

GALVANIC STIMULATION AND
THE PERCEPTION OF ROTATION

by

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"Concern for man, himself, and his
fate must always form the chief
interest of all technical endeavor...

....Never forget this in the midst of
your diagrams and equations."

-Albert Einstein

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John Roy Tole

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ABSTRACT

The influence of galvanic vestibular stimulation on the perception of rotation was investigated. The study was intended to lay the groundwork for future, more detailed study of the galvanic reaction. Of particular interest are possible clinical applications in the treatment of vertigo and the diagnosis of certain vestibular disorders.

A set of experiments were designed to measure the gross effects of current intensity and point of application on a subject's perception of rotation. An approximate threshold for the intensity effect was determined. Among points of application only polarity differences could be shown to be significant. A tentative linear relation between the bias in perception threshold and the intensity of current was found. The galvanic reaction of one vestibularly abnormal subject is also discussed.

Comparisons were made between galvanic stimulation and other common means of vestibular stimulation. Current mathematical models of vestibular function were reviewed and the extension of these models to include the galvanic reaction was examined.

Possible future directions for research in this area are also discussed.

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CHAPTER 1

INTRODUCTION

Most animals, including man obtain information about their spatial orientation in several ways: visual cues, proprioceptive and tactile cues and vestibular cues. The vestibular labyrinth, the non-auditory portion of the inner ear, plays a particularly important role in providing this information. The vestibular system has been studied by a variety of researchers for many different reasons. The physiologist approaches it as he would any biological organ, the clinician as an important sensor which can and does fail, and the bioengineer as a control system element which is coupled to other systems in order to guide the animal through its environment.

1.1 Background

Clinical interest in the vestibular system has always been high. Additional impetus for vestibular research has been provided in recent years by the manned space flight program due to the special orientation difficulties experienced by man in space. Nevertheless, much about the vestibular system is not fully understood, especially in those areas concerning the diagnosis and treatment of vestibular disorders.

Of particular interest to the clinician and to the space physician are the responses of the vestibular system to rotation and disorders related to rotation or to movement. Vertigo, dizziness, and motion sickness are familiar problems related to this area of concern.

A number of stimuli have been employed to study the response of the vestibular system. The most common two have been rotation and caloric stimulation. The latter is a common clinical technique in which hot or cold water irrigation of the ear produces a response similar to that obtained during rotation.

Using the caloric test, which is discussed in more detail in Chapter 2, the physician is able to obtain a good idea of the functioning of a portion of the vestibular system one ear at a time whereas rotation stimulates both ears.

Another means of stimulation has been observed to produce disorientation effects similar to those experienced during rotation. It has been known for some time that direct current passed through the head gives rise to a swaying or rotatory sensation. The galvanic vestibular reaction, as this effect is called, has been studied with varying interest since the 1800's. The lack of enthusiasm has apparently resulted from several factors. One is that the action site of the current is not known exactly making it of somewhat questionable value in clinical testing. A second reason is that until comparatively

recent, constant current stimulation equipment and precise response measurement devices were not readily available, making it difficult to perform repeatable experiments.

Though the action site is not known exactly, it is currently felt that galvanic stimuli do not act at the same points as rotational or caloric stimuli. Rather the current is thought to act closer to the central nervous system. This suggests that the galvanic stimulus might be used to distinguish between certain vestibular disorders and indeed this approach has been taken by a number of people with some apparent success. Most studies have been rather qualitative however. What seems to have been lacking in the past was an attempt to establish quantitatively the effects of current intensity and polarity on subjective sensations of rotation and on eye movements.

If quantitative measures of response were available and if the action site of the stimulus were well understood, the galvanic reaction might be of definite value as a clinical diagnostic test. Quantitative knowledge of the effects might also make galvanic stimulus useful as a treatment for such disorders as vertigo. For example, a certain current intensity might be shown to cause a sensation similar to that experienced during a specified angular stimulus or during vertigo. A patient with vertigo might then receive a galvanic stimulus of proper polarity in an attempt to cancel his dizziness sensation (In Chapter

3 will be noted that reversing polarity generally reverses the effect of a galvanic stimulus).

A number of questions must be answered before such a treatment could be used however.

1.2 Scope of Thesis

This thesis is intended to lay the groundwork for a future more detailed study of the galvanic vestibular reaction. Past work on vestibular response to rotational, caloric and galvanic stimuli is reviewed. Similarities in rotational and galvanic reactions are discussed.

A group of experiments were designed to study the gross effects of vestibular stimulation on the perception of rotation. Both voluntary subject response and eye movements were studied. The primary objective of the experiments was to determine whether galvanic stimulation can indeed bias the threshold for rotation sensation. Secondary related objectives were to determine which intensity levels and modes (electrode locations), if any, influenced the results. Also, if a threshold bias could be found, some quantitative measure of the cause-effect relationship would be sought.

1.3 Results

The experimental results indicate that it is possible to bias the threshold for rotational perception in a predictable manner. Further substantiation was also given to the belief that a certain constant bias or

directional preponderance is present in so called normal subjects without the galvanic stimulus. Polarity of the stimulus was found to have a significant influence on the results bearing out past findings. For a given polarity however, no significant differences in response could be found between the various standard electrode modes (see Chapter 3 for a discussion of these modes).

A threshold for current intensity effect was found to be between 400 and 800 μ a. Using this information and the observed bias in perception, a probable plot of bias in perception vs current intensity was drawn. On the same basis, a first hypothesis of how to add the galvanic reaction to existing vestibular control theory models is hypothesized.

The work performed also suggested a number of future directions for the research.

1.4 Outline of the Thesis

The thesis is arranged as follows:

Chapter 2 reviews the anatomy and physiology of the vestibular system with emphasis on rotation sensing mechanisms. Techniques for vestibular study are discussed as are current mathematical models of vestibular response including the caloric reaction.

Chapter 3 outlines the history of research into the galvanic vestibular reaction and discusses the various types of tests which can be run in order to study the reaction in a gross sense. An attempt is made to organize

what is presently considered to be the nature of the reaction.

The experimental method used to study the gross influence of galvanic stimulation on the perception of rotation is the subject of Chapter 4 and Chapter 5 discusses the results of these experiments.

Chapter 6 presents the conclusions and gives suggestions for further research.

The Appendices contain discussions and listings of the computer programs used for data analysis.

CHAPTER 2

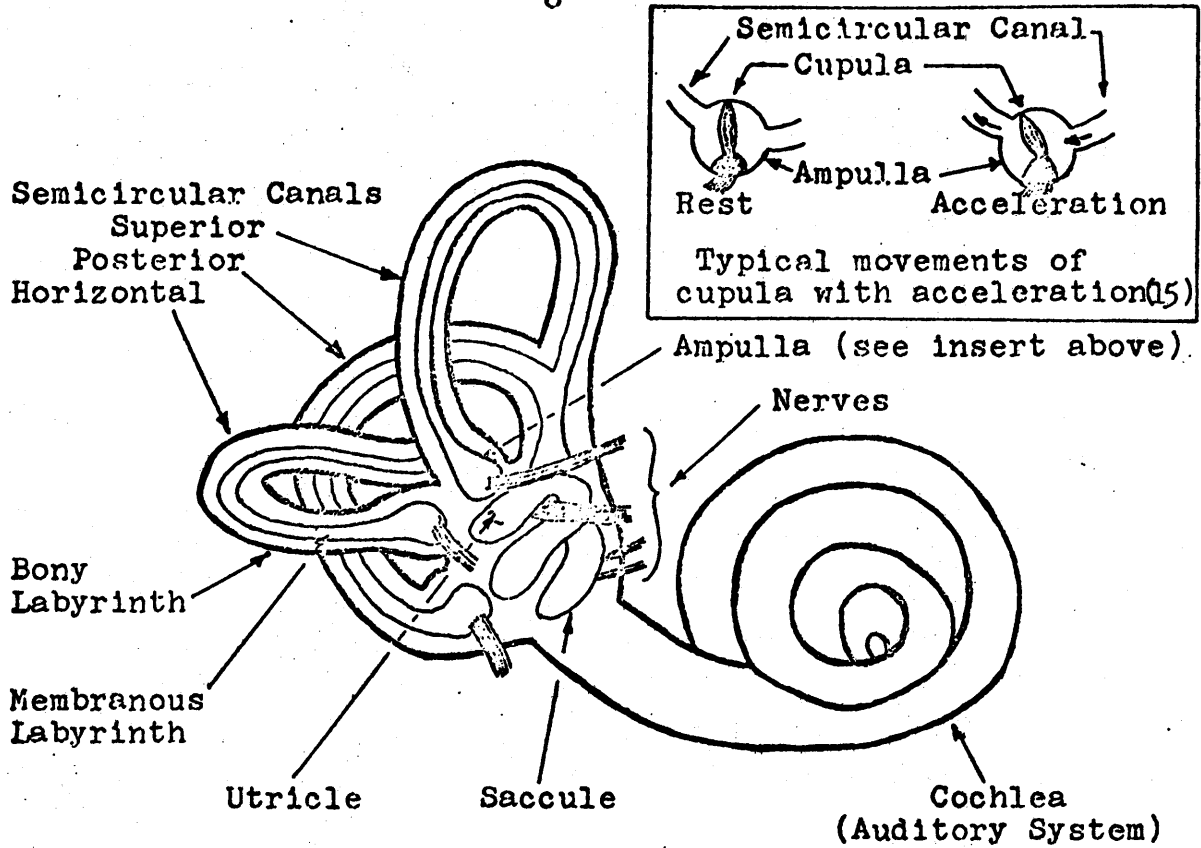
THE ANATOMY AND PHYSIOLOGY OF THE
VESTIBULAR SYSTEM

The vestibular system, the non-auditory portion of the inner ear, enables an animal to sense its motion and verticality with respect to its environment. So basic is the vestibular system that in lower animals, its proper function is essential for the maintenance of life. Higher animals, including man, experience difficulty maintaining orientation if vestibular function is lost, but are partially able to compensate for the loss by using other cues such as vision.

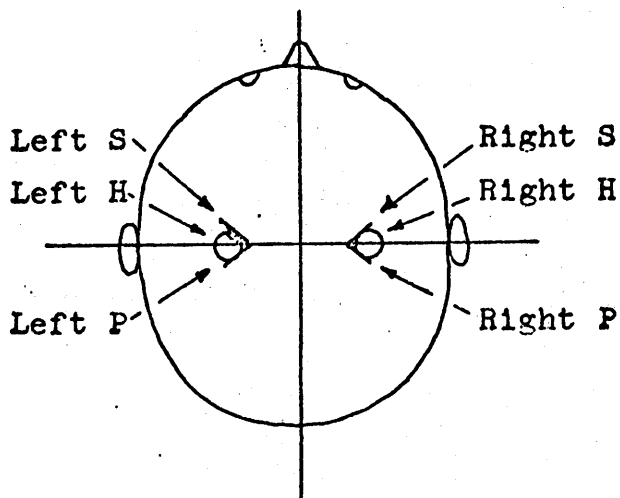
This chapter discusses the structure and function of the human vestibular system with particular emphasis on the features which enable it to sense angular accelerations. Means of studying vestibular response to rotation are discussed and current mathematical models of this response are reviewed briefly.

2.1 Location and Gross Structure of the Labyrinth^{14,27,29}

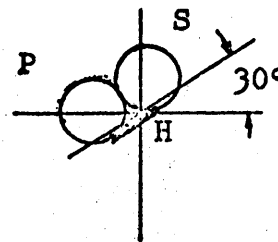
The paired vestibular system is contained within the temporal bone of the skull in a cavity known as the bony labyrinth. Figure 2.1 shows the approximate location of both and the structure of the vestibular apparatus.



a, Vestibular labyrinth of the right ear (21)



b. Top view of head showing approximate locations of semicircular canals (29)



c. View into right ear (29)

Figure 2.1

Gross structure and location of the vestibular apparatus

A portion of the labyrinth consists of the cochlea, an organ of hearing. The vestibular system is connected to the cochlea and occupies the remainder of the cavity. Each side of the system is composed of an utricle, a saccule, and three semicircular canals.

The utricle and saccule are located between the cochlea and the semicircular canals in an area known as the vestibule. Each has a structure called the maculae which is fixed with respect to the labyrinth. In the maculae are imbedded sensory hair cells with several types of innervation. The hairs extending from these cells support a gelatinous mass containing calcium carbonate crystals known as the otolith. Surrounding the otoliths in the utricle and saccule is a fluid called endolymph which serves as a damping medium.

Motion of the otoliths with respect to their maculae stimulates the hair cells and induces a linear motion sensation. The utricle is thought to sense linear accelerations omnidirectionally. Thus it is sensitive to the acceleration due to gravity.

The function of the saccule is not clear and some researchers feel it may be more an auditory than a vestibular organ. The utricles are not of primary importance in rotational sensation.

Continuous with the utricle and saccule are the three semicircular canals whose function is to sense angular accelerations. Each resembles a flexible toroid

with an enlarged portion at one end. The flexible toroid, known as the membranous canal, is enclosed in a second more rigid toroid called the bony canal. (See Figure 2.1) The membranous canal contains endolymph while the space between the inner and outer toroid contains another fluid known as perilymph.

The enlarged end of each toroid is the ampulla. The ampulla contains a gelatinous, flapper type valve called the cupula. (See insert, Figure 2.1) The cupula is attached to a raised area of the inner wall of the ampulla, the cristae. The free end of the cupula is in close contact with the ampulla wall. The latter is fixed by connective tissue to the skull and may be considered stationary with respect to the head.

When an angular acceleration is imparted to the head, the endolymph lags behind the canal due to inertia and causes a deflection of the cupulae. Hair cells within the cristae receive this deflection information and translate it into nerve impulses.

The hair cells in the cristae are direction specific, i.e. they are able to distinguish the direction of cupula deflection. These hairs are grouped in bundles known as stereocilia. At one side of each bundle is a single stiff hair, the kinocilium. Deflections of the cupula toward the kinocilium cause an increase in the discharge rate of the nerves in the sensory cells. Deflections in the opposite direction cause a decrease in this

discharge rate. Ewald first described this phenomenon in the cat and it is often known by his name.²¹

The fact that there are three semicircular canals in each labyrinth suggests that angular accelerations about the three principal axes of the body are each sensed by a separate canal. With the head held erect however, none of the canals lies exactly in one of the principal planes. Coupling between the three canals is thus to be expected though it is not of great consequence.

The corresponding canals on each side also act as pairs in most situations. This action has an especially important role in the conjugated eye movements experienced when the head is turned.

2.2 Central Nervous System Connections^{15,32}

Figure 2.2 shows the principal central nervous system connections of the vestibular system. The various nerve fibers and nuclei appear on both sides of the brain stem. For clarity, the figure shows only those of the left side.

The cell bodies of the sensory neurons of the cristae and maculae are found in the vestibular ganglion. The nerves terminate in the ipsilateral (same side) vestibular nuclei and in the cerebellum. From the vestibular nuclei, fibers descend in the vestibulo-spinal tract as shown and also in the lower portion of the medial longitudinal fasciculus (not shown). The vestibulo-spinal tract plays an important role in postural reflexes and in muscle tone. Some of the descending medial longitudinal fasciculus

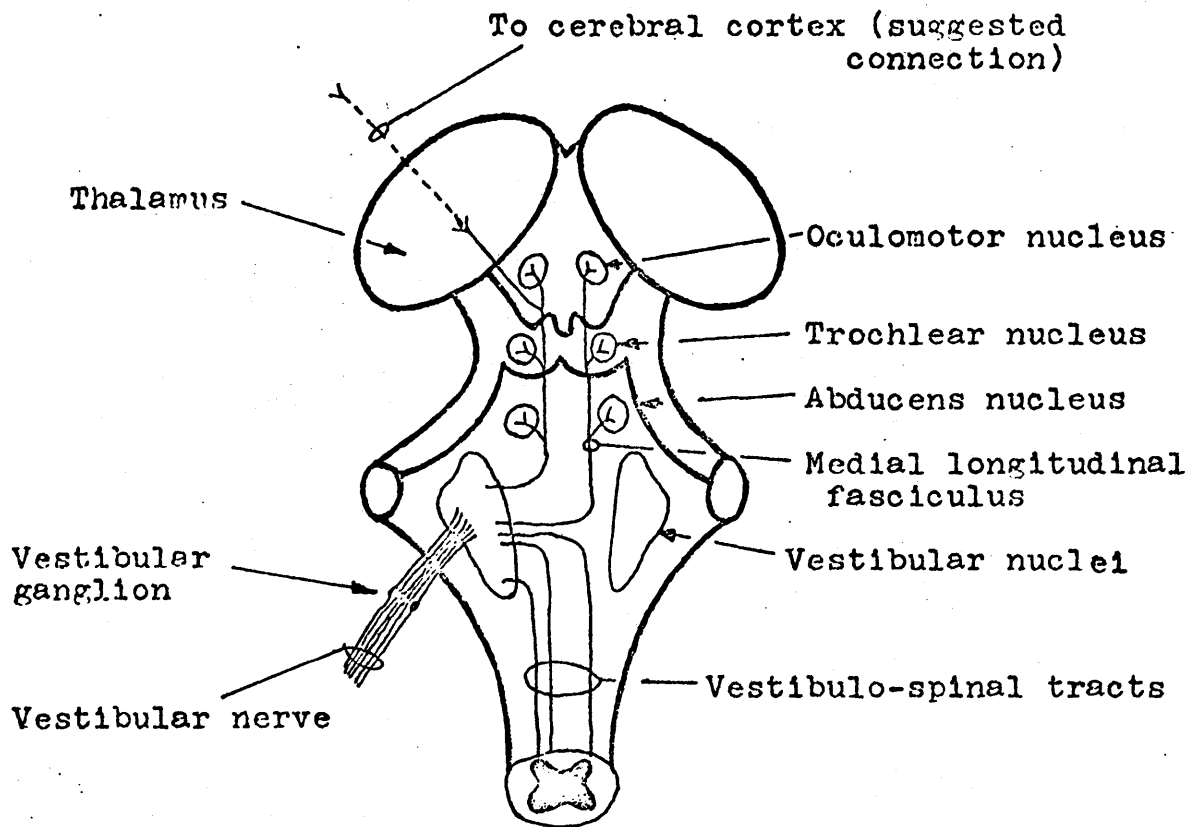


Figure 2.2

Dorsal view of the brain stem showing the principal vestibular pathways (15)

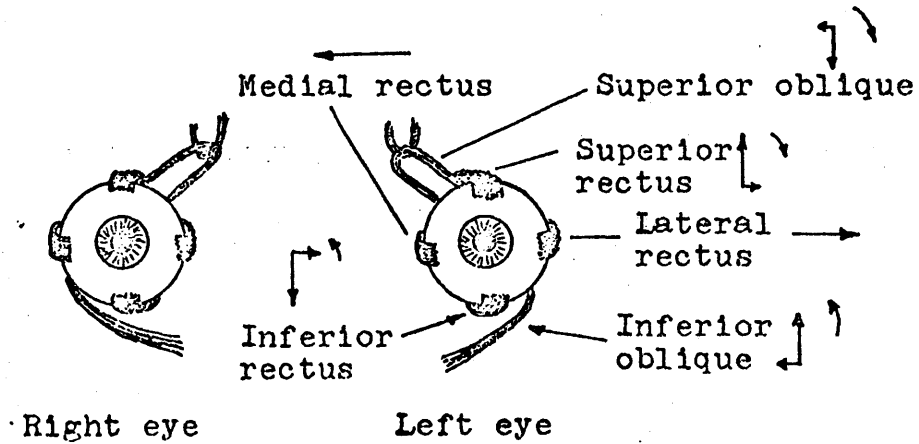


Figure 2.3

Extrinsic ocular muscles (arrows represent movements effected by each muscle) (21)

fibers are thought to reach the visceral motor nuclei thereby effecting the nausea, vomiting, and other symptoms of excessive vestibular stimulation such as motion sickness.

The upper portion of the medial longitudinal fasciculus contains fibers passing from the vestibular nuclei to the abducens, trochlear, and oculomotor nuclei and to the cerebral cortex via the thalamus. The latter connection is probably responsible for conscious sensation of motion. The three nuclei to which the fibers pass are responsible for the control of eye movements.

2.3 Vestibular-Oculomotor Connections ²¹

If one fixates on some object while turning one's head, compensatory eye movements (i.e. opposite to the direction of head movement) are necessary in order to keep the object in view. These movements depend on a sensation of head motion which is given to a large extent by the vestibular apparatus.

Eye movements are produced by three pairs of muscles, the lateral and medial recti, the superior and inferior recti, and the superior and inferior oblique as shown in Figure 2.3. The arrows in the figure represent the approximate eye movements effected by each muscle. All of the muscles except the lateral rectus and the superior oblique are controlled by the oculomotor nucleus (see Figure 2.2 and the discussion in the last section). The trochlear nucleus controls the superior oblique muscle while the abducens nucleus controls the lateral rectus.

It has been shown by Szentágothai,³⁰ Cohen, and others,

and reported by Peters that electrical stimulation of a single ampullary nerve of one of the semicircular canals of the cat produces compensatory movements in both eyes similar to those observed during rotation.²¹ As Figure 2.2 indicates, there are connections between each set of vestibular nuclei and both the ipsilateral and contralateral nuclei controlling eye motion. Stimulation of the horizontal canals, which is of the most interest in this thesis, causes compensatory eye movements about the yaw (vertical) axis of the head. These movements are determined primarily by the medial and lateral recti but, as with all eye motion, are modified somewhat by the states of the other extraocular muscles. Several authors have studied the various connections between the semicircular canals and these muscles. Peters has summarized the results of these studies.²¹

Szentagothai has also studied the neural connections between the utricles and the oculomotor system and has developed a theory of the possible pathways. These are also reviewed by Peters but are probably not of consequence in the present work however.²¹

Eye movements are thus a direct external indication of vestibular function and are of great interest in most vestibular research.

2.4 Techniques for Vestibular Study

A number of techniques are employed to study vestibular response. These may generally be distinguished either by the type of stimulus used or by the form of response obtained.

Several of the most popular methods are reviewed below. These and other methods are discussed in detail in the literature. The galvanic test is discussed separately in Chapter 3.

In what is sometimes called a subjective test, a subject is placed in a darkened Barany chair (a device which rotates about the yaw axis) and a random input of zero mean and known frequency content is applied to the chair's drive motor.²¹ The subject indicates by pressing a button or a "joy" stick the direction and/or magnitude of his motion. A "normal" subject is able to detect most motions above some threshold, but will generally not have a zero mean response. Mirchandani recently employed this technique to study directional preponderance, a condition in which a subject is more sensitive to movements in one direction than the opposite.²⁰ He found that even clinically "normal" subjects displayed at least slight directional preponderance.

The subjective test can be run about the other two axes also but certain additional complicating factors relating to otolith function enter to a greater extent than about the yaw axis. Meiry, in particular, has conducted extensive experiments of this sort about the roll axis.¹⁹

The Barany chair or a similar device may be employed in a more objective test of vestibular response. Such a test employs eye movements as discussed above as an objective indication of vestibular state.²¹ Thus if a

subject is placed in a darkened chair and given a test input, either sinusoidal or random rotation or a transient such as a step or ramp, and his eye movements are monitored, a good indication can be had of vestibular "output," mathematical models of this input-output relation can then be hypothesized. Several of these models are discussed below.

2.5 Eye Movement Monitoring 23,29,38

Several techniques are presently in use to record eye movements.

One is the electro-oculogram or E.O.G. which is a measure of the differential corneo-retinal potential. Surface electrodes near the corners of the eyes sense these potentials which change as the eyes move. The electrodes also pick up muscle noise, however, and are subject to drift.

High speed movies of the eye have also been employed in experiments but these do not yield an analog output and are not readily useful for data analysis.

The technique used in the experiments described in this thesis measures the difference in light reflected from the iris and the sclera. An infrared source and two photoelectric cells are mounted on a standard eye glass frame. The electronics are battery operated and are mounted in a separate case. The frame is mounted with relative ease and adjustment is simple. The unit tends to irritate most subjects if left on for more than

about thirty minutes, due to the drying effect of the infrared source on the eye. Also the resolution ($\pm\frac{1}{4}^{\circ}$) and the linearity ($\pm 15^{\circ}$) are inadequate for some experiments.

These techniques are discussed in detail in several of the references.

2.6 The Caloric Test ^{14,27,29}

A common clinical technique for determining vestibular condition is the caloric test. In this test, the external auditory canal is irrigated with a fluid which is slightly above or below ambient body temperature. Barany and others state that this irrigation sets up a convection current in the endolymph. This current in turn causes displacement of the cupula resulting in rotational sensation and nystagmus eye movements. The intensity of the response depends upon subject threshold, the temperature of the irrigating fluid, and certain other factors. The test is relatively simple to administer and requires the least equipment of the techniques mentioned. It is perhaps the most widely used vestibular test.

2.7 Control Models of Vestibular Response ^{19,21,29,39}

Considerable effort has been devoted to mathematical formulations of vestibular response, mostly for the semi-circular canals. Such models are useful in describing vestibular function and in predicting labyrinth response

to various input stimuli including rotation. In particular, such models have helped to explain the threshold, adaptation, and habituation phenomena associated with the canals. These phenomena are of interest in studies of rotation perception and will be discussed at the end of this section.

2.7.1 The cupula model

The basic response of the semicircular canals to motion inputs is usually deemed analogous to that of a damped torsion pendulum, an analogy first proposed by Steinhausen in 1931. Mathematically, this response is expressed, for a single semicircular canal as:

$$I\ddot{\theta} + B\dot{\theta} + K\theta = I\alpha \quad (2.1)$$

where

I = moment of inertia of the endolymph about the sensitive axis of the canal

B = viscous damping torque of endolymph with respect to the skull at unit angular velocity

K = stiffness, or torque per unit angular deflection of cupula with respect to the skull

θ = angular deflection of cupula with respect to the skull

α = input angular acceleration about the sensitive axis of the canal

This equation is often expressed in the Laplace domain as

$$(s^2 + \frac{B}{I}s + \frac{K}{I}) \theta = \alpha \quad (2.2)$$

It is also generally assumed that the viscous torque is much greater than the elastic torque, i.e. $\frac{B}{I} \gg \frac{K}{I}$.

With this assumption, equation 2.2 becomes:

$$\frac{\theta}{\alpha} = \frac{1}{(s + \frac{K}{B})(s + \frac{B}{I})} \quad (2.3)$$

Typical values for the time constants B/K and $\frac{I}{B}$ are

$$\frac{B}{K} = 10 \text{ seconds} \quad \frac{I}{B} = 0.1 \text{ seconds}$$

These constants and other useful information are obtained in the following manner. First, taking the inverse Laplace transform and using the fact that $\frac{K}{B} < \frac{B}{I}$ the following time relationship is obtained for a velocity step input, γ .

$$\theta \approx \gamma \frac{I}{B} [e^{-\frac{Kt}{B}} - e^{-\frac{Bt}{I}}] \quad (2.4)$$

Also for a unit acceleration step input, α , one finds

$$\theta \approx \alpha \frac{I}{K} [1 - \frac{K}{B} (\frac{B}{K} e^{-\frac{Kt}{B}} - \frac{I}{B} e^{-\frac{Bt}{I}})] \quad (2.5)$$

If it is noted that the exponential $e^{-K/Bt}$ dominates equation 2.4 it may finally be written as:

$$\theta \approx \gamma \frac{I}{B} e^{-\frac{Kt}{B}} \quad (2.6)$$

Taking the logarithm of this expression, one has:

$$\ln \theta = \ln \gamma \frac{I}{B} - \frac{Kt}{B} \quad (2.7)$$

A plot of $\ln \theta$ versus t has the slope $\frac{K}{B}$ and thus determines this constant. The determination of I/B involves a slightly different technique which is discussed in the literature.

2.7.2 Perception Thresholds

A number of useful results are obtained if equation 2.7 is solved for t to yield

$$t = \frac{B}{K} \ln \frac{\gamma I}{\theta B} \quad (2.8)$$

If θ in equation 2.8 is taken to be the threshold cupula deflection (i.e. the minimum deflection for which a sensation of rotation occurs), then t may be interpreted as the time from stimulus onset to the end of rotation sensation.

Thus 2.8 becomes

$$t_{\mu} = \frac{B}{K} \ln \frac{\gamma I}{\theta_{\min} B} \quad (2.9)$$

Now suppose a stimulus of exactly threshold intensity is applied. The time from stimulus onset to cessation of sensation is then ≈ 0 . Taking $t_{\mu} = 0$ in 2.9, we can then solve for θ_{\min} to get:

$$\theta_{\min} = \frac{I}{B} \gamma_{\min} \quad (2.10)$$

Values of θ_{\min} for subjective and nystagmus responses to velocity step inputs can be estimated from figure 2.4. This is done by looking at the value for the velocity at zero ordinate for the two cupulograms shown there.

γ_{\min} is found to be ≈ 2.7 deg/sec for subjective response and 9 deg/sec for nystagmus. Assuming a value of 0.1 sec for I/B , θ_{\min} is found to be 0.27 degrees and 0.9 degrees respectively.

It can also be shown that the threshold of angular acceleration sensation is given by

$$\alpha_{\min} = \frac{\theta_{\min}}{I/K} \quad (2.11)$$

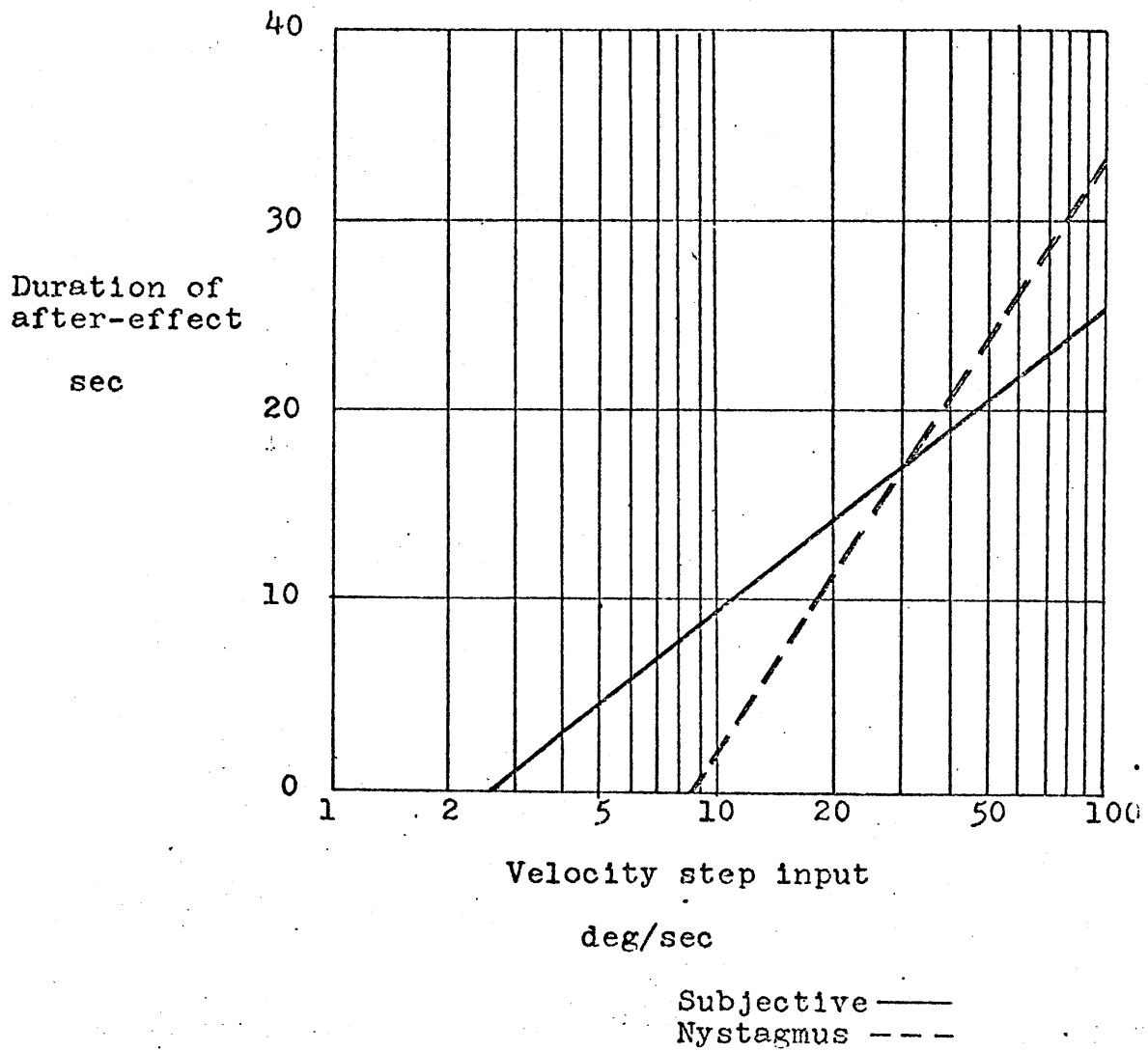


Figure 2.4

Average cupulograms for subjective and nystagmus responses to velocity step input (Modified from 21)

where for the nominal values of $\frac{K}{B}$ and $\frac{I}{B}$ given above $I/K = 1 \text{ sec}^2$. Thus approximate values of α_{\min} are easily found to be

$$\alpha_{\min} = 0.27 \text{ deg/sec}^2 \text{ for subjective sensation}$$

$$\alpha_{\min} = 0.9 \text{ deg/sec}^2 \text{ for nystagmus}$$

These values of acceleration perception thresholds are in rather good agreement with the experimental results of a number of researchers.⁴²¹ As might be expected, values for nystagmus response are generally much closer to the nominal value above, reflecting the objective nature of nystagmus studies. Subjective response is much more dependent on individual differences and hence yields a larger experimental data spread.

2.7.3 Latency

In some instances, the simple measure of threshold stimulus intensity may not be adequate to describe rotational perception. Low intensity stimuli may, if applied for a sufficient period of time, result in perceived motion. The period of time required in such a circumstance is termed the latency. Indeed, every stimulus intensity has a certain latency period associated with it. The latency concept has a direct parallel, chronaxia, in galvanic stimulation studies which will be discussed in Chapter 3.

In order to obtain an analytic expression for latency times for angular acceleration perception, one begins with equation 2.5, noting once again that $I/B \ll B/K$.

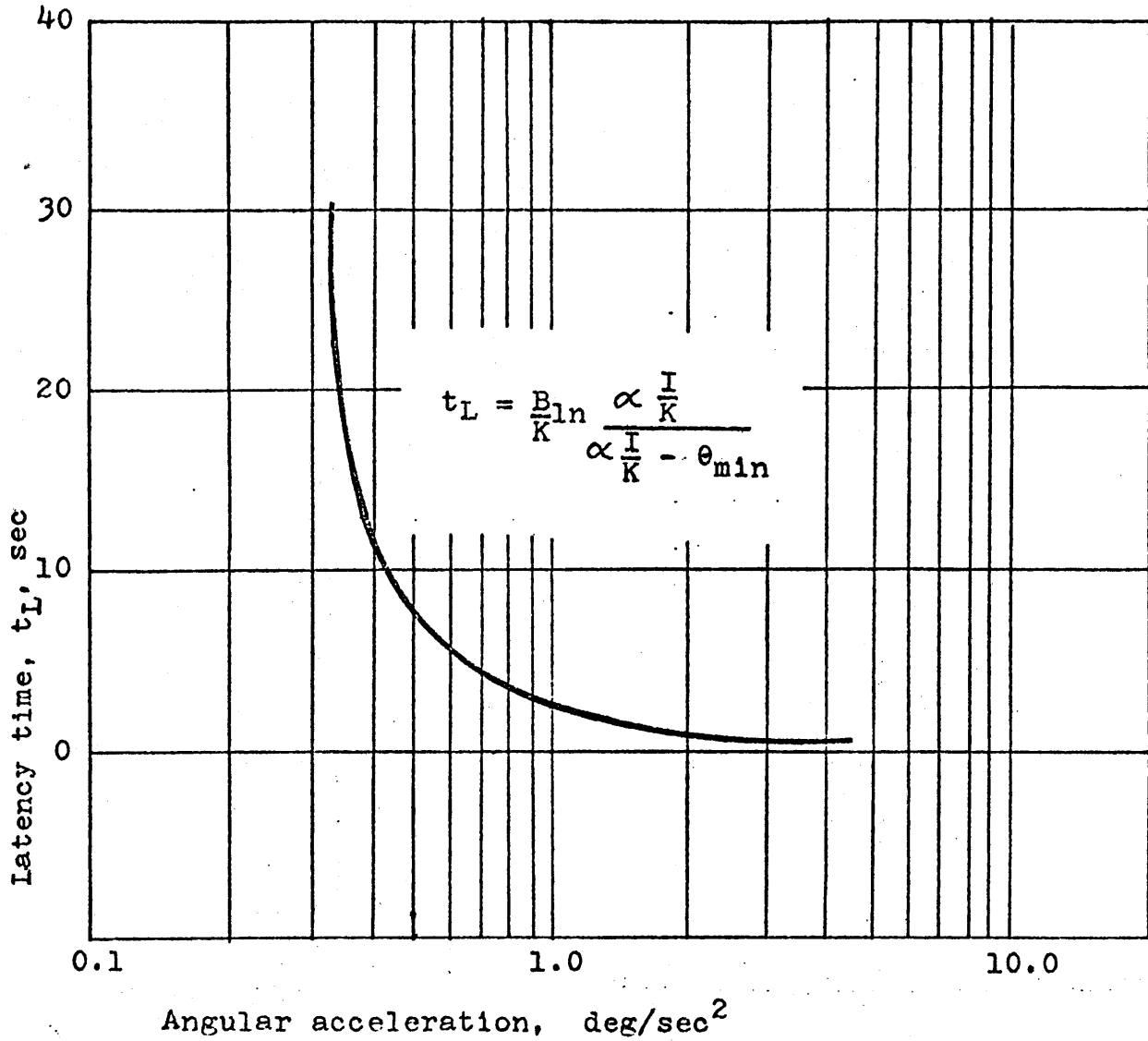


Figure 2.5

Perception latency time vs. angular acceleration for rotation about the vertical axis ($\theta_{\min} = 0.25$, $\frac{B}{K} = 8 \text{ sec}$, $\frac{I}{K} = 0.8 \text{ sec}^2$) (Modified from 21)

With the latter assumption equation, 2.5 becomes

$$\theta = \alpha \frac{I}{K} (1 - e^{-Kt/B}) \quad (2.12)$$

Letting $\theta = \theta_{\min}$ and solving for t yields

$$t = \frac{B}{K} \ln \left[\frac{\alpha \frac{I}{K}}{\alpha \frac{I}{K} - \theta_{\min}} \right] \quad (2.13)$$

or the latency time as a function of α . An approximate plot of 2.13 is shown in figure 2.5 with $\theta_{\min} = 0.25$ deg. Experimental data often reveals much lower thresholds when sufficient time is allowed for response.²¹ Still 2.13 is useful for describing latency.

2.7.4 Response decline with Prolonged or Repeated Stimulation

If stimulation of the semicircular canals continues at a constant level for an extended period (more than several seconds) the sensation of angular velocity gradually decreases and eventually disappears. This phenomenon can be understood if one remembers that the cupula is deflected due to the inertia of the endolymph in the semicircular canals. With a prolonged constant stimulus, the cupula is able to return to its rest position. Figure 2.6 shows the approximate canal response when a term of the form $s/(s + 0.033)$ is added to equation 2.3.³⁹ This term, which is sometimes called an adaptation, brings the response to approximately below the threshold in thirty seconds as shown in the figure.

Repeated application of the same or similar stimulus

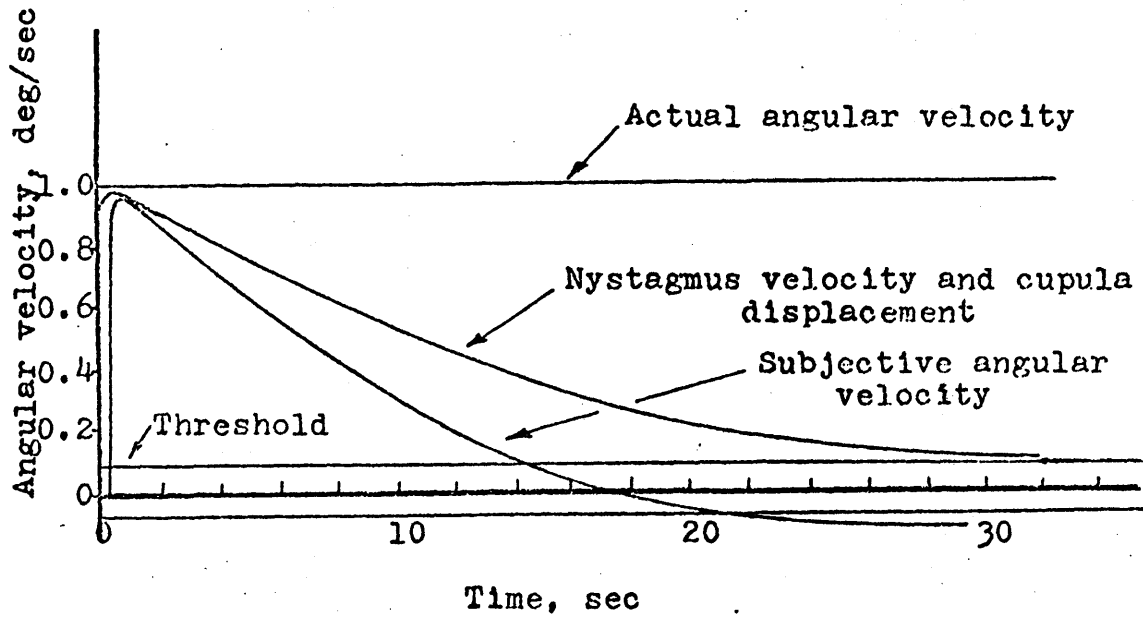


Figure 2.6

Velocity step response of semicircular canal model including adaptation dynamics (39)

also results in response decline. This decline, which manifests itself in higher thresholds and increased ratio of adaptation, is most noticeable in pilots and others who undergo regular intense vestibular stimulation.

2.7.5 Caloric Stimulation Model

Steer has proposed a model for caloric stimulation based on theoretical considerations and actual caloric test results. It is outlined briefly here. For further information, the reader is referred to Steer's thesis.²⁹

The model, in the Laplace domain, is given by:

$$\frac{\theta_c(s)}{T(s)} = \frac{20KT/T_1}{(s+1/T_1)} \frac{T_2}{(s+1/T_2)} \frac{T_3 \cos \phi}{(s+1/T_3)} \quad (2.14)$$

where

$\theta_c(s)$ = cupular displacement due to caloric stimulus

$T(s)$ = temperature at tympanic membrane

T_1 = thermal lag (≈ 25 sec)

T_2 = $B/K = 10$ sec

T_3 = $B/I = 0.1$ sec

ϕ = angle between plane of thermal gradient and the perpendicular to the gravity vector

KT = system gain

Equation 2.14 may be written as

$$\frac{\theta_c(s)}{T(s)} = \frac{20KT \cos \phi}{25s+1} \left[\frac{1}{(0.1s+1)(10s+1)} \right] \quad (2.15)$$

where the term in brackets is recognized as the model, just described, of cupula response to angular stimuli.

The caloric model therefore provides a useful comparison of caloric and rotational responses.

$$G(s) = \frac{B/I s}{(s+K/B)(s+B/I)}$$

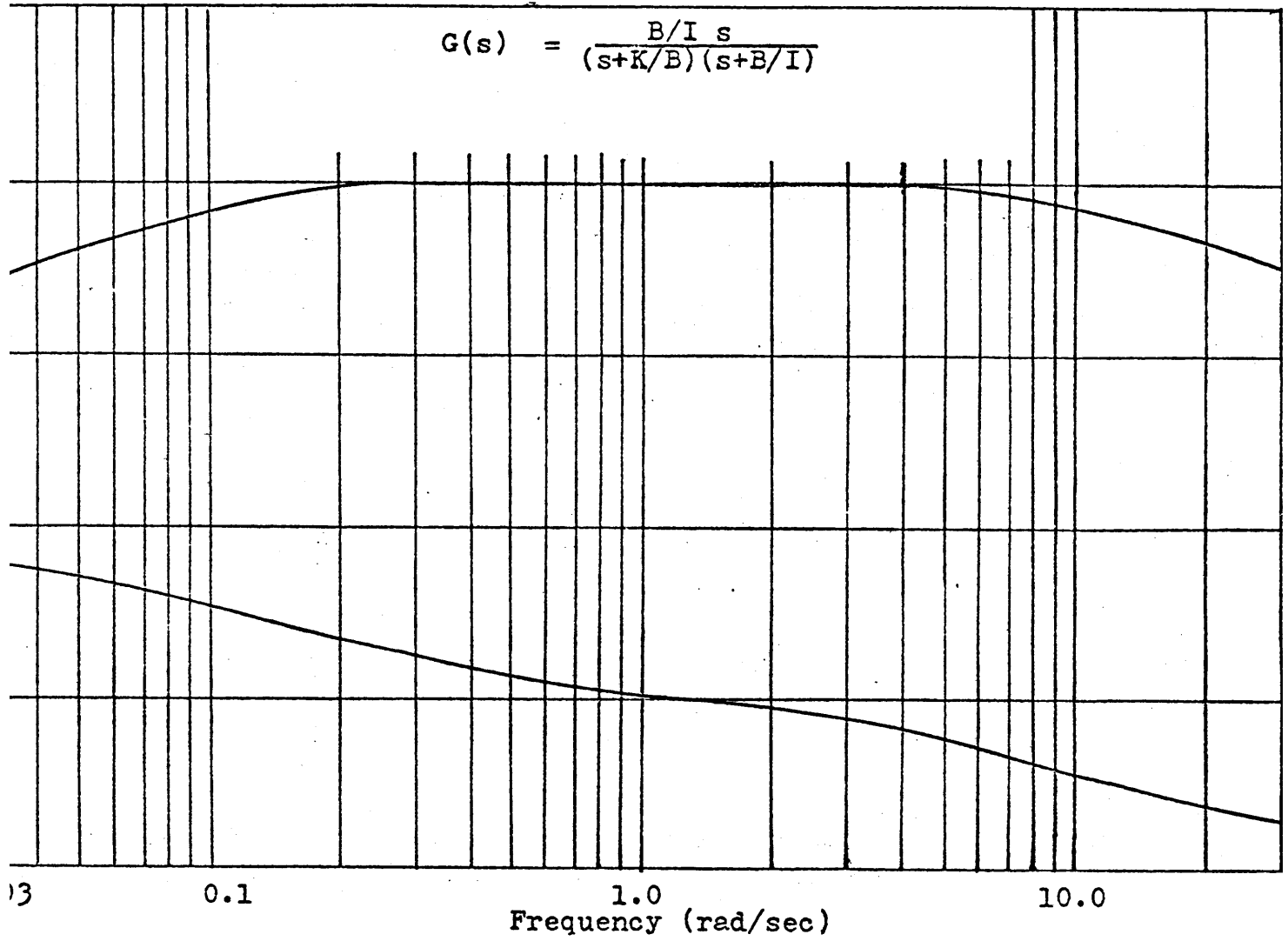


Figure 2.7
 Frequency response of subjective perception model of semicircular canals (1)

2.7.6 Subjective Perception Model^{19,21}

It is interesting in the present work to consider a model of subjective perception of the semicircular canals. The model is expressed as

$$\frac{\dot{\theta}_p(s)}{\dot{\theta}_1(s)} = \frac{B/I \ s}{(s + \frac{K}{B})(s + \frac{B}{I})} \quad (2.16)$$

where

$\dot{\theta}_p(s)$ = Subjective Perception of angular velocity

$\dot{\theta}_1(s)$ = Input angular velocity

Typical values of the constants are $B/I = 10$ and $K/B = 0.12$.

This model is obtained by performing the "subjective" test discussed in section 2.4. A Bode plot of the model is shown in figure 2.7. Note that over the range $\omega = 0.1$ to $\omega = 10$ rad/second the model indicates subjective perception to be that of angular velocity.

2.8 Comments on Vestibular Models

It must be emphasized that mathematical models of any physiological response are only useful conceptual tools. They are seldom, if ever, totally accurate descriptions of the underlying physiological events. The models discussed in the last section must be viewed in that light.

CHAPTER 3

THE GALVANIC VESTIBULAR REACTION

It has been recognized for some 150 years that passing a direct current between the mastoid processes brings about one or several responses similar to those characteristic of vestibular stimulation. The use of D.C. (galvanic) stimulation in diagnosis and treatment of certain vestibular disorders has been suggested with varying enthusiasm since that time.

This chapter reviews the past research into the galvanic vestibular reaction, discusses the various reported responses, especially those related to the sensation of rotation, and outlines the methods for conducting galvanic stimulation tests.

3.1 Action Site of the Stimulus ^{14,27}

Shapiro and others report that Jan Perkinje about 1820 found that an electric current passed through the head caused vertigo. It was recognized by Hitzig in 1871 that such a current also elicited eye movements. Breur later noted such a current also stimulated the vestibular system in some manner. A number of persons since have described a variety of effects on the vestibular system and oculomotor response due to galvanic stimulation.

Among the reported reactions are: deviations of the eyes toward the anode, nystagmus with fast phase component toward the cathode, tilting of the body and/or head toward the anode depending on whether the subject is sitting or standing, and subjective sensation of movement, especially rotation.

The degree and direction of these responses are felt to depend, at least qualitatively, on the polarity, points of application and intensity of the galvanic stimulus. Of particular interest in clinical work has been the point of action of the stimulus.

Barany postulated that a cathodic stimulus on the mastoid process increased the catelectrotonus (sensitivity to negative electrical current) in the vestibular nerve thus increasing its excitability. Anodic stimulation, he felt, had a depressing effect on excitation. Bruning opposed this theory, arguing that nerves could only be stimulated by alternating current, and postulated that galvanic current acted directly on the vestibular receptor organs. Hennebert felt that both the vestibular and auditory receptors were affected.

The Bruning theory held that the galvanic current caused an electrokinetic flow in the endolymph of the semicircular canals. Such a flow would be somewhat analogous to the flow due to a thermal gradient set up by caloric stimulation as discussed in Chapter 2.

Most evidence is in support of Barany's theory, however. Marx plugged the semicircular canals of guinea pigs and still obtained a "normal" D.C. reaction. He obtained similar reactions if he destroyed the semicircular canals or the entire labyrinth. Neumann and others found clinical cases where patients had no caloric or rotational responses but did react to galvanic stimulation. Steinhausen was able to demonstrate in experiments with a pike(fish) that the cupula was not deflected due to a galvanic current.

Other researchers, including Spiegel and Scala,²⁶ have severed the 8th cranial(vestibular and acoustic) nerve and observed the disappearance of galvanic response. Pfaltz and Koiche have reported that brainstem lesions which do not elicit spontaneous nystagmus appear to have little or no influence on a patient's galvanic reaction.²²

On the basis of the evidence above, it would thus appear that the peripheral vestibular neuron is the action site of the galvanic stimulus. Detailed study of this or other sites on a system level is hindered by a number of factors: difference in conductivity of various tissues, unknown current distributions, changes in current level, and polarization.¹⁴

Some researchers, including Spiegel,²⁷ feel that within the vestibular neuron, it is principally the fibers from the maculae(see Chapter 2) which are affected by galvanic current. They point to such indications as

eye rolling and head inclination as evidence. Also, using the double galvanic test, which is discussed below, Spiegel and Scala were able to decrease tonic impulses to the forelegs in decerebrate cats by using anodic stimulation. Cathodic stimulation increased muscle tonus thus suggesting a sort of modulating influence by the galvanic stimulus.

The final answer to the point of action of galvanic vestibular stimulation will probably not be available for some time.

3.2 Differing Response to Anodic and Cathodic Stimulation

The differences in response observed for anodic and cathodic stimuli have had several explanations. Those theories mentioned above, Barany's of electrotonus, and Spiegel's of action on the fibers from the maculae, are of a qualitative nature. Another theory, first proposed by Wilson and Pike, is sometimes called the quantitative explanation. This theory holds that the vestibular nerve has two types of endings. One type was considered highly sensitive to anodic stimulus and responsible for eye movements toward the side of the anode. A second, more numerous, but less sensitive type of fiber was felt to respond to cathodic stimulus and to cause contralateral eye movements.

The correctness of any of these theories has yet to be established conclusively, but the idea of a qualitative

difference in the two polarities has had the most interest.

3.3 Methods of Stimulation 14,27

There are several types of galvanic tests which may be performed. The simplest are of the unipolar and bipolar varieties.

In the unipolar test, the stimulating electrode is placed on either the tragus or mastoid and an indifferent electrode is placed on either the forehead or the back of the neck. Bipolar stimulation employs electrodes on both tragi or mastoid processes so that current passes directly through the head. In both tests, the cathode is designated as the stimulating electrode.

Another possible test which is a combination of the two above is the double galvanic method. In this test, electrodes are placed on both mastoids or in the meati of the ear as in the bipolar test. Both electrodes are connected to the stimulus current. An indifferent electrode is placed on the neck, forehead, or abdomen. This method is less specific than the former two.

Pulsed current, which Spiegel calls rhythmic stimulation, has also been shown to bring about nystagnus at pulse frequencies of less than 10 per second. This is not, strictly speaking, galvanic stimulation since it is not a constant stimulus.

A number of interesting items can be learned with the aid of a different type of technique known as the chronaxia test. A general measure of neural threshold,

chronaxia compares a standard current intensity acting on a specific nerve with the time required for that current to travel the length of the nerve. The intensity of direct current which will just traverse a nerve given an infinite amount of time is termed a rheobase. In the standard chronaxia test, a current of two rheobase magnitude is applied and the passage time is noted. The time is called the chronaxia for the nerve. The measurement of the response in the case of galvanic vestibular stimulation is the time from application of current until head movement or eye deviation occurs (with errors which can be partially accounted for).

Chronaxia is relatively constant between individuals for a given nerve. The reported values for chronaxia for the vestibular nerve vary considerably, however, from about one millisecond to well over ten milliseconds. This is probably due to difference in experimental techniques.

3.4 Associated Eye Movements

The eye movements associated with galvanic vestibular stimulation have a number of characteristics. One is a shift in mean eye position away from straight ahead toward the side of the anode. Also, beyond a certain intensity threshold, which may vary with mode (anatomical location of electrodes), nystagmus is elicited with fast phase toward the cathode. As mentioned above, Spiegel²⁷ hypothesizes that the anode has a depressor action on

tonic labyrinthine impulses. He feels nystagmus may result from an imbalance in the two vestibular nuclei as a consequence of this depressor effect.

Ruis and Garcia have also noted slow eye movements of a drift nature prebeding the onset of nystagmus and at a lower current threshold.²⁵ These movements appear to be a type of onset phenomenon and disappear with repeated stimulus even if nystagmus persists. They did not use a constant stimulus but instead employed 20 millisecond pulses of from 5-70 volts at a frequency of 5 pulses/second.

The movements are biphasic with a fast first phase lasting about 1-2 seconds. The vertical component was found to be larger than the horizontal component. For long duration pulses, nystagmus was observed but only after the initial biphasic period. Increased stimulus amplitude shortened the nystagmus latency time.

3.5 Eye Movement Monitoring during Galvanic Stimulation ^{2,3}

A comment on the monitoring of eye movements during galvanic stimulation is of interest. A number of researchers have employed electro-oculography (see Chapter 2) in such experiments and most report that the galvanic current severely alters the corneo retinal potential in one or several ways. All suggest that the photoelectric technique or other which will not be directly influenced by the D.C. current be used in measuring eye movements

during galvanic stimulation.

3.6 Other Responses

In addition to eye movement, head inclination and body sway have been used as objective measures of response to galvanic vestibular stimulation. Both of these phenomenon normally exhibit, when present, an inclination toward the side of the body on which the anode is located. They are probably manifestations of the stimulus modulation of tonic impulses to the body musculature as Spiegel demonstrated in the experiment mentioned above. Spiegel also reports that the falling tendency may occur at lower current levels than necessary to elicit nystagmus.

Blonder reports using a version of the falling reaction as a standard measure of galvanic response in clinical tests.^{14,27}

3.7 Subjective Sensations

Subjective sensations as a result of galvanic stimulation are often difficult to interpret. Subjects report sensations of sway, both side ways and front ot back, dizziness, and rotation. Also, above some threshold current(which varies with subject), a tingling sensation is experienced under the electrodes with strongest sensation under the cathode.

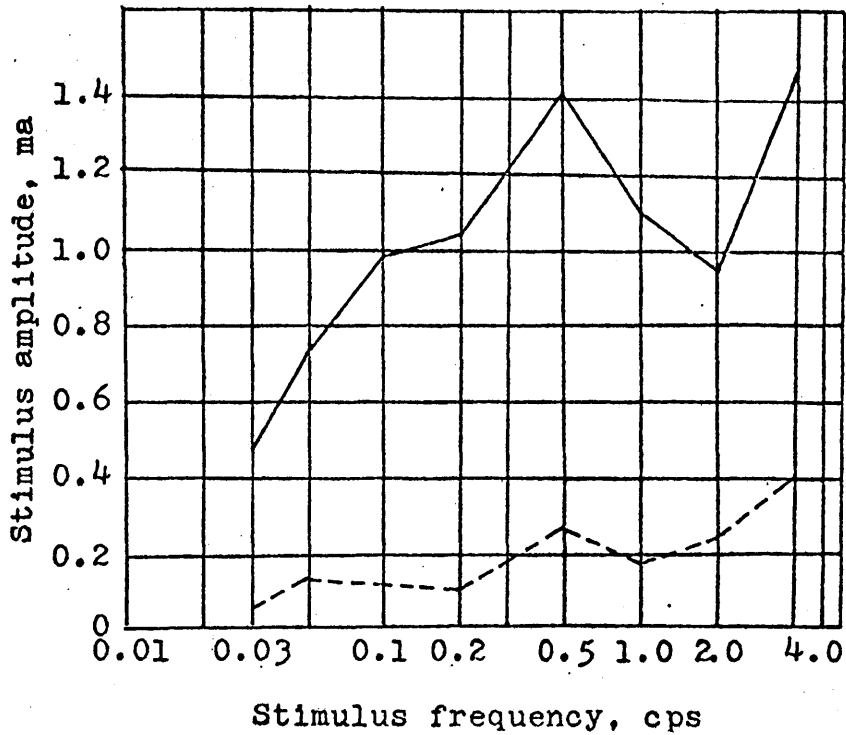
The nature of the subjective sensation may be related to subject experience and adaptation. For this reason, it may be well to group all such sensations

under the admittedly vague heading of disorientation.

Malcik has employed a binaural D.C. stimulation of 3 ma. to 350 pilots in order to simulate illusions such as sway or rotation experienced during flight.¹⁷ His subjects were asked to fly an instrument flight simulator while under the influence of this current. He reports that all experienced illusory sensations to some degree. Those subjects with more instrument experience were able to compensate for the illusions more readily than those with limited instrument practice. Performance also improved for all subjects as habituation developed for the galvanic stimulus. Since the eyes were fixated on instruments, no noticeable nystagnus was observed.

3.8 Low Frequency Sinusoidal Stimulation^{10,11,12,13}

In recent years, Dzendolet and his associates have studied the effects of sinusoidal galvanic stimulation on body sway and subjective sensation. The stimulus was applied binaurally at the mastoid processes of blindfolded standing subjects. Eight stimulus frequencies ranging from 0.030 - 4.0 cps were presented in random order. The stimulus amplitude was increased continuously on each run starting from 0 ma. and increasing at a constant rate of 0.0050 ma/second. Objective and subjective responses were determined including thresholds. A plot of the latter is shown in figure 3.1 It is interesting to note the relative



Subjective Treshold ———
Objective Treshold - - -

Figure 3.1

Subjective and objective current thresholds for sinusoidal vestibular galvanic stimulation as a function of stimulus frequency (12)

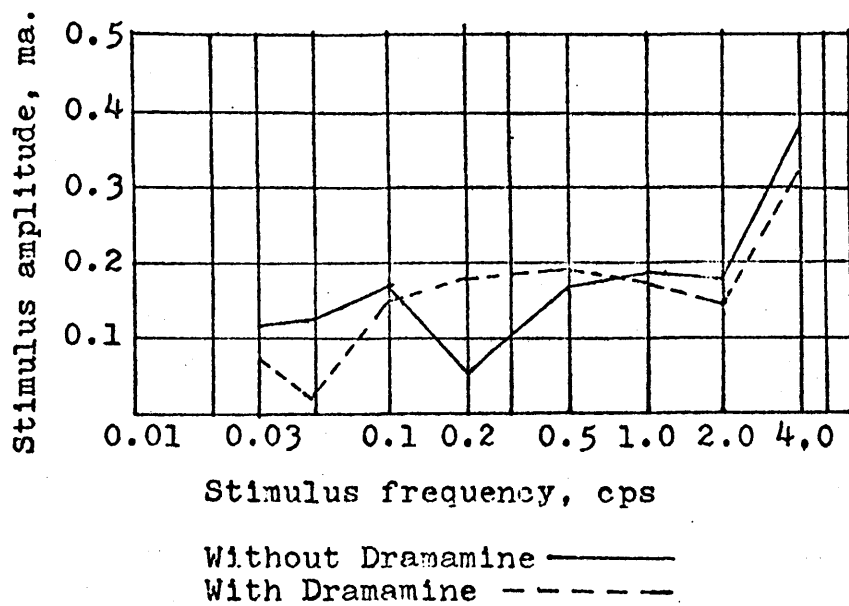


Figure 3.2

The effect of Dramamine on the objective threshold for sinusoidal galvanic vestibular stimulation (13)

difference in threshold between subjective sensation and objective response. (The latter is determined from body sway, the former by subject indication) At low frequencies, the objective response threshold is fairly constant at a stimulus of $100\mu\text{a}$ and increases to about $400\mu\text{a}$ at 4 cps. Subjective thresholds are all considerably higher varying from $500\mu\text{a}$ to 1.4 ma over the frequencies used.

The subjective thresholds agree rather well with those reported above for D.C. stimulation. The objective values are considerably lower. The difference in the type of stimulus is undoubtedly a factor in these differences.

Subject sway was found to be proportional to the frequency of the input stimulus. Reported subject sensation varied considerably: oscillation of head and torso, oscillating sideways and back and forth, and a few instances of vertigo. These are consistent with those reported above for direct current stimulation.

An interesting sidelight to this work with possible clinical applications is as follows. These researchers noted that the sinusoidal galvanic stimulus is comparable in some way to the factors causing motion sickness (i.e. slowly oscillating ship or automobile).

In particular, they find a lowered objective threshold for sinusoidal stimulation at a frequency of 0.2 cps. (See figures 3.1 and 3.2) They report the findings of other researchers of a high incidence of motion sickness phenomena (nausea, vomiting, etc.) at frequencies near

this value. When they administered dramamine, a common anti-motion sickness drug, the threshold at 0.2 cps was raised considerably as shown in figure 3.2. This may indicate that the drug acts on the same site in galvanic stimulation as in motion sickness, though no conclusive evidence exists on the actual site in either instance.

Whether there is any significance to this comparison is yet to be substantiated. It is nevertheless an interesting observation.

3.9 Summary

This chapter has reviewed the nature and point of action of the galvanic vestibular reaction. At present, no final answer is available concerning the action site of the stimulus though evidence generally points to the peripheral sensory nerve.

Cathodic and anodic stimuli bring about different qualitative responses with those at the anode apparently more significant. Eye deviation and/or nystagmus are usually elicited by the stimulus above a certain intensity level. Nystagmus, when present, has its fast phase directed toward the side of the cathode.

CHAPTER 4

DESCRIPTION OF EXPERIMENTAL METHOD

This chapter discusses the experimental procedures used to study the influence of galvanic vestibular stimulation on the perception of rotation.

4.1 The Basic Experiment

The intent of this research was to study, in a qualitative manner, the relationships between modes of application and intensities of galvanic stimuli and a subjects' perception of rotation. Thus an experiment was sought which would employ both rotatory and galvanic stimuli administered independently of one another.

The experiment which was used consisted of the following. The subject was placed in a darkened Barany chair and a zero mean random input was applied to the chair. The subject was provided with a three state controller and was given the task of countering any sensations of motion which he experienced. That is if he felt he was moving to the right he should press his controller to the left until he no longer sensed motion and so on. Assuming that the random signal indeed has a zero mean and that the subject has no directional preponderance, one would expect, theoretically, that

the subject would counter any motion above his threshold and that the chair would not move more than slightly away from the reference position.

If a galvanic stimulus is applied to the subject together with the random input to the chair, one would expect the subjects' motion sensation to be altered in some manner (On the basis of the discussion in Chapter 3). This approach was adapted with the postulate that the galvanic stimulus would bias the threshold for rotation perception. The measure of response would be the deviation of the chair position over the course of a run.

The experiment thus places the subject in an active role as opposed to the passive role of the similar experiment described in Chapter 2. The three state controller was employed since it appeared important that the subject respond only to a sensation of motion in the clockwise direction and not to the magnitude as he might were a graded controller such as a joy stick used.

The average subject would not be expected to differentiate between various types of angular movement. Hence, the subject's were only asked to counter motion, and not, say, velocity or accelerations which might be vague concepts for some subjects.

Angular accelerations are kept relatively small with these conditions thus no large cupula deflections or extended reactions to any given stimulus are to be expected.

Each subject was to be run with each of the six possible modes, unipolar right cathode and right anode, unipolar left cathode and left anode, and bipolar left cathode and right cathode and at six different intensity levels. The latter number was not completely arbitrary but related to the overall experimental design which will be discussed in the next section.

The lowest intensity level was chosen at $100\mu\text{a}$ partially due to Dzendolet's reported objective threshold for low frequency sinusoidal vestibular stimulation as discussed in Chapter 2.¹² Successive intensity values were doubled up to a maximum of 3 ma. in order to cover as wide a range as possible and still remain within pain and safety levels.

In addition to six runs with combined rotational and galvanic stimulus, two control runs, one at the beginning and the other at the end of the session were added to make a total of eight runs per subject. The controls were added not only to determine the normal response without current but also to discover, if possible, any overall effect on this norm after the combined experiments.

Eye movements were to be monitored in addition to the subjective response in an attempt to obtain an involuntary measure of response.

4.2 Experimental Design 6,18

Once the basic experiment was decided upon, a suitable experimental design was required in order to

study a number of different variables in a systematic way. A design was sought which would incorporate all of the following features: 1.) all six possible modes of unipolar and bipolar galvanic stimulation, 2.) a number of different intensity levels, 3.) yield as much information as possible about effects of galvanic stimulus, 4.) employ as few subjects as possible, 5.) balanced for the elimination of order effects.

Since there were six possible modes, it was decided arbitrarily to use six intensity levels in the experiments as mentioned above. If each such were run at every mode and intensity, however, thirty-six runs per subject would have been required to include all of the possible combinations. In order to reduce the number of runs required per subject and in order to achieve the randomness of application desired, a slightly modified form of the graeco-latin square experimental design was employed. 6,18

The graeco-latin square is an extension of the latin square design. An example of a 6x6 latin square is shown in figure 4.1. The rows represent subjects, the columns represent the order of experimental runs, and the letters entered in each position represent six experimental conditions, in this case representing the six modes of galvanic stimulation. Each letter appears only once in each row and each column. In addition, no letter precedes or follows any other letter more than

A	B	C	D	E	F
B	D	A	F	C	E
C	A	E	B	F	D
D	F	B	E	A	C
E	C	F	A	D	B
F	E	D	C	B	A

Figure 4.1

Completely orthogonal 6X6 Latin Square

		Run Number					
		1	2	3	4	5	6
Subject Number	1	AU	BV	CX	DY	EZ	FW
	2	BZ	DW	AV	FU	CY	EX
	3	CZ	AW	EY	BX	FV	DU
	4	DZ	FY	BW	EV	AX	CU
	5	EW	CV	FZ	AY	DX	BU
	6	FX	EU	DV	CW	BY	AZ

KeyIntensities

U = 100 μ a
 V = 200 μ a
 W = 400 μ a
 X = 800 μ a
 Y = 1.6ma
 Z = 3.0ma

Modes

A = Unipolar Right Cathode
 B = Unipolar Right Anode
 C = Unipolar Left Cathode
 D = Unipolar Left Anode
 E = Bipolar Left Cathode
 F = Bipolar Right Cathode

Figure 4.2

Graeco-Latin Square used in experimental design.

once in the square. An array such as this is said to be completely orthogonalized, which means practically that all the elements are independent. (Another way of viewing this is to consider the six letters to be unit vectors in a six dimensional vector space. If any row or column is considered a six dimensional vector then its inner product with any other row or column will = 0 implying orthogonality in the mathematical sense.)

A graeco-latin square is composed of latin squares imposed one upon the other and allows the introduction of a second set of conditions into an experiment with a fixed number of subjects and runs. In the ideal case, each of the two latin squares would be orthogonal with respect to itself and with respect to the other square. The latter property would require that no pair of conditions, one from each latin square, would appear more than once in the graeco-latin square.

The graeco-latin square used in this thesis is shown in figure 4.2. The letters A-F represent the modes and the letters U-Z represent six intensity levels. The dimension of the square was restrained at 6x6 by the modes as mentioned above. This restraint introduced a slight difficulty however. Euler and others have shown it to be impossible to construct a completely orthogonal graeco-latin square with no repetitions of conditions in all rows and columns. ⁶

If two completely orthogonal 6x6 latin squares are imposed one upon the other, a repetition will always occur in some entry. (e.g. the combination BU representing mode B and intensity U or a similar combination would appear more than once in the square) A repetition of conditions is not desirable since each combination of mode and intensity should be present once in the series of experiments.

The solution to this difficulty lies in relaxing the orthogonality condition on one of the squares. In order to accomplish this an assumption was made that the modes, in general, were likely to have a greater effect on the results than the intensities. (This assumption was based on findings reported in the literature and as discussed in Chapter 3). On this premise, the modes were made completely orthogonal in a latin square corresponding to figure 4.1.

The intensity conditions were then added over this square in such a way that no mode-intensity pair was repeated and that the square of intensities was as nearly orthogonal as possible. As shown in figure 4.2, the intensities increase in magnitude as their code letters in the square were also balanced so that the sum of the current given to all subjects as a whole on the first three runs was approximately equal to the total over the last three runs. This was done to avoid a trend in the application of current over all subjects. With these

provisions, the design was then considered to be entirely random for the purpose of later data analysis.

The graeco-latin square lends itself well to variance analysis as will be noted in Chapter 5. Other experimental designs such as balanced incomplete blocks were considered but were rejected since they appeared to offer no advantages over the graeco-latin square for this study.

4.3 Description of Equipment

This section describes the equipment used to rotate, galvanically stimulate and to monitor the responses of the subjects during the experiments described above.

4.3.1 Rotating Chair

The Man Vehicle Laboratory's rotating chair was employed to provide angular motion stimulation about the vertical axis. It is driven by two 15 ft.-lb. torque motors controlled from a pulse width modulated servo system. Details on the chair may be found in Katz's thesis.¹⁶ The command signal consisted of the sum of a zero mean pseudo-random input and the subjects' response stick. The random signal was obtained by summing seven sinusoids of frequencies ranging from 0.1 to 0.61 radians/second and recorded on magnetic tape. The gain of the signal was adjusted as shown in figure 4.7 so that the maximum amplitude deviation caused the chair to move 540 degrees away from a zero reference position with a 150 pound subject in the chair.

In order to counter any motion sensation due to either the random input or the galvanic stimulus, the subject was provided a three state controller which he operated with his right hand. With this controller, the subject was able to apply a step input to the servo system so as to cause the chair to move either CW or CCW. In the middle position, the switch had no effect on chair movement. The amplitude of the step was adjusted so that, in the absence of the random input, it caused a step change in chair position of 540 degrees.

Chair position was monitored with a 20K potentiometer attached through gears to the axis of chair rotation. This potentiometer produces an output of 0.1 volt/radian of chair movement which is scaled so that 0.25 volts = 360 degrees (2π radians).

4.3.2 Galvanic Stimulation Equipment

Galvanic stimulation was applied through two specially designed circular electrodes approximately one inch in diameter affixed to the subjects' mastoid processes. A diagram of one of these electrodes is shown in figure 4.3. A layer of wetted gauze impregnated with electrode paste was included in the electrode in order to avoid metal to skin contact and to obtain a relatively uniform current distribution. The two electrodes were mounted on a standard headband.

A so called indifferent electrode consisting of a 2 inch by 3 inch gauze pad was placed on the back of the

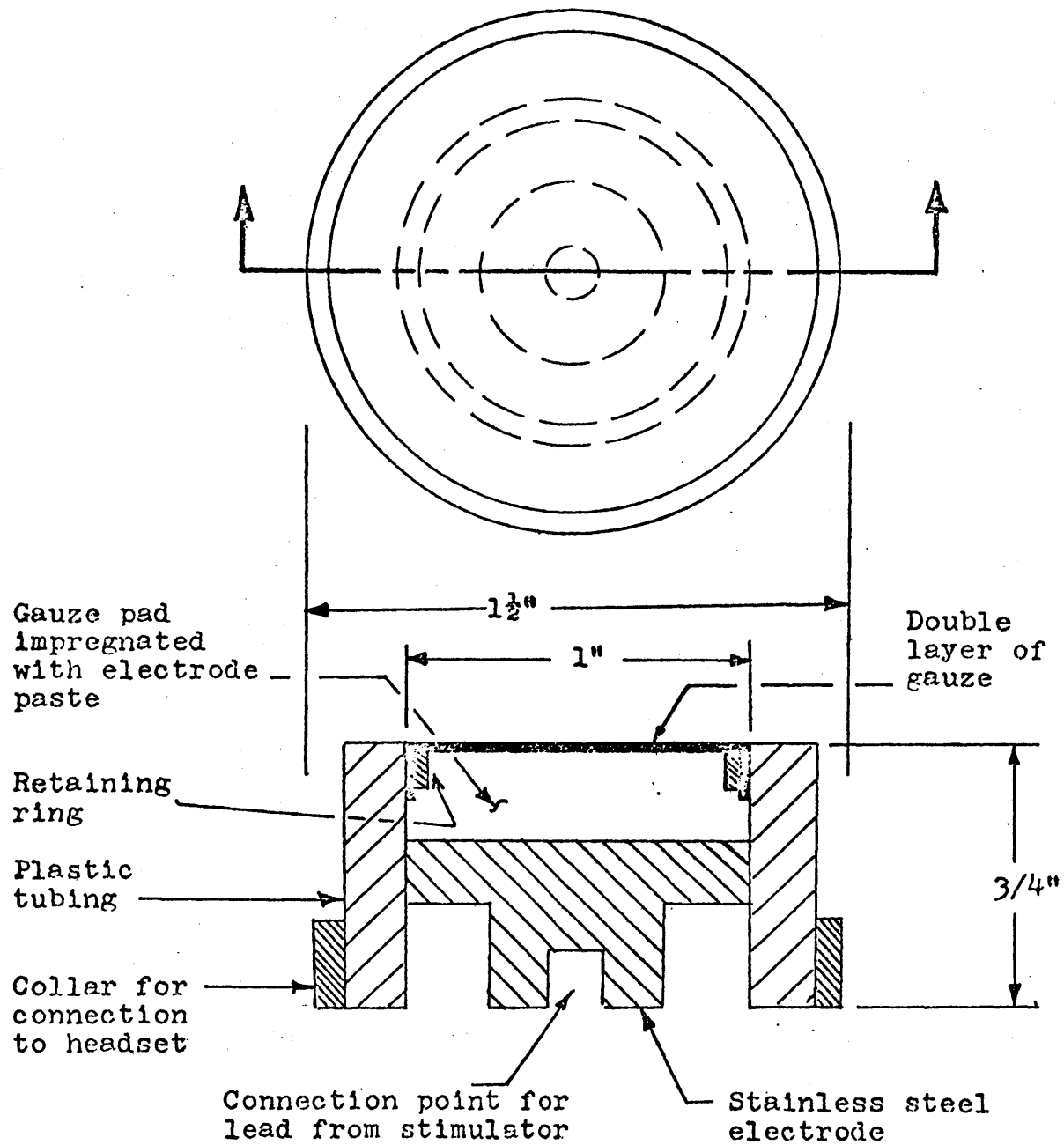


Figure 4.3
 Stimulating Electrode
 (approximately twice actual size)

subject's neck and held in place with surgical tape. This electrode was used as the common in unipolar tests.

All three contact areas on the subject were treated with electrode paste before the runs in an effort to achieve a nominal inter-electrode D.C. resistance of 2-3K ohms.

The positioning of the three electrodes on the subject is shown in figure 4.4. Figure 4.5 shows a schematic for the stimulus circuitry. D.C. current was obtained from an Electronics for Life Sciences Constant Current Stimulator Model CCS-1A. This stimulator is battery powered and has a maximum output capacity of 10 ma. at 90 volts. Switching was provided between the stimulator and the electrodes in order to select either bipolar or right or left unipolar connections. Polarity reversal is accomplished at the stimulator, thus allowing for all six possible modes as outlined earlier.

The maximum current to be used was 3 ma., hence the stimulator was fused at 5 ma. The subject was able to disconnect the galvanic stimulus at any time during the experiment by depressing a "panic" button with his left hand. Pressing this button also rang a bell to alert the experimenter to the subject's difficulty.

A 20K potentiometer was added as shown in figure 4.5 to allow gradual application of current during an experimental run because at higher intensities particularly, a step input in current is often discomforting to the subject.

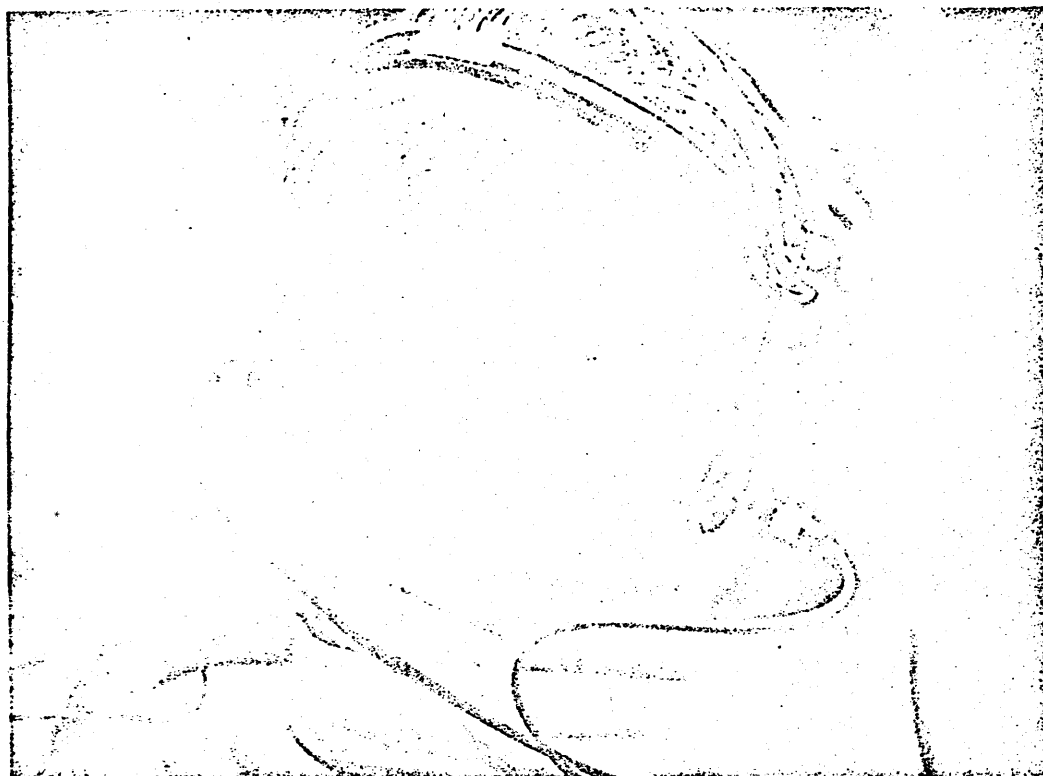


Figure 4.4

Locations of Stimulating Electrodes

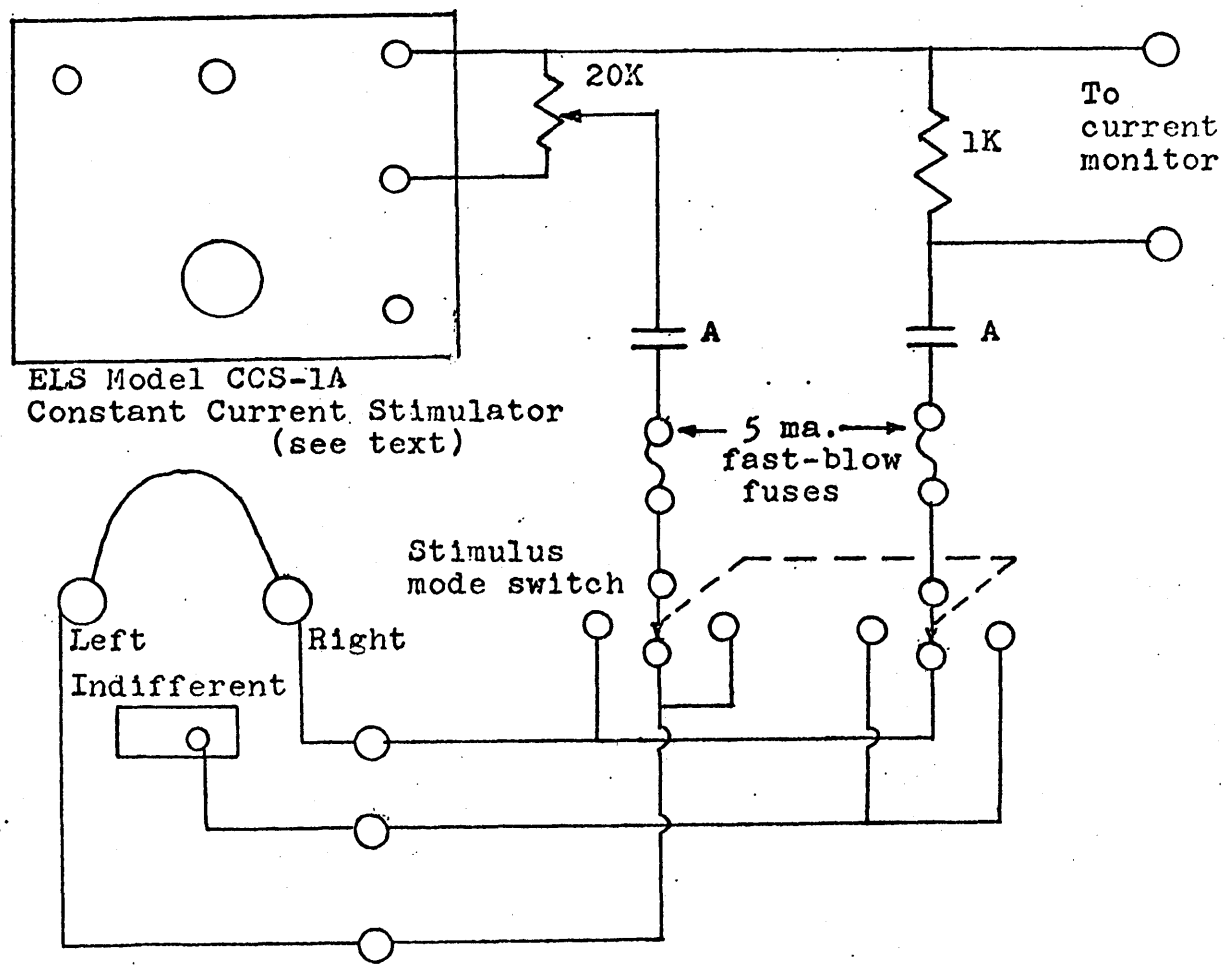
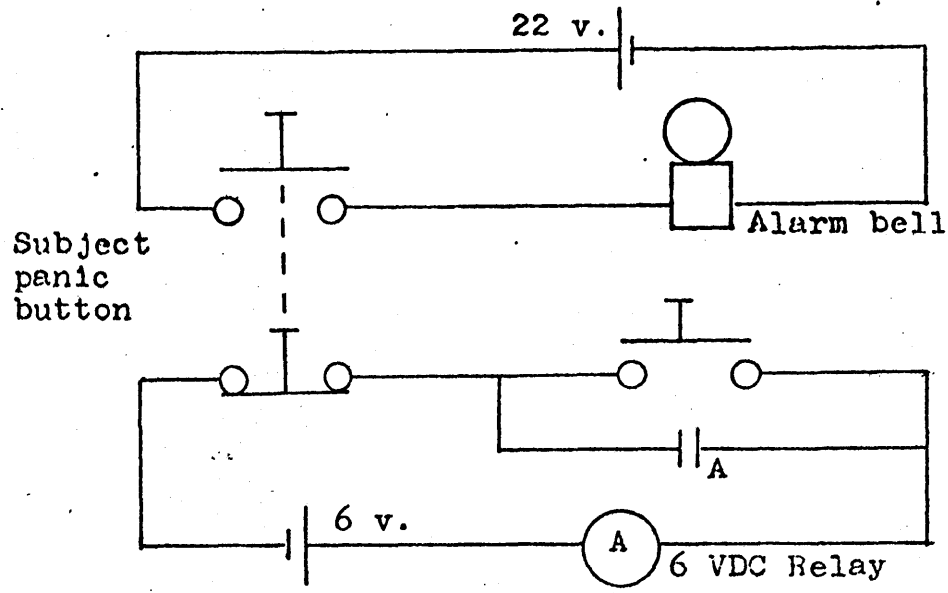


Figure 4.5
Galvanic Stimulus Connections

Current was monitored by measuring the voltage across a 1K ohm resistor in series with the stimulation circuit. The measuring circuit had a floating ground in order to isolate the subject from possible ground loops.

4.3.3 Eye Movement Monitoring

Subject eye movements were monitored using a Biometrics model SG HV - 2 photoelectric eye monitor, the operation of which was discussed in Chapter 2. The positioning of the monitor on the subject is shown in figure 4.6. In order to calibrate the instrument, the following procedure was employed. A white screen with three small black crosses drawn upon it was placed in the subject's line of sight in the rotating chair. The crosses were arranged so that one was directly ahead of the subject and the other two were 15 degrees to either side of this central point. With all lights out, as during the experiment, the screen is invisible. A very dim light, under subject control, was used to make the screen barely visible during calibration. With this light on the subject was asked to look straight, right, and left. The gain of the monitor was adjusted so that 20 degrees of horizontal eye movement = 1 volt. At the conclusion of the calibration, the subject turned off the light and was allowed to adapt to the darkness. The calibration was checked at the end of each run for possible drift or other changes.

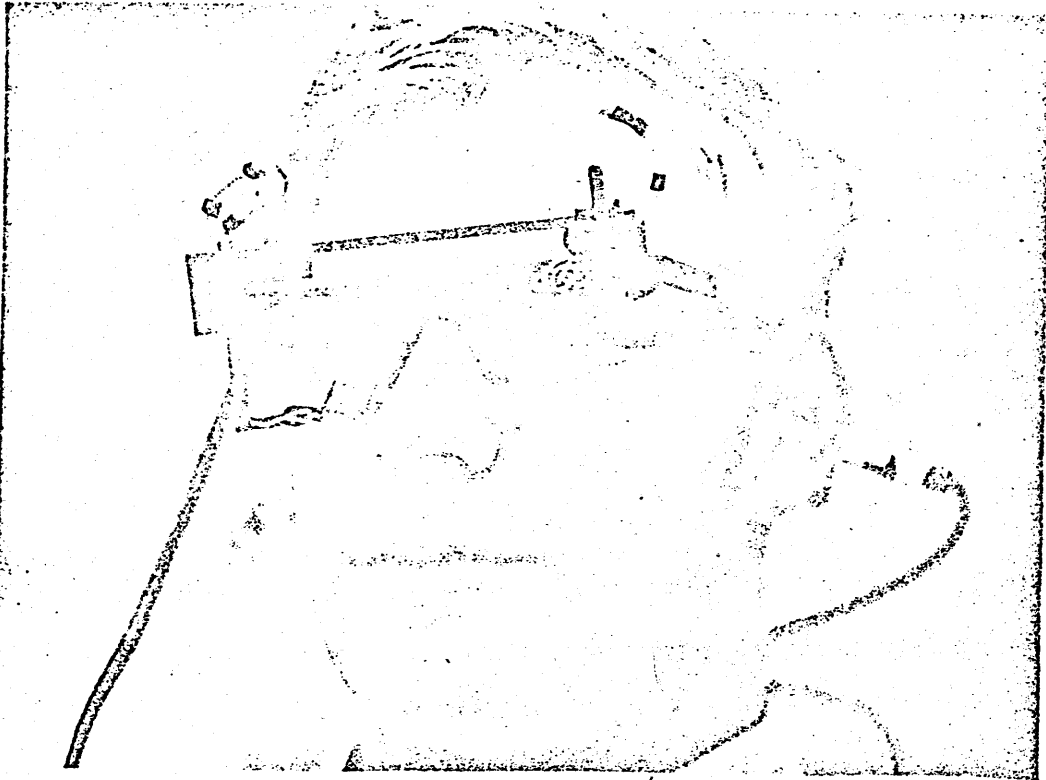


Figure 4.6

Positioning of the Eye Movement Monitor

4.4 Selection of Subjects

Six subjects, five males and one female, were used in the experimental design described above. Each of the subjects underwent a standard clinical vestibular examination in the Otoneurology Laboratory at the Massachusetts Eye and Ear Infirmary. All were judged normal tests for the purposes of this experiment. One showed a slight left directional preponderance but the amount was not considered extreme hence he was retained.

In addition to the normal subjects, one female subject with no vestibular function was run. Her clinical condition was described as neurofibromatosis and she had had a bilateral acoustic neuromas removed surgically.

4.5 Experimental Protocol

Approximately one and one half hours were required to run each subject, including approximately one half hour of subject and equipment preparation.

Subject preparation consisted of mounting the electrodes, checking inter-electrode resistances, calibration of the current monitor, mounting and calibration of the eye movement monitor and general instructions.

The general instructions were consistent from subject to subject and included instructions for the eye movement calibration. A copy of these instructions is given in table 4.1.

A total of eight runs per subject were made. These were an initial control run, six runs with current, and a

1. The chair may rotate. Your job is to stop the movement of the chair by pressing the switch with your right hand. Pushing down the switch on the right will make the chair turn right; pushing down on the left will make it move left. In the center position, there is no effect on chair movement. (demonstrate) So, if you feel the chair is standing still, do not press the switch. If you feel it is turning to the right for example you push the left side of the switch until you feel the turning has stopped and then release the switch. (demonstrate)
2. Keep your eyes looking straight ahead and do not move your head.
3. You may feel a tingling sensation under the electrodes at times. It will not be painful-just disregard it.
4. If you need help, push the alarm button. (demonstrate)
5. (Eye Movement Monitor Calibration) On the card in front of you there are three crosses, one at the center, one to your right, and one to your left. When you are asked to look straight ahead, look at the center cross. Look to the right, straight, or left on command and continue to look at the cross until the next command.

We will repeat this when the room is dark. There is a small panel light which will allow you to see the crosses. When we have finished with this, turn the light off. (show subject the location of the light switch)

6. Now we will run the chair as before but with the curtains closed and the lights out. Be sure to keep your eyes open looking straight ahead.

Table 4.1

Instructions to subjects prior to experimental runs.

final control run. The modes and intensities for the galvanic stimulation runs were determined from the experimental design and were set manually before each run. Each of the eight runs lasted slightly more than two minutes with a five minute rest period between runs, the latter to reduce the chance of residual effects. During the six runs with galvanic stimulus, the chair motors were started first and the current was then immediately applied by turning the intensity potentiometer up (the 20 K potentiometer is shown in figure 4.5).

No attempt was made to eliminate subject audio cues. Ambient noise level during the experiments was fairly high due to the chair torque motor hum and to a small exhaust fan in the chair. The noise level was deemed high enough to prevent any significant audio cues of motion.

Much has been made of the effect of subject arousal state on the quality of eye movements elicited during vestibular experiment.⁷ It was felt initially that the subject's task would maintain a high enough arousal level for this purpose. This may not have been the case in the experiments. Some discussion is given in the next chapter.

4.6 Data Records

Data for each experimental run was recorded on an eight channel Precision Instrument instrumentation recorder model P.S.200A. Five channels of analog data

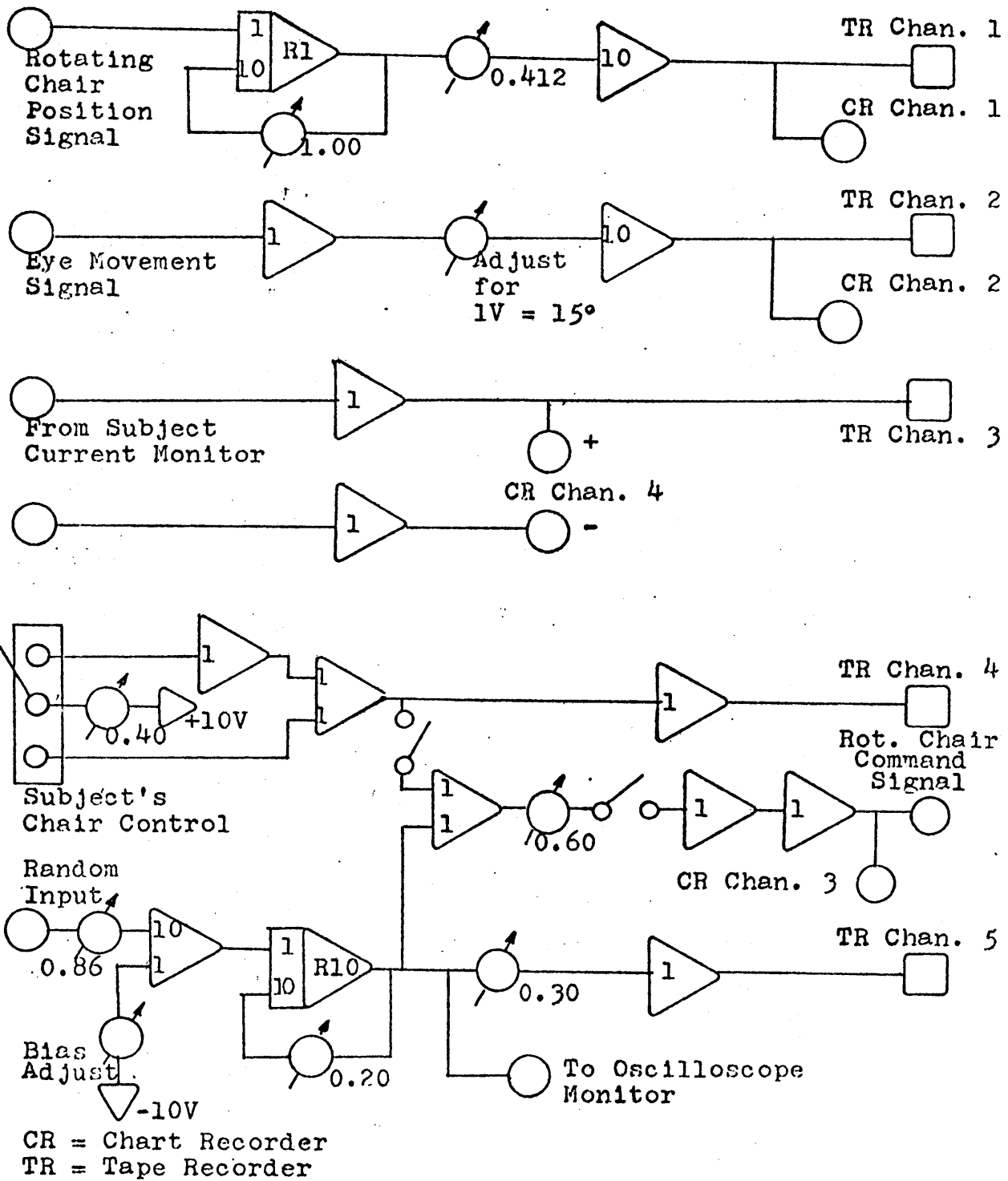


Figure 4.7

Monitoring and command signal connections

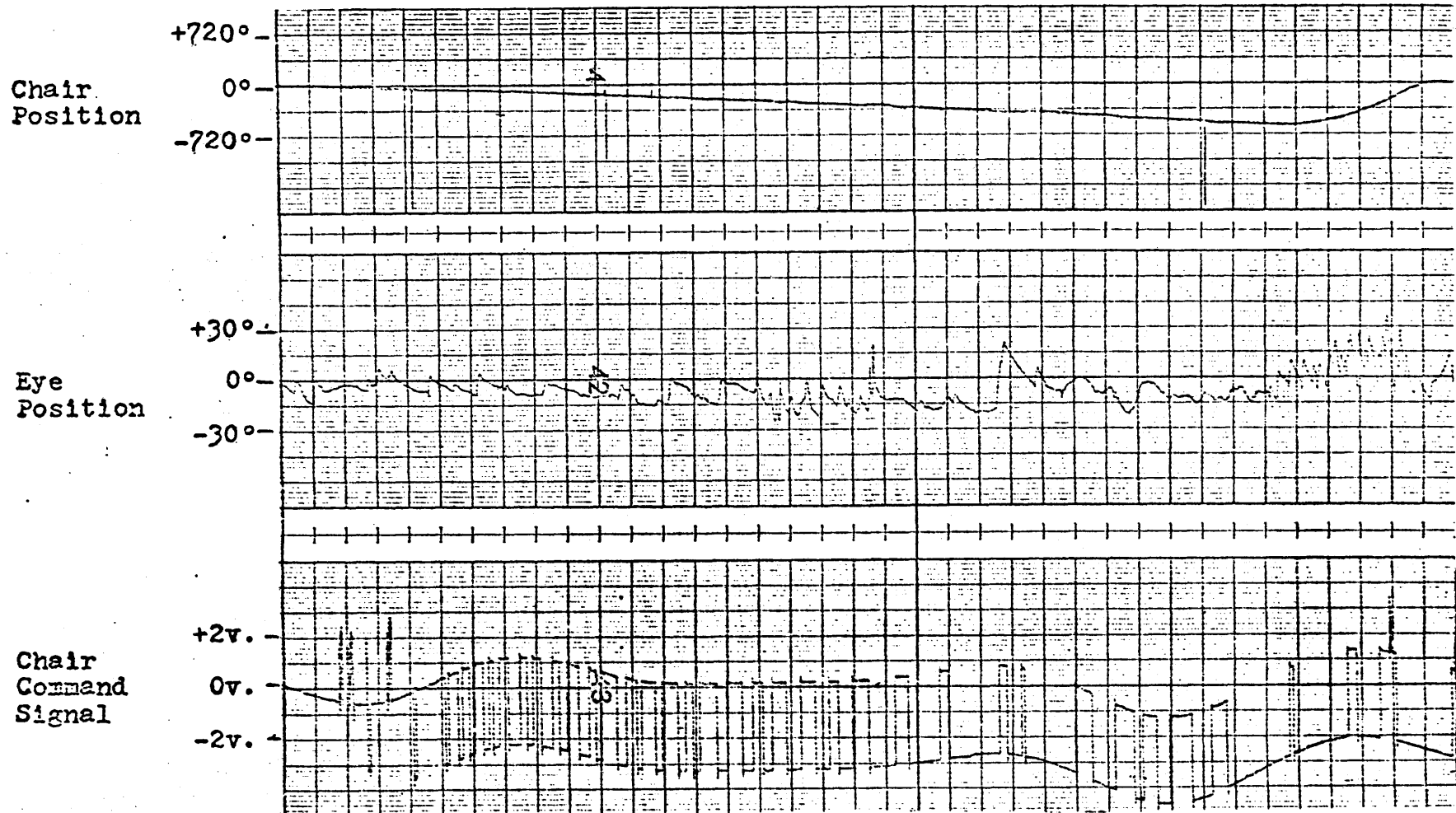


Figure 4.8

Time →

5 sec.

Typical Experiment Data
 (Galvanic Stimulus: Unipolar Left Anode; 1.6 ma.)

were recorded as shown in figure 4.8. These included 1.) chair position, 2.) eye position, 3.) random input to the chair, 4.) subject's stick control and 5.) stimulating current. The data was simultaneously recorded on a four-channel Brush chart recorder model 240. The random input and subject stick control were combined in order to display all data graphically on the four channels.

The current monitor channel is not shown in figure 4.8 due to space limitations. The galvanic stimulus consisted of unipolar left anode at an intensity of 1-6 ma. Note the right beating nystagmus (toward the cathode) and the leftward drift of the chair as the experiment progresses and the subject's use of right control almost exclusively.

It is also noted that the chair returns toward zero near the end of the run. This occurrence was observed in a number of runs but the cause is not clear. It might be an indication of cessation or reversal of the galvanic stimulus effect but this has not been substantiated.

CHAPTER 5

EXPERIMENTAL RESULTS

This chapter presents the results of the experiments performed in Chapter 4. The data analysis techniques are presented first followed by a discussion of the chair movement data. This is followed by a discussion of the eye movement data and the chapter concludes with some brief comments on the responses of the one abnormal subject tested.

5.1 Data Analysis

The experiments described in Chapter 4 produced two types of data: eye position and chair position versus time for each two minute run. In order to estimate the average drift away from the zero reference position, it was decided to calculate the mean value of chair position and of cumulative slow phase eye position over each run. The latter was used since it represents total amplitude of eye deviation during the experimental run.

5.1.1 Method for Determination of Cumulative Slow Phase Eye Position

Cumulative slow phase position was obtained from the original eye data by processing with the hybrid program, MITNYS. This program removes saccades and blinks which may

be present in the raw eye position signal and pieces the slow phase portions of the record together to form a continuous cumulative position signal. MITNYS was originally developed for use in on-line vestibular experiments and is discussed in detail elsewhere.³¹ It is also discussed briefly in appendix B which also presents a block diagram and a listing of the program.

5.1.2 Determination of Statistics of the Data

The mean, variance, and standard deviation for chair position and cumulative slow phase eye position for each run were calculated using the hybrid program, MAN, which is described in appendix C.

The mean value of position for each run with current was then entered in its respective location in the graeco-latin square used in the experimental design. Mean values for the control runs were also calculated and added in their respective locations at the beginning and end of each subject's data set. These results are given in table 5.1 for chair data and table 5.2 for eye data. All entries represent angular position measured in degrees. The tables also show the data rearranged according to modes and intensities of the galvanic stimulus (recall that these two parameter groups were randomized in the original graeco-latin square).

		66 Order							
		0	1	2	3	4	5	6	7
Subjects	1	213	62	168	235	-150	225	65	138
	2	-95	231	26	37	77	167	95	-235
	3	193	180	175	182	51	143	153	211
	4	-17	-9	13	4	40	49	7	84
	5	-10	74	179	-296	36	-172	115	77
	6	-2	-108	22	-21	192	157	-308	6

		Modes					
		A	B	C	D	E	F
Intensities	U	62	115	7	153	22	77
	V	37	168	179	-21	40	143
	W	175	4	192	26	74	65
	X	49	51	235	-172	95	-108
	Y	36	157	167	-150	182	13
	Z	-308	231	180	-9	225	-296

Table 5.1

Raw mean chair position data arranged according to subjects vs. order and intensities vs. modes (Orders 0 and 7 represent control runs. All entries are expressed in degrees)

		Order							
		0	1	2	3	4	5	6	7
Subjects	1	-263	-221	-20	56	-75	226	-88	-39
	2	-22	88	77	-63	12	112	-82	-199
	3	49	323	13	90	76	43	-59	180
	4	18	53	-124	164	83	41	55	90
	5	351	343	311	-199	41	-340	213	427
	6	7	48	14	78	-21	13	-66	-197

		Modes					
		A	B	C	D	E	F
Intensities	U	-221	213	55	-59	14	12
	V	-63	-20	311	78	83	43
	W	13	164	-21	77	343	-88
	X	41	76	56	-340	-82	48
	Y	41	13	112	-75	90	-124
	Z	-66	88	323	53	226	-199

Table 5.2

Raw mean eye position data arranged according to subjects vs. order and intensities vs. modes (Orders 0 and 7 represent control runs. All entries are expressed in degrees)

5.1.3 Tests for Significance of Various Parameters

In order to determine which of the parameter groups among subjects, order, modes, and intensities had significant influence on the data, a standard analysis of variance was performed. The analysis of variance is common technique for studying experimental data and is probably familiar to most readers. In brief, it involves operations on a set of data in such a way as to independently estimate the variance of each of the parameter groups contributing to the data. A residual variance is also estimated. This term represents the variance of random error contributions. The residual variance is assumed to be unbiased by differences among the parameters.

To test for possible significance of any parameter group, a null hypothesis is introduced. This hypothesis assumes that each parameter is normally distributed and that all parameter group means are identical. The variance estimate of each parameter group is then compared with the residual variance estimate. If the ratio of the two estimates is small (more accurately, below a certain F level, to be discussed below) then the null hypothesis holds indicating the parameter group being tested was not a significant factor in the data.

If the variance ratio is large however, the null hypothesis must be rejected. This leads to the conclusion that the mean of the parameter group being tested does differ significantly from the means of the other groups. Thus, this group is concluded to have a significant influence on the results.

The significance level of the variance ratio, VR, is determined with the aid of the so-called F distribution. This distribution is a function of the degrees of freedom of the parameter group and of the residual. It is commonly tabulated in statistical handbooks according to various probability of occurrence levels. One has then only to decide how large a chance for error he will allow in establishing significance. The table of F for this probability level will then indicate the variance ratio required for the given degrees of freedom of the parameter and the residual. The .05 probability level is often used in experiments such as the present one and was chosen as the standard here.

The graeco-latin square lends itself well to an analysis of variance study. Two computer programs, ANVAR and ANVAR2, were written to perform this analysis on the experimental data. The two programs are identical except that ANVAR2 takes into account the control runs while ANVAR does not. Both programs are discussed in appendix D.

If the analysis of variance indicates that a certain parameter group has a significant influence on the results, one would then like to know where differences lie within the group. A student "t" test may be used for this purpose.

The "t" test compares the differences between two means with a standard error term derived from the residual variance found in the analysis of variance and also depending upon the number of samples in each of the two

means being tested. The standard error term is often called the error variance and the latter term is used here.

The ratio of differences in mean to error variance yields a "t" value. Values of "t" are tabulated according to degrees of freedom of the residual and the percentage probability of occurrence. For significance, the ratio in the test must equal or exceed the value of t for the two parameters of the table. .05 is often the standard for the latter.

Two straightforward programs, T TEST and T TEST₂, were written to perform the student "t" on the experimental data. They are identical except that T TEST₂ makes provisions for control runs while T TEST does not. The two programs are described in Appendix E.

Details on the theory of the analysis of variance and the student "t" test may be found in the references.^{6,18}

5.2 Analysis of Chair Position Data

Using the analysis of variance methods discussed above, the chair position data shown in Table 5.1 was studied. Table 5.3 gives the results of performing the analysis of variance on this data without consideration of control runs. The data, as it appears in the graeco-latin square, is at the top of the table, the variance table is in the middle, and the means for each subject, mode, and intensity are at the bottom. Below the table, the error variance is printed out for possible use in a

		Order					
Subjects	=	62=	168=	235=-	150=	225=	65
	=	231=	26=	37=	77=	167=	95
	=	180=	175=	182=	51=	143=	153
	=	9=	13=	4=	40=	49=	7
	=	74=	179=-	296=	36=-	172=	115
	=	108=	22=-	21=	192=	157=-	308

SOURCE	DF	SS	VE	VR
MODES	5	= 194547.00	= 38909.50	= 2.67
INTENSITIES	5	= 38393.30	= 7678.65	= 0.53
SUBJECTS	5	= 139206.00	= 27841.20	= 1.91
ORDER	5	= 35478.90	= 7095.78	= 0.49
RESIDUAL	15	= 218361.00	= 14557.40	
TOTAL	35	= 625986.00		

Mean Responses

	SUBJECTS	MODES	INTENSITIES
1	= 100.8	A = 8.5	U = 72.7
2	= 105.5	B = 121.0	V = 91.0
3	= 147.3	C = 160.0	W = 89.3
4	= 17.3	D = 28.8	X = 25.0
5	= 10.7	E = 106.3	Y = 67.5
6	= 11.0	F = 17.7	Z = 3.8

ERROR VARIANCE= 69.66

Table 5.3

Analysis of Variance of Raw Chair Position Data

"t" test.

The variance ratio for each parameter group is listed in the variance table under the heading, VR. Each parameter group has five degrees of freedom. The value of F required at 0.95 level for these degrees of freedom is 2.90. It is seen that none of variance ratios equal or exceed this value, hence no conclusion can be drawn concerning significance.

It is useful to note the low value of VR obtained for order. Recall that the graeco-latin square was employed to reduce the effects on the results of order of presentation of the stimuli. A low VR value for order indicates the design has been successful in achieving the goal.

It is also useful to note that the VR value for modes is closest to the required F level. In an attempt to enhance the effects of the modes, a correction of the data to account for subject differences was made. This was accomplished by adding to each subject's data the difference between the overall mean and that subject's mean. For example, the overall mean of the 36 data entries was 58 degrees and the mean of subject 1 is found from Table 5.3 to be 100.8 degrees. The difference between the two values is $58 - 100.8 \approx -43$ degrees. If -43 degrees is added to each data point from subject 1, the mean of his data will become equal to the overall mean, eliminating the effect of his mean response from the data set.

This procedure was repeated for each of the six subjects. An analysis of variance was then run on the corrected data. The results are given in Table 5.4. Note that the value of VR for subjects has dropped almost to zero(it is not exactly zero due to round-off error). Also the VR value for modes is now 3.01, which is above the required F level of 2.90. The VR for order has not changed appreciably.

Since the modes are now shown to be significant, a t test may be conducted to determine where the actual differences lie. Such a test was conducted using the T TEST program. The results are shown in Table 5.5. Mode 1 is found to differ significantly from mode 3, 2 from 4, 3 from 4, and 3 from 6(Note modes 1,4 and 6 correspond to A,D and F; 2,3, and 5 to B,C and E in the experimental design). In each of these four cases, the difference occurs between an anodic and a cathodic mode. No differences are found between modes of the same polarity.

It may also be noted that the means for the anodic modes have large positive values(121, 172, 107) while the cathodic modes have smaller magnitude and tend to the negative direction(9, -28, -17). This result appears at first to be in agreement with the discussion in Chapter 3 where the anode was reported to have a greater effect than the cathode. If one considers the control runs, however, this result is not as clear.

	Order					
Subjects =	19=	125=	192=-	193=	182=	22
=	189=-	16=-	5=	35=	125=	53
=	91=	86=	93=-	38=	54=	64
=	32=	54=	45=	81=	90=	115
=	143=	248=-	227=	105=-	103=	184
=-	39=	91=	48=	261=	226=-	239

SOURCE	DF	SS	VE	VR
MODES	5	= 208809.00	= 41761.80	= 3.01
INTENSITIES	5	= 40952.20	= 8190.44	= 0.59
SUBJECTS	5	= 670.22	= 134.04	= 0.01
ORDER	5	= 31136.90	= 6227.38	= 0.45
RESIDUAL	15	= 208239.00	= 13882.60	
TOTAL	35	= 489807.00		

Mean Responses
SUBJECTS MODES INTENSITIES

1 =	57.8	A =	9.3	U =	84.7
2 =	63.5	B =	121.8	V =	91.8
3 =	58.3	C =	172.0	W =	90.2
4 =	69.5	D =	28.0	X =	25.8
5 =	58.3	E =	107.2	Y =	68.3
6 =	58.0	F =	16.8	Z =	4.7

ERROR VARIANCE= 68.03

*

Table 5.4

Analysis of Variance of Chair Data Corrected for Subject Differences

T TEST

ERROR VARIANCE= 68.03 T(P=0.05)= 2.13

MODES		INTENSITIES
= 1.0	= 9.3	= 84.7
= 2.0	= 121.8	= 91.8
= 3.0	= 172.0	= 90.2
= 4.0	=- 28.0	= 25.8
= 5.0	= 107.2	= 68.3
= 6.0	=- 16.8	= 4.7

M= 1	M= 3	T= 2.39
M= 2	M= 4	T= 2.20
M= 3	M= 4	T= 2.94
M= 3	M= 6	T= 2.78*

Table 5.5

"t" Test on Chair Data Corrected for
Subject Differences

The control run means are both 47 degrees. The mean of all six mode responses taken together is 61 degrees. The proximity of these two values suggests that an inherent bias may be present in the experiment, either due to the equipment or to subject response. If such a bias indeed exists, then correction of the mode means for it would make the magnitude of anodic and cathodic responses approximately equal. One would then conclude that anodic and cathodic stimulus produce approximately the same magnitude of effect.

It was also desired to learn if any of the intensities were significant. The VR value for intensities in both of the above analysis was small however. In order to enhance the intensity effects, the original data was corrected for differences between modes. This correction was made in a manner similar to that for the subjects above except that the overall mean was not used. Hence the mean of each mode after the correction would be \approx zero.

A difficulty arises here due to the fact that three modes are of one polarity and the other three of the opposite polarity. In order to truly eliminate the mode effects the polarity differences must also be accounted for. This is accomplished by correcting for the expected effects of either the anodic or the cathodic modes.⁵ The anodes were chosen arbitrarily and the corrections made by changing the signs of all data obtained during anodic stimulation. (modes B, C, and E). The data then corresponds

	Order					
Subjects =	53=-	47=-	75=-	121=-	119=	83
" =	110=	55=	28=	95=-	7=	11
" =	20=	166=-	76=	70=	161=-	182
" =	20=	31=	117=	66=	40=	153
" =	32=-	19=-	278=	27=-	143=-	6
" =	90=	84=	8=-	32=-	36=-	317

SOURCE	DF	SS	VE	VR
MODES	5 =-	3942.00	=- 788.40	=- 0.12
INTENSITIES	5 =	209004.00	= 41800.90	= 6.46
SUBJECTS	5 =	87565.70	= 17513.10	= 2.71
ORDER	5 =	37815.30	= 7563.07	= 1.17
RESIDUAL	15 =	97029.70	= 6468.65	
TOTAL	35 =	427473.00		

Mean Responses					
	SUBJECTS	MODES	INTENSITIES		
1 =-	37.7	A =-	0.5	U =	93.5
2 =	12.0	B =-	2.0	V =	32.8
3 =	19.8	C =	0.0	W =	70.2
4 =	71.2	D =	0.2	X =-	31.2
5 =-	64.5	E =-	0.3	Y =-	30.3
6 =-	63.8	F =	0.3	Z =-	137.3

ERROR VARIANCE= 46.44

Table 5.6

Analysis of Variance of Chair Data Corrected for
Mode Differences-no controls

T TEST

ERROR VARIANCE= 46.44 T(P=0.05)= 2.13

MØDES		INTENSITIES			
=	1.0	==	0.5	=	93.5
=	2.0	==	2.0	=	32.8
=	3.0	=	0.0	=	70.2
=	4.0	=	0.2	==	31.2
=	5.0	==	0.3	==	30.3
=	6.0	=	0.3	==	137.3

S= 1	S= 4	T=	2.69
S= 1	S= 5	T=	2.67
S= 1	S= 6	T=	4.97
S= 2	S= 6	T=	3.67
S= 3	S= 4	T=	2.18
S= 3	S= 5	T=	2.17
S= 3	S= 6	T=	4.47
S= 4	S= 6	T=	2.29
S= 5	S= 6	T=	2.31*

Table 5.7

"t" Test of Chair Data Corrected for
Mode Differences-no control

to that which might be expected had all cathodic stimuli been used. (Since the mode means have been forced to zero, it makes no difference whether anodic or cathodic modes are changed.)

The corrected data was processed with the analysis of variance program with the results given in Table 5.6. V.R. of the modes is now \approx zero and subject and order V.R.'s are not significant. The VR of the intensities has now become 6.46 however, well above the required 2.90. Thus a "t" test is justified for the intensity data in this form. The results of this test are given in Table 5.7.

The "t" test reveals that intensities 1, 2, and 3 (U, V, and W in the original notation) do not differ from one another but that all differ with one or more of the intensities 4, 5, and 6 (X, Y, Z). Intensities 4 and 5 do not differ from one another but both differ from intensity 6.

Some results were obtained if the control were also taken into consideration in this case. These results obtained with the ANVAR 2 and T TEST 2 programs are given in Tables 5.8 and 5.9. Again the analysis of variance finds the intensities to be significant. Due to an increase in error variance, the t test (with 23 degrees of freedom in the residual) indicates differences only between each of the lower three intensities and intensity 6. (Note: The effect of adding the controls

		Order							
		0	1	2	3	4	5	6	7
Subjects	1	166	53	-47	-75	-121	-119	83	91
	2	-142	-110	55	28	95	-7	11	-282
	3	146	-20	166	-76	70	161	-182	164
	4	-64	20	31	117	66	40	153	37
	5	-57	32	-19	-278	27	-143	-6	30
	6	-49	-90	84	8	-32	-36	-317	41

SOURCE	DF	SS	VE	VR
MODES	7	717.19	102.46	0.01
INTENSITIES	5	211136.00	42227.10	3.49
SUBJECTS	5	97310.20	19462.00	1.61
ORDER	7	41040.10	5862.88	0.49
RESIDUAL	23	278269.00	12008.60	
TOTAL	47	627037.00		

Mean Responses

Subjects	Modes	Intensities
= 3.88	-- 0.50	= 93.50
-- 44.00	-- 2.00	= 32.83
= 53.63	= 0.00	= 70.17
= 50.00	= 0.17	-- 31.17
-- 51.75	-- 0.33	-- 30.33
-- 48.88	= 0.33	-- 137.33*

Error Variance = 63.51

Table 5.8

Analysis of Variance of Chair Data Corrected for
Mode Differences-with control runs

T TEST

ERROR VARIANCE= 63.51 T(P=0.05)= 2.07

MØDES		INTENSITIES	
= 0.0	= 0.0	= 0.0	
= 1.0	=- 0.5	= 93.5	
= 2.0	=- 2.0	= 32.8	
= 3.0	= 0.0	= 70.2	
= 4.0	= 0.2	=- 31.2	
= 5.0	=- 0.3	=- 30.3	
= 6.0	= 0.3	=- 137.3	
= 7.0	= 6.7	= 0.0	

S= 1 S= 6 T= 3.64
 S= 2 S= 6 T= 2.68
 S= 3 S= 6 T= 3.27*

Table 5.9

"t" Test of Chair Data Corrected for
 Mode Differences-with control runs

could be predicted from the original considerations of the analysis of variance. One purpose of the control runs is to establish a subject norm and possible order effects over the course of an experiment. Thus their addition to the analysis of variance would be expected to decrease subject and order effects. At the same time, they add to the overall sum of squares which in turn increases the residual term. Thus all V.R. values are generally lower and the error variance for use in the "t" test becomes larger.)

The results with and without control both strongly suggest that the lower three intensities used in the experiments lie at or below the threshold for the galvanic reaction under the given experimental conditions. The average of the means of these three intensities is 66 degrees which is close to the value of 47 degrees obtained for the control runs. These two values and the value obtained for the overall mean of the modes above are all approximately the same, thus further substantiating the indication that an inherent bias was present in the experiment.

The various results above may be summarized as follows: Significant differences were found between anodic and cathodic mode effects, with anodic stimuli seemingly producing larger effects. If control runs are taken into account, the effects of the two mode types become nearly equal. Intensities below the 800 μ level,

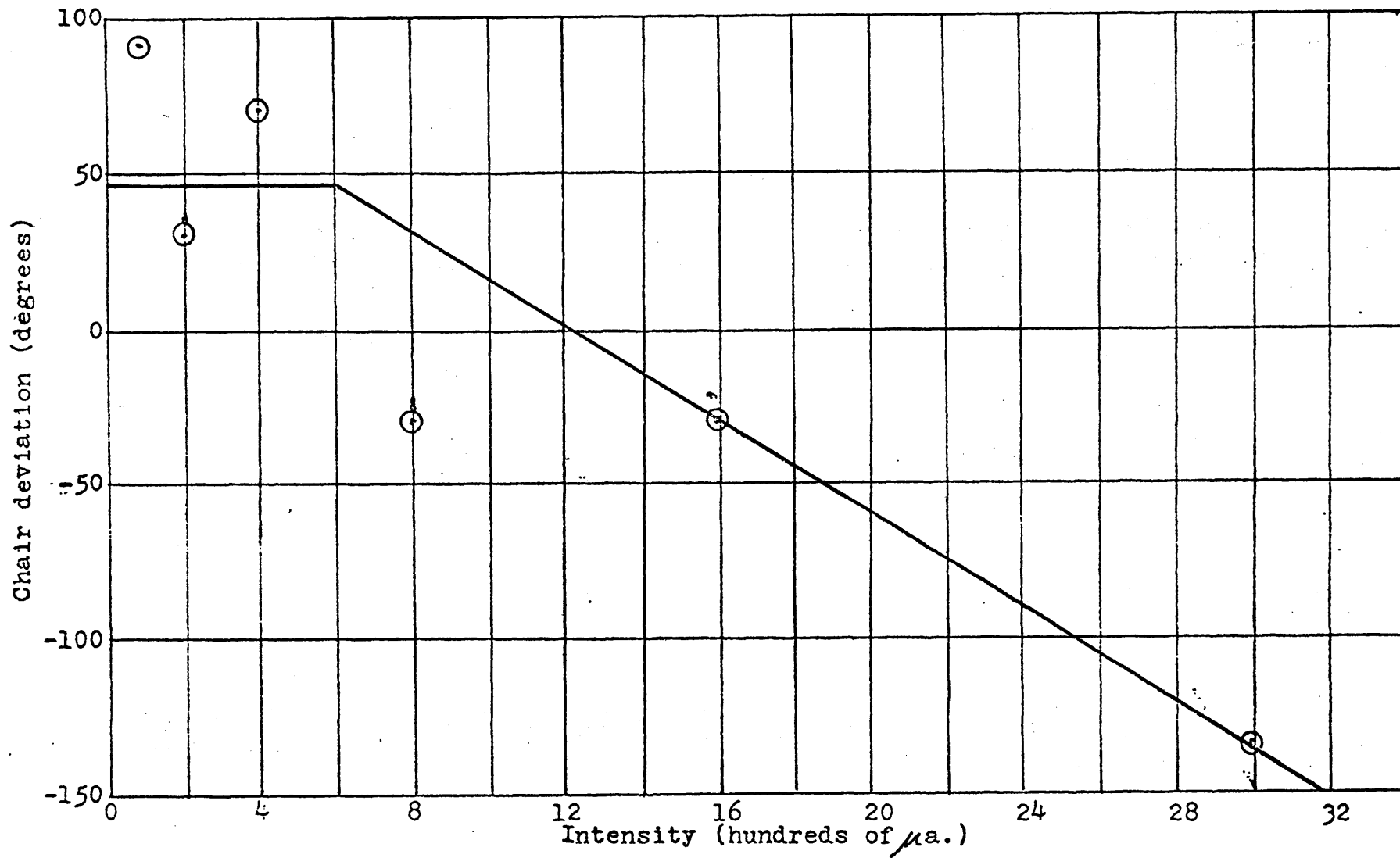


Figure 5.1

Chair deviation versus galvanic stimulus intensity

appear to have no effect on the results with responses being approximately the same as for the control runs. At intensity levels at and above 800 a significant effects were apparent. A threshold for current effect between 400 and 800 a was thus suggested. A plot of these results is shown in Figure 5.1.

The plot shows the apparent bias below the threshold of the current effect. The bias is chosen somewhat arbitrarily at 47 degrees, the mean of the control runs. The means of the three intensities below threshold are shown scattered about this value. The threshold is also set somewhat arbitrarily at $600\mu\text{a}$. A least mean squared linear plot is then made through this point and the three intensity means above threshold. The line was forced to pass through the $600\mu\text{a}$ point.

5.3 Analysis of Eye Position Data

The mean cumulative slow phase eye position data from the experiments is given in Table 5.2. This data was processed with the ANVAR program and the results are shown in Table 5.10. The F value required for significance is again 2.90. None of the variance ratios equals or surpasses the value though, as in the raw chair position data, the VR for modes is highest at 2.13. Corrections similar to those used to enhance the chair data were employed on the eye data but failed to improve the significance of any of the parameter groups. Thus no definite conclusions may be drawn concerning the influence

	Order					
Subjects	221	20	56	75	226	88
"	88	77	63	12	112	82
"	323	13	90	76	43	59
"	53	124	164	83	41	55
"	343	311	199	41	340	213
"	48	14	78	21	13	66

SOURCE	DF	SS	VE	VR
MODES	5	= 237156.00	= 47431.20	= 2.13
INTENSITIES	5	= 67200.20	= 13440.10	= 0.60
SUBJECTS	5	= 40046.60	= 8009.31	= 0.36
ORDER	5	= 44740.90	= 8948.17	= 0.40
RESIDUAL	15	= 334277.00	= 22285.20	
TOTAL	35	= 723421.00		

Mean Responses

SUBJECTS MODES INTENSITIES

1	=	20.3	A	=	42.5	U	=	2.3
2	=	24.0	B	=	89.0	V	=	72.0
3	=	81.0	C	=	139.3	W	=	81.3
4	=	45.3	D	=	44.3	X	=	33.5
5	=	61.5	E	=	112.3	Y	=	9.5
6	=	11.0	F	=	51.3	Z	=	70.8

ERROR VARIANCE= 86.19

Table 5.10

Analysis of Variance of Raw Eye Position Data

of the experimental conditions on eye movements.

One interesting observation can be made on the eye data however. The modes had the highest VR and a comparison of the means of each mode with the corresponding means in the chair data analysis certain similarities can be noted. All right cathodic modes have negative mean responses while all right anodic modes have positive mean responses. In addition, the anodic effects have larger magnitudes than the cathodic as in the chair data. This suggests that a similar net effect due to modes is being observed in both chair and eye movement data.

The peculiarities of the experimental scheme may well have masked the eye movement data. Only relatively low angular accelerations were present which would naturally decrease eye deviations due to rotation. Eye drift (other than that due to the galvanic stimulus) may have decreased the ability to measure the deviations due to the current. It is possible that a fixation point might aid this latter problem.

Despite the inability to find significance in the eye movement data, the results nevertheless appear to be in definite pattern. Additional experiments would, therefore, seem warranted to further uncover the effects of the current on eye movements.

5.4 Subject's Reported Sensations

The subjects reported several sensations during the experiments. These included disorientation, head tilt, and one report of the sensation of "spinning in two directions simultaneously." Several subjects also reported an after effect following stimulation at 3 ma. This manifested itself in a spinning sensation but died out before the beginning of the next run.

Subjects complained somewhat about the electrode head band which became painful when worn for a long period.

5.5 Comments on One Abnormal Subject

One abnormal subject was also run on the experiment under protocol #1. The subject was an eighteen year old female with Von Recklinhausens' disease (neurofibromatosis) who had had bilateral acoustic neuromas removed surgically. She reported no sensation of rotation during any of the experimental runs. The chair position followed the random signal almost exactly. Her only indication of current effect came at the 3 ma. level at which she repeatedly was unable to tolerate the skin effects of the stimulus and terminated the run by pressing the panic button.

Eye movements displayed large right beating nystagmus at the onset of the experiment. Nystagmus remained right beating on all runs but decreased markedly in amplitude. The large deviations at the beginning were attributed to

subject apprehension which apparently subsided as the experiment period wore on.

The results for this subject then indicated that galvanic stimulation does not produce sensation of rotation or disorientation when both vestibular nerves have been sectioned.

CHAPTER 6

CONCLUSIONS AND RECOMMENDATIONS

The object of this thesis was to determine the gross influence of galvanic vestibular stimulation on the perception of rotation and on eye movements. The intent was to determine which parameters might effect these phenomena and to lay the groundwork for future study in this area, particularly in clinical application. In order to accomplish this, the effects of stimulation modes and intensities on subject threshold for motion sensation and eye movements were examined.

Modes (the various electrode combinations) were found to be significant only with reversed polarities. Whereas quantitative differences in effect between anodic and cathodic stimulation had been reported in the literature no such differences were found in the present experiments when correcting for reversal of polarity and the control bias. After these corrections, anodic and cathodic stimulation produced effects of opposite sign but of the same magnitude.

Similarly, differences in magnitude of effect had been reported between unipolar and bipolar stimulation. No such differences were found in the present work.

The threshold for intensity effect in the experiments was found to lie at approximately $600\mu\text{a}$. Runs with current below this level gave results no different than those of the control runs. Above $600\mu\text{a}$, the current acts in an apparent linear manner to bias the threshold of rotation perception.

With a five minute rest period between runs, no order effects were observed.

Analysis of eye movements suggested results similar to those of the voluntary responses but not at statistically significant levels.

One abnormal subject with peripheral vestibular nerves destroyed was run on the experimental set-up. No reaction could be obtained with or without galvanic stimulus. Thus, for this subject, absence of the peripheral nerve implies absence of the galvanic reaction. Thus the action site of the stimulus appears to be distal to the brain stem though the exact point remains to be established.

The experimental results are in apparent agreement with the findings of Mirchandani that all persons, even so called vestibularly "normal" subjects, exhibit a slight directional preponderance over a period of time. In the present case this was manifested in a consistent chair drift away from a zero reference position during control runs and during runs with current but below threshold for current effect. The drift in each case was to the right, the same as in Mirchandani's experiments.

The results of this research indicate possible extensions of the subjective perception model of the semicircular canals, discussed in Chapter 2. The proposed additions to the model are shown in figure 6.1. These include a threshold, a gain, K_G , and an as yet unknown dynamic transfer function $K(s)$ to reflect possible transient or response decline phenomena.

The galvanic stimulus has an apparent additive effect on perception of rotation. The best estimate of the action site at present indicates that it is probably central to the hair cells in the macula of the semicircular canals. The proposed addition to the model reflects these considerations by making the galvanic stimulus response terms additive with the output of the existing perception model but before the central nervous system. The evaluation of $K(s)$ and exact determination of the threshold and K_G will be required in future work.

A number of topics related to galvanic vestibular stimulation deserve future attention.

The threshold and gain for intensity effects should be established more accurately by more extensive testing of several subjects under fewer conditions. One means of accomplishing this is an alternative form of the experiment above with the subject in a passive role.

Various transient analyses might also be useful. In particular, step inputs in rotating chair velocity in the presence of galvanic stimulation might yield

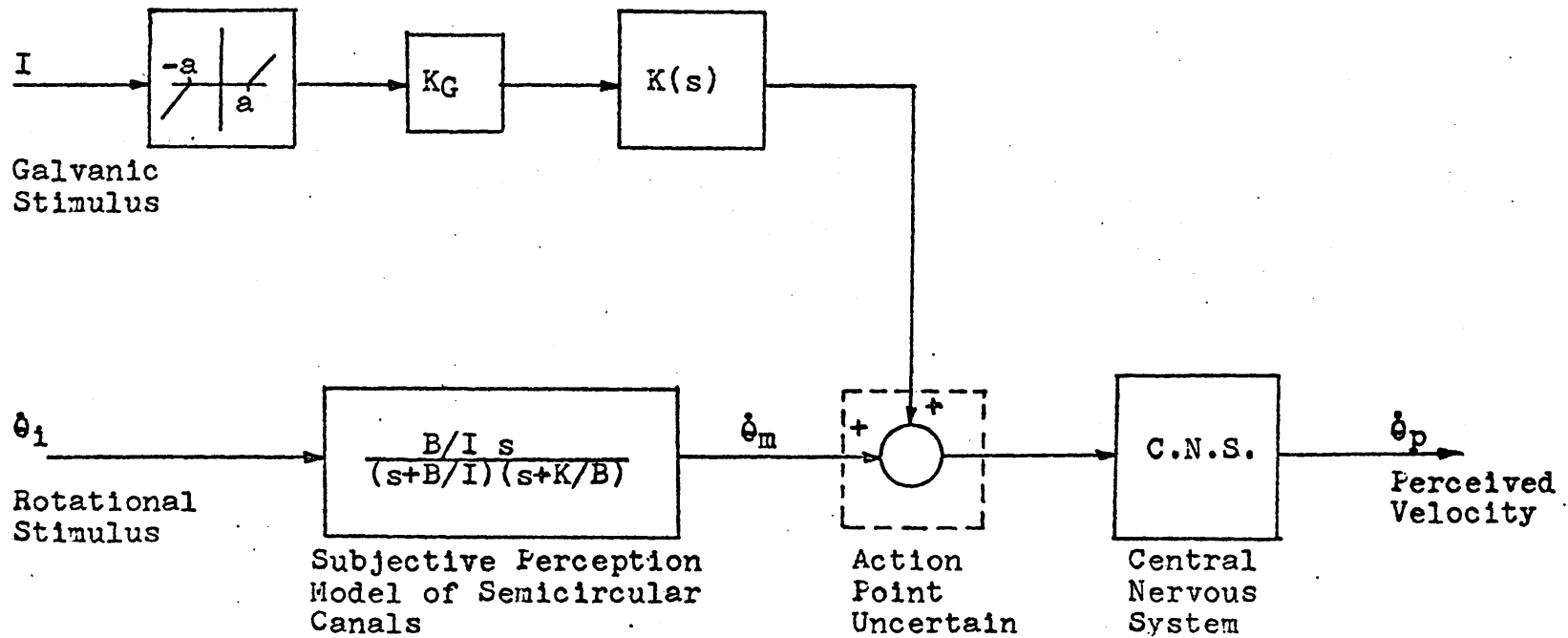


Figure 6.1

Proposed extension of subjective perception model to include galvanic stimulus

information on response latency times. Chronaxia study might also be further considered. As pointed out in Chapter 3, results have not been consistent between researchers for vestibular nerve chronaxia. If a repeatable method of performing this test were available it might become useful clinically.

The effects of galvanic stimulation on posture as discussed in Chapter 3 might also be a particularly fruitful area for future consideration.

An important consideration for future work is the eye movement response to galvanic stimulation. The experiments performed here indicated that eye movements might provide useful quantitative measures of rotation sensation if signal to noise ratios were improved. A possible means of improving this ratio would be to provide a fixation point, either visual or proprioceptive (such as asking the subject to "look" at his outstretched thumb).

Eye movements, if shown to be a consistent good indication of the galvanic vestibular reaction would be much more practical to use in a clinical test as compared with the rotational tests employed here.

APPENDIX A

COMPUTATION EQUIPMENT USED IN DATA ANALYSIS

All data analysis for this thesis was performed on the MIT Man Vehicle Laboratory hybrid computer facility. This equipment consists of a Digital Equipment Corporation PDP-8 digital computer interfaced to a GPS model 290 T analog computer. The PDP-8 has a 12 bit, fixed word length, $1\frac{1}{2}$ second cycle time, and $4,096_{10}$ memory locations. Programs are written and stored using a modified version of the DEC tape programming system supplied by the manufacturer.

The analog machine uses a 10 volt reference. There are 7 A/D and 8 D/A channels each with a range of ± 10 volts. Sampling rate is determined by a real time clock actuating a program interrupt line at the analog machine.

APPENDIX B

MITNYS, A HYBRID PROGRAM TO DETERMINE
CUMULATIVE SLOW PHASE OF NYSTAGMUS

The eye movement data obtained during the experiments described in this thesis was processed using the hybrid program, MITNYS, the digital portion of which is written in PAL, the assembly language for the PDP-8 computer.

MITNYS receives the raw analog eye movement data, removes saccades and blinks which may be present, and pieces the slow phase eye movements together to form a cumulative slow phase output. This output may be thought of as the total amplitude of slow phase eye movements during the experiment.

In addition, the program differentiates this output to obtain slow phase velocity, however, this was not required in the present research.

A simplified block diagram for MITNYS is given in figure B.1, and an annotated listing follows. The required analog connections are shown in figure B.2. A complete discussion of the algorithm is somewhat involved and is omitted here. It has been reported elsewhere for those who may be interested.

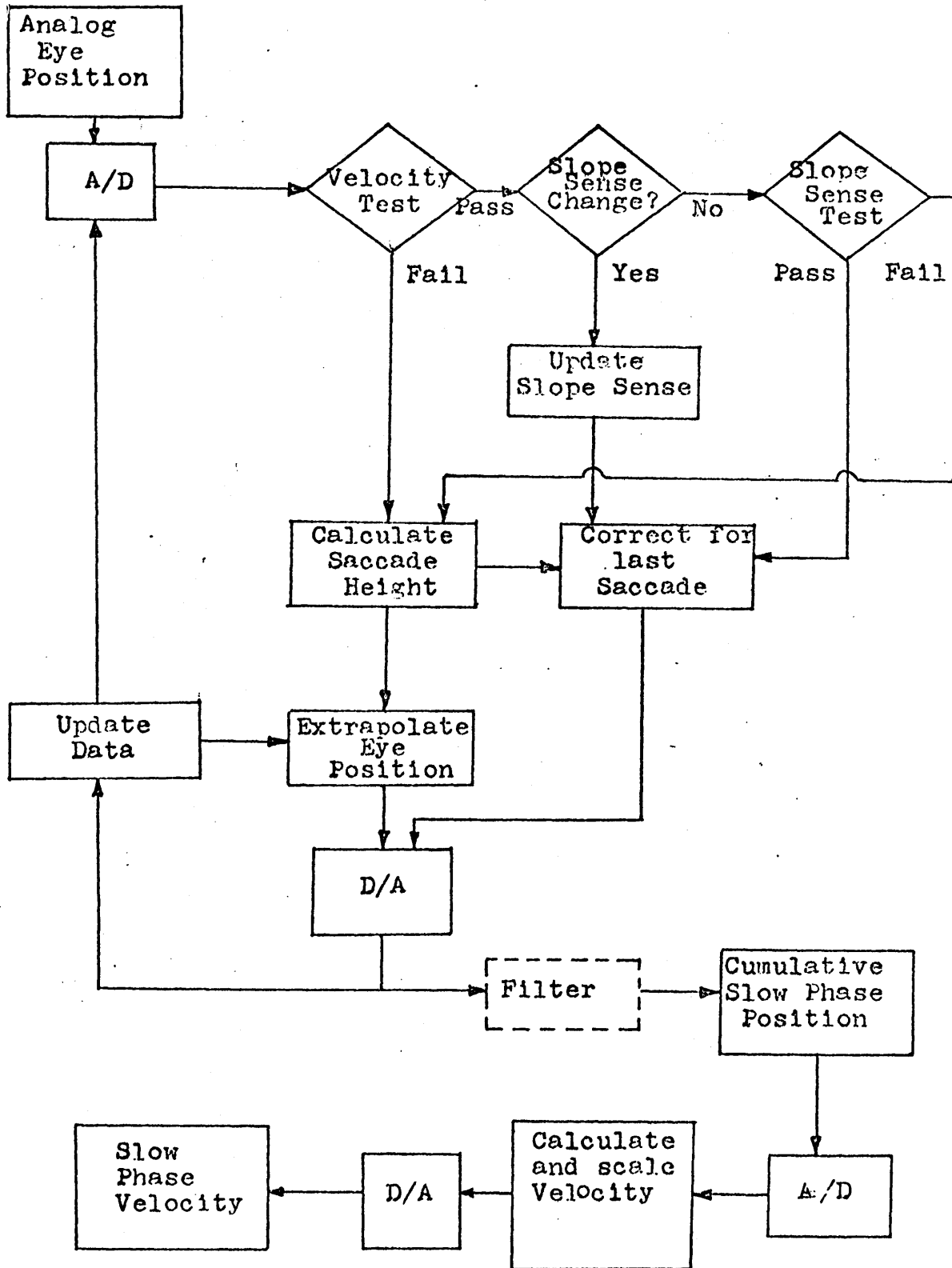


Figure B.1

Simplified block diagram for the hybrid program MITNYS

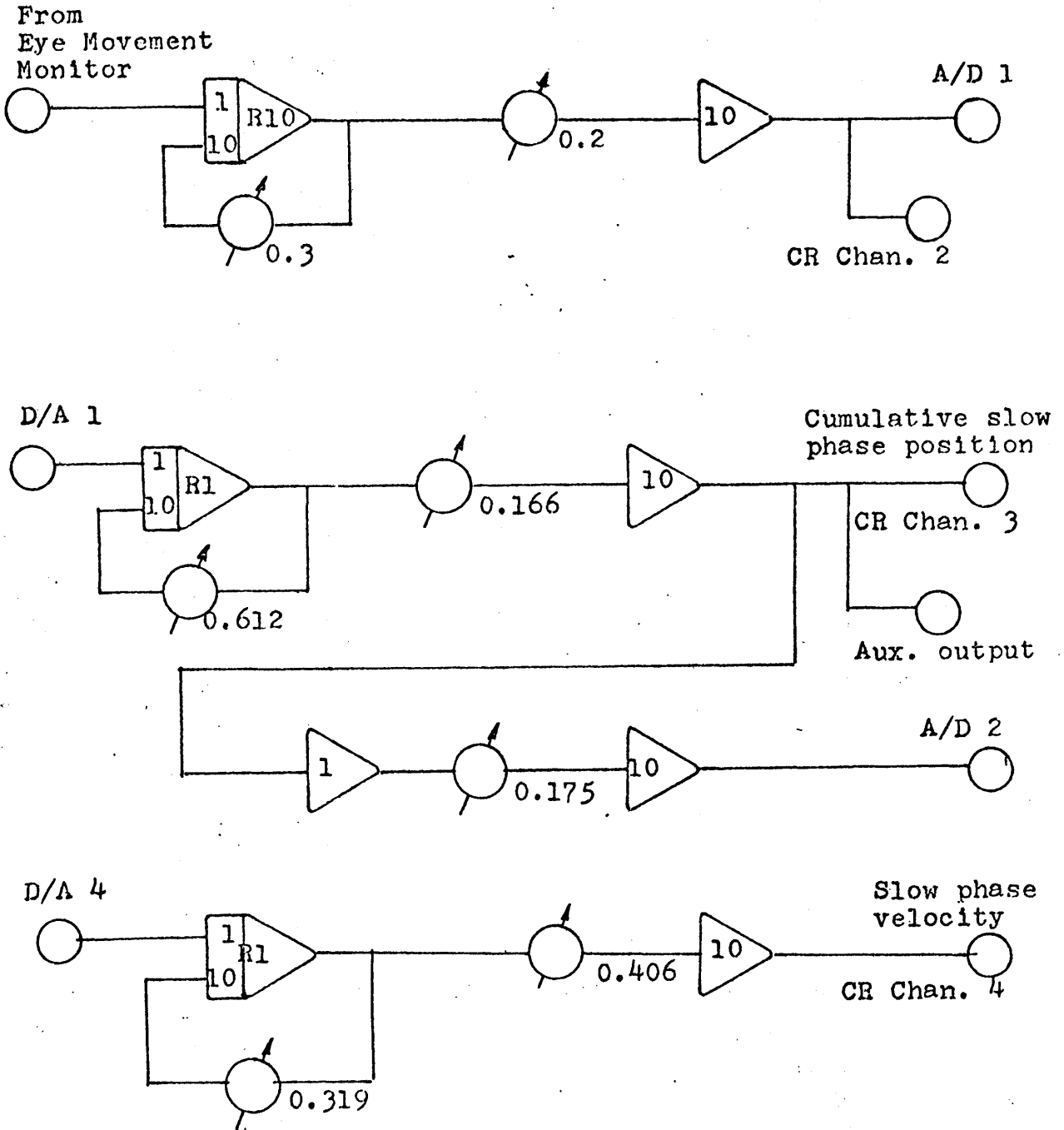


Figure B.2

Analog Connections for the hybrid program, MITNYS

*200 /MITNYS-DOUBLE PRECISION
 /ON-LINE NYSTAGMUS PROCESSOR

 /MAN-VEHICLE LAB, MIT, FEBRUARY, 1970

 /INPUT CALIBRATION: 1V = 15DEG
 /SAMP RATE = 32 PER SEC

```

0200  7200      START,CLA /INITIALIZE CONSTANTS
0201  3040      DCA SAMP0
0202  3032      DCA APP0A
0203  3033      DCA APP0B
0204  3044      DCA TEMP1
0205  3047      DCA SLOPE
0206  3052      DCA SS
0207  1021      TAD B
0210  3055      DCA CNTR1
0211  1022      TAD C
0212  3056      DCA CNTR2

0213  7604      TOP,LAS /PAUSE IF AC0=1
0214  7510      SPA
0215  5200      JMP START
0216  7604      LAS
0217  3020      DCA A/ SET VELOCITY CRITERIA;
0220  6454      CLAF                    /0020 = 50 DEG PER SEC
0221  6461      SNAF
0222  7610      SKP CLA
0223  5221      JMP .-2
0224  6422      DACG
0225  6545      ADCC ADIC/SAMPLE AMPLITUDE
0226  6532      ADCV
0227  6531      ADSF
0230  5227      JMP .-1
0231  6534      ADRB
0232  3037      DCA SAMP1
0233  6544      SPV,ADIC /SAMPLE CUMULATIVE POSITION
0234  6532      ADCV
0235  6531      ADSF
0236  5235      JMP .-1
0237  6534      ADRB
0240  3063      DCA POS1
0241  2060      ISZ CNTR4
0242  5273      JMP DIF
0243  1025      TAD F
0244  3060      DCA CNTR4
0245  1064      TAD POS0 /DETERMINE SLOW PHASE VELOCITY
0246  7041      CIA
0247  1063      TAD POS1
0250  3065      DCA VEL
0251  1065      TAD VEL
0252  7104      CLL RAL

```

0253	7204	CLA RAL
0254	3061	DCA SD1
0255	1065	TAD VEL
0256	7510	SGEZ
0257	7041	CIA
0260	7106	CLL RTL
0261	3062	DCA V1
0262	1061	TAD SD1
0263	7110	CLL RAR
0264	7620	SNL CLA
0265	5473	JMP I PVL
0266	1062	TAD V1
0267	7041	CIA
0270	3062	DCA V1
0271	1063	VL,TAD POS1
0272	3064	DCA POS0
0273	1040	DIF,TAD SAMP0 /CALCULATE AMPLITUDE DIFFERENCE
0274	7041	CIA
0275	1037	TAD SAMP1
0276	3043	DCA DIF1
0277	1043	TAD DIF1
0300	7104	CLL RAL
0301	7204	CLA RAL
0302	3050	DCA SIGN
0303	1043	CHK,TAD DIF1 /VELOCITY CRITERIA
0304	7540	SLEZ
0305	7041	CIA
0306	1020	TAD A
0307	7710	SGEZ CLA
0310	5476	JMP I PEPK
0311	1053	TAD WAIT
0312	7640	SZA CLA
0313	5507	JMP I PST
0314	2057	ISZ CNTR3
0315	5477	JMP I PLOK
0316	2053	ISZ WAIT
0317	1052	ST,TAD SS
0320	7640	SZA CLA
0321	5500	JMP I PSET
0322	1043	TAD DIF1 /TEST FOR EXTREMUM
0323	7540	SLEZ
0324	7041	CIA
0325	1026	TAD Q
0326	7710	SGEZ CLA
0327	5466	JMP I POK
0330	2052	ISZ SS
0331	5466	JMP I POK
0332	1054	SET,TAD KEY
0333	7640	SZA CLA
0334	5503	JMP I PSN
0335	1032	TAD APP0A
0336	3051	DCA SEMP
0337	2054	ISZ KEY
0340	2055	SN,ISZ CNTR1

0341	5466	JMP I POK
0342	1051	TAD SEMP /UPDATE SLOPE SENSE
0343	7041	CIA
0344	1032	TAD APP0A
0345	7104	CLL RAL
0346	7204	CLA RAL
0347	3047	DCA SLOPE
0350	3053	DCA WAIT
0351	3052	DCA SS
0352	3054	DCA KEY
0353	1024	TAD E
0354	3057	DCA CNTR3
0355	1021	TAD B
0356	3055	DCA CNTR1
0357	5466	JMP I POK
0360	1024	EPK, TAD E
0361	3057	DCA CNTR3
0362	5475	JMP I PEPL
0363	1054	LOK, TAD KEY /SLOPE SENSE CRITERIA
0364	7640	SZA CLA
0365	5466	JMP I POK
0366	1047	TAD SLOPE
0367	1050	TAD SIGN
0370	7110	CLL RAR
0371	7620	SNL CLA
0372	5466	JMP I POK
0373	1041	EPL, TAD DEL1 /EXTRAPOLATE POSITION
0374	1042	TAD DEL2
0375	4110	JMS RUN
0376	4144	JMS APP
0377	2106	ISZ DF
0400	5502	JMP I PFT
0401	1106	OK, TAD DF /BOTH TESTS PASSED; SCALE SAMPLE
0402	7650	SNA CLA
0403	5501	JMP I PGO
0404	1041	TAD DEL1
0405	1042	TAD DEL2
0406	4110	JMS RUN
0407	4144	JMS APP
0410	1037	TAD SAMP1
0411	4110	JMS RUN
0412	1034	TAD EXTRA
0413	7040	CMA
0414	3034	DCA EXTRA
0415	1035	TAD EXTRB
0416	7141	CLL CIA
0417	3035	DCA EXTRB
0420	7004	RAL
0421	1034	TAD EXTRA
0422	3034	DCA EXTRA
0423	1035	TAD EXTRB
0424	1031	TAD APP1B
0425	3046	DCA JUMPB
0426	7004	RAL

0427	1034	TAD EXTRA
0430	1030	TAD APP1A
0431	3045	DCA JUMPA
0432	3106	DCA DF
0433	5502	JMP I PFT
0434	1037	GO, TAD SAMPI
0435	4110	JMS RUN
0436	1035	TAD EXTRB
0437	1046	TAD JUMPB
0440	3031	DCA APP1B
0441	7004	RAL
0442	1034	TAD EXTRA
0443	1045	TAD JUMPA
0444	3030	DCA APP1A
0445	1032	FT, TAD APP0A
0446	7040	CMA
0447	1030	TAD APP1A
0450	3034	DCA EXTRA
0451	3036	DCA LINK
0452	7100	CLL
0453	1033	TAD APP0B
0454	7041	CIA
0455	7430	SZL
0456	2036	ISZ LINK
0457	7100	CLL
0460	1031	TAD APP1B
0461	7421	MQL
0462	7004	RAL
0463	1036	TAD LINK
0464	1034	TAD EXTRA
0465	7413	SHL
0466	0001	0001
0467	3041	DCA DEL1
0470	1030	TAD APP1A
0471	3032	DCA APP0A
0472	1031	TAD APP1B
0473	3033	DCA APP0B
0474	1041	FIX, TAD DEL1 /LIM ERR IN 1ST DIF
0475	7540	SLEZ
0476	7041	CIA
0477	1020	TAD A
0500	7710	SGEZ CLA
0501	7610	SKP CLA
0502	5467	JMP I PUP
0503	1047	TAD SLOPE
0504	7650	SNA CLA
0505	5470	JMP I PCS
0506	1020	TAD A
0507	3041	CIA
0510	3041	DCA DEL1
0511	5467	JMP I PUP
0512	1020	CS, TAD A
0513	3041	DCA DEL1
0514	1044	UP, TAD TEMP1 /UPDATE DIFFERENCE TABLE

0515	7041	CIA
0516	1041	TAD DEL1
0517	3042	DCA DEL2
0520	1041	TAD DEL1
0521	3044	DCA TEMP1
0522	2056	IN, ISZ CNTR2 /CONVERT DATA
0523	5474	JMP I POUT
0524	1022	TAD C
0525	3056	DCA CNTR2
0526	1032	TAD APP0A
0527	7540	SLEZ
0530	7041	CIA
0531	1023	TAD D
0532	7740	SLEZ CLA
0533	5472	JMP I PRS
0534	3045	DCA JUMPA /RESET CUM POS IF OVERFLOW
0535	3046	DCA JUMPB
0536	3032	DCA APP0A
0537	3033	DCA APP0B
0540	1032	RS, TAD APP0A
0541	6552	DAL1
0542	7200	CLA
0543	1043	TAD DIF1
0544	6554	DAL2
0545	7200	CLA
0546	1055	TAD CNTR1
0547	6562	DAL3
0550	7200	CLA
0551	1062	TAD V1
0552	6564	DAL4
0553	7200	CLA
0554	1047	TAD SLOPE
0555	6572	DAL5
0556	7200	CLA
0557	1037	OUT, TAD SAMP1
0560	3040	DCA SAMP0
0561	6435	LASL /CHK SENSE LINE 12 FOR MANUAL
0562	7110	CLL RAR /SLOPE CORRECTION
0563	7620	SNL CLA
0564	5427	JMP I PKO
0565	1047	TAD SLOPE
0566	7001	IAC
0567	7110	CLL RAR
0570	7204	CLA RAL
0571	3047	DCA SLOPE
0572	5505	KO, JMP I PTOP

*20

0020	0000	A,0
0021	7774	B,7774
0022	7774	C,7774
0023	3750	D,3750

0024	7770	E,7770
0025	7776	F,7776
0026	0001	Q,0001
0027	0572	PKO,KO
0030	0000	APP1A,0
0031	0000	APP1B,0
0032	0000	APP0A,0
0033	0000	APP0B,0
0034	0000	EXTRA,0
0035	0000	EXTRB,0
0036	0000	LINK,0
0037	0000	SAMP1,0
0040	0000	SAMP0,0
0041	0000	DEL1,0
0042	0000	DEL2,0
0043	0000	DIF1,0
0044	0000	TEMP1,0
0045	0000	JUMPA,0
0046	0000	JUMPB,0
0047	0000	SLOPE,0
0050	0000	SIGN,0
0051	0000	SEMP,0
0052	0000	SS,0
0053	0000	WAIT,0
0054	0000	KEY,0
0055	0000	CNTR1,0
0056	0000	CNTR2,0
0057	0000	CNTR3,0
0060	0000	CNTR4,0
0061	0000	SD1,0
0062	0000	V1,0
0063	0000	POS1,0
0064	0000	POS0,0
0065	0000	VEL,0
0066	0401	PQK,OK
0067	0514	PUP,UP
0070	0512	PCS,CS
0071	0522	PIN,IN
0072	0540	PRS,RS
0073	0271	PVL,VL
0074	0557	POUT,OUT
0075	0373	PEPL,EPL
0076	0360	PEPK,EPK
0077	0363	PLOK,LOK
0100	0332	PSET,SET
0101	0434	PGO,GO
0102	0445	PFT,FT
0103	0340	PSN,SN
0104	0000	EX1,0
0105	0213	PTOP, TOP
0106	0000	DF,0
0107	0317	PST,ST
0110	0000	RUN,0 /SCALING SUBROUTINE
0111	3104	DCA EX1

0112	1104	TAD EX1
0113	7500	SLZ
0114	5120	JMP MS
0115	7041	CIA
0116	3104	DCA EX1
0117	2036	ISZ LINK
0120	7200	MS,CLA
0121	1104	TAD EX1
0122	7415	ASR
0123	0001	0001
0124	3034	DCA EXTRA
0125	7501	MQA
0126	3035	DCA EXTRB
0127	1036	TAD LINK
0130	7450	SNA
0131	5143	JMP OT
0132	1034	TAD EXTRA
0133	7040	CMA
0134	3034	DCA EXTRA
0135	1034	TAD EXTRA
0136	7141	CLL CIA
0137	3035	DCA EXTRB
0140	7004	RAL
0141	1034	TAD EXTRA
0142	3034	DCA EXTRA
0143	5510	OT,JMP I RUN
0144	0000	APP,0 /EXTRAPOLATION SUBROUTINE
0145	1035	TAD EXTRB
0146	1033	TAD APP0B
0147	3031	DCA APP1B
0150	7004	RAL
0151	1034	TAD EXTRA
0152	1032	TAD APP0A
0153	3030	DCA APP1A
0154	3036	DCA LINK
0155	5544	JMP I APP
A	0020	
APP	0144	
APP0A	0032	
APP0B	0033	
APP1A	0030	
APP1B	0031	
B	0021	
C	0022	
CHK	0303	
CNTR1	0055	
CNTR2	0056	
CNTR3	0057	
CNTR4	0060	
CS	0512	
D	0023	
DEL1	0041	
DEL2	0042	
DF	0106	

DIF	0273	SS	0052
DIF1	0043	ST	0317
E	0024	START	0200
EPK	0360	TEMP1	0044
EPL	0373	TOP	0213
EXTRA	0034	UP	0514
EXTRB	0035	VEL	0065
EX1	0104	VL	0271
F	0025	V1	0062
FIX	0474	WAIT	0053
FT	0445		
GO	0434		
IN	0522		
JUMPA	0045		
JUMPB	0046		
KEY	0054		
KO	0572		
LINK	0036		
LOK	0363		
MS	0120		
OK	0401		
OT	0143		
OUT	0557		
PCS	0070		
PEPK	0076		
PEPL	0075		
PFT	0102		
PGO	0101		
PIN	0071		
PKO	0027		
PLOK	0077		
POK	0066		
POS0	0064		
POS1	0063		
POUT	0074		
PRS	0072		
PSET	0100		
PSN	0103		
PST	0107		
PTOP	0105		
PUP	0067		
PVL	0073		
Q	0026		
RS	0540		
RUN	0110		
SAMP0	0040		
SAMP1	0037		
SD1	0061		
SEMP	0051		
SET	0332		
SIGN	0050		
SLOPE	0047		
SN	0340		
SPV	0233		

APPENDIX C

MAN, A HYBRID PROGRAM TO CALCULATE
STATISTICS OF EXPERIMENTAL DATA

This program was used to determine the statistics of the slow phase eye position as determined by the hybrid program MITNYS (see appendix B) and of chair position for each experimental run. The digital portion of MAN is written in PAL, the PDP-8 assembly language. Analog chair or eye position is scaled with the analog machine such that 1 volt = 72 degrees. For each run, 128 seconds of data is sampled once per second, the first sample corresponding to the instant just after all stimuli have been applied. These samples are stored in memory. At the completion of sampling, the digital machine calculates the mean, variance, and standard deviation of the sampled data according to the following algorithms where θ indicated angular position and T = sampling period.

$$\text{Mean: } \bar{\theta} = \frac{1}{N} \sum_{n=1}^N \theta(nT) \quad (\text{C.1})$$

$$\text{Variance: } \sigma_{\theta}^2 = \frac{1}{N} \sum_{n=1}^N \theta^2(nT) - (\bar{\theta})^2 \quad (\text{C.2})$$

$$\text{Standard Deviation: } \sigma_{\theta} = \sqrt{\frac{1}{N} \sum_{n=1}^N \theta^2(nT) - (\bar{\theta})^2} \quad (\text{C.3})$$

The results of the calculations are outputted in two ways. The mean and standard deviation are converted to analog signals for possible display. All three of the statistics are also outputted on the teletype in digital form.

The format for this latter output is shown below:

```
GALVANIC STIMULATION DATA
SUBJECT #X      RUN #X
CHAIR(EYE) POSITION MEAN = XXXX.X DEGREES
VARIANCE = XXXXXX.XX DEGREES SQUARED
STANDARD DEVIATION = XXXX.X DEGREES
```

The subject number, run number and specification of eye or chair data are determined manually on the switch register prior to each set of calculations.

The square root routine necessary for determination of the standard deviation and the scaled decimal output routine are calculated by the utility subroutine SUBTAB, written by N.A.J. Van Houtte. A listing of SUBTAB may be found in his thesis.

An annotated listing of MAN follows.

*200

/MEAN AND VARIANCE PROGRAM
 /MIT MAN-VEHICLE LAB, DECEMBER 1969

/THIS PROGRAM TO BE OPERATED IN
 /CONJUNCTION WITH THE UTILITY
 /PROGRAM "SUBTAB"

/SAMP RATE = 1 PER SEC
 /CHAIR CALIBRATION: 1V=72 DEG
 /EYE CALIBRATION: 1V=72 DEG

0200	7604	LAS /SET NUMBER OF SAMPLES
0201	7041	CIA
0202	3043	DCA A
0203	7402	HLT
0204	7604	STR,LAS
0205	7104	CLL RAL
0206	7100	CLL
0207	7415	ASR
0210	0003	0003
0211	3020	DCA H /STORE SUBJECT NO. FROM SR6-SR8
0212	7421	MLQ
0213	7604	LAS
0214	7415	ASR
0215	0002	0002
0216	7200	CLA
0217	7413	SHL
0220	0002	0002
0221	3021	DCA J /STORE RUN NO. FROM SR9-SR11
0222	7604	LAS
0223	7104	CLL RAL
0224	7104	CLL RAL
0225	7204	CLA RAL
0226	3022	DCA KEY /STORE DATA INDEX FROM AC1; 0=CHAIR; 1=EYE
0227	1045	TAD PLIST /INITIALIZE SAMPLE LIST
0230	3010	DCA 10
0231	1043	TAD A
0232	3023	DCA CNTRI
0233	7604	TOP,LAS /RESTART IF AC0=1
0234	7710	SPA CLA
0235	5204	JMP STR
0236	6552	DAL1 /CLEAR DIGITAL TO ANALOG CHANNELS
0237	6554	DAL2
0240	6551	DACX
0241	6454	CLAF /READ IN DATA
0242	6461	SNAF
0243	7610	SKP CLA
0244	5242	JMP .-2
0245	6545	ADCC ADIC
0246	6532	ADCV

0247	6531	ADSF
0250	5247	JMP .-1
0251	6534	ADRB
0252	3410	DCA I 10
0253	2023	ISZ CNTRI
0254	5446	JMP I PTOP
0255	7402	HLT
0256	1043	MN, TAD A
0257	3023	DCA CNTRI
0260	1045	TAD PLIST
0261	3010	DCA 10
0262	3025	DCA HIGH
0263	3024	DCA LOW
0264	3026	DCA UP
0265	3027	DCA MID
0266	3030	DCA DOWN
0267	7604	MAV, LAS /RECALCULATE MEAN IF AC0=1
0270	7710	SPA CLA
0271	5256	JMP MN
0272	1410	TAD I 10 /CALCULATE SUM OF SAMPLES
0273	3031	DCA SAMP
0274	1031	TAD SAMP
0275	7710	SPA CLA
0276	7040	CMA
0277	1025	TAD HIGH
0300	3025	DCA HIGH
0301	7100	CLL
0302	1031	TAD SAMP
0303	1024	TAD LOW
0304	3024	DCA LOW
0305	7430	SZL
0306	2025	ISZ HIGH
0307	7000	NOP
0310	1031	TAD SAMP /SQUARE CURRENT SAMPLE
0311	4076	JMS SQ
0312	3035	DCA SSHI
0313	7501	MQA
0314	3036	DCA SSLO
0315	1030	TAD DOWN /CALCULATE SUM OF SQUARED TERMS
0316	1036	TAD SSLO
0317	3030	DCA DOWN
0320	7004	RAL
0321	1035	TAD SSHI
0322	1027	TAD MID
0323	3027	DCA MID
0324	7004	RAL
0325	1026	TAD UP
0326	3026	DCA UP
0327	2023	ISZ CNTRI
0330	5447	JMP I PMAV
0331	1024	TAD LOW /CALCULATE MEAN
0332	7421	MQL

0333	1025	TAD HIGH
0334	7415	ASR
0335	0006	0006
0336	7701	CLA MQA
0337	3034	DCA MEAN
0340	1030	TAD DOWN /CALCULATE MEAN SQUARE
0341	7421	MQL
0342	1027	TAD MID
0343	7415	ASR
0344	0006	0006
0345	7701	CLA MQA
0346	3033	DCA MSLO
0347	1027	TAD MID
0350	7421	MQL
0351	1026	TAD UP
0352	7415	ASR
0353	0006	0006
0354	7701	CLA MQA
0355	3032	DCA MSHI
0356	1034	TAD MEAN /SQUARE MEAN
0357	4076	JMS SQ
0360	3037	DCA SQMNH
0361	7501	MQA
0362	3040	DCA SQMNL
0363	1037	TAD SQMNH /CALCULATE VARIANCE
0364	7040	CMA
0365	3037	DCA SQMNH
0366	1040	TAD SQMNL
0367	7141	CLL CIA
0370	3040	DCA SQMNL
0371	7004	RAL
0372	1037	TAD SQMNH
0373	3037	DCA SQMNH
0374	1040	TAD SQMNL
0375	1033	TAD MSLO
0376	3042	DCA VARB
0377	7004	RAL
0400	1037	TAD SQMNH
0401	1032	TAD MSHI
0402	3041	DCA VARA
0403	1041	TAD VARA /CALCULATE STANDARD DEVIATION
0404	7510	SGEZ
0405	5211	JMP .+4
0406	7421	MQL
0407	1042	TAD VARB
0410	4471	JMS I PSQRT
0411	3044	DCA SIGMA
0412	1034	TAD MEAN /CONVERT RESULTS FOR ANALOG DISPLAY
0413	6552	DAL1
0414	7200	CLA
0415	1044	TAD SIGMA
0416	6554	DAL2
0417	7200	CLA
0420	6551	DACX

0421	1051	TAD POUT1
0422	4124	JMS PRINT /TYPE "GALVANIC STIMULATION DATA"
0423	1052	TAD POUT2
0424	4124	JMS PRINT
0425	1020	TAD H
0426	1065	TAD C60
0427	4106	JMS TYPE /TYPE "SUBJECT # 00"
0430	1053	TAD POUT3
0431	4124	JMS PRINT
0432	1021	TAD J
0433	1065	TAD C60
0434	4106	JMS TYPE /TYPE "RUN # 0"
0435	1022	TAD KEY
0436	7640	SZA CLA
0437	5463	JMP I PEYE
0440	1054	CHR, TAD POUT4A
0441	4124	JMS PRINT
0442	5464	JMP I PDEG
0443	1055	EYE, TAD POUT4B
0444	4124	JMS PRINT
0445	1056	DEG, TAD POUT4
0446	4124	JMS PRINT
0447	1066	TAD SPEC1
0450	3470	DCA I PSPEC
0451	1074	TAD FACI1
0452	4473	JMS I PFACI
0453	7421	MQL
0454	1034	TAD MEAN
0455	4472	JMS I PPRNTQ
0456	1057	TAD POUT5
0457	4124	JMS PRINT /TYPE "EYE (CHAIR) POSITION MEAN /= XX DEGREES
0460	1060	TAD POUT6
0461	4124	JMS PRINT
0462	1067	TAD SPEC2
0463	3470	DCA I PSPEC
0464	1075	TAD FACI2
0465	4473	JMS I PFACI
0466	1042	TAD VARB
0467	7421	MQL
0470	1041	TAD VARA
0471	4472	JMS I PPRNTQ
0472	1057	TAD POUT5
0473	4124	JMS PRINT
0474	1061	TAD POUT7
0475	4124	JMS PRINT /TYPE "VARIANCE = XX DEGREES SQUARED"
0476	1062	TAD POUT8
0477	4124	JMS PRINT
0500	1066	TAD SPEC1
0501	3470	DCA I PSPEC
0502	1074	TAD FACI1
0503	4473	JMS I PFACI
0504	7421	MQL
0505	1044	TAD SIGMA

0506	4472	JMS I PPRNTQ
0507	1057	TAD POUT5 /TYPE "STANDARD DEVIATION = XX DEGREES"
0510	4124	JMS PRINT
0511	7402	HLT
0512	5450	JMP I PSTR
0513	3636	OUT1,3636 /CRLF,CRLF
0514	3607	3607 /CRLF,G
0515	0114	0114 /AL
0516	2601	2601 /VA
0517	1611	1611 /NI
0520	0340	0340 /C
0521	2324	2324 /ST
0522	1115	1115 /IM
0523	2514	2514 /UL
0524	0124	0124 /AT
0525	1117	1117 /IO
0526	1640	1640 /N
0527	0401	0401 /DA
0530	2401	2401 /TA
0531	0000	0000 /00
0532	3623	OUT2,3623 /CRLF,S
0533	2502	2502 /UB
0534	1205	1205 /JE
0535	0324	0324 /CT
0536	4043	4043 / #
0537	4000	4000 /
0540	0000	0000 /00
0541	4040	OUT3,4040 /
0542	2225	2225 /RU
0543	1640	1640 /N
0544	4340	4340 /#
0545	0000	0000 /00
0546	3603	OUT4A,3603 /CRLF,C
0547	1001	1001 /HA
0550	1122	1122 /IR
0551	0000	0000 /00
0552	3605	OUT4B,3605 /CRLF,E
0553	3105	3105 /YE
0554	0000	0000 /00
0555	4020	OUT4,4020 / P
0556	1723	1723 /OS
0557	1124	1124 /IT
0560	1117	1117 /IO
0561	1640	1640 /N
0562	1505	1505 /ME
0563	0116	0116 /AN
0564	4075	4075 / =

0565	4000	4000 /
0566	0000	0000 /00
0567	4004	OUT5,4004 / D
0570	0507	0507 /EG
0571	2205	2205 /RE
0572	0523	0523 /ES
0573	0000	0000 /00
0574	3626	OUT6,3626 /CRLF,V
0575	0122	0122 /AR
0576	1101	1101 /IA
0577	1603	1603 /NC
0600	0540	0540 /E
0601	7540	7540 /=
0602	0000	0000 /00
0603	4023	OUT7,4023 / S
0604	2125	2125 /QU
0605	0122	0122 /AR
0606	0504	0504 /ED
0607	0000	0000 /00
0610	3623	OUT8,3623 /CRLF,S
0611	2401	2401 /TA
0612	1604	1604 /ND
0613	0122	0122 /AR
0614	0440	0440 /D
0615	0405	0405 /DE
0616	2611	2611 /VI
0617	0124	0124 /AT
0620	1117	1117 /IO
0621	1640	1640 /N
0622	7540	7540 /=
0623	0000	0000 /00

*20

0020	0000	H,0
0021	0000	J,0
0022	0000	KEY,0
0023	0000	CNTR1,0
0024	0000	LOW,0
0025	0000	HIGH,0
0026	0000	UP,0
0027	0000	MID,0
0030	0000	DOWN,0
0031	0000	SAMP,0
0032	0000	MSHI,0
0033	0000	MSLO,0
0034	0000	MEAN,0
0035	0000	SSHI,0
0036	0000	SSLO,0
0037	0000	SQMNH,0

0040	0000	SQMNL,0
0041	0000	VARA,0
0042	0000	VARB,0
0043	0000	A,0
0044	0000	SIGMA,0
0045	1177	PLIST,LIST-1
0046	0233	PTOP,TOP
0047	0267	PMAV,MAV
0050	0204	PSTR,STR
0051	0513	POUT1,OUT1
0052	0532	POUT2,OUT2
0053	0541	POUT3,OUT3
0054	0546	POUT4A,OUT4A
0055	0552	POUT4B,OUT4B
0056	0555	POUT4,OUT4
0057	0567	POUT5,OUT5
0060	0574	POUT6,OUT6
0061	0603	POUT7,OUT7
0062	0610	POUT8,OUT8
0063	0443	PEYE,EYE
0064	0445	PDEG,DEG
0065	0060	C60,60
0066	4401	SPEC1,4401
0067	4701	SPEC2,4701
0070	5100	PSPEC,5100
0071	7510	PSQRT,7510
0072	5114	PPRNTQ,5114
0073	5155	PFACI,5155
0074	1320	FACI1,1320 /= 720(10)
0075	2014	FACI2,2014 /= 1036(10)
0076	0000	SQ,0 /SQUARING SUBROUTINE
0077	7510	SPA
0100	7041	CIA
0101	3104	DCA .+3
0102	1104	TAD .+2
0103	7425	ML MUY
0104	0000	0
0105	5476	JMP I SQ
0106	0000	TYPE,0 /TYPE SUBROUTINE
0107	6046	TLS
0110	6041	TSF
0111	5110	JMP .-1
0112	7200	CLA
0113	5506	JMP I TYPE
0114	0000	CRLF,0 /CARRIAGE RETURN LINE FEED SUBROUTINE
0115	1122	TAD K215
0116	4106	JMS TYPE
0117	1123	TAD K212
0120	4106	JMS TYPE
0121	5514	JMP I CRLF
0122	0215	K215,215

```
0123 0212 K212,212

0124 0000 PRINT,0 /MESSAGE UNPACK AND DECODE SUBROUTINE
0125 3134 DCA PDEX
0126 1534 TAD I PDEX
0127 2134 ISZ PDEX
0130 7450 SNA
0131 5524 JMP I PRINT
0132 4135 JMS DECODE
0133 5126 JMP .-5
0134 0000 PDEX,0
0135 0000 DECODE,0
0136 3147 DCA PACK
0137 1147 TAD PACK
0140 7012 RTR
0141 7012 RTR
0142 7012 RTR
0143 4150 JMS OUTPT
0144 1147 TAD PACK
0145 4150 JMS OUTPT
0146 5535 JMP I DECODE
0147 0000 PACK,0
0150 0000 OUTPT,0
0151 0167 AND C0077
0152 7450 SNA
0153 5550 JMP I OUTPT
0154 1170 TAD C7742 /CRLF
0155 7440 SZA
0156 5161 JMP .+3
0157 4114 JMS CRLF
0160 5550 JMP I OUTPT
0161 1171 TAD M2
0162 7500 SMA
0163 1172 TAD M100
0164 1173 TAD C340
0165 4106 JMS TYPE
0166 5550 JMP I OUTPT
0167 0077 C0077,77
0170 7742 C7742,7742
0171 7776 M2,7776
0172 7700 M100,7700
0173 0340 C340,340

      *1200

1200 0000 LIST,0 /CURRENT SAMPLE LIST
```

A	0043	POUT4B	0055
CHR	0440	POUT5	0057
CNTR1	0023	POUT6	0060
CRLF	0114	POUT7	0061
C0077	0167	POUT8	0062
C340	0173	PPRNTQ	0072
C60	0065	PRINT	0124
C7742	0170	PSPEC	0070
DECODE	0135	PSQRT	0071
DEG	0445	PSTR	0050
DOWN	0030	PTOP	0046
EYE	0443	SAMP	0031
FACI1	0074	SIGMA	0044
FACI2	0075	SPEC1	0066
H	0020	SPEC2	0067
HIGH	0025	SQ	0076
J	0021	SQMNH	0037
KEY	0022	SQMNL	0040
K212	0123	SSHI	0035
K215	0122	SSLO	0036
LIST	1200	STR	0204
LOW	0024	TOP	0233
MAV	0267	TYPE	0106
MEAN	0034	UP	0026
MID	0027	VARA	0041
MN	0256	VARB	0042
MSHI	0032		
MSLO	0033		
M100	0172		
M2	0171		
OUTPT	0150		
OUT1	0513		
OUT2	0532		
OUT3	0541		
OUT4	0555		
OUT4A	0546		
OUT4B	0552		
OUT5	0567		
OUT6	0574		
OUT7	0603		
OUT8	0610		
PACK	0147		
PDEG	0064		
PDEX	0134		
PEYE	0063		
PFACI	0073		
PLIST	0045		
PMAV	0047		
POUT1	0051		
POUT2	0052		
POUT3	0053		
POUT4	0056		
POUT4A	0054		

APPENDIX D

ANVAR AND ANVAR 2 PROGRAMS TO
CALCULATE ANALYSIS OF VARIANCE

These programs are used to determine the possible significance of the various experimental parameters by performing a standard analysis of variance on data entered in the Graeco-Latin experimental design. The two programs are similar except that ANVAR 2 takes into account the control runs while ANVAR does not. Both programs are written in the conversational programming language FOCAL which was modified slightly so that data could be read in on prepunched paper tape.

A standard analysis of variance algorithm is employed.¹⁸ For a 6x6 square[A] each data entry (here chair or eye mean position) may be represented as a_{ij} where i = row and j = column in the square $i, j = 1, 6$. This original square of data is arranged so that rows represent subjects and columns represent order. For convenience, this square was mapped into a second square[B] with rows representing intensities and columns representing modes. Each entry in the second square may be represented by a term b_{ij} where $i, j = 1, 6$.

Calculations performed are then as follows for ANVAR (ANVAR 2 is similar).

$$\text{Total Sum: } X = \sum_{i=1}^6 \sum_{j=1}^6 a_{ij} \quad (\text{D.1})$$

$$\text{Correction Factor: } Z = (X/36)^2 \quad (\text{D.2})$$

$$\text{Total Sum of Squares: } Y = \left(\sum_{i=1}^6 \sum_{j=1}^6 a_{ij}^2 \right) - CF \quad (\text{D.3})$$

$$\text{Sum for Each Subject: } R_i = \sum_{j=1}^6 a_{ij}; \quad i = 1, 6 \quad (\text{D.4})$$

$$\text{Sum for Each Order: } C_j = \sum_{i=1}^6 a_{ij}; \quad j = 1, 6 \quad (\text{D.5})$$

$$\text{Sum for Each Intensity: } S_i = \sum_{j=1}^6 b_{ij}; \quad i = 1, 6 \quad (\text{D.6})$$

$$\text{Sum for Each Mode: } M_j = \sum_{i=1}^6 b_{ij}; \quad j = 1, 6 \quad (\text{D.7})$$

Sum of Squares:

$$\text{Between Subjects: } P = \sum_{i=1}^6 (R_i)^2/6 - Z \quad (\text{D.6})$$

$$\text{Between Order: } C = \sum_{j=1}^6 (C_j)^2/6 - Z \quad (\text{D.7})$$

$$\text{Between Modes: } M = \sum_{i=1}^6 (M_i)^2/6 - Z \quad (\text{D.8})$$

$$\text{Between Intensities: } L = \sum_{i=1}^6 (S_i)^2/6 - Z \quad (\text{D.8})$$

$$\text{Residual Sum of Squares: } R = T - P - C - M - L \quad (\text{D.10})$$

Variance Estimates:

$$\text{Subjects: } = \frac{P}{5}$$

$$\text{Order: } = \frac{C}{5}$$

Variance Estimates (continued):

$$\text{Modes:} = \frac{M}{5}$$

$$\text{Intensities:} = \frac{L}{5}$$

$$\text{Residual: } W = \frac{R}{15}$$

Variance Ratios:

$$\text{Subjects: } P/5W$$

$$\text{Order: } C/5W$$

$$\text{Modes: } M/5W$$

$$\text{Intensities: } L/5W$$

Error Variance (for T Test)

$$EV = \sqrt{W\left(\frac{1}{6} + \frac{1}{6}\right)} = \sqrt{W/3} \quad (D.11)$$

The variance ratios obtained from ANVAR and ANVAR 2 may be used with a standard F test to determine significance of the various parameters as discussed in the text. The error variance is calculated for possible use in a standard student t test if the F test indicates significance of a certain parameter.

Listings of ANVAR and ANVAR 2 follow.

C-FOCAL, 1969

```

01.10 E
01.20 F I=1,36;A V(I)
01.30 F I=1,36;A U(I)
01.40 F I=1,36;S X=X+V(I);S Y=Y+V(I)+2;S Z=(X/6)+2;S T=Y-Z
01.50 F I=1,6;D 4
01.60 F I=1,6;D 6
01.70 S M=M-Z;S L=L-Z;S P=P-Z;S C=C-Z;S R=T-M-L-P-C;S W=R/15

02.10 F I=1,6;D 7
02.40 T !!, " SOURCE DF SS VE VR"
02.41 T %8.02, !!, " MODES 5 ",M," ",M/5," ",M/5*W,!!
02.51 T %8.02, " INTENSITIES 5 ",L," ",L/5," ",L/5*W,!!
02.61 T %8.02, " SUBJECTS 5 ",P," ",P/5," ",P/5*W,!!
02.71 T %8.02, " ORDER 5 ",C," ",C/5," ",C/5*W,!!
02.81 T %8.02, " RESIDUAL 15 ",R," ",W,!!
02.90 T %8.02, " TOTAL 35 ",T,!!
02.91 T !, " SUBJECTS MODES INTENSITIES",!
02.92 F I=1,6;D 8
02.93 T %6.02, !!, " ERROR VARIANCE",FSQT(W/3),!!
02.95 Q

04.10 F J=<(I-1)*6+1>,<(I-1)*6+6>;S R(I)=R(I)+V(J);S S(I)=S(I)+U(J)
04.20 F J=0,5;S C(I)=C(I)+V(I+J*6);S M(I)=M(I)+U(I+J*6)

06.10 S M=M+M(I)+2/6;S L=L+S(I)+2/6;S P=P+R(I)+2/6;S C=C+C(I)+2/6

07.10 T !, " ";F J=<(I-1)*6+1>,<(I-1)*6+6>;T %4,V(J)

08.10 T %5.01, !, " ",R(I)/6," ",M(I)/6," ",S(I)/6

```

ANVAR, Analysis of Variance program for a 6X6 Graeco-Latin Square

C-FOCAL, 1969

01.10 E
01.20 F I=1,48;A V(I)
01.30 F I=1,36;A U(I)
01.40 F I=1,48;S X=X+V(I);S Y=Y+V(I)*2;S Z=(X*2)/48;S T=Y-Z
01.50 F I=1,6;D 4
01.60 F I=1,8;S M=M+M(I)*2/6;S C=C+C(I)*2/6
01.65 F I=1,6;S P=P+R(I)*2/8;S L=L+S(I)*2/6
01.70 S M=M-Z;S L=L-Z;S P=P-Z;S C=C-Z;S R=T-M-L-P-C;S W=R/23

		SOURCE	DF	SS	VE	VR
02.40	T	!!,"				
02.41	T	%8.02,!!,"		7	","M,"	","M/7,"
02.51	T	%8.02,"			","M/7*W,!!	","M/7*W,!!
02.51	T	%8.02,"	INTENSITIES	5	","L,"	","L/5,"
02.61	T	%8.02,"	SUBJECTS	5	","P,"	","P/5*W,!!
02.71	T	%8.02,"	ORDER	7	","C,"	","C/7*W,!!
02.81	T	%8.02,"	RESIDUAL	23	","R,"	","W,!!
02.90	T	%8.02,"	TOTAL	47	","T,!!	
02.91	F	I=1,6;T%5.01,!,,"			","R(I)/8,"	","M(I+1)/6,"
02.95	Q				","S(I)/6	

04.10 F J=<(I-1)*8+1>,<(I-1)*8+8>;S R(I)=R(I)+V(J)
04.20 F J=1,8;S C(J)=C(J)+V(J+(I-1)*8);S M(1)=C(1);S M(8)=C(8)
04.30 F J=<(I-1)*6+1>,<(I-1)*6+6>;S S(I)=S(I)+U(J)
04.40 F J=0,5;S M(I+1)=M(I+1)+U(I+J*6)

ANVAR2, Analysis of Variance program for a 6X6 Graeco-Latin Square + two control runs per subject

APPENDIX E

T TEST AND T TEST 2PROGRAMS TO PERFORM STUDENT T TEST

This program is a simple implementation of the student t test in order to determine where the significant differences between means lie. T TEST is for data without consideration of controls while T TEST 2 takes control runs into account. Both programs are written in the conversational language "FOCAL."

The error variance is read in as calculated by ANVAR and the value of t required is read in from a table of such values. A significant difference between means exists if

$$\frac{\text{mean A} - \text{mean B}}{\text{error variance}} - t > 0 \quad (\text{E.1})$$

The programs test all possible combinations of corresponding means and print out those which differ significantly together with the actual t value for the comparison.

Listings of T TEST and T TEST 2 follow.

C-FCCAL, 1969

```
01.10 E
01.20 A "A"A;A "T" T;F I=1,36;A U(I)
01.40 F I=1,6;D 4
01.45 T " T TEST"
01.46 T %4.02,!!," ERROR VARIANCE",A," T(P=0.05)",T
01.50 T !!," MODES INTENSITIES",!
01.60 F I=1,6;D 3
01.65 T !!
01.70 F I=1,5;F J=I+1,6;D 7
01.80 F I=1,5;F J=I+1,6;D 8
01.90 Q

03.10 T %5.01,!,," ",I," ",M(I)/6," ",S(I)/6

04.10 F J=<(I-1)*6+1>,<(I-1)*6+6>;S S(I)=S(I)+U(J)
04.20 F J=0,5;S M(I)=M(I)+U(I+J*6)

07.10 S B=FABS(M(I)-M(J))/6*A-T;I (B)7.3;
07.20 T %1,!,," M",I," M",J," T";T %5.02,B+T
07.30 R

08.10 S B=FABS(S(I)-S(J))/6*A-T;I (B)8.3;
08.20 T %1,!,," S",I," S",J," T";T %5.02,B+T
08.30 R
```

TTEST, Program to perform Student "t" test
on means of parameters found significant in
analysis of variance-no control runs

C-FOCAL,1969

```
01.10 E
01.20 A "A"A;A "T" T;F I=1,48;A U(I)
01.40 F I=1,6;D 4
01.45 T " T TEST"
01.46 T %4.02,!!," ERROR VARIANCE",A," T(P=0.05)",T
01.50 T !!," M0DES INTENSITIES",!
01.60 F I=0,7;D 3
01.65 T !!
01.70 F I=0,6;F J=I+1,7;D 7
01.80 F I=1,5;F J=I+1,6;D 8
01.90 Q

03.10 T %5.01,!, " ",I," ",M(I)/6," ",S(I)/6

04.10 F J=<(I-1)*8+2>,<(I-1)*8+7>;S S(I)=S(I)+U(J)
04.20 F J=0,7;S M(J)=M(J)+U(J+1+(I-1)*8)

07.10 S B=FABS(M(I)-M(J))/6*A-T;I (B)7.3;
07.20 T %1,!, " M",I," M",J," T";T %5.02,B+T
07.30 R

08.10 S B=FABS(S(I)-S(J))/6*A-T;I (B)8.3;
08.20 T %1,!, " S",I," S",J," T";T %5.02,B+T
08.30 R
```

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TTEST2, Program to perform Student "t" test
on means of parameters found significant in
analysis of variance-control runs included

REFERENCES

1. Bekey, G.A., and Karplus, W.J., Hybrid Computation, John Wiley and Sons, Inc., New York, 1968.
2. Bos, H.J., Jongkees, L.B., and Kruidenier, C., "The Artefact on Electronystagmography During Galvanic Labyrinth Stimulation," Practical Oto Rhinolaryngology, No. 30, pp. 214-217, 1968.
3. Breson, K., and Krag, E., "Galvanic Pseudonystagmus," Acta Oto-Laryngologica, Vol. 64, pp. 403-414, Nov.-Dec., 1967.
4. Clerk, B., and Stewart, J.D., "Effects of Angular Acceleration on Man: Thresholds for the Perception of Rotation and the Oculogyral Illusion," Aerospace Medicine, 40:952, September, 1969.
5. Cochran, W., Personal Communication, May, 1970.
6. Cochran, W. and Cox, G., Experimental Designs, 2nd Edition, Wiley and Sons, Inc., New York, 1957.
7. Collins, W., and Guedry, F., Jr., "Arousal Effects and Nystagmus during prolonged constant angular acceleration," Acta-Oto-Laryngologica, Supp. 54, pp. 349-361.
8. Focal 8 Programming Manual, Digital Equipment Corporation, 1969.
9. Small Computer Handbook, Digital Equipment Corporation, 1967.
10. Dunstone, J.J., and Dzendolet, E., "Types of Objective Electrical Vestibulograms," Perceptual and Motor Skills, 19, pp. 899-904, Southern University Press, 1964.
11. Dunstone, J.J., Dzendolet, E., and Heuckeroth, O., "Effect of Some Personality Variables on Electrical Vestibular Stimulation," Perceptual and Motor Skills, 18, pp. 689-695, Southern University Press, 1964.
12. Dzendolet, Ernest, "Sinusoidal Electrical Stimulation of the Human Vestibular Apparatus," Perceptual and Motor Skills, 17, pp.171-185, Southern University Press, 1963.

13. Dzendolet, Ernest, "Effect of Dramamine on the Objective Electrical Vestibulogram", *Perceptual and Motor Skills*, 18, pp. 465-468, Southern Universities Press, 1964.
14. Fischer, Joseph J., The Labyrinth, Grune and Stratton, New York, 1956, pp. 78-81, 157-160.
15. Ganong, William F., Review of Medical Physiology, 4th Edition, Lange Medical Publications, Los Altos, California, 1969.
16. Katz, Gerald B., "Perception of Rotation-Nystagmus and Subjective Response at Low Frequency Stimulation", S.B. Thesis, M.I.T., June, 1967.
17. Malcik, Vladmir, "Performance Decrement in a Flight Simulator Due to Galvanic Stimulation of the Vestibular Organ and its Validity for Success in Flight Training", *Aerospace Medicine*, 39:9, pp. 941-943, September, 1968.
18. Maxwell, A.E., Experimental Design in Psychology and the Medical Sciences, Methuen and Co., Ltd., London, 1958.
19. Meiry, J.L. "The Vestibular System and Human Dynamic Spatial Orientation", Sc.D. Thesis, M.I.T., 1965.
20. Mirchandani, Pitu B., "Directional Preponderance in the Semicircular Canals", M.V.L. Report, Fall, 1969.
21. Peters, Richard A., "Dynamics of the Vestibular System and their Relation to Motion Perception, Spatial Disorientation and Illusions", Systems Technology, Inc., Hawthorne, California, NASA CR-1309, April, 1969.
22. Pfaltz, C.R.P., and Koike, Y., "Galvanic Test in Central Vestibular Lesions", *Acta Oto-Laryngologica*, Vol. 65, pp. 161-168, January-February, 1968.
23. Pulec, J.L., "Clinical Electronystagmography", *Laryngoscope*, Vol. 78, #12, pp. 2033-48, December, 1968.
24. Reason, James T., "Motion Sickness-Some Theoretical Considerations", *International Journal of Man Machine Studies*, Vol. 1, No. 1, January, 1969.
25. Ruis, M. and Garcia Austt, E., "Slow Eye Movements Determined by Vestibular Electrical Stimulation in Man", *Acta Neurologica Latin America*, Vol. 11, #4, pp. 350-9, 1965.
26. Spiegel, E. and Scala, N., "Response of the Labyrinthine Apparatus to Electrical Stimulation", *Archives Oto-laryngologica*, 38, pg. 131, 1943.

27. Spiegel, E., and Sommer, I., Neurology of the Eye, Ear, Nose, and Throat, Grune and Stratton, New York, New York, 1944.
28. Standard Mathematical Tables, 14th Edition, Chemical Rubber Co., Cleveland, Ohio, 1965.
29. Steer, Robert W., Jr., "The Influence of Angular and Linear Acceleration and Thermal Stimulation on the Human Semicircular Canal," Sc. D. Thesis, M.I.T., August, 1967.
30. Szentogthai, J., "The Elementary Vestibulo-Ocular Reflex Arc," Journal of Neurophysiology, 13, pp. 395-407, 1950.
31. Tole, John R., "MITNYS, A Hybrid Program to Analyze Nystagmus," M.V.L. Report, to be published.
32. Truex, R.C., and Carpenter, M.B., Human Neuroanatomy, Sixth Edition, The Williams and Wilkins Co., Baltimore, Maryland, 1969.
33. Vandervelde, W., Notes from M.I.T. course #16.37, Spring, 1970.
34. Van Houtte, Noel A.J., "Display Instrumentation for V/STOL Aircraft in Landing," Vol. 3, Description and Listing of Subroutines and Other Programs, Sc. D. Thesis, M.I.T., 1970.
35. Werner, Gerhard, and Whitsel, Barry L., "The Activity of Afferent Nerve Fibers from the Vestibular Organ and of Neurons in the Vestibular Nuclei of Unanesthetized Primates," Interim Report on Air Force Contract No. AF - AFOSR - 66- 1005B, March, 1968.
36. Wilson, J. and Pike, F., "Effects of Stimulation and Extirpation of the Labyrinth," Philanthropic Royal Society, London, 203:127, 1912.
37. Yemelyanov, M.D., and Kuznetsov, A.G., "On the Role of the Interactions Among Vestibular, Visual and Proprioceptive Sensations in the Incidence of Illusions in Pilots," Vestnick Otorinolar, No. 3, p. 63, 1962, In Russian translated by J.L. Meiry.
38. Young, L.R., "Recording Eye Position," chapter to appear in forthcoming book, Medical Electronics and Engineering, McGraw-Hill.
39. Young, L.R., "The Current Status of Vestibular Models," Automatica, Vol. 5, pp. 369-383, 1969.