

## 23. THE LAPLACE TRANSFORM AND MORE GENERAL SYSTEMS

This section gives a hint of how flexible a device the Laplace transform is in engineering applications.

**23.1. Zeros of the Laplace transform: stillness in motion.** The mathematical theory of functions of a complex variable shows that the *zeros* of  $F(s)$ —the values  $r$  of  $s$  for which  $F(r) = 0$ —are just as important to our understanding of it as are the poles. This symmetry is reflected in engineering as well; the location of the zeros of the transfer function has just as much significance as the location of the poles. Instead of recording resonance, they reflect stillness.

**Example 23.1.1.** We envision the following double spring system: there is an object with mass  $m_1$  suspended by a spring with spring constant  $k_1$ . A second object with mass  $m_2$  is suspended from this first object by a second spring with constant  $k_2$ . The system is driven by motion of the top of the top spring according to a function  $f(t)$ . Pick coordinates so that  $x_1$  is the position of the first object and  $x_2$  is the position of the second, both increasing in the downward direction, and both zero at rest. Direct the position function  $f(t)$  downwards also. Figure 13 shows this system.

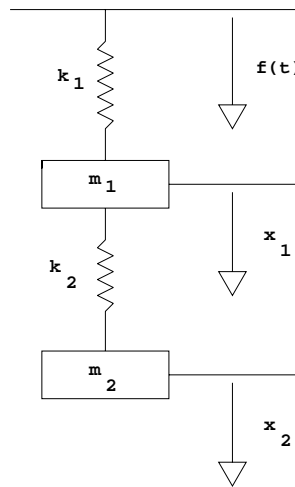


FIGURE 13. Two spring system

The equations of motion are

$$(1) \quad \begin{cases} m_1 \ddot{x}_1 &= k_1(f(t) - x_1) - k_2(x_1 - x_2) \\ m_2 \ddot{x}_2 &= k_2(x_1 - x_2) \end{cases}$$

This is a *system of second order equations*, and as you can imagine mechanical engineering is full of similar systems.

Suppose that our main interest is in  $x_1$ . Let's take Laplace transforms, and assume rest initial conditions.

$$\begin{cases} (m_1s^2 + (k_1 + k_2))X_1 &= k_2X_2 + k_1F \\ (m_2s^2 + k_2)X_2 &= k_2X_1. \end{cases}$$

Use the second equation to express  $X_2$  in terms of  $X_1$ , and substitute this value into the first equation. Then solve for  $X_1$  to get:

$$X_1(s) = \frac{m_2s^2 + k_2}{(m_1s^2 + (k_1 + k_2))(m_2s^2 + k_2) - k_2^2} \cdot k_1F(s).$$

The “transfer function”  $W(s)$  is then the ratio of the LT of the system response,  $X_1$ , and the LT of the input signal,  $F$ :

$$W(s) = \frac{k_1(m_2s^2 + k_2)}{(m_1s^2 + (k_1 + k_2))(m_2s^2 + k_2) - k_2^2}.$$

It is still the case that  $W(r)$  is the multiple of  $e^{rt}$  which occurs as  $x_1$  in a solution to the equations (1) when we take  $f(t) = e^{rt}$ . Thus the zeros of  $W(s)$  at  $s = \pm i\sqrt{k_2/m_2}$ —the values of  $s$  for which  $W(s) = 0$ —reflect a “neutralizing” circular frequency of  $\omega = \sqrt{k_2/m_2}$ . If  $f(t)$  is sinusoidal of this circular frequency then  $x_1 = 0$  is a solution. The suspended weight oscillates with  $(k_1/k_2)$  times the amplitude of  $f(t)$  and reversed in phase (independent of the masses!), and exactly cancels the impressed force. Check it out!

**Example 23.1.2.** To see another way in which a transfer function can have a nonconstant numerator, let's model a shock absorber. A platform is caused to move vertically according to a displacement function  $y(t)$ . A mass  $m$  is supported by a spring (with spring constant  $k$ ) and a dashpot (with damping constant  $b$ ), arranged in parallel so to speak. Use a variable  $x$  to measure the the elevation of the mass, and arrange that when  $x = y$  the spring is relaxed. Ignore gravity. The system is diagrammed in Figure 14.

The equation of motion is

$$m\ddot{x} = k(y - x) + b(\dot{y} - \dot{x})$$

If we put the “system” on the left we have

$$(2) \quad m\ddot{x} + b\dot{x} + kx = b\dot{y} + ky.$$

Now, in 18.03 we would tend to consider the “input signal” to be the right hand side here. But it is more meaningful to consider the

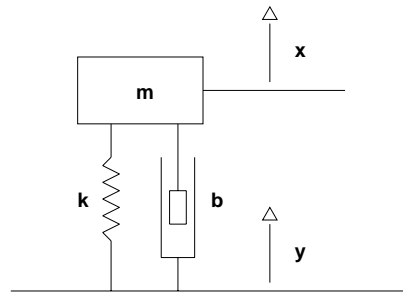


FIGURE 14. A car suspension system

input signal to be simply  $y$ . After all, if the platform is actually the chassis of a car, bumping over a Cambridge street, then it's  $y$  that's making things happen. We would like to get from knowledge of  $y$  to the solution of this equation (with rest initial conditions, say). If we apply the Laplace transform to both sides we find  $p(s)X = (bs + k)Y$  where  $p(s) = ms^2 + bs + k$  is the characteristic polynomial of the system. We can solve:

$$X = WY, \quad W(s) = \frac{bs + k}{ms^2 + bs + k}.$$

Remember the significance of the transfer function:  $W(r)$  is the multiple of the signal  $e^{rt}$  which occurs as a system response to the input signal  $e^{rt}$ . Since  $W(-k/b) = 0$ , the system response to  $y = e^{-kt/b}$  is  $x = 0$ , constant. In fact, the right hand side of (2) is then zero, so the solutions are the solutions of the homogeneous equation  $m\ddot{x} + b\dot{x} + kx = 0$ .

**23.2. General LTI systems.** The weight function  $w(t)$ , or its Laplace transform, the transfer function  $W(s)$ , completely determine the system. The transfer function of an ODE has a very restricted form—it is the reciprocal of a polynomial; but the mechanism for determining the system response makes sense for much more general complex functions  $W(t)$ , and, correspondingly, much more general “weight functions”  $w(t)$ : given a very general function  $w(t)$ , we can define an LTI system by declaring that a signal  $f(t)$  results in a system response (with null initial condition, though in fact nontrivial initial conditions can be handled too, by absorbing them into the signal using delta functions) given by the convolution  $f(t) * w(t)$ . The apparatus of the Laplace transform helps us, too, since we can compute this system response as the inverse Laplace transform of  $F(s)W(s)$ . This mechanism allows us to represent the *system*, the *signal*, and the *system response*, all three, using *functions* (of  $t$ , or of  $s$ ). Differential operators have vanished from the scene. This flexibility results in a tool of tremendous power.