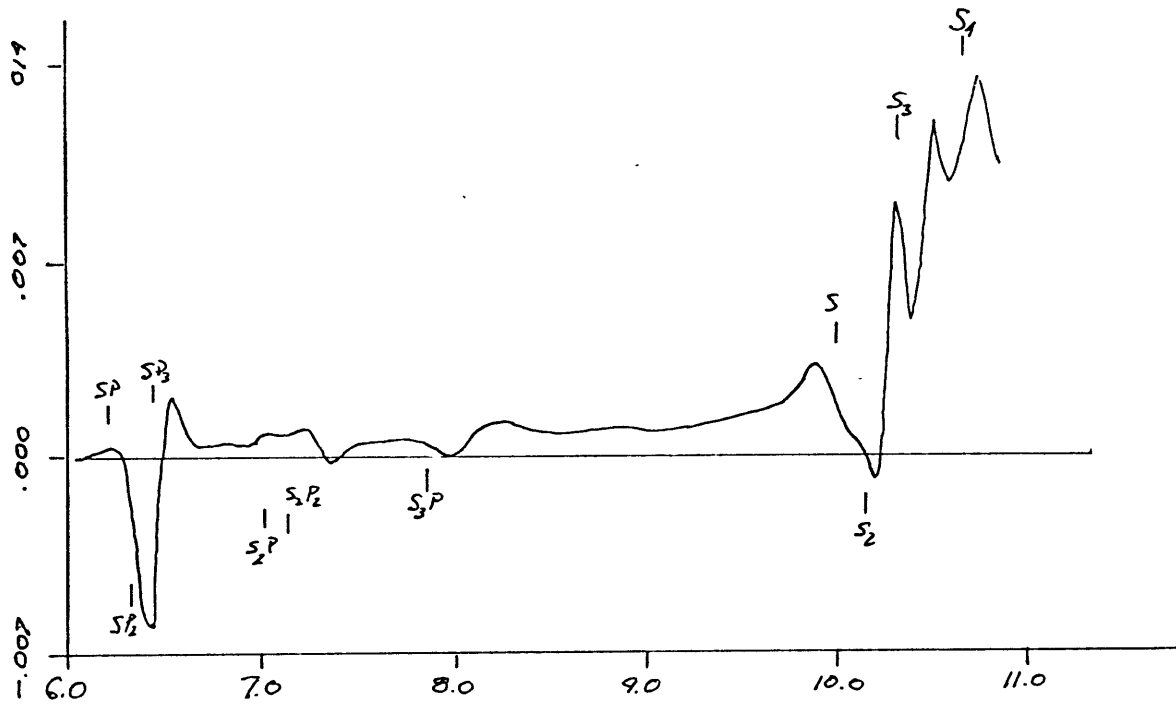


Fig. 24: r,10,I,S

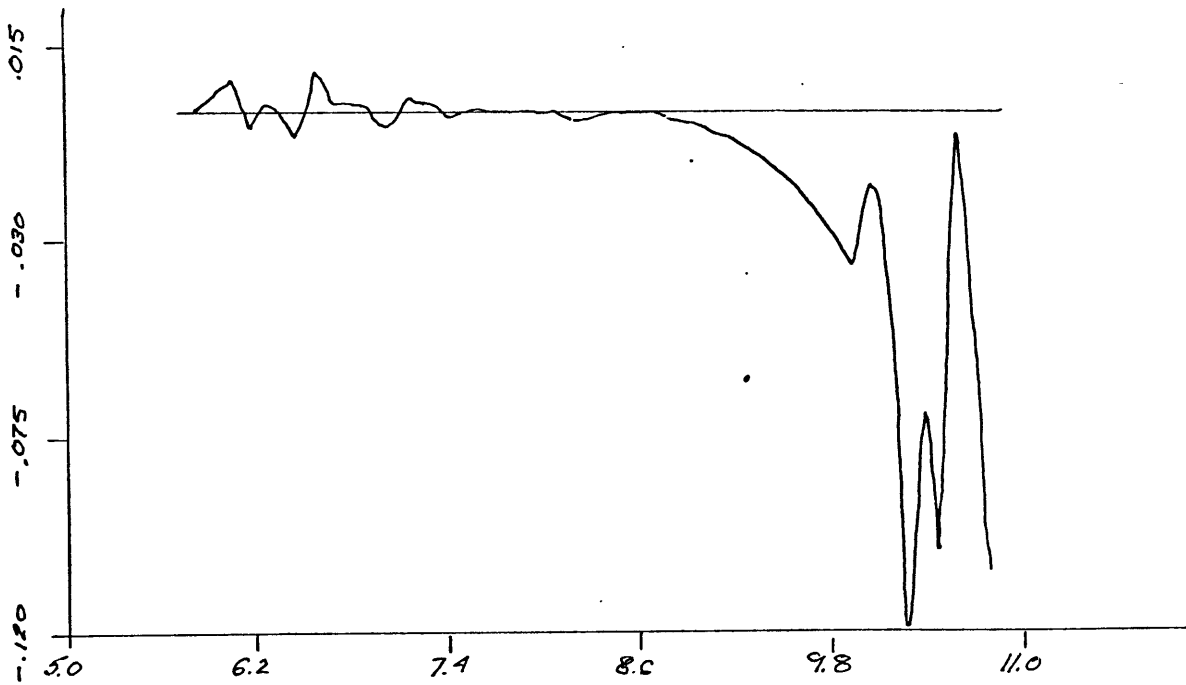


Fig. 25: z,10,I,C

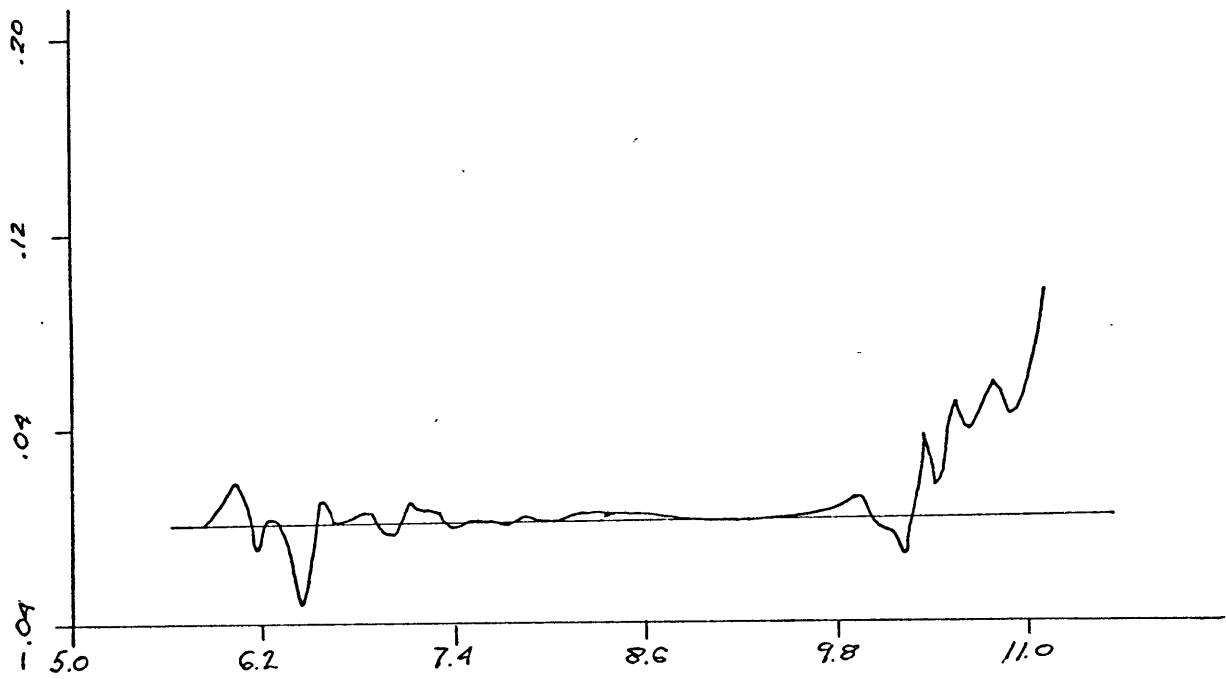


Fig. 26: r,10,I,C

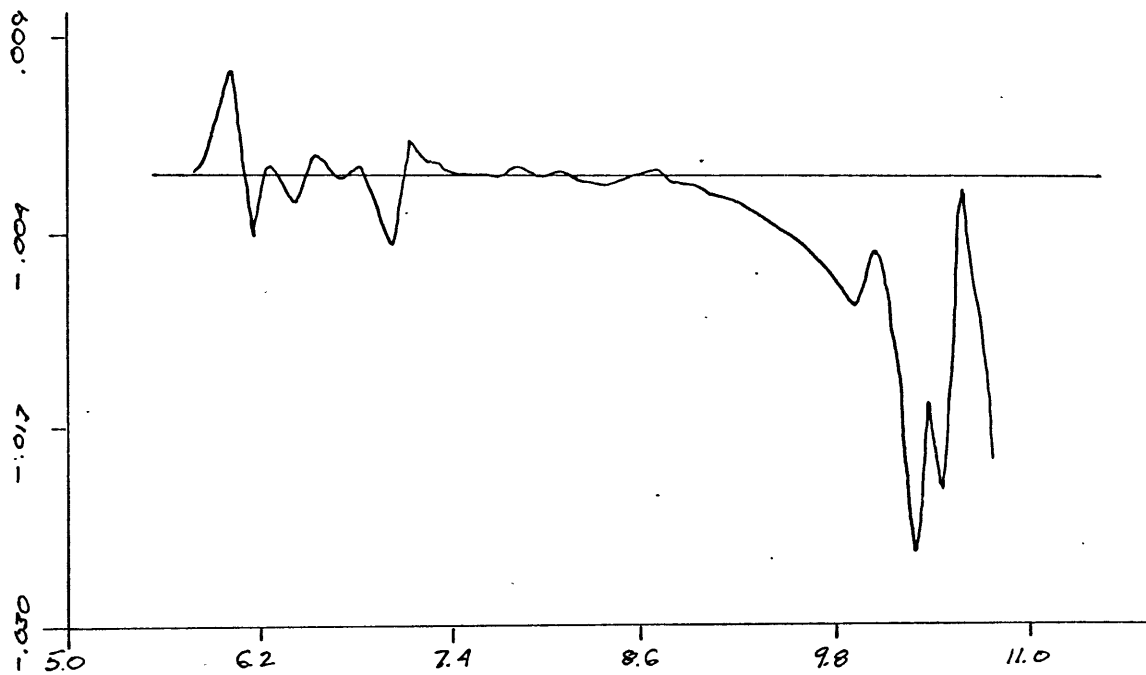


Fig. 27: $z, 10, I, C$ Shear source has been multiplied by 0.2 .

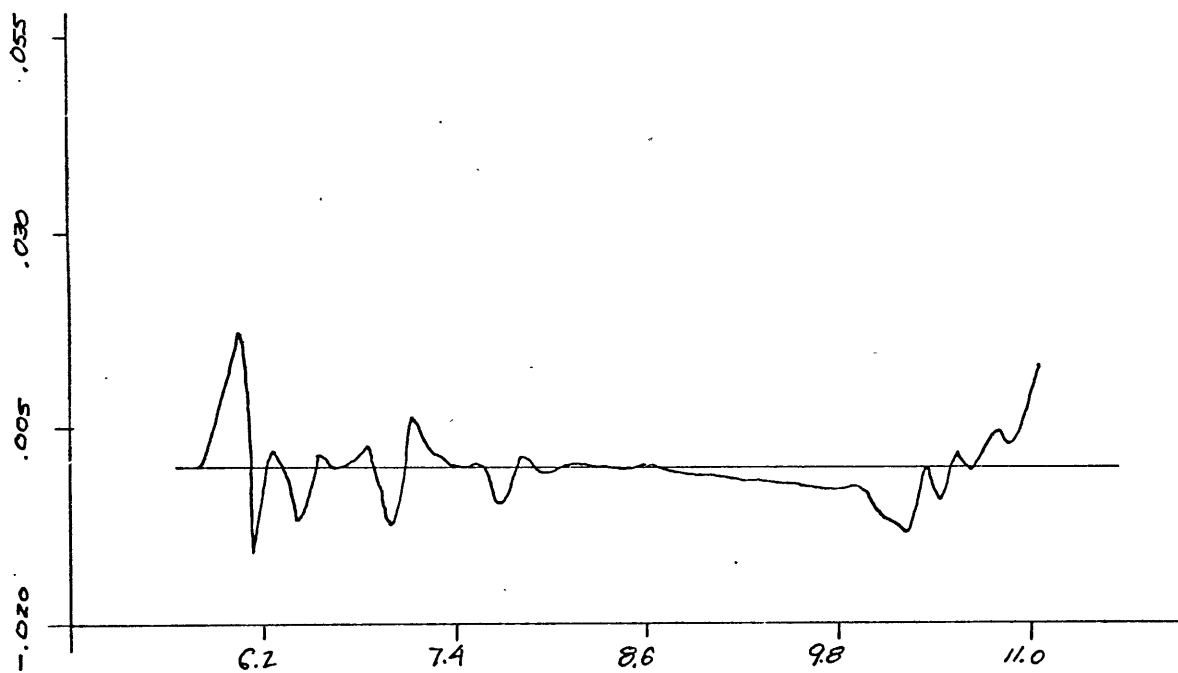
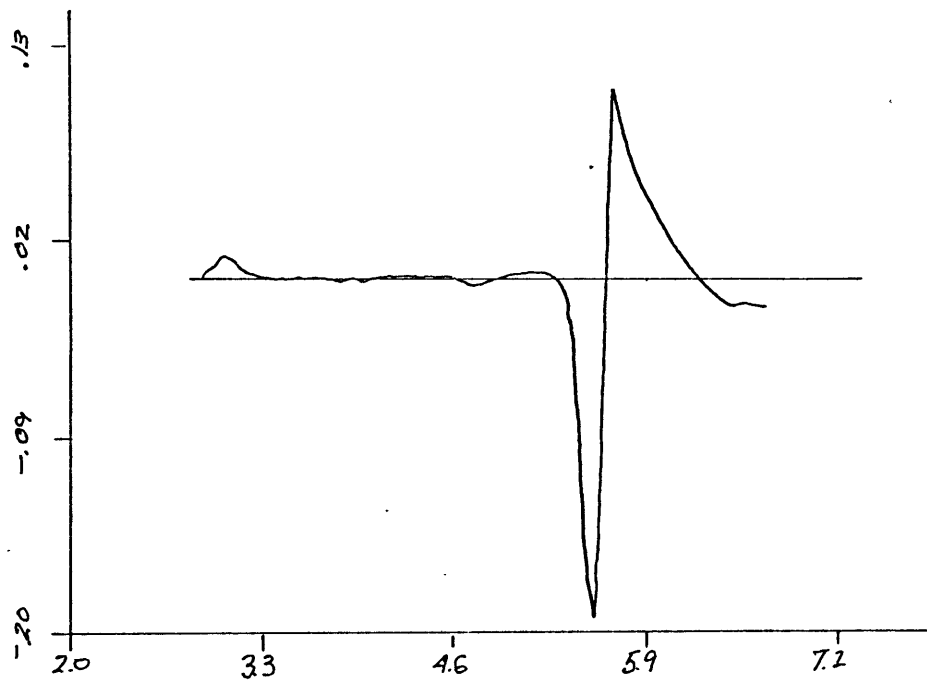
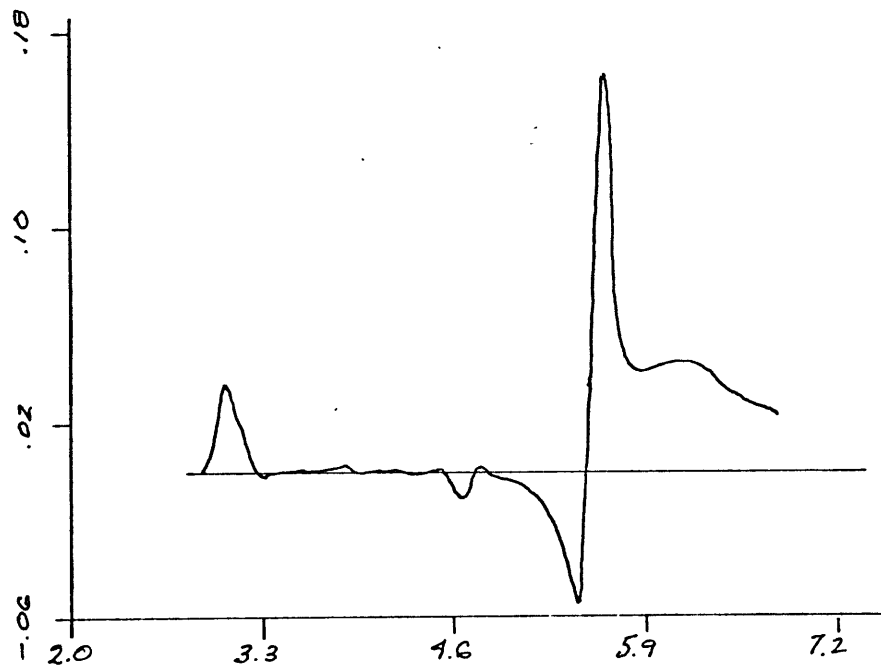
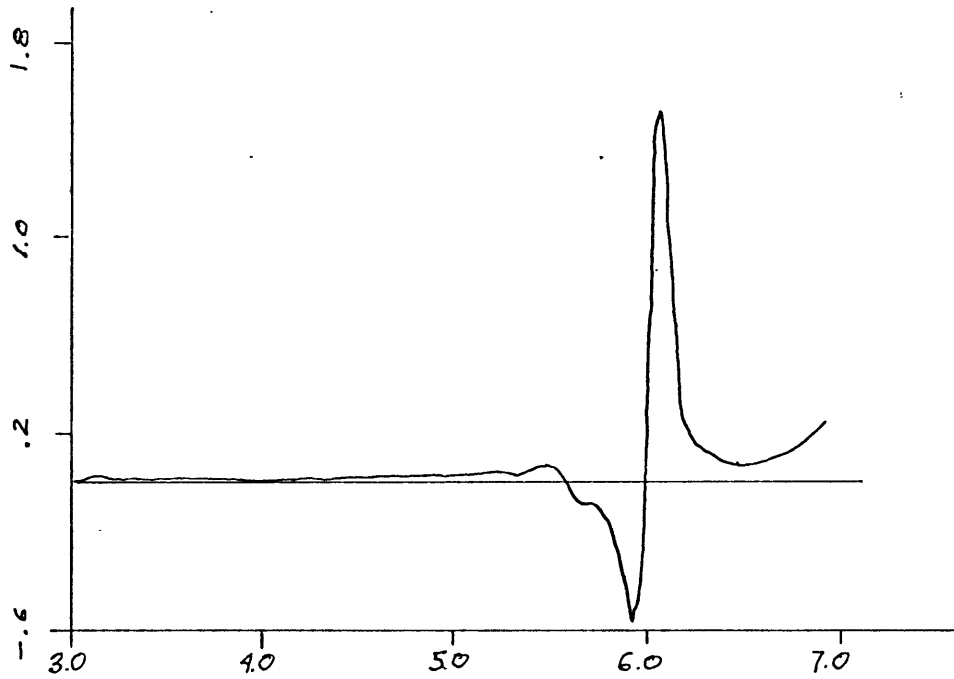
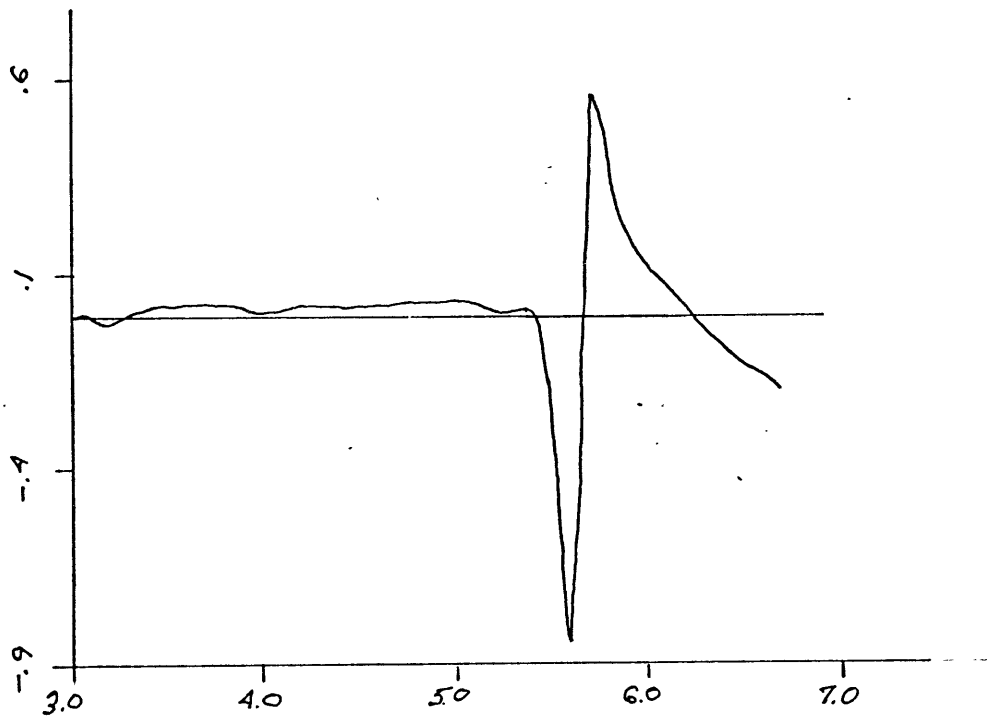
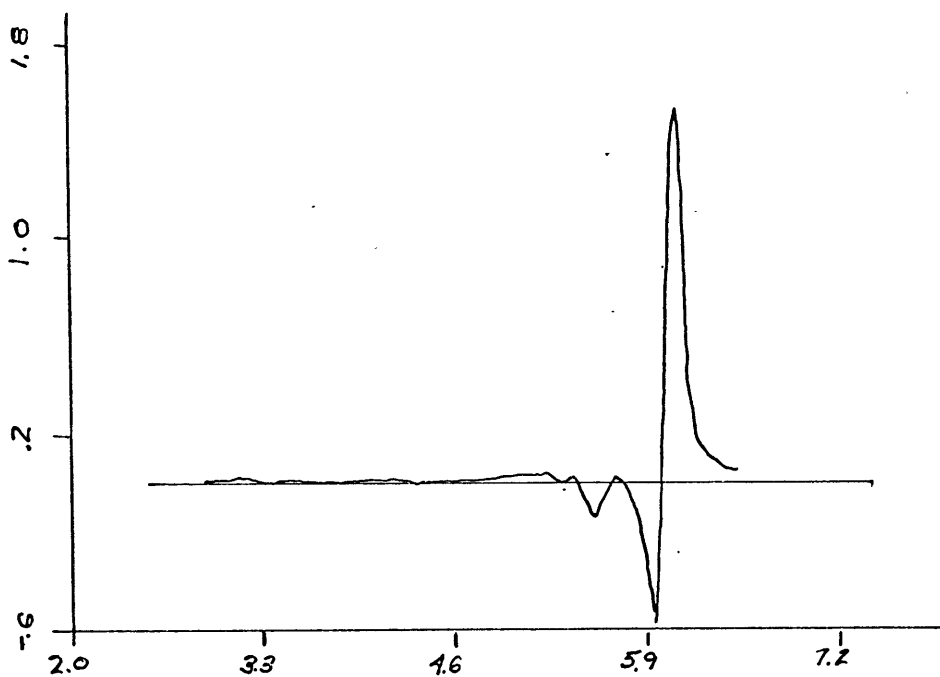
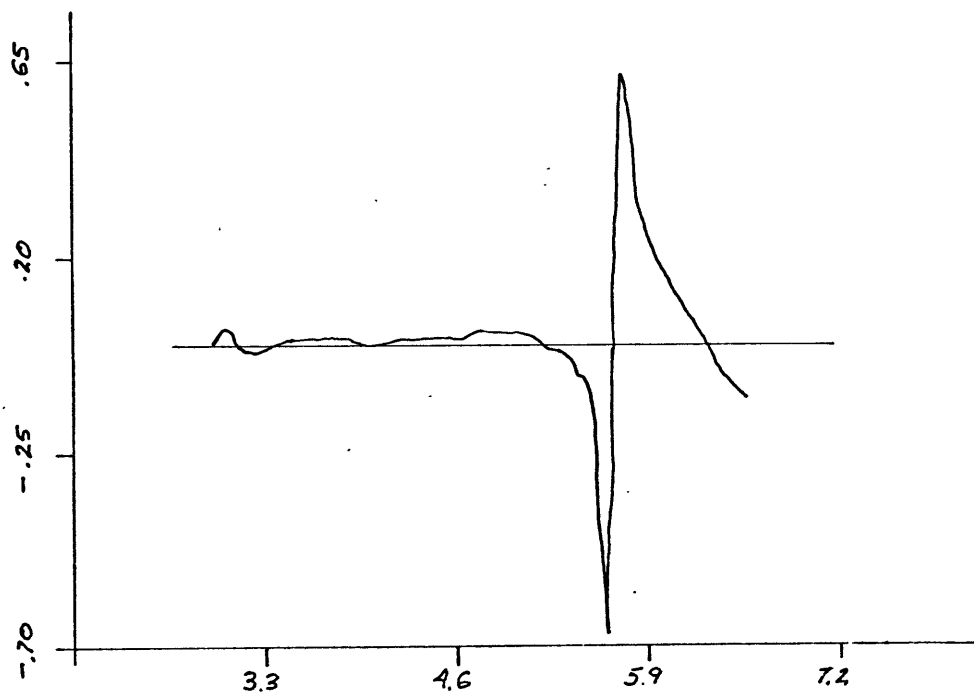


Fig. 28: $r, 10, I, C$ Shear source has been multiplied by 0.2 .

Fig. 29: $z, 5, I, P, h=0.05$ Fig. 30: $r, 5, I, P, h=0.05$

Fig. 31: $z, 5, I, S, h=0.05$ Fig. 32: $r, 5, I, S, h=0.05$

Fig. 33: $z, 5, I, C, h=0.05$ Fig. 34: $r, 5, I, C, h=0.05$

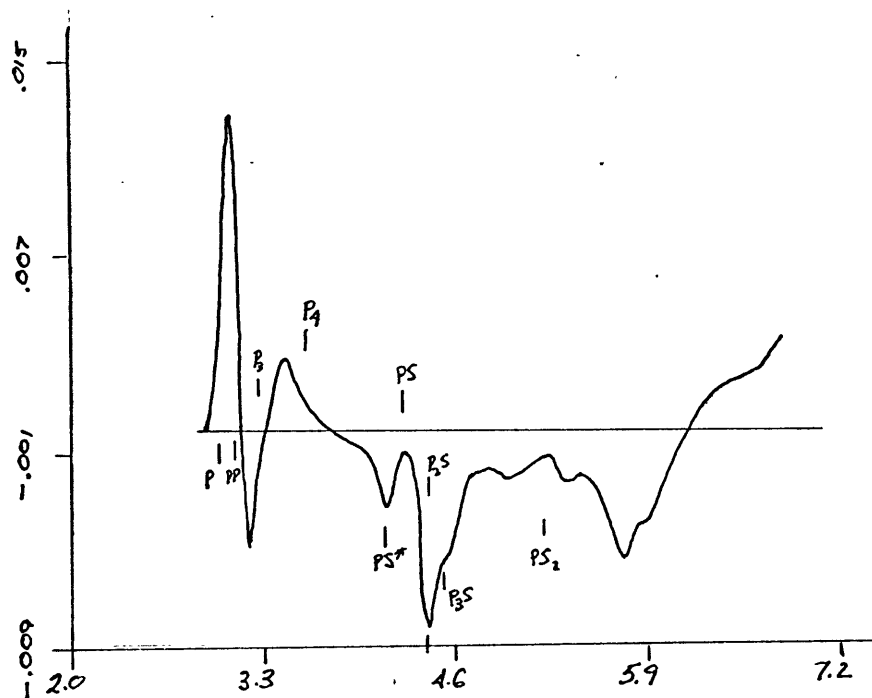


Fig. 35: z,5,II,P

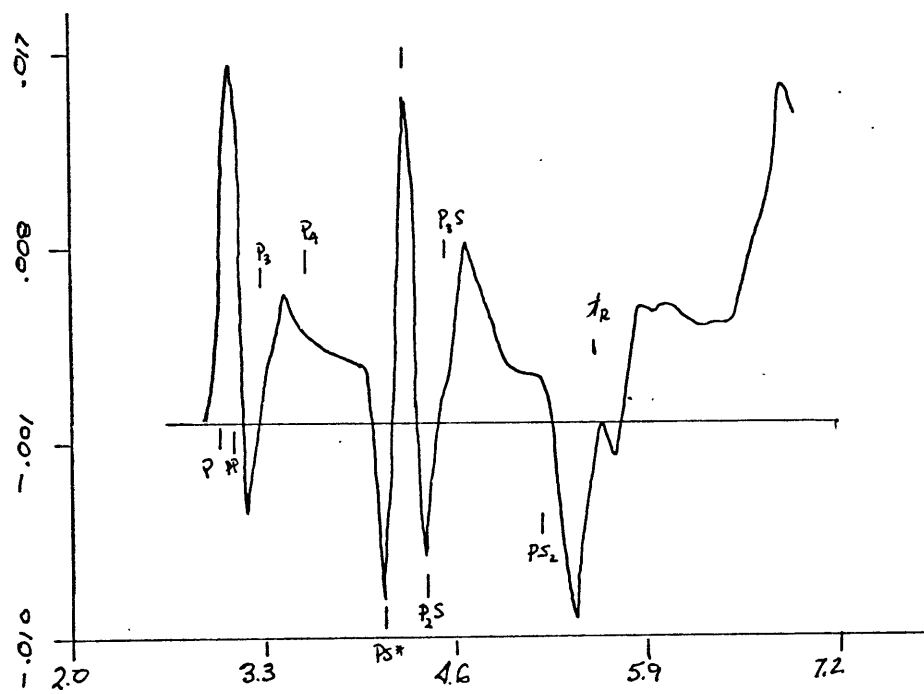


Fig. 36: r,5,II,P

Fig. 38: 1,5,II,S

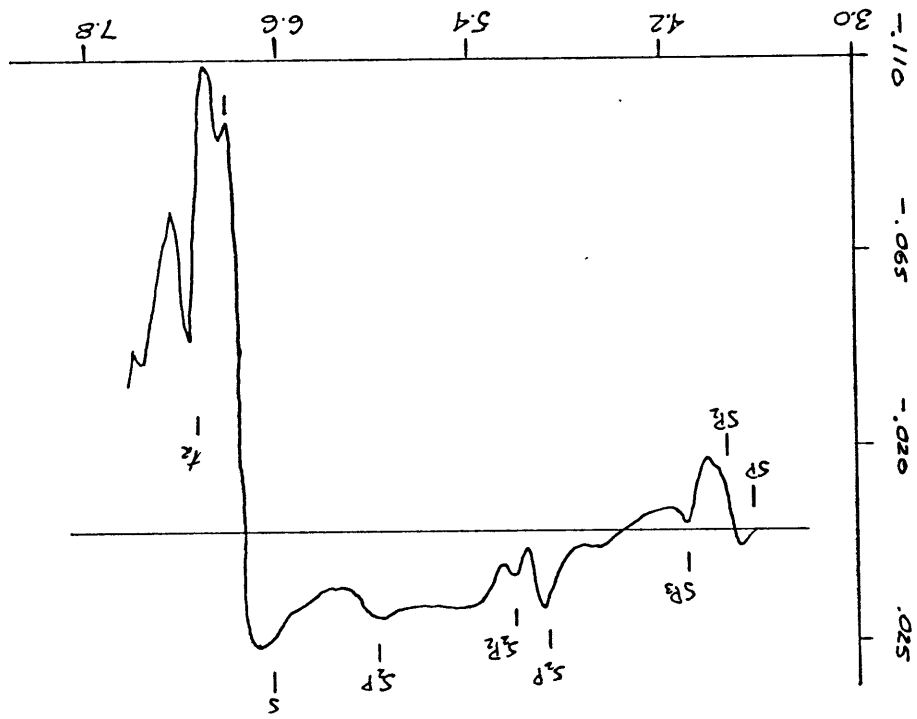
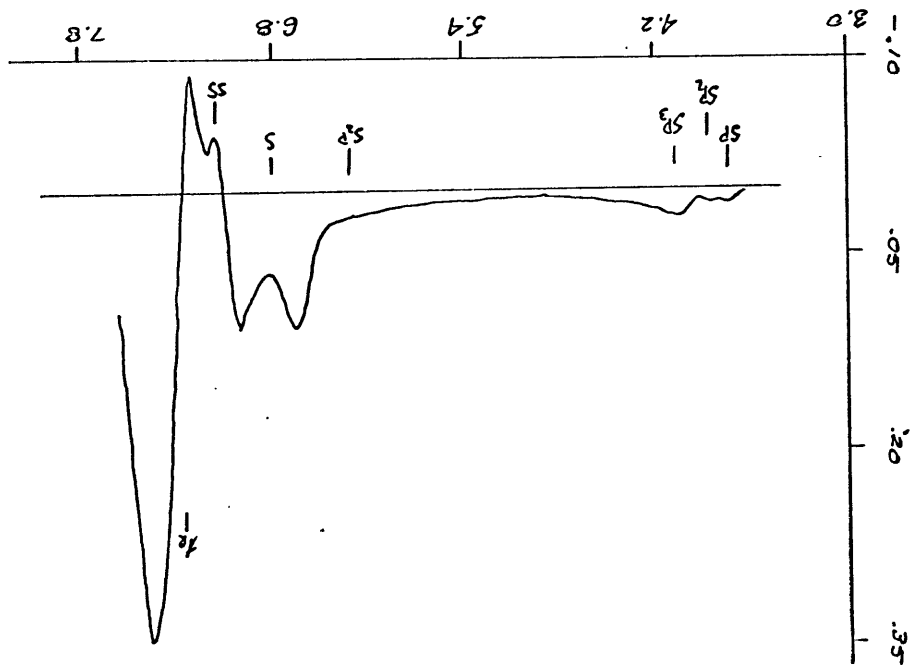


Fig. 37: 2,5,II,S



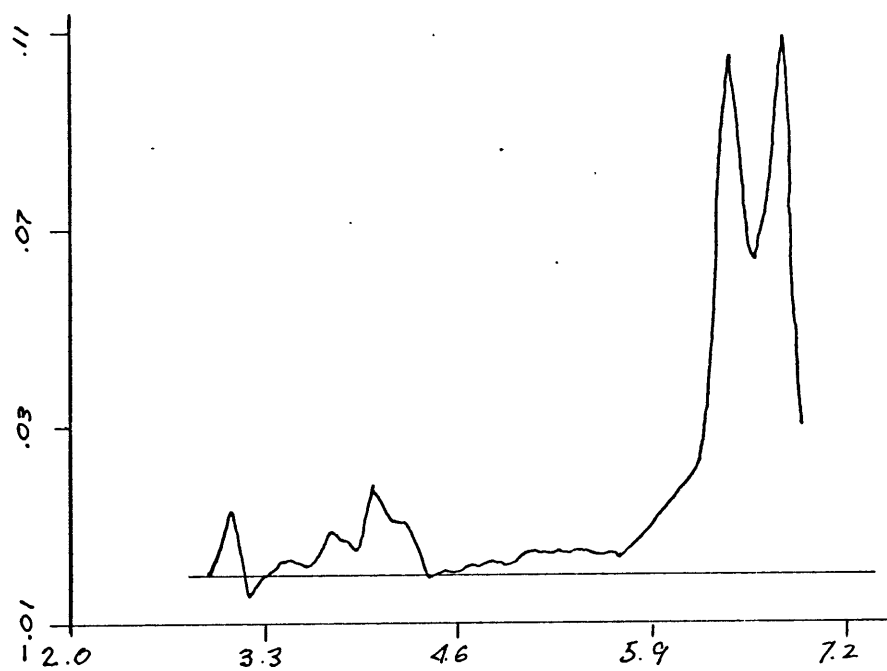


Fig. 39: z,5,II,C

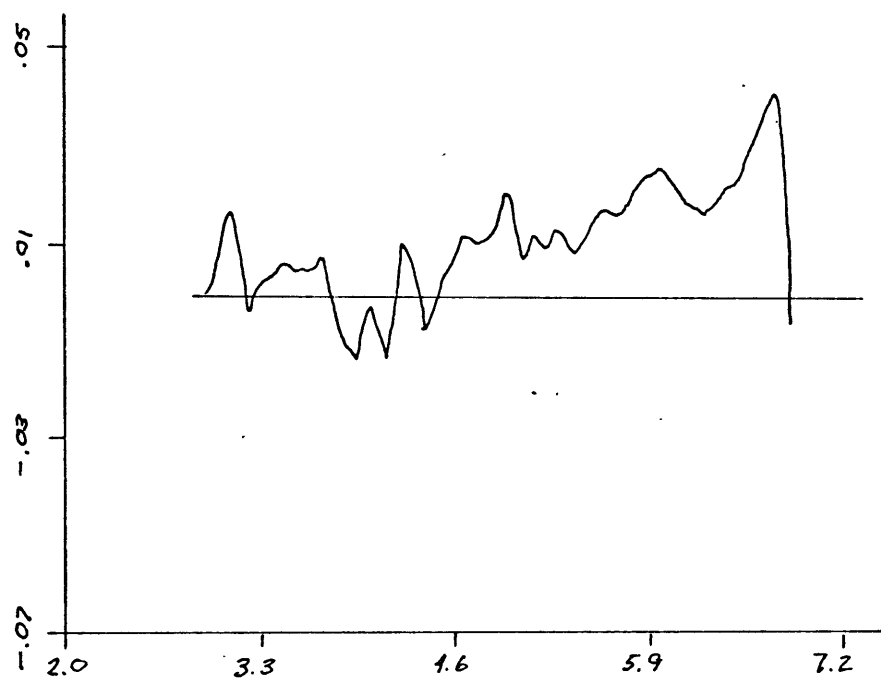


Fig. 40: r,5,II,C

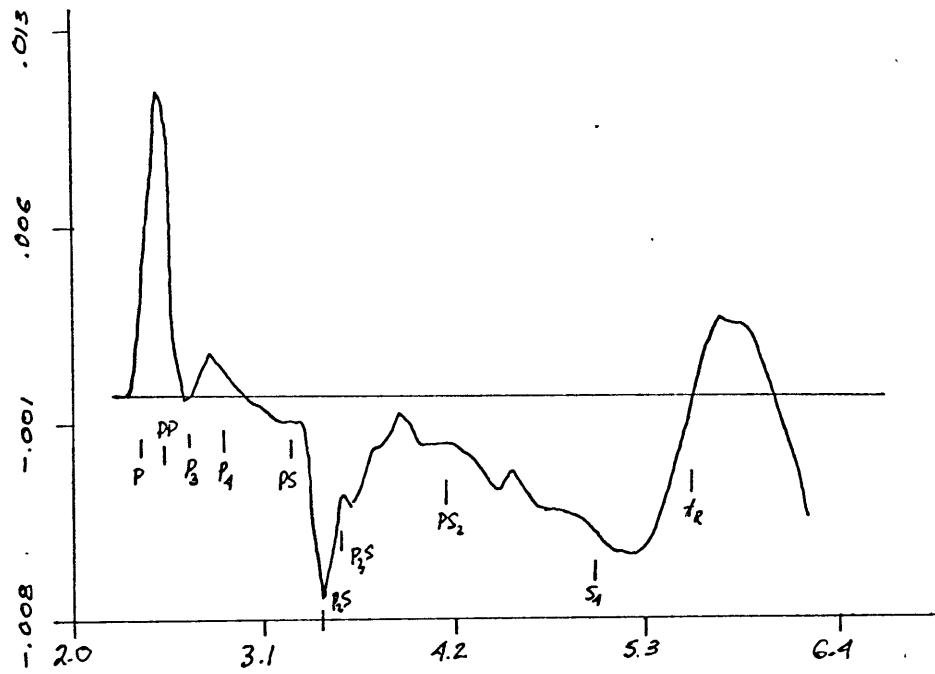


Fig. 41: z,5,III,P

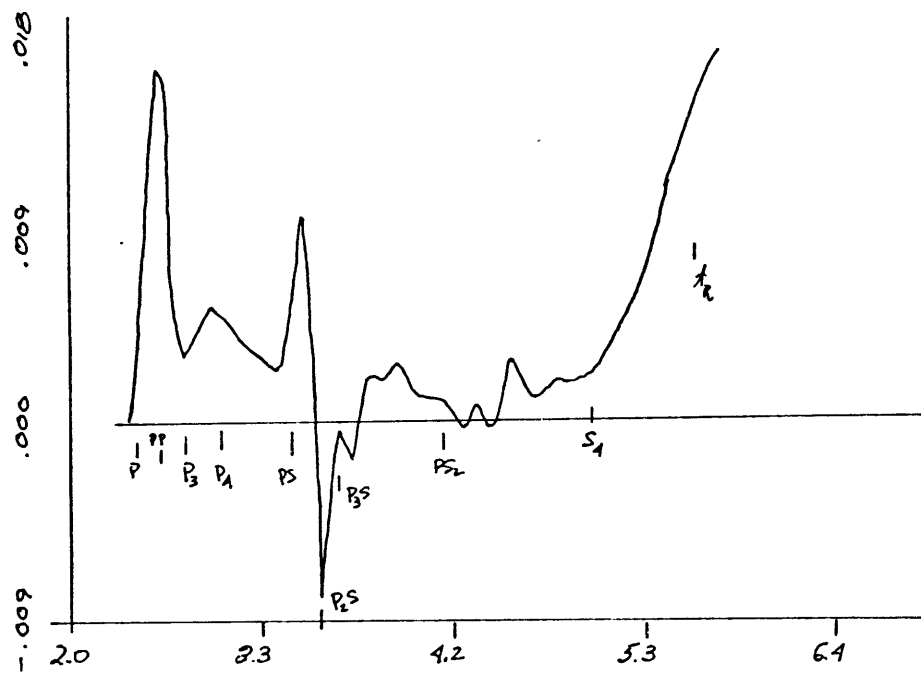


Fig. 42: r,5,III,P

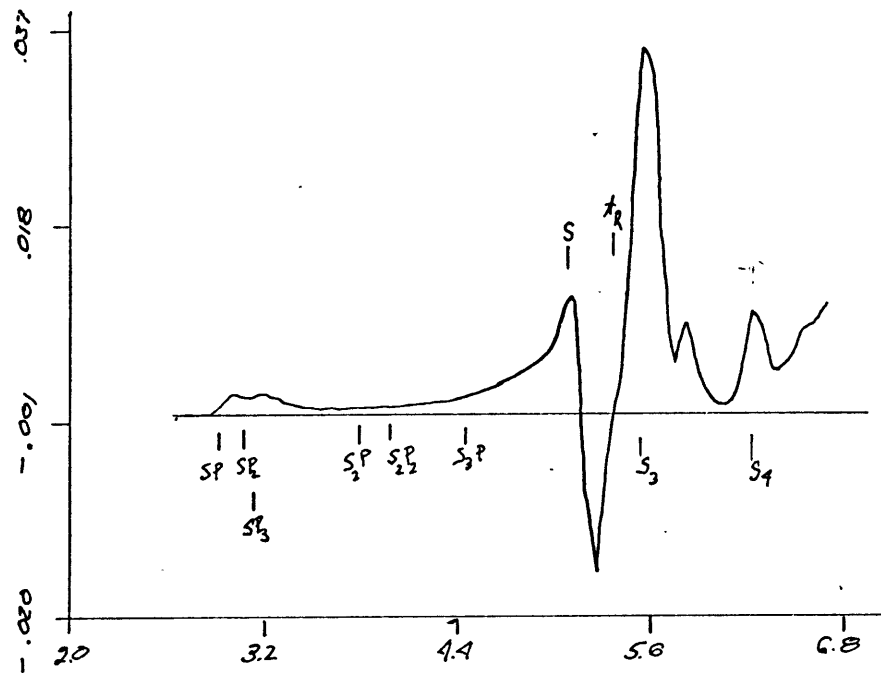


Fig. 43: z, 5, III, S

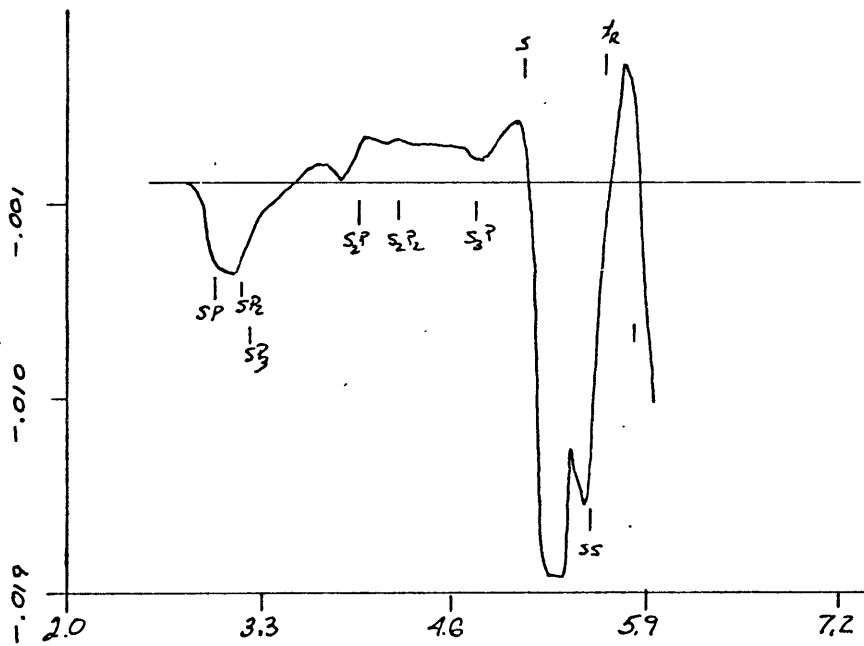


Fig. 44: r, 5, III, S

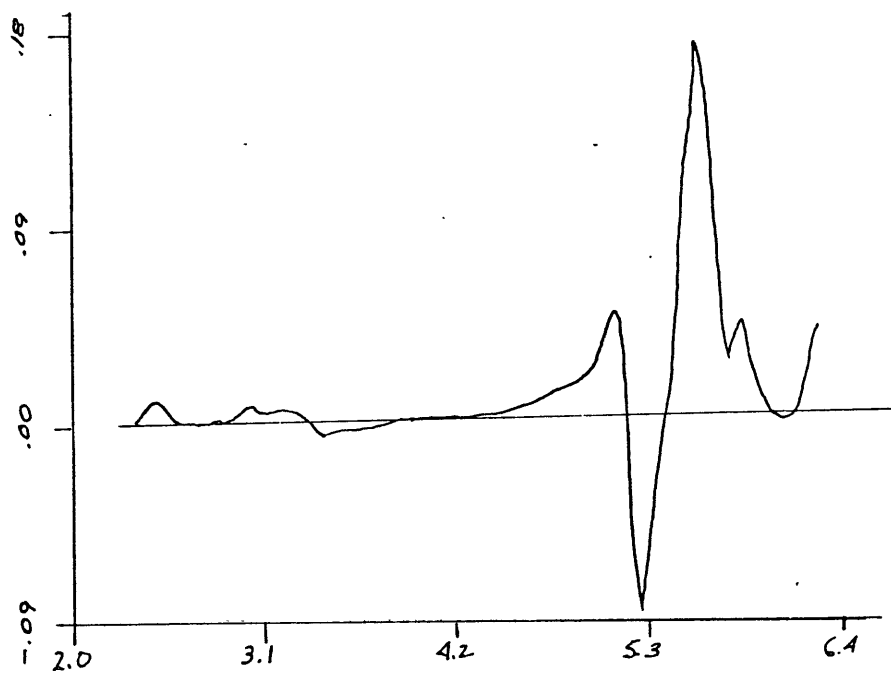


Fig. 45: z,5,III,C

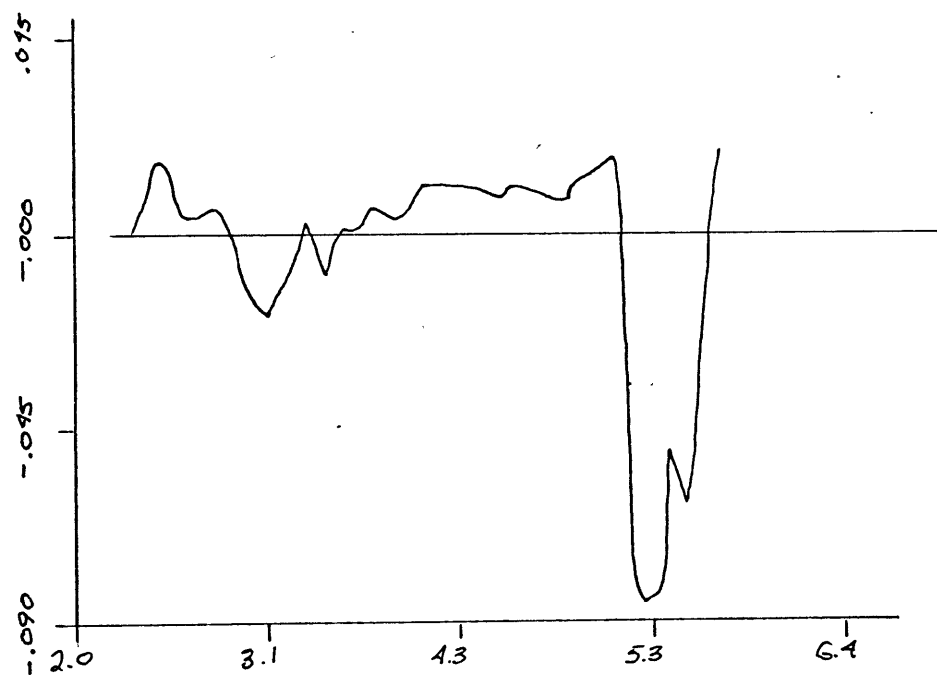


Fig. 46: r,5,III,C

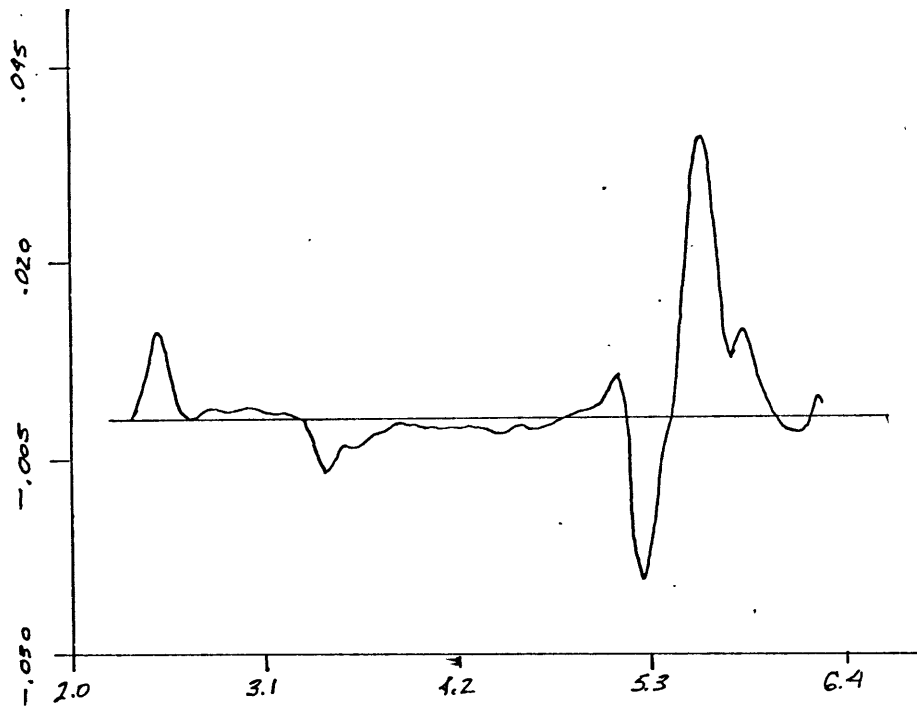


Fig. 47: z,5,III,C Shear source has been multiplied by 0.2 .

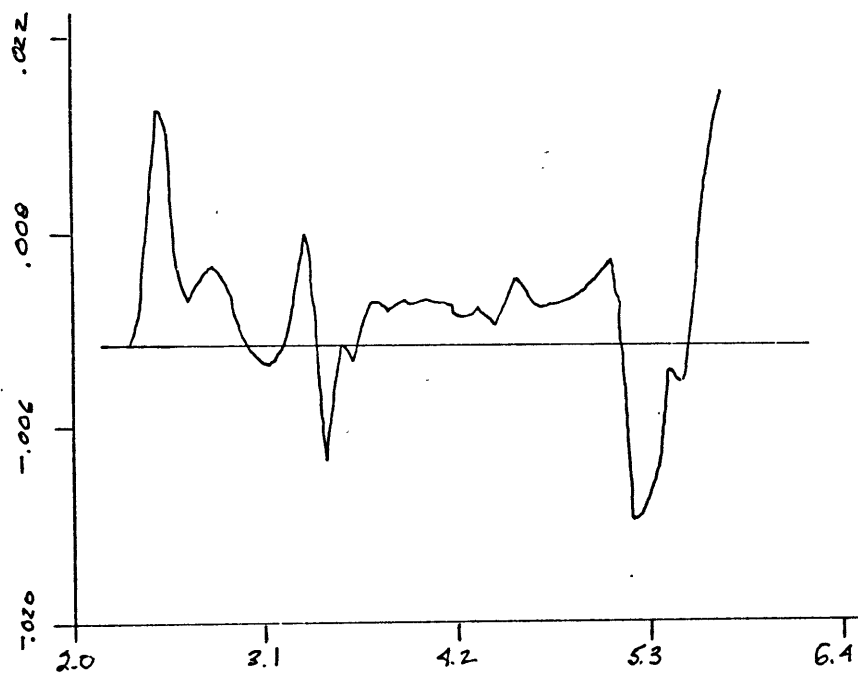


Fig. 48: r,5,III,C Shear source has been multiplied by 0.2 .

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3. Pekeris, C. L., Alterman, Z., Abramovici, F., and Jarosch, H., 1965, Propagation of a compressional pulse in a layered solid, Reviews of Geophysics, 3, p. 25.
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APPENDIX I

The reflection function describes the attenuation of energy due to internal reflections. The reflection function

$C_{\eta}(p)$ is given by

$$C_{\eta}(p) = R_{DPP}^{l_{DPP}^{(n)}} R_{DPS}^{l_{DPS}^{(n)}} R_{DSP}^{l_{DSP}^{(n)}} R_{DSS}^{l_{DSS}^{(n)}} R_{UPP}^{l_{UPP}^{(n)}} R_{UPS}^{l_{UPS}^{(n)}} R_{USP}^{l_{USP}^{(n)}} R_{USS}^{l_{USS}^{(n)}}$$

$l_{DPP}^{(n)}$ is the number of reflections of the P to P type off the lower boundary, $l_{UPP}^{(n)}$ is the number of P to P reflections off the free surface, etc. The reflection coefficients are computed from the conditions of continuity of stress and displacement at the interface, and are given by (from Helmburger, 1965):

$$R_{DPP} = (-① + ② + ③ - ④ + ⑤ + ⑥) / \mathcal{D}_1$$

$$R_{DPS} = 2p\eta_1 [(k_2 - p^2)(k_3 - p^2) - \eta_2 \eta_2' (k_1 - p^2)] / \mathcal{D}_1$$

$$R_{DSP} = -2p\eta_1' [(k_2 - p^2)(k_3 - p^2) - \eta_2 \eta_2' (k_1 - p^2)] / \mathcal{D}_1$$

$$R_{DSS} = (-① + ② + ③ - ④ + ⑤ - ⑥) / \mathcal{D}_1$$

$$\mathcal{D}_1 = ① + ② + ③ + ④ - ⑤ - ⑥$$

$$① = p^2 (k_3 - p^2)^2$$

$$② = \eta_1 \eta_2 \eta_1' \eta_2' p^2$$

$$③ = \eta_1 \eta_1' (k_3 - p^2)^2$$

$$④ = \eta_2 \eta_2' (k_1 - p^2)^2$$

$$⑤ = \eta_1 \eta_2' k_1 k_2$$

$$⑥ = \eta_2 \eta_1' k_1 k_2$$

$$k_1 = -\frac{1}{2} \left(\frac{\rho_1}{\mu_2 - \mu_1} \right) ; \quad k_2 = \frac{1}{2} \left(\frac{\rho_2}{\mu_2 - \mu_1} \right) ; \quad k_3 = k_1 + k_2$$

$$R_{UPP} = R_{USS} = [4\beta_1^4 p^2 \eta_1 \eta_1' - (1 - 2\beta_1^2 p^2)^2] / \mathcal{D}_2$$

$$R_{UPS} = 4p\eta_1 (1 - 2\beta_1^2 p^2) / \mathcal{D}_2$$

$$R_{USP} = -4p\eta_1' (1 - 2\beta_1^2 p^2) / \mathcal{D}_2$$

$$\mathcal{D}_2 = 4\beta_1^4 p^2 \eta_1 \eta_1' + (1 - 2\beta_1^2 p^2)^2$$

The receiver functions are included to take into account the effect of the free surface. For an impinging P (or SV) wave, we must add the upgoing P (or SV) wave to the reflected SV and P waves. The reflection coefficients are evaluated with the shear wave velocity and the rigidity set to zero for the medium above the free surface. The once-transformed displacements at the free surface due to an upgoing P wave are (derived from the stress free boundary condition--see Phinney, 1967):

$$(A1) \quad \bar{u}_z^P(r, 0, \Delta) = \frac{1}{2\pi^2(\lambda + 2\mu)} \, d\ln \int_0^{j\infty} \frac{p}{\eta_1} K_0(apr) \{ -\eta_1 + \eta_1' R_{UPP} - p R_{UPS} \} e^{-\eta_1 h}$$

$$(A2) \quad \bar{u}_r^P(r, 0, \Delta) = \frac{1}{2\pi^2(\lambda + 2\mu)} \, d\ln \int_0^{j\infty} \frac{p}{\eta_1} K_1(apr) \{ p + p R_{UPP} + \eta_1' R_{UPS} \} e^{-\eta_1 h}$$

and due to an upgoing SV wave are

$$(A3) \quad \bar{u}_z^S(r, 0, p) = \frac{1}{2\pi^2\mu} \text{clm} \int_0^{+\infty} \frac{p}{\eta_1'} K_0(\rho p r) \{-\rho - \rho R_{USS} + \eta_1 R_{USP}\} e^{-\eta_1' h}$$

$$(A4) \quad \bar{u}_r^S(r, 0, p) = \frac{1}{2\pi^2\mu} \text{clm} \int_0^{+\infty} \frac{p}{\eta_1'} K_1(\rho p r) \{-\eta_1' + \eta_1' R_{USS} + \rho R_{USP}\} e^{-\eta_1' h}$$

The functions in the brackets are our receiver functions. One need only to substitute the reflection coefficients given above and grind out the algebra. When this is done, the results are:

$$R_z^P(p) = \frac{-2\eta_1 (1 - 2p^2\beta_1^2)}{D}$$

$$R_r^P(p) = \frac{-4\beta_1^2 p \eta_1 \eta_1'}{D}$$

$$R_z^S(p) = \frac{-4\beta_1^2 p \eta_1 \eta_1'}{D}$$

$$R_r^S(p) = \frac{-2\eta_1' (1 - 2p^2\beta_1'^2)}{D}$$

where

$$D = (1 - 2p^2\beta_1^2)^2 + 4\beta_1^4 \eta_1 \eta_1' p^2$$

APPENDIX II

COMPUTER PROGRAM

Included here is a printout of the program used to evaluate equations (9) and (10). This program is an adaptation of one written by D. V. Helmberger. A brief description of how it works may be helpful. The program begins by defining the rays. A ray is described by the number of traverses across the layer that are made as a P wave, the number as an S wave, the reflection coefficients needed to be multiplied to form $C_r(\rho)$, and the mode at the receiver. For each ray the following procedure is followed. The program then computes the exact position p_0 at which $\frac{dp}{dc} \rightarrow \infty$, i.e., where the contour leaves the real axis. There is a singularity in the integrand at this point and special precautions must be taken. A series of values of real p are then generated. The spacing is weighted so that computation points are closely spaced near reflection, refraction, and surface wave arrival times, and sparsely spaced elsewhere. The imaginary parts of p corresponding to the real values just generated are computed. The functions of p are then evaluated for these values of complex p . The higher order terms are convolved with their appropriate functions of t and added to the lowest order term. The result is then convolved with $\frac{1}{\sqrt{x}}$. This is repeated for all the ray paths and the results are summed. An auxiliary program differentiates the output and convolves it with a source and receiver function to give the final answer.

```

C      MAIN
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON/ORSTF/C(100),S(100),D(100),TH(100),X
      COMMON/CONFIX/DEL,NN,NDP,TMX,XDIM,YDIM,DP,KD
      COMMON/STUFF/CC(100),SS(100),DD(100),TTH(100),XX,RCSQ(100),
1      RSSQ(100)
      COMMON/THY/T(1000),PP(1000),RP(600)
      DIMENSION R(10)
      COMMON/SYTH/XD11,YD11,XD22,YD22,XD33,YD33
      COMMON/PLOT/CON,NNF,NPT,NSYN
      COMMON/FIXP/DDN(100),ARN(100),FLAT
      COMMON/STOR/P(1000),TD(1000)
      COMMON/THZ/TT(1000),PPZ(1000),PPR(1000)
      COMMON/TINP/DELT,DLTM,NDA,MTD,DLTP,NDB,JO,NDIRT
      COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET
      COMMON/CTRSTF/NCASE,NPRAY,NYT,NDUM,VRL2,VRL3
      DIMENSION XL(2),YL1(4),YL2(4),YL3(4)
      DATA XL/'TIME SEC'/
      DATA YL2/' THEORETICAL UZ'/
      DATA YL3/' THEORETICAL UR'/
      LOGICAL PRNT,PRNTS,PRNTC,FLAT
      FLAT=.TRUE.
      PRNTS=.FALSE.
      PRNT=.FALSE.
      PRNTC=.FALSE.
      READ (5,100) NMDD
      DO 200 J=1,NMOD
200  READ (5,300) C(J),S(J),D(J),TH(J)
100  FORMAT (I10)
300  FORMAT (4F10.0)
600  READ(5,500) X,IGO,KPEK
500  FORMAT (F10.0,2I10)
      READ (5,501) DP,TMX,NN
501  FORMAT (2F10.0,I10)
      IF (KPEK) 700,800,800
800  S(3)=1.1*S(2)

```



```

C(2)=S(2)*SQRT(3.)
D(3)=D(2)/0.605
C(3)=S(2)*SQRT(3.63)
700 CONTINUE
XD22=10.
YD22=3.
YDIM=YD22
XDIM=XD22
CALL NEWPLT('M5207','5852','WHITE ','BLACK')
NNF=1
NPT=0
JO=3
CALL CURAY (JO)
DO 30 M=1,1
AMU=D(2)*(C(2)**2)/3.
CON=1./(6.*3.14159*AMU)
CON=1.
XX=X
MTD=2
DELT M=.0025
DMAX=1.E-4
DLTM=.1
NDP=30
DET=1.E-5
DTIM=DP
DEL=DP
DLTP=DP
NYT=3
VRL2=.92*S(2)
VRL3=.92*S(3)
NPRAY=40
K=NN/2
NCASE=1
CALL SETUP (1,0,01,01,0,0,0)
DO 20 J=1,NN
20 PP(J)=PPZ(J)

```

```

CALL STEP (NN,1,2,0,0,DP)
DO 21 J=1,NN
21  PP(J)=PPR(J)
CALL STEP (NN,1,2,0,0,DP)
IF (IGO) 30,30,600
30  CONTINUE
CALL ENDPLT
FND
SUBROUTINE RECVR (A1,B1,P,KR,DZ,DR,KSSP,RPP,RPS,RSP,RSS)
C      TO COMPUTE SURFACE RECEIVER AND REFLECTION FUNCTIONS
IMPLICIT COMPLEX*16 (A-H,O-Z)
REAL*8 A1,B1,BSQ
BSQ      = B1**2
PSQ      = P*P
ET       =CDSQRT((1./A1**2)-PSQ)
EP       =CDSQRT((1./BSQ )-PSQ)
D1       = 1.-2.*BSQ*PSQ
EE       = ET*EP*P*BSQ*4.
D2 = P*BSQ*EE
SDF=ET
IF (KSSP .EQ. 0) SDF=EP
DENA = D1**2 + D2
DEN   = SDF*DENA
R1    = 2.*D1/DEN
R2    = EE/DEN*(-1.)
IF (KR .EQ. 0) GO TO 100
C      P AT RCVR
DZ    = R1*ET
DR    =-R2
GO TO 200
100  CONTINUE
C      S AT RCVR
DZ    =-R2
DR    = R1*EP
200  CONTINUE
RPP = (-D1**2 + D2)/DENA

```

00000040

00000050

00000080

00000090

00000110

00000120

00000130

00000140

0000 V

00000170

00000180

00000190

00 210

00000220

R3 = 4.*P*D1/DENA	
RPS = R3*ET	
RSP = -R3*EP	
RSS = RPP	
RETURN	00000230
END	00000240
SUBROUTINE PLN1(PO,TO,K,N,TC,NRY,V2)	00000010
IMPLICIT REAL*8 (A-H,O-Z)	
COMMON/TINP/DELTM,DLTM,NDA,MTD,DLTP,NDB,JO,NDIRT	
COMMON/SPE/DELP(800),DD1,DD2,DD3,DD4,NO	
COMMON/ORSTF/C(100),S(100),D(100),TH(100),X	00000040
COMMON/TRESL/PZ1(500),PRI(500)	00000050
COMMON/MAGIC/PQ(1200),DDPT(1200),TTT(1200)	
COMMON/EXACT/PHIZ(1000),PHIR(1000),TT(1000),NEND,NM	
COMMON / LPRINT/ PRNT,PRNTS	00000080
LOGICAL PRNT,PRNTS	00000090
COMPLEX*16 PQ,DDPT,FNZ,FNR,FNZ1,FNR1,Q	
P = 1./V2	00000110
DO 80 I=2,NO	00000120
J = I-1	00000130
P = P+DELP(J)	00000140
Q = P+0.*(0.,1.)	00000150
CALL HELP(K,N,P,TTP,DTP,NRY)	00000160
IF(PRNT) PRINT 100,Q,P,DTP,TTP	00000170
TT(I) = TTP	00000180
DDPT(I) = DTP	00000190
CALL PSICO(Q,FNZ,FNR,FNZ1,FNR1,I,NRY)	00000200
IF(PRNT) PRINT 100,FNZ,FNR,FNZ1,FNR1	00000210
PHIZ(I) = FNZ * (0.,-1.)	
PHIR(I) = FNR * (0.,-1.)	
PZ1(I) = FNZ1 * (0.,-1.)	
PRI(I) = FNR1 * (0.,-1.)	
IF ((TO-TTP) .LT. DLTP) GO TO5	00000260
80 CONTINUE	00000270
100 FORMAT(8E15.4)	00000280
WRITE(6,100) PQ,TO	00000290

5	NO	= J+1	00000300
	I	= NO	00000310
4	IF(TO-TTP.LT.DLTP)	GO TO 3	00000320
	PP	= PO - P	00000330
	P	= P + PP/2.0	00000340
	I	= I+1	00000350
	NO	= I	00000360
	Q	= P	00000370
	CALL HELP(K,N,P,TTP,DTP,NRY)		00000380
	TT(I)	= TTP	00000390
	DDPT(I)	= DTP	00000400
	CALL PSICO(Q,FNZ,FNR,FNZ1,FNR1,I,NRY)		00000410
	IF(PRNT)	PRINT 100,FNZ,FNR,FNZ1,FNR1	00000420
	PHIZ(I)	= FNZ * (0.,-1.)	
	PHIR(I)	= FNR * (0.,-1.)	
	PZ1(I)	= FNZ1 * (0.,-1.)	
	PR1(I)	= FNR1 * (0.,-1.)	
	GO TO 4		00000470
3	TT(1)	= TC	00000480
	PHI7(1)	= 0.	00000490
	PHIR(1)	= 0.	00000500
	PR1(1)	= 0.	00000510
	PZ1(1)	= 0.	00000520
	RETURN		00000530
	END		00000540
	SUBROUTINE PLN2(PO,TO,K,MO,M,NRY)		00000010
	IMPLICIT REAL*8 (A-H,O-Z)		
	COMMON/FIXP/DDN(100),ARN(100)		00000020
	COMMON/TINP/DELT,DLTM,NDA,MTD,DLTP,NDB,JO,NDIRT		
	COMMON/MAGIC/PP(1200),DDPT(1200),TT(1200)		
	COMMON/EXACT/PHI7(1000),PHIR(1000),TTT(1000),NEND,NM		
	COMMON/TRESL/PZ1(500),PR1(500)		00000060
	COMMON/ORSTF/C(100),S(100),D(100),TH(100),X		00000070
	DIMENSION FF(50),GG(50)		00000080
	COMMON / LPRINT/ PRNT,PRNTS		00000090
	LOGICAL PRNT,PRNTS		00000100

	COMPLEX*16	PP,BT,DDPT,RP,RPP,GC,P	
	COMPLEX*16	FNZ,FNR,FNZ1,FNR1	
	DO 5	I=MO,M	00000130
	TTT(I)	= TT(I)	00000140
	P	= PP(I)	00000150
	CALL PSICO	(P,FNZ,FNR,FNZ1,FNR1,I,NRY)	00000160
	PHIZ(I)	= FNZ *(0.,-1.)	
	PHIR(I)	= FNR *(0.,-1.)	
	PR1(I)	= FNR1 *(0.,-1.)	
	PZ1(I)	= FNR1 *(0.,-1.)	
	IF(PRNT)	PRINT 100,FNZ,FNR,FNZ1,FNR1	00000210
5		CONTINUE	00000220
100		FORMAT(8E15.4)	00000230
3	NO	= MO-2	00000240
	DP	= DLTP	00000250
	P	= PD*(1.,0.)+0.*(0.,1.)	00000260
	I	= MO-1	00000270
	Q	= PD	00000280
	DDPT(I)	= SF2(Q,K,NRY,DP)	00000290
	TTT(I)	= TO	00000300
	WRITE(6,100)	P,DDPT(I)	00000310
	CALL PSICO	(P,FNZ,FNR,FNZ1,FNR1,I,NRY)	00000320
	IF(PRNT)	PRINT 100,FNZ,FNR,FNZ1,FNR1	00000330
	PREZ	= FNZ	
	PIMZ	= FNZ *(0.,-1.)	
	PRER	= FNR	
	PIMR	= FNR *(0.,-1.)	
	IF (PRNT)	PRINT 100,PREZ,PIMZ,PRER,PIMR	00000380
	F1	= 0.	00000390
	G1	= 0.	00000400
	SUM	= 0.	00000410
	TUM	= 0.	00000420
	IF(MO.LE.3)	GO TO 46	00000430
	TNN	= TO-DP	00000440
	CALL INTERP	(TTT,PHIZ,M,TNN,Y)	00000450
	F1	= Y	00000460

	FF(1) = Y	00000470
	CALL INTERP(TTT,PHIR,M,TNN,Y)	00000480
	G1 = Y	00000490
	GG(1) = Y	00000500
	SUM = SUM+2.*PIMZ*DSQRT(TO-TTT(NO))	
	TUM = TUM+2.*PIMR*DSQRT(TO-TTT(NO))	
	IF (PRNT) PRINT 4, SUM	00000530
	IF (PRNT) PRINT 7, TUM	00000540
7	FORMAT (5X'TUM = 'G18.6)	00000550
4	FORMAT (5X'SUM = 'G18.6)	00000560
	DELL = (TTT(NO)-TNN)/5.	00000570
	TT(1) = TNN	00000580
	FF(6) = PHIZ(NO)	00000590
	GG(6) = PHIR(NO)	00000600
	PHI7(I) = PHIZ(NO)	00000610
	PHIR(I) = PHIR(NO)	00000620
	DO 41 J=2,6	00000630
	TT(J) = TT(J-1) +DELL	00000640
	CALL INTERP(TTT,PHIZ,M,TT(J),Y)	00000650
	FF(J) = Y	00000660
	CALL INTERP(TTT,PHIR,M,TT(J),Y)	00000670
	GG(J) = Y	00000680
	TUM = TUM+(GG(J-1)+GG(J))/2.*DELL	00000690
	SUM = SUM+(FF(J-1)+FF(J))/2.*DELL	00000700
	IF (PRNT) PRINT 4, SUM	00000710
	IF (PRNT) PRINT 7, TUM	00000720
41	CONTINUE	00000730
46	TPP = TTT(MO)	00000740
	TT(1) = TTT(MO)	00000750
	IF(TTT(MO)-TO.GT.DP) GO TO 43	00000760
	SUM = SUM+2.*PREZ*DSQRT(TTT(MO)-TO)	
	TUM = TUM+2.*PRER*DSQRT(TTT(MO)-TO)	
	IF (PRNT) PRINT 4, SUM	00000790
	IF (PRNT) PRINT 7, TUM	00000800
	CALL INTERP(TTT,PHIZ,M,TPP,Y)	00000810
	FF(1) = Y	00000820

	CALL INTERP(TTT,PHIR,M,TPP,Y)	00000830
	GG(1) = Y	00000840
	DELL = (TO+DP-TTT(MO))/5.	00000850
	DO 42 J=2,6	00000860
	TT(J) = TT(J-1) +DELL	00000870
	CALL INTERP(TTT,PHIZ,M,TT(J),Y)	00000880
	FF(J) = Y	00000890
	CALL INTERP(TTT,PHIR,M,TT(J),Y)	00000900
	GG(J) = Y	00000910
	TUM = TUM+(GG(J-1)+GG(J))/2.*DELL	00000920
	SUM = SUM+(FF(J-1)+FF(J))/2.*DELL	00000930
	IF (PRNT) PRINT 4, SUM	00000940
	IF (PRNT) PRINT 7, TUM	00000950
42	CONTINUE	00000960
	F3 = FF(6)	00000970
	G3 = GG(6)	00000980
	PHIZ(I) = (3.*SUM/DP-F1-F3)/4.	00000990
	PHIR(I) = (3.*TUM/DP-G1-G3)/4.	00001000
	GO TO 44	00001010
43	TTT(MO) = TO+DP	00001020
	PHIZ(MO) = PREZ/(DP**0.5)	00001030
	PHIR(MO) = PRER/(DP**0.5)	00001040
	F3 = PHIZ(MO)	00001050
	G3 = PHIR(MO)	00001060
	SUM = SUM+2.*PREZ*DSQRT(DP)	
	TUM = TUM+2.*PRER*DSQRT(DP)	
	PHIZ(I) = (3.*SUM/DP-F1-F3)/4.	00001090
	PHIR(I) = (3.*TUM/DP-G1-G3)/4.	00001100
	IF (PRNT) PRINT 4, SUM	00001110
	IF (PRNT) PRINT 7, TUM	00001120
44	CONTINUE	00001130
	PREZ1 = FNZ1	
	PIMZ1 = FNZ1 * (0.,-1.)	
	PRER1 = FNR1	
	PIMR1 = FNR1 * (0.,-1.)	
	IF (PRNT) PRINT 100, PREZ1,PIMZ1,PRER1,PIMR1	00001180

	IF(MO.LE.3) GO TO 47	00001190
	DO 81 J=2,NO	00001200
	AREA = (PR1(J)+PR1(J-1))*(TTT(J)-TTT(J-1))	00001210
	PHIR(J) = PHIR(J)+AREA/2.	00001220
	AREA = (P71(J)+PZ1(J-1))*(TTT(J)-TTT(J-1))	00001230
	PHIZ(J) = PHIZ(J)+AREA/2.	00001240
81	CONTINUE	00001250
	PHIZ(I) = PHIZ(I)+2.*PIMZ1*DSQRT(TTT(I)-TTT(NO))	
	PHIR(I) = PHIR(I)+2.*PIMR1*DSQRT(TTT(I)-TTT(NO))	000 27
47	CONTINUE	00001280
	PHIZ(MO) = PHIZ(MO)+2.*PREZ1*DSQRT(TTT(MO)-TTT(I))	00 29
	PHIR(MO) = PHIR(MO)+2.*PRER1*DSQRT(TTT(MO)-TTT(I))	0000130
	JM = MO+1	00001310
	DO 82 J=JM,M	00001320
	AREA = (PR1(J)+PR1(J-1))*(TTT(J)-TTT(J-1))	00001330
	PHIR(J) = PHIR(J)+AREA/2.	00001340
	AREA = (PZ1(J)+PZ1(J-1))*(TTT(J)-TTT(J-1))	00001350
	PHIZ(J) = PHIZ(J)+AREA/2.	00001360
82	CONTINUE	00001370
	WRITE (6,111) TTT(I),PHIZ(I),PHIR(I)	
111	FORMAT (2X,'CRITICAL TIME',G20.8,5X,'PHIZ',G20.8,'PHIR',G20.8)	
	END	00001380
	SUBROUTINE CONTOR(TMX,M,KN,N,MO)	00000010
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMMON/MAGIC/PP(1200),DDPT(1200),TT(1200)	
	COMMON/SPE/DELP(800),DD1,DD2,DD3,DD4,NO	
	COMMON/PATHC/PO,TQ,K	00000040
	COMMON/TINP/DELTM,DLTM,NDA,MTD,DLTP,NDB,JO,NDIRT	
	COMMON/TFIX/TN1,TN2,TN3,TN4,JN1,JN2,JN3,JN4	00000060
	COMMON/CTRSTF/NCASE,NPRAY,NYT,NDUM,VRL2,VRL3	
	DIMENSION DER(400)	00000080
	LOGICAL PRNT,PRNTS,PRNTC	00000090
	COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET	
	COMPLEX*16 PP,DDPT,P,CT,DEV	
	JN = 10	00000120
1	Q = PO	00000130

	I	= MO-1	00000140
	PIL	= 1.E-6	00000150
	PP(I)	= PO	00000160
	TT(I)	= TO	00000170
	KM	= 100	00000180
	IF(DELP(1).LE.DELTM)	DELP(1)=DELTM	00000190
33	I	= KM-1	00000200
	L	= 0	00000210
	DO 10 J=1,JN		00000220
	L	= L+1	00000230
	I	= I+1	00000240
9	Q	= Q+DELP(J)	00000250
	PI	= PO*.2	00000260
	DL	= PI*.45	00000270
	CALL TIME2(Q,PI,DL,P,DEV,CT,KN,N,PIL)		00000280
	RTIME	= CT	
	TIMEI	= CT*(0..-1.)	
	DR	= DEV	
	DDPT(I)	= DEV	00000320
	TT(I)	= RTIME	00000330
	PP(I)	= P	00000340
	IF(TT(I)-TO.LE.DTIM)	GO TO 32	00000350
	IF(DR.LE.0.)	GO TO 30	00000360
	IF(DABS(TIMEI).GT.1.E-3)	GO TO 30	00000370
	IF(RTIME-TO.LT..001)	GO TO 30	00000380
	JJ	= J+1	00000390
	DELP(JJ)	= ((PO-PP(I))/2.)	
10	CONTINUE		00000410
30	IF(I.LE.KM)	DELP(1)=5.*DELP(1)	00000420
	IF(I.LE.KM)	GO TO 33	00000430
	I	= I-1	00000440
32	JJ	= I-KM+1	00000450
	DO 31 J=1,JJ		00000460
	LL	= MO+J-1	00000470
	NN	= I-J+1	00000480
	TT(LL)	= TT(NN)	00000490

	PP(LL) = PP(NN)	00000500
	DDPT(LL) = DDPT(NN)	00000510
31	CONTINUE	00000520
	I = LL	00000530
	DELP(JN) = (PP(LL)-PP(LL-1))	
	J = JN	00000550
	MM = 1	00000560
	TM = TMX+TO	00000570
	PI = PP(LL)*(0.-1.)	
	Q = PP(LL)	
	IF(NCASE.EQ.1)RG=DABS(1./VRL2-Q)	
	IF(NCASE.EQ.2)RG=DABS(1./VRL3-Q)	
	CALL DFLPS(NPRAY,RG,1,NYT)	00000620
	J1 = LL	00000630
	J2 = J1+NO	00000640
	IJ = 0	00000650
	DO 21 J=J1,J2	00000660
	IJ = IJ+1	00000670
21	DER(J) = DELP(IJ)	00000680
	JF = J2	00000690
	IF(NCASE.EQ.1) GO TO 23	00000700
	RG = DABS(1./VRL2-1./VRL3)	
	CALL DELPS(NPRAY,RG,1,NYT)	00000720
	J1 = J2+1	00000730
	J2 = J1+NO	00000740
	IJ = 0	00000750
	DO 24 J=J1,J2	00000760
	IJ = IJ+1	00000770
24	DER(J) = DELP(IJ)	00000780
	JF = J2	00000790
23	IF(PRNTC) WRITE(6,100) (DER(J),J=J1,J2)	00000800
100	FORMAT(6E12.4)	00000810
	DO 25 J=LL,JF	00000820
	Q = Q+DER(J)	00000830
	I = I+1	00000840
	DELPR = (PP(I-1)-PP(I-2))	

	DELPI	=	(PP(I-1)-PP(I-2))	*(0.,-1.)	
	PI	=	(DELPI*DER(J))/DELPR +PI	00000870
	DL	=	PI*.5		00000880
	CALL TIME2(Q,PI,DL,P,DEV,CT,KN,N,PIL)				00000890
	PP(I)	=	P		00000900
	RTIME	=	CT		
	DDPT(I)	=	DEV		00000920
	TT(I)	=	RTIME		00000930
	IF(TT(I).GT.TM) GO TO 13				00000940
25	CONTINUE				00000950
12	Q	=	Q+MM*DER(JF)		00000960
	I	=	I+1		00000970
	DELPR	=	(PP(I-1)-PP(I-2))		
	DELPI	=	(PP(I-1)-PP(I-2))	*(0.,-1.)	
	PI	=	(DELPI*MM*DER(JF))/DELPR +PI		00001000
	DL	=	PI*.5		00001010
	CALL TIME2(Q,PI,DL,P,DEV,CT,KN,N,PIL)				00001020
	PP(I)	=	P		00001030
	RTIME	=	CT		
	DDPT(I)	=	DEV		00001050
	TT(I)	=	RTIME		00001060
	IF(TT(I).GT.TM) GO TO 13				00001070
14	IF(TT(I)-TT(I-1).LE.DLTM) MM=MTD*MM				00001080
	GO TO 12				00001090
13	CONTINUE				00001100
	M	=	I		00001110
	FND				00001120
	SUBROUTINE DELPS (NNN,RG,NN,N)				00000010
	IMPLICIT REAL*8 (A-H,O-Z)				
	DIMENSION PP(200)				00000020
	COMMON/SPE/DELP(800),DD1,DD2,DD3,DD4,NO				00000030
	RG	=	RG-1.E-08		00000040
	PI	=	3.141593		00000050
	AN	=	PI/(NNN*2.)		00000060
	J	=	NN		00000070
	A	=	AN		00000080

	DEL P(J) = RG*(DSIN(A)**N)	00000090
	TO = DELP(J)	00000100
	A = A+AN	00000110
	K = 1	00000120
1	PP(1) = DELP(1)	00000130
	J = J+1	00000140
	K = K+1	00000150
	PP(K) = RG*DSIN(A)**N	
	DEL P(J) = PP(K)-PP(K-1)	00000170
	DEL P(J) = DABS (DELP(J))	00000180
	TO = TO+DELP(J)	00000190
	A = A+AN	00000200
	IF(TO.LT.RG) GO TO 1	00000210
2	NO = J-1	00000220
	END	00000230
	REAL FUNCTION SF2*8 (P,K,NRY,DP)	
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)	00000020
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)	00000030
	PSQ = P ** 2	00000040
	J = 2	00000050
	FSQ = DABS (RCSQ(J)-PSQ)	00000060
	E = DSQRT(ESQ)	00000 7
	TE = (TH(4)+TH(2)*LTP(NRY))*RCSQ(2)/(ESQ*E)	00000080
	ESQ = DABS (RSSQ(J)-PSQ)	000 0 9
	E = DSQRT(ESQ)	00000 00
	TF = (TH(3) + TH(2)*LTS(NRY))*RSSQ(2)/(ESQ*E) + TE	00000110
	TE = TE*2.	00000120
	SR = 1.	00000130
	SF2 = SR/DSQRT(TE)	00000140
	END	00000150
	SUBROUTINE HELP(K,N,P,TTP,DTP,NRY)	00000010
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)	00000020
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)	00000030
	COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET	

	LOGICAL PRNT,PRNTS,PRNTC,FLAT	00000050
100	FORMAT(10X,'SUB. HELP,P,E,TOTEM,BLTEM,DTP,TPP',/,6(E16.6))	00000060
	PSQ = P**2	00000070
	J = 2	00000080
	E = DSQRT(DABS(RCSQ(J)-PSQ))	00 0 9
	TOTEM = E*(TH(4)+TH(2)*LTP(NRY))	00000100
	BLTEM = -(TH(4)+TH(2)*LTP(NRY))/E	00000110
	IF(PRNTC) WRITE(6,100) P,E,TOTEM,BLTEM,DTP,TPP	00000120
	F = DSQRT(DABS(RSSQ(J)-PSQ))	0000 T
	TOTEM = TOTEM+TH(2)*LTS(NRY)*E +TH(3)*E	00000140
	BLTEM = BLTEM-TH(2)*LTS(NRY)/E -TH(3)/E	00000150
	BL = X + P*BLTEM	00000160
	TO = P*X + TOTEM	00000170
	DTP = 1./BL	00000180
	TPP = TO	00000190
	IF(PRNTC) WRITE(6,100) P,E,TOTEM,BLTEM,DTP,TPP	00000200
	RETURN	00000210
	END	00000220
	SUBROUTINE TIME2(PR,PI,DL,Q,DPT,T,KN,N,PIL)	00000010
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)	00000020
	COMMON/PATHC/PO,TO,K	00000030
	DIMENSION E(100)	00000040
	COMPLEX*16 P,E,BL,T,PC,DPT,Q	00000060
	DIMENSION Y1(50),Y4(50),X1(50),X4(50)	00000070
	COMMON/STUFF/C(100),S(100),D(100),TH(100),R	00000080
	LOGICAL PRNT,PRNTS,PRNTC	00000090
	COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET	
	NRY = N	00000110
	X1M = 1.E+4	00000120
	X4M = 0.0	00000130
	NNN = 0	00000140
	I = 0	00000150
6	P = PR*(1.,0.)+PI*(0.,1.)	00000160
	T = P*R	00000170
	J = 2	00000180

	BL	= 1./ (C(J)**2)-P*P	00000190
	E(J)	= CDSQRT(BL)	00000200
	T	= T+E(J)*(TH(4)+TH(2)*LTP(NRY))	00000210
	J	= 3	00000220
	BL	= 1./ (S(2)**2)-P*P	00000230
	E(J)	= CDSQRT(BL)	00000240
	T	= T+E(J)*(TH(3)+TH(2)*LTS(NRY))	00000250
	IF(PRNTC)	WRITE(6,110) P,E(2),T	00000260
	TI	= T*(0.,-1.)	
	IF (DABS(TI) .LE. DET)	GO TO 2	
	IF(I.GT.15)	GO TO 2	00000290
	I	= I+1	00000300
	X1(I)	= 100.	00000310
	X4(I)	= 0.0	00000320
	IF(TI.GT.0.)	Y1(I)=TI	00000330
	IF(TI.GT.0.)	X1(I)=PI	00000340
	IF(TI.LT.0.)	Y4(I)=TI	00000350
	IF(TI.LT.0.)	X4(I)=PI	00000360
	IF(I.EQ.1)	GO TO 43	00000370
	IF(NNN.GT.1)	GO TO 44	00000380
	IF(TI*TL.LF.0.)	GO TO 44	00000390
43	IF(TI.GT.0.)	PI=PI-DL	00000400
	IF(TI.LE.0.)	PI= PI+DL	00000410
	IF(PI.LE.1.E-5)	PI=PK/2.	00000420
	NNN	= 1	00000430
	PK	= PI	00000440
	TL	= TI	00000450
	GO TO 6		00000460
44	DO 52 J=1,I		00000470
	IF(X1(J).GT.X1M)	GO TO 53	00000480
	X1M	= X1(J)	00000490
	NJ	= J	00000500
53	IF(X4(J).LE.X4M)	GO TO 54	00000510
	X4M	= X4(J)	00000520
	MJ	= J	00000530
54	CONTINUE		00000540

52	CONTINUE	00000550
	Y1M = Y1(NJ)	00000560
	Y4M = Y4(MJ)	00000570
	DPI = (X1M-X4M)/(Y1M-Y4M)	00000580
	DPM = Y1M*DPI	00000590
	PI = X1M-DPM	00000600
	NNN = 2	00000610
	IF(PI.LE.PIL) PI=PIL	00000620
	GO TO 6	00000630
2	CONTINUE	00000640
	BL = 0.	00000650
	BL = BL-(TH(4)+TH(2)*LTP(NRY))/E(2)	00000660
	BL = BL-TH(2)*LTS(NRY)/E(3)-TH(3)/E(3)	00000670
	BL = R+P*BL	00000680
	Q = P	00000690
	DPT = 1./BL	00000700
	IF(PRNTC) WRITE(6,110) P,E(2),T,DPT	00000710
110	FORMAT (1H0,4X'P = '2G18.6/5X'E(1) ='2G17.6/5X'T = '2G18.6/ +5X'DPT ='2G18.6)	00000720
	END	00000730
	SUBROUTINE HIGH(NDP, TMX, K, KI, N)	00000740
	IMPLICIT REAL*8 (A-H, O-Z)	00000010
	COMMON/RAYPAR/KUD(100), KRSP(100), LTS(100), LTP(100), LREF(100, 8)	00000020
	COMMON/PLACE/THIC, H, KSSP	00000030
	COMMON/EXACT/PHIZ(1000), PHIR(1000), TD(1000), NEND, NM	
	COMMON/MAGIC/PP(1200), DDPT(1200), TT(1200)	
	COMMON/SPE/DELP(800), DD1, DD2, DD3, DD4, NO	
	COMMON/PATHC/PO, TO, KK	00000070
	COMMON/TINP/DELTM, DLTM, NDA, MTD, DLTP, NDB, JO, NDIRT	
	COMMON/ORSTF/CC(100), SS(100), DD(100), TTH(100), XX	00000090
	COMMON / LPRINT/ PRNT, PRNTS	00000100
	LOGICAL PRNT, PRNTS	00000110
	COMPLEX*16 PP, DDPT	
	JN1 = 12	00000130
	JN2 = 10	00000140
	JN3 = 8	00000150

	JN4	= 100	00000160
	TN1	= .8	00000170
	TN2	= .2	00000180
	TN3	= .1	00000190
	TN4	= .001	00000200
	V2	= CC(3)	00000210
	NRV	= N	00000220
	KNRY	= NRV*KSSP	00000230
	DEL	= 1./SS(2)	00000240
	IF(LTP(NRV).GT.0)	GO TO 82	00000250
	IF(KSSP.EQ.0)	GO TO 81	00000260
82	DEL	= 1./CC(2)	00000270
81	P	= -1.E-9	00000280
	DET	= 1.E+12	00000290
	CALL FIND2(P, KK, DEL, DET, PO, TO, N)		00000300
	NNN	= NDP	00000310
	NK	= 2	00000320
	IF(NRV.EQ.1)	V2= CC(2)	00000330
	IF(KNRY.EQ.1)	V2=.9*CC(2)	00000340
	P	= 1./V2	00000350
	RG	=DABS(PO-P)	
	CALL HELP(K, N, P, TTP, DTP, N)		00000370
	TC	= TTP	00000380
	TG	= TO-TTP	00000390
	IF(PO.LE.1./V2)	GO TO 6	00000400
	IF(TG.GT.TN1)	GO TO 6	00000410
	JN	= JN1	00000420
	IF(TG.GT.TN2)	GO TO 18	00000430
	JN	= JN2	00000440
	IF(TG.GT.TN3)	GO TO 18	00000450
	JN	= JN3	00000460
18	QZ	= RG/(JN+1)	00000470
	DO 15 J = 1, JN		00000480
	DELP(J)	= QZ	00000490
15	CONTINUE		00000500
	NO	= JN	00000510

	IF(TG.LT.TN4) GO TO 2	00000520
	GO TO 19	00000530
6	CALL DELPS(NNN, RG, 1, NK)	00000540
	IF (.NOT.PRNT) GO TO 19	00000550
	PRINT 7, V2, XM, PO, RG, TC, TO, (DELP(J), J=1, NO)	00000560
7	FORMAT (1H0, 4X'V2 = 'G13.6, 5X'XM = 'G13.6, 5X'PO = 'G13.6/5X'RG = 'G13.6, 5X'TC = 'G13.6, 5X'TO = 'G13.6/5X'DELP'/(G15.6))	00000570
19	IF(PO.LE.1./V2) GO TO 2	00000590
	CALL PLN1(PO, TO, K, N, TC, N, V2)	00000600
2	MO = NO+2	00000610
	IF(TG.LT.TN4) MO=2	00000620
	IF(PO.LT.1./V2) MO=2	00000630
	CALL CONTOR(TMX, M, KN, N, MO)	00000640
	IF (.NOT.PRNT) GO TO 620	00000650
	WRITE (6, 5)	00000660
5	FORMAT (1H0, 13X'PP'27X'DDPT'24X'TT')	00000670
	JJ = MO	00000680
	WRITE(6, 200) (PP(J), DDPT(J), TT(J), J=JJ, M)	00000690
200	FORMAT(5E15.4)	00000700
620	CALL PLN2(PO, TC, K, MO, M, N)	00000710
	NEND = M	00000720
	NM = NO	00000730
	IF(PO.LT.1./V2) NM=0	00000740
	IF(TG.LT.TN4)NM= 0	00000750
	LK =-19	00000760
	WRITE (6, 98)	00000770
	KJMP = 5	
	LK = 1-KJMP	
97	LK =LK+KJMP	
	IF (LK .GT. NFND) GO TO 99	00000790
	WRITE (6, 100) TD(LK), PHIZ(LK), PHIR(LK), LK	00000800
	GO TO 97	00000810
99	CONTINUE	00000820
98	FORMAT (12X, 'SUB. HIGH TD, PHIZ, PHIR', 2X)	00000830
100	FORMAT (3E18.6, I10)	
	FND	00000850

	SUBROUTINE RAYDEF	00000010
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)	00000020
	COMMON/PLACE/THIC,H,KSSP	00000030
	COMMON /LPRINT/ PRNT,PRNTS	00000040
	LOGICAL PRNT,PRNTS	00000050
	REAL*8 THIC,H	
	WRITE (6,800)	00000060
	READ (5,400) THIC,H,KSSP	00000070
1200	FORMAT(4I1)	00000080
	WRITE (6,700) THIC,H	
700	FORMAT (/10X,'LAYER THICKNESS ',F6.3/10X,'SOURCE DEPTH',F6.3)	
	IF (KSSP .EQ. 0) WRITE (6,1300)	
	IF (KSSP .EQ. 1) WRITE (6,1400)	
1300	FORMAT (15X,'SHEAR SOURCE')	
1400	FORMAT (15X,'COMPRESSIGNAL SOURCE')	
	READ(5,1200) (KUD(J),LTS(J),LTP(J),KRSP(J),J=19,64)	00000090
	LTP(1) = 0	00000100
	LTP(2) = 1	00000110
	LTP(3) = 0	00000120
	LTP(4) = 2	00000130
	LTP(5) = 1	00000140
	LTP(6) = 0	00000150
	LTP(7) = 3	00000160
	LTP(8) = 2	00000170
	LTP(9) = 1	00000180
	LTP(10) = 0	00000190
	LTP(11) = 1	00000200
	LTP(12) = 2	00000210
	LTP (13)= 1	00000220
	LTP (14)= 2	00000230
	LTP (15)= 1	00000240
	LTP (16)= 4	00000250
	LTP (17)= 0	00000260
	LTP (18)= 5	00000270
	LTS(1) = 0	00000280
	LTS(2) = 0	00000290

LTS(3)	= 1	00000300
LTS(4)	= 0	00000310
LTS(5)	= 1	00000320
LTS(6)	= 2	00000330
LTS(7)	= 0	00000340
LTS(8)	= 1	00000350
LTS(9)	= 2	00000360
LTS(10)	= 3	00000370
LTS(11)	= 2	00000380
LTS(12)	= 1	00000390
LTS (13)	= 1	00000400
LTS (14)	= 1	00000410
LTS (15)	= 2	00000420
LTS (16)	= 0	00000430
LTS (17)	= 4	00000440
LTS (18)	= 0	00000450
KUD(1)	= 1	00000460
KUD(2)	= 0	00000470
KUD(3)	= 0	00000480
KUD(4)	= 1	00000490
KUD(5)	= 1	00000500
KUD(6)	= 1	00000510
KUD(7)	= 0	00000520
KUD(8)	= 0	00000530
KUD(9)	= 0	00000540
KUD(10)	= 0	00000550
KUD(11)	= 0	00000560
KUD(12)	= 0	00000570
KUD (13)	= 1	00000580
KUD (14)	= 0	00000590
KUD (15)	= 0	00000600
KUD (16)	= 1	00000610
KUD (17)	= 1	00000620
KUD (18)	= 0	00000630
KRSP(1)	= 1	00000640
KRSP(2)	= 1	00000650

	KRSP(3) = 0		00000660
	KRSP(4) = 1		00000670
	KRSP(5) = 0		00000680
	KRSP(6) = 0		00000690
	KRSP(7) = 1		00000700
	KRSP(8) = 0		00000710
	KRSP(9) = 0		00000720
	KRSP(10) = 0		00000730
	KRSP(11) = ①	— WRONG, IMPOSSIBLE	00000740
	KRSP(12) = ①	— WRONG	00000750
	KRSP (13)= 1		00000760
	KRSP (14)= 1		00000770
	KRSP (15)= 0		00000780
	KRSP (16)= 1		00000790
	KRSP (17)= 0		00000800
	KRSP (18)= 1		00000810
	KR = 18		00000820
	DO 200 NR=1,KR		00000830
	DO 100 K=1,8		00000840
100	LREF(NR,K) = 0		00000850
200	CONTINUE		00000860
	IF (KSSP .EQ. 0) GO TO 300		00000870
C	P SOURCE		00000880
	LREF(2,1)= 1		00000890
	LREF(3,2)= 1		00000900
	LREF(4,5)= 1		00000910
	LREF(4,1)= 1		00000920
	LREF(5,5)= 1		00000930
	LREF(5,2)= 1		00000940
	LREF(6,6)= 1		00000950
	LREF(6,4)= 1		00000960
	LREF(7,1)= 2		00000970
	LREF(7,5)= 1		00000980
	LREF(8,1)= 1		00000990
	LREF(8,5)= 1		00001000
	LREF(8,2)= 1		00001010

LREF(9.4)= 1		00001020
LREF(9.1)= 1		00001030
LREF(9.6)= 1		00001040
LREF(10.2)	= 1	00001050
LREF(10.8)	= 1	00001060
LREF(10.4)	= 1	00001070
LREF(11.7)	= 1	00001080
LREF(11.8)	= 1	00001090
LREF(11.3)	= 1	00001100
LREF(12.2)	= 1	00001110
LREF(12.7)	= 1	00001120
LREF(12.1)	= 1	00001130
LREF(13.3)	= 1	00001140
LREF(13.6)	= 1	00001150
LREF(14.1)	= 1	00001160
LREF(14.3)	= 1	000 X
LREF(14.6)	= 1	00001180
LREF(15.2)	= 2	00001190
LREF(15.7)	= 1	00001200
LREF(16.1)	= 2	00001210
LREF(16.5)	= 2	00001220
LREF(17.4)	= 2	00001230
LREF(17.6)	= 1	00001240
LREF(17.8)	= 1	00001250
LREF(18.1)	= 3	00001260
LREF(18.5)	= 2	00001270
READ(5.1000) IB,IE		00001280
RFAD(5.1100) ((LREF(II,JJ),JJ=1,8),II=IB,IE)		00001290
GO TO 900		00001300
CONTINUE		00001310
S SOURCE		00001320
LREF(2.3)= 1		00001330
LREF(3.4)= 1		00001340
LREF(4.7)= 1		00001350
LREF(4.1)= 1		00001360
LREF(5.7)= 1		00001370

300

C

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LREF(5,2)= 1
LREF(6,8)= 1
LREF(6,4)= 1
LRFF(7,3)= 1
LREF(7,1)= 1
LREF(7,5)= 1
LREF(8,3)= 1
LREF(8,5)= 1
LRFF(8,2)= 1
LREF(9,3)= 1
LREF(9,6)= 1
LREF(9,4)= 1
LREF(10,4) = 2
LREF(10,8) = 1
LREF(11,4) = 1
LREF(11,8) = 1
LREF(11,3) = 1
LREF(12,4) = 1
LREF(12,7) = 1
LREF(12,1) = 1
LREF(13,3) = 1
LREF(13,8) = 1
LREF(14,3) = 2
LREF(14,6) = 1
LREF(15,2) = 1
LREF(15,4) = 1
LREF(15,7) = 1
LRFF(16,1) = 2
LREF(16,5) = 1
LREF(16,7) = 1
LREF(17,4) = 2
LREF(17,8) = 2
LREF(18,1) = 2
LREF(18,3) = 1
LREF(18,5) = 2
RFAD(5,1000) IB,IE

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00001380
00001390
00001400
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0000147C
00001480
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00001570
00001580
00001590
00001600
0000161C
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730

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	READ(5,1100) ((LREF(II,JJ),JJ=1,8),II=IB,IE)	00001740
C		00001750
	900 CONTINUE	00001760
	1000 FORMAT(2I5)	00001770
	1100 FORMAT(8I1)	00001780
	IF (PRNT) WRITE(6,500) (KUD(J),J=1,KR),(KRSP(J),J=1,KR),	00001790
	1 (LTP(J),J=1,KR),(LTS(J),J=1,KR)	00001800
	IF (PRNT) WRITE (6,600) ((LREF(J,L),L=1,8),J=1,6)	00001810
	IF (PRNT) WRITE (6,600) ((LREF(J,L),L=1,8),J=7,12)	00001820
	400 FORMAT (2F10.0,I10)	00001840
	500 FORMAT (' RAYDEF',4(12I2,2X))	00001850
	600 FORMAT (' R2',6(8I2,2X))	00001860
	800 FORMAT (10X,'WHOOPIE, WE MADE IT TO RAYDEF')	00001880
	RETURN	00001890
	END	00001900
	COMPLEX FUNCTION CR*16 (P,C)	
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMPLEX*16 P,CZ	
	CZ=1./C**2-P*P	
	U=CZ	
	X=CZ*(0.-1.)	
	R=DSQRT(X*X + U*U)	
	W1= DABS(R+U)/2.	
	W2= DABS(R-U)/2.	
	R1=DSQRT(W1)	
	R2=DSQRT(W2)	
	CR=R1-R2*(0..1.)	
	END	
	REAL FUNCTION CONVS*8 (FA,FP,DEL,NF,N)	
	IMPLICIT REAL*8 (A-H,O-Z)	
	DIMENSION FP(1000),FA(1000)	
C	COMPUTES CONVOLUTION OF FP AND FA T=DEL*2N	00000030
C	NF MUST BE ODD	00000040
	NN = N	00000050
	DN = DEL	00000060
	IF(NN.LT.1) GO TO 2	00000070

	NDO	=	MINO(NN,(NF-1)/2)	00000080
	IP	=	2	00000090
	NP	=	2*NN	00000100
	EVEN	=	FP(IP)*FA(NP)	00000110
	ODD	=	0	00000120
	IF(NDO.LT.2)	GO TO 11		00000130
	DO 10 I=2,NDO			00000140
	IP	=	IP+1	00000150
	NP	=	NP-1	00000160
	ODD	=	ODD+FP(IP)*FA(NP)	00000170
	IP	=	IP+1	00000180
	NP	=	NP-1	00000190
	EVEN	=	EVEN+FP(IP)*FA(NP)	00000200
10	CONTINUE			00000210
11	CONTINUE			00000220
	ENDS	=	FP(1)*FA(2*NN+1)+FP(IP+1)*FA(NP-1)	00000230
	CONVS	=	DN*(ENDS+4.*EVEN+2.*ODD)/3.	00000240
	RETURN			00000250
2	CONVS	=	0.	00000260
	END			00000270
	SUBROUTINE FA(DEL,J2)			00000010
	IMPLICIT REAL*8 (A-H,O-Z)			
	COMMON/SRF/F(1000)			00000020
	DO 5 J=2,J2			00000030
	F(J)	=	1./(((J-1)*DEL)**.5)	00000040
5	CONTINUE			00000050
	F(1)	=	(11.-4.*2.**.5)/((2.*DEL)**.5)	00000060
	END			00000070
	SUBROUTINE STEP(NFA,NFAD,NDECK,NPLOT,NPRT,DP)			00000010
	IMPLICIT REAL*8 (A-H,O-Z)			
	COMMON/SYTH/XD11,YD11,XD22,YD22,XD33,YD33			00000020
	COMMON/SRF/F(1000)			00000030
	COMMON/THY/T(1000),PP(1000),RP(600)			
	COMMON/STOR/P(1000),TD(1000)			
	DIMENSION XL(2),YL1(4),YL2(4),YL3(4)			00000060
	DATA XL/'TIME SEC'/			00000070

	DATA YL3/' STEP RESPONSE '/	00000080
	L = 0	00000090
	CALL FA(DP,NFA)	00000100
	NFF = NFA/2	00000110
	DO 20 N=1,NFF,NFAD	00000120
	L = L+1	00000130
	P(L) = CONVS(PP,F,DP,NFA-1,N-1)	00000140
	TD(L) = 2.*DP*(N-1)	00000150
20	CONTINUE	00000160
	IF(NDECK.LT.1) GO TO 1	00000170
	NN = L	00000180
	WRITE(7,200) NN,NN,NN	00000190
	WRITE(7,100) TD(1),DP,DP	00000200
	WRITE(7,100) (P(J),J=1,L)	00000210
1	IF(NPRT.LT.1) GO TO 2	00000220
	WRITE(6,300) (TD(J),P(J),J=1,L)	00000230
2	IF(NPLOT.LT.1) GO TO 3	00000240
	CALL PICTUR(XD22,YD22,XL,-8,YL3,-16,	00000250
	2 TD,P,L,0.,0)	00000260
3	CONTINUE	00000270
100	FORMAT(5E15.6)	00000280
200	FORMAT(3I10)	00000290
300	FORMAT(4E15.6)	00000300
	END	00000310
	SUBROUTINE SETUP(K,MM,NS,NO,MO,MPL0T,MPUNCH)	00000010
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMMON/CONFIX/DEL,NN,NDP,TMX,XDIM,YDIM,DP,KO	00000020
	COMMON/FOURCT/MF,NMF,KMF,KNMF	00000030
	COMMON/THZ/TT(1000),PPZ(1000),PPR(1000)	
	COMMON/EXACT/PHI7(1000),PHIR(1000),TD(1000),NEND,NM	
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)	00000060
	COMMON/PLACE/THIC,H,KSSP	00000070
	COMMON/LPRINT/PRNT,PRNTS	00000080
	LOGICAL PRNT,PRNTS	00000090
	DIMENSION XL(2),YL1(4),YL2(4),YL3(4)	00000100
	DATA YL2/' THEORETICAL PD '/	00000110

	DATA XL/'TIME SEC'/	00000120
	IF(MO.EQ.0) CALL RAYDEF	00000130
	NF = 1	00000140
	IF(MO.GT.1) GO TO 11	00000150
	I = K	00000160
	TT(1) = TS(I)	00000170
	PPZ(1) = 0.	00000180
	PPR(1) = 0.	00000190
	DO 10 J=2,NN	00000200
	TT(J) = TT(J-1) +DEL	00000210
	PPZ(J) = 0.	00000220
	PPR(J) = 0.	00000230
10	CONTINUE	00000240
11	CONTINUE	00000250
	DO 32 N=NS,NO	00000260
	WRITE (6,103) N	
103	FORMAT (5X,'RAY NUMBER',I3)	
	CALL HIGH(NDP,TMX,K,KI,N)	00000270
	CALL ADJUST(NN,NFIX)	00000280
	N2 = 1	00000290
	M = NM+1	00000300
	IF(NFIX.LT.1) GO TO 37	00000310
	N2 = NFIX+1	00000320
	N1 = NFIX-1	00000330
	IF(N1.LE.2) GO TO 42	00000340
	DO 31 J=1,N1	00000350
	CALL INTERP(TD,PHIZ,NEND,TT(J),Y)	00000360
	PPZ(J) = PPZ(J)+Y*NF	00000370
	CALL INTERP(TD,PHIR,NEND,TT(J),Y)	00000380
	PPR(J) = PPR(J)+Y*NF	00000390
31	CONTINUE	00000400
42	CONTINUF	00000410
	PPZ(NFIX)= PPZ(NFIX)+NF*PHIZ(M)	00000420
	PPR(NFIX)= PPR(NFIX)+NF*PHIR(M)	00000430
37	CONTINUF	00000440
	DO 33 J=N2,NN	00000450

	CALL INTERP(TD,PHI7,NEND,TT(J),Y)	00000460
	PPZ(J) = PPZ(J)+Y*NF	00000470
	CALL INTERP(TD,PHIR,NEND,TT(J),Y)	00000480
	PPR(J) = PPR(J)+Y*NF	00000490
33	CONTINUE	00000500
	L=0	
32	CONTINUE	00000510
7	IF(.NOT.PRNT) GO TO 12	00000520
	PRINT 13,(TD(J),PHIZ(J),PHIR(J),J=1,NEND)	00000530
	PRINT 14,(TT(J),PPZ(J),PPR(J),J=1,NN)	00000540
13	FORMAT (1H0,15X,'TD',15X,'PH',/,3(E18.6))	00000550
14	FORMAT (1H0,15X,'TT',15X,'PP',/,3(E18.6))	00000560
12	IF(MPLOT.LT.1) GO TO 1	00000570
	CALL PICTUR(XDIM,YDIM,XL,-8,YL2,-16,	00000580
	2 TT,PPZ,NN,0.,0)	00000590
	CALL PICTUR(XDIM,YDIM,XL,-8,YL2,-16,	00000600
	2 TT,PPR,NN,0.,0)	00000610
1	CONTINUE	00000620
	IF(MPUNCH.LT.1) GO TO 2	00000630
	LN = NN	00000640
	NK = LN	00000650
	DEL = DP	00000660
	WRITE(7,100) TT(1),DP,DEL	00000670
	WRITE(7,200) NN,LN,NK	00000680
	WRITE(7,100) (PPZ(J),J=1,LN)	00000690
	WRITE(7,100) (PPR(J),J=1,LN)	00000700
2	CONTINUE	00000710
200	FORMAT(3I10)	00000720
100	FORMAT (5E15.6)	00000730
	RETURN	00000740
	END	00000750
	SUBROUTINE ADJUST(NN,NFIX)	00000010
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMMON/EXACT/PHIZ(1000),PHIR(1000),TD(1000),NEND,NM	
	COMMON/THZ/ T(1000),PPZ(1000),PPR(1000)	
	M = NM+1	00000040

	TR	= TD(M)	00000050
	I	= 0	00000060
80	I	= I+1	00000070
	IF(I.GT.NN)	GO TO 70	00000080
	IF(T(I).GT.TR)	GO TO 81	00000090
	GO TO 80		00000100
81	DNE	= TR-T(I-1)	00000110
	DPL	= T(I)-TR	00000120
	IF (DABS(DNE) .GT. DABS(DPL))	GOT 0 83	
	DELTA	= -DNE	00000140
	NFIX	= I-1	00000150
	GO TO 85		00000160
83	DELTA	= DPL	00000170
	NFIX	= I	00000180
85	DO 84 J=1,NEND		00000190
	TD(J)	= TD(J)+DELTA	00000200
84	CONTINUE		00000210
	RETURN		00000220
70	NFIX	= 0	00000230
	END		00000240
	REAL FUNCTION TS*8 (K)		
	IMPLICIT REAL*8 (A-H,O-Z)		
	COMMON/PLACE/THIC,H,KSSP		00000020
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)		00000030
	COMMON/ORSTF/CC(100),SS(100),DD(100),TTH(100),XX		00000040
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)		00000050
	DIMENSION T(200)		00000060
	COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET		
	LOGICAL PRNT,PRNTS		00000080
	DO 10 N=1,2		00000090
	DEL	= 1./SS(2)	00000100
	IF(KSSP.EQ.0)	GO TO 81	00000110
	IF(LTS(N).GT.0)	GO TO 81	00000120
	DEL	= 1./CC(2)	00000130
81	P	= -1.E-9	00000140
	DET	= 1.E+12	00000150

	CALL FIND2(P,M,DEL,DET,PO,TO,N)	00000160
	P = 1./CC(N+1)	00000170
	TTP = TO	00000180
	IF(PO.LE.P) GO TO 6	00000190
	CALL HELP(K,N,P,TTP,DTP,N)	00000200
6	T(N) = DMIN1(TO,TTP)	00000210
10	CONTINUE	00000220
	TS = DMIN1(T(1),T(2))	000 02T
	N = 2	00000240
	IF (PRNT)WRITE (6,1) (T(J),J=1,N)	00000250
1	FORMAT (5X,'T 1,2,3',3(E18.6))	00000260
100	FORMAT(I10,2E18.6)	00000270
	RETURN	00000280
	END	00000290
	SUBROUTINE PSICO (P,FNZ,FNR,FNZ1,FNR1,I,NRY)	00000010
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)	00000020
	COMMON/ORSTF/C(100),S(100),D(100),TH(100),X	00000030
	COMMON/MAGIC/PP(1200),DDPT(1200),TT(1200)	
	COMMON/PLOTG/CCN,NNF,NPT	00000050
	COMMON/PLACE/THIC,H,KSSP	00000060
	COMMON /LPRINT/ PRNT,PRNTS	00000070
	COMPLEX*16 P,RF,DZ,DR,G1,G2,G3,FNZ,FNR,FNZ1,FNR1,RC ,DDPT ,PP	
1	,RPP,RPS,RSP,RSS	00000090
	LOGICAL PRNT,PRNTS	00000100
	DIMENSION RF(16)	00000110
	ROD = D(2)/D(3)	00000120
	CALL REFFT (P,C(2),S(2),C(3),S(3),ROD,RPP,RPS,RSP,RSS)	00000130
	RF(1) = RPP	00000140
	RF(2) = RPS	00000150
	RF(3) = RSP	00000160
	RF(4) = RSS	00000170
	CALL RECVR (C(2),S(2),P,KRSP(NRY),DZ,DR,KSSP,RF(5),RF(6),RF(7),	
1	RF(8))	
	RC = (1.,0.)	00000240
	DO 100 J=1,8	00000250

	IF (LREF(NRY,J) .EQ. 0) GOTO 200	00000260
	RC = RC*RF(J)**LREF(NRY,J)	00000270
200	CONTINUE	00000280
100	CONTINUE	00000290
	IF(KSSP.EQ.1) GO TO 3	00000300
	IF(NRY.EQ.1) KRSP(NRY)=0	00000310
3	CONTINUE	00000320
	G1 = DDPT(I)*RC*CON	00000340
	G2 = G1*CDSQRT(P/(2.*X))	
	FNZ = DZ*G2	00000360
	FNR = DR*G2	00000370
	G3 = G1/(-8.*CDSQRT(2.*P*X**3))	
	FNZ1 = G3*DZ	00000390
	FNR1 = G3*DR*(-3.)	00000400
	IF (I .EQ. 20) GO TO 600	00000410
	IF (I .EQ. 40) GO TO 600	00000420
	IF (I .EQ. 60) GO TO 600	00000430
	GO TO 700	00000440
600	CONTINUE	00000450
	IF (PRNT) WRITE (6,300) P,C(3),C(2),S(3),S(2),KUD(NRY),KRSP(NRY),	00000460
1	LTS(NRY),LTP(NRY)	00000470
	IF (PRNT) WRITE (6,400) (RF(J),LREF(NRY,J), J=1,4)	00000480
	IF (PRNT) WRITE (6,400) (RF(J),LREF(NRY,J), J=5,8)	00000490
	IF (PRNT) WRITE (6,500) G1,G2,G3,RC	00000500
300	FORMAT (1X,'RECVR',2(E15.4),4(F10.3),2X,4(I2))	00000510
400	FORMAT (1X,'RECVR',4(2(E13.4),I2))	00000520
500	FORMAT (1X,'RECVR',8(E13.4))	00000530
700	CONTINUE	00000540
	RETURN	00000550
	END	00000560
	SUBROUTINE CURAY(JO)	00000010
	IMPLICIT REAL*8 (A-H,O-Z)	
	COMMON /SENSE/ DRCSQ(100),DRSSQ(100)	00000020
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)	00000030
	COMMON/ORSTF/CC(100),SS(100),DD(100),TTH(100),XX	00000040
	COMMON/FIXP/DDN(100),ARN(100),FLAT	00000050

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LOGICAL FLAT
DIMENSION DEPTH(100)
DIMENSION DT(100)
X = XX
PRINT 2, X
2 FORMAT (1H1,10X'CURAY'/11X'RANGE'F10.0/16X'THICKNESS'9X'DEPH'5X'P
+-VELOCITY'5X'S-VELOCITY'8X'DENSITY')
DEPTH(1) = TTH(1)/2.0
DO 10 J = 2,JO
10 DEPTH(J) = DEPTH(J-1) + (TTH(J) + TTH(J-1))/2.
DO 5 J = 1,JO
Q = 6371.0 / (6371.0 - DEPTH(J))
IF(FLAT) Q = 1.
ARN(J) = 1./Q
C(J) = CC(J)*Q
S(J) = SS(J)*Q
D(J) = DD(J)*Q
TH(J) = TTH(J)*Q
DRCSQ(J) = 1.0 / C(J) **2
DRSSQ(J) = 1.0 / S(J) **2
RCSQ(J) = DRCSQ(J)
RSSQ(J) = DRSSQ(J)
5 CONTINUE
DT(1) = TTH(1)
DO 20 J=2,JO
20 DT(J) = DT(J-1) + TTH(J)
CONTINUE
DO 25 J=1,JO
IF(FLAT) DT(J) = 0.0
DDN(J) = (6371.-DT(J))/6371.
25 CONTINUE
PRINT 1, (J,TH(J),DEPTH(J),C(J),S(J),D(J),ARN(J),DDN(J),J=1,JO)
1 FORMAT (I5,5X,7G15.4)
RETURN
END
SUBROUTINE FIND2 (Q,K,DEL,DET,PQ,TQ,NRY)

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00000410
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IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION E(100)
COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)
COMMON/PLACE/THIC,H,KSSP
COMMON/STUFF/C(100),S(100),D(100),TH(100),X
COMMON /SENSE/ RCSQ(100),RSSQ(100)
COMMON / LPRINT/ PRNT,PRNTS
LOGICAL PRNT,PRNTS
TH(1) = (1.-KUD(NRY))*(THIC-H) + KUD(NRY)*H
TH(3) = 0.
TH(4) = 0.
IF (KSSP .EQ. 1) TH(4)=TH(1)
IF (KSSP .EQ. 0) TH(3)=TH(1)
KF = 1
KOUNT = 0
TDE = DEL
8 P = Q
KOUNT = KOUNT + 1
5 P = P+DEL
PSQ = P ** 2
E(2) = DSQRT(DABS(RCSQ(2)-PSQ))
E(3) = DSQRT(DABS(RSSQ(2)-PSQ))
BLTEM = -TH(2)*LTP(NRY)/E(2) -TH(2)*LTS(NRY)/E(3)
BLTFM = BLTEM-TH(4)/E(2)
BLTEM = BLTEM-TH(3)/E(3)
BL = X + BLTEM*P
IF(DABS (DEL).LE.1.E-18) GO TO 1
6 IF (DABS(BL).LE.X/DET) GO TO 1
2 IF(BL)3,1,4
3 DEL =-DABS (DEL*.5)
GO TO 5
4 DEL =DABS(DEL*.5)
GO TO 5
1 IF(DABS(BL).LT.1.E-8) GO TO 7
IF (KOUNT.GE.5) GO TO 7
Q = Q/10.0

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00000100
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00000230
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00000250
00000260
00000270
00000280
00000290
00  0  0
00000310
00  0  3S
00000330
00000340
00000350
00000360

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	DEL	= TDE	00000370
	GO TO	8	00000380
7	PO	= P	00000390
	TOTEM	= E(2)*TH(4)+E(2)*LTP(NRY)*TH(2)+E(3)*LTS(NRY)*TH(2)	00000400
1		+E(3)*TH(3)	00000410
	TO	= P*X + TOTEM	00000420
	PQ	= PO	00000430
	TQ	= TO	00000440
	IF (DABS(BL).LT.1.0E-6)	RETURN	00000450
	IF (.NOT.PRNT)	RETURN	00000460
	WRITE (6,17)	PO,TO,BL	00000470
17	FORMAT (1H0,4X,'PO ',E18.6,10X,'TO ',E18.6,10X,'BL ',E18.6)		0000048C
	RETURN		00000490
	END		00000500
	REAL FUNCTION PTIM*8	(P,K,NRY)	
	IMPLICIT REAL*8	(A-H,O-Z)	
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,8)		00000020
	COMMON/PLACE/THIC,H,KSSP		00000030
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)		00000040
	PSQ	= P ** 2	00000050
	J	= 2	00000060
	F	= DSQRT(DABS(RCSQ(J)-PSQ))	000000
	PTIM	= (TH(4) + LTP(NRY)*TH(2)) *E	00000080
	E	=DSQRT(DABS(RSSQ(J)-PSQ))	0000009
	PTIM	= PTIM + (TH(3) + LTS(NRY)*TH(2))*E	00000100
	PTIM	= P*X + PTIM	00000110
	END		00000120
	SUBROUTINE INTERP(XP,YP,N,X,Y)		00000010
	IMPLICIT REAL*8	(A-H,O-Z)	
	DIMENSION	XP(1000),YP(1000)	
1	IF (X .GT. XP(N))	GO TO 6	00000040
	IF (X .LT. XP(1))	GO TO 6	00000050
2	DO 10 I=1,N		00000060
	IF (XP(I) -X)	10,102,3	00000070
10	CONTINUE		00000080
3	K	= I-1	00000090

	DIF1	= XP(I) -XP(K)	00000100
	DIF2	= XP(I) -X	00000110
	RATIO	= DIF2/DIF1	00000120
	DIFY	=DABS (YP(I) - YP(K))	00000 3C
	DR	= DIFY*RATIO	00000140
	IF (YP(I) .GT. YP(K)) GO TO 4		00000150
5	Y	= YP(I) + DR	00000160
	RETURN		00000170
4	Y	= YP(I) - DR	00000180
	RETURN		00000190
102	Y	= YP(I)	00000200
	RETURN		00000210
6	Y	= 0.	00000220
	RETURN		00000230
	END		00000240
	SUBROUTINE REFFT(P,V1,S1,V2,S2,D ,RPP,RPS,RSP,RSS)		00000010
	IMPLICIT COMPLEX*16 (A-H,O-Z)		
	REAL*8 K1,K2,K3,K4,D,V1,V2,S1,S2		
	K4	= S2**2/(S1**2*D)	00000060
	B1	= .5/(1-K4)	00000070
	B2	= .5*K4/(K4-1)	00000080
	K1	= B1/S1**2	00000090
	K2	= B2/S2**2	00000100
	K3	= K1+K2	00000110
	F1	= CR(P,V1)	00000120
	E2	= CR(P,V2)	00000130
	E1P	= CR(P,S1)	00000140
	F2P	= CR(P,S2)	00000150
	C1	= (P**2)*(K3-P**2)**2	00000160
	C2	= P**2*E1*E1P*E2P	00000170
	C3	= (E1*E1P)*(K2-P**2)**2	00000180
	C4	= E2P*(K1-P*P)**2	00000190
	C5	= K1*K2*E1*E2P	00000200
	C6	= K1*K2*E1P	0000021C
	AP	= C1+C3-C5	00000220
	BP	= C2+C4-C6	00000230

A	= -C1+C3-C5	00000240
B	= -C2+C4-C6	00000250
BT	= AP+BP*E2	00000260
RPP	= (A-B*E2)/BT	00000270
APS	= 2.*P*E1 *(K2-P*P)*(K3-P*P)	00000280
BPS	= 2.*P*E1*(K1-P*P)*E2P	00000290
RPS	= (APS-BPS*E2)/BT	00000300
A	= -C1 +C3 +C5	00000310
B	= -C2 +C4 +C6	00000320
RSS	= (A-B*E2)/BT	00000330
ASP	= 2.*P*E1P*(K2-P*P)*(K3-P*P)	00000340
BSP	= 2.*P*E1P*(K1-P*P)*E2P	00000350
RSP	= -(ASP-BSP*E2)/BT	00000360
END		00000370