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GAKIN II: A ONE-DIMENSIONAL
MULTIGROUP DIFFUSION THEORY
REACTOR KINETICS CODE

by

K.F. Hansen, J.H. Mason

August 1973

Department of Nuclear Engineering
Massachusetts Institute of Technology
Cambridge, Massachusetts 02139

AEC Research and Development Report
Contract AT(11-1)- 2262
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John Herbert Mason

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Engineering, September, 1973 in partial
fulfillment of the requirements for the
degree of Master of Science.

ABSTRACT

GAKIN II is a time dependent neutron diffusion code. It solves the time dependent multigroup neutron diffusion equations in one space dimension using the usual finite difference approximation. Time integration is accomplished using an exponential transformation and semi-implicit differencing.

GAKIN II is a revision of the existing code GAKIN. The temporal treatment has been improved, a simplified and more implicit algorithm has been used, and the coding has been improved and simplified.

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1. INTRODUCTION

GAKIN II is a one-dimensional multigroup diffusion theory kinetics code. The code solves the time dependent multigroup diffusion equations in slab, cylindrical, or spherical geometry. An arbitrary number of space points, regions and energy groups may be used. Optionally, the effects of time dependent cross sections, external sources, and xenon poisoning may be included. Time step adjustment can be automatic. GAKIN II has been written for the IBM System 370, or System 360.

GAKIN II is a revision of GAKIN (Reference 1) designed to decrease the storage requirements and running time of the original code. The iterative frequency predictor in GAKIN has been replaced by an explicit scheme, the steady state initialization calculation has been streamlined, and a large number of programming improvements have been made. As a result, GAKIN II is substantially more economic to use than GAKIN. A complete summary of the changes made to GAKIN can be found in Section 7.

The theoretical basis for GAKIN II is presented in Sections 2 through 5. Section 6 describes some of the terms a user may need, defines the cross sections used, and explains how cross section variation is treated. Section 8 contains necessary user information and section 9 contains two sample problems. The code is listed in the appendix.

2. Algorithm Development

In this section the basic numerical scheme used in GAKIN II is derived. In 2.1 the time dependent multigroup diffusion equations are set forth. Discretization is accomplished by finite differencing of the spatial variable in 2.2 and by exponential transformation of time in 2.3. The resulting system of equations is proven consistent in 2.4 and numerically stable in 2.5.

2.1 The Time Dependent Multigroup Diffusion Equations

Considering only one fissionable isotope and assuming that the neutron energy group velocities are time independent, the time dependent diffusion equation for group g is

$$\begin{aligned}
 v_g \frac{\partial}{\partial t} \phi_g(\underline{r}, t) &= \underline{\nabla} \cdot D_g(\underline{r}, t) \underline{\nabla} \phi_g(\underline{r}, t) \\
 &\quad - \Sigma_{tg}(\underline{r}, t) \phi_g(\underline{r}, t) \\
 &\quad + \sum_{g'=1}^G \Sigma_{sgg'}(\underline{r}, t) \phi_{g'}(\underline{r}, t)
 \end{aligned}
 \tag{1a}$$

$$\begin{aligned}
& + (1-\beta) \chi_g^P \sum_{g'=1}^G v \Sigma_{fg'}(\underline{r}, t) \phi_{g'}(\underline{r}, t) \\
& + \sum_{i=1}^I \chi_{ig}^d \lambda_i c_i(\underline{r}, t) + S_g(\underline{r}, t),
\end{aligned}$$

where,

v_g is the group speed of neutrons in group g ,

$\phi_g(\underline{r}, t)$ is the neutron flux in group g at location \underline{r} , and at time t ,

$D_g(\underline{r}, t)$ is the group g diffusion coefficient,

$\beta = \sum_{i=1}^I \beta_i$, where β_i is the fraction of all neutrons produced due to decay of delayed neutron emitters in group i ($i=1, 2, \dots, I$),

χ_g^P is the fractional yield of prompt neutrons into group g ,

v is the number of neutrons emitted per fission,

$\Sigma_{fg}(\underline{r}, t)$ is the macroscopic fission cross section for neutrons in group g ,

χ_{ig}^d is the fractional yield of delayed neutrons
into group g from emitters in group i ,

λ_i is the decay constant for emitters in group i ,

$c_i(\underline{r}, t)$ is the concentration of delayed neutron
emitters in group i ,

$S_g(\underline{r}, t)$ is the rate at which neutrons are
introduced into group g from extraneous
sources,

$\Sigma_{sgg'}(\underline{r}, t)$ is the macroscopic cross section for
scattering from group g' to group g , and

Σ_{tg} is the total macroscopic cross section for
interaction of neutrons in group g . The
associated equations for the delayed neutron
emitter concentrations are:

$$\frac{\partial c_i(\underline{r}, t)}{\partial t} = \beta_i \sum_{g=1}^G v \Sigma_{fg}(\underline{r}, t) \phi_g(\underline{r}, t) - \lambda_i c_i(\underline{r}, t) \quad (2)$$

for $i = 1, 2, \dots, I$.

By defining the vectors

$$\underline{\phi}(\underline{r}, t) = \text{Column } [\phi_1(\underline{r}, t), \dots, \phi_G(\underline{r}, t)],$$

$$\underline{S}(\underline{r}, t) = \text{Column } [S_1(\underline{r}, t), \dots, S_G(\underline{r}, t)],$$

$$\underline{v}^{\Sigma_f}(\underline{r}, t) = \text{Column } [v^{\Sigma_{f1}}(\underline{r}, t), \dots, v^{\Sigma_{fG}}(\underline{r}, t)],$$

$$\chi^p = \text{Column } [\chi_1^p, \dots, \chi_G^p], \text{ and}$$

$$\chi_i^d = \text{Column } [\chi_{i1}^d, \dots, \chi_{iG}^d]$$

and the matrices

$$[v] = \text{Diagonal } [v_1, \dots, v_G],$$

$$[D(\underline{r}, t)] = \text{Diagonal } [D_1(\underline{r}, t), \dots, D_G(\underline{r}, t)], \text{ and}$$

$$[A(\underline{r}, t)] = \begin{bmatrix} \Sigma_{t1} - \Sigma_{s11} & -\Sigma_{s12} & \dots & -\Sigma_{s1G} \\ -\Sigma_{s21} & & & \\ \cdot & & & \cdot \\ \cdot & & & \cdot \\ \cdot & & & \cdot \\ -\Sigma_{sG1} & \dots & & \Sigma_{tG} - \Sigma_{sGG} \end{bmatrix}$$

where $\Sigma_{tg} = \Sigma_{tg}(\underline{r}, t)$ and $\Sigma_{sgg'} = \Sigma_{sgg'}(\underline{r}, t)$, it is possible to write the time dependent multigroup diffusion equations in matrix form (Reference 2):

$$\begin{aligned}
[\underline{v}]^{-1} \frac{\partial}{\partial t} \underline{\phi}(\underline{r}, t) &= \underline{\nabla} \cdot [D(\underline{r}, t)] \underline{\nabla} \underline{\phi}(\underline{r}, t) \\
&- [A(\underline{r}, t)] \underline{\phi}(\underline{r}, t) + (1-\beta) \underline{\chi}^P \underline{v} \underline{\Sigma}_f(\underline{r}, t)^T \underline{\phi}(\underline{r}, t) \\
&+ \sum_{i=1}^I \lambda_i c_i(\underline{r}, t) \underline{\chi}_i^d + \underline{s}(\underline{r}, t) .
\end{aligned} \tag{1b}$$

2.2 Spatial Dependence

The simplest and most commonly applied method of discretizing the space coordinate in the diffusion equations is to replace (formally) the derivative in the leakage term, $\underline{\nabla} \cdot [D] \underline{\nabla}$ with a finite difference expression and to replace the continuous functions $\phi_g(\underline{r}, t)$ with discrete values $\phi_{gp}(t) = \phi_g(\underline{r}_p, t)$. As a result, the elements of $\underline{\phi}$ must be expanded into vectors.

Let ϕ_{gp} ($g=1, \dots, G$; $p=1, \dots, P$) be the neutron flux in group g at spatial mesh point p . And similarly, let c_{ip} ($i=1, \dots, I$; $p=1, \dots, P$) be the concentration of delayed neutron precursors in group i at point p .

We may now define the following.

$\underline{\psi} =$

$$\begin{bmatrix} \phi_{1,1} \\ \phi_{1,2} \\ \cdot \\ \cdot \\ \cdot \\ \phi_{1,P} \\ \phi_{2,1} \\ \cdot \\ \cdot \\ \cdot \\ \phi_{G,P} \\ c_{1,1} \\ c_{1,2} \\ \cdot \\ \cdot \\ \cdot \\ c_{1,P} \\ \cdot \\ \cdot \\ \cdot \\ c_{I,P} \end{bmatrix}$$

(3)

$$[\Gamma] = \text{Diagonal } [\Gamma_i], i=1,2, \dots, G+I \quad (4)$$

where,

$$[\Gamma_i] = v_i \{ \Sigma_{s_{ii}} + (1-\beta) \chi_i^P v \Sigma_{f_i} - \Sigma_{t_i} \} [I]$$

for $i \leq G$

$$[\Gamma_i] = -\lambda_i [I]$$

for $G < i \leq G+I$.

[I] is the P by P identity matrix.

$$[H] = \text{Diagonal } [H_i] i=1,2, \dots, G+I$$

where, for a homogeneous reactor,

$$[H_i] = v_i D_i \begin{bmatrix} -a & b & & & 0 \\ b & -a & b & & \\ & b & -a & & \\ & & & \cdot & \\ & & & & \cdot \\ & & & & & \cdot \\ 0 & & & & -a & b \\ & & & & b & -a \end{bmatrix}$$

$$a = \frac{2r^n}{\Delta r^2},$$

$$b = \frac{r^n}{\Delta r^2},$$

$n = 0$ for plane geometry,

1 for cylindrical geometry,

2 for spherical geometry,

and Δr is the mesh spacing.

$$[H_i] = [0] \text{ for } G < i \leq G + I.$$

Note that $[\Gamma] = [\Gamma(t)]$ is diagonal and $[H] = [H(t)]$ is tridiagonal.

$$[L] = \begin{bmatrix} [L_{11}] & \dots & [L_{1,G+I}] \\ \cdot & & \cdot \\ \cdot & & \cdot \\ \cdot & & \cdot \\ [L_{G+I,1}] & \dots & [L_{G+I,G+I}] \end{bmatrix}$$

where

$$[L_{ij}] = [0]$$

for $i \leq j$

and for $G < j < i$,

$$[L_{ij}] = v_i \{ \Sigma_{sij} + (1-\beta) \chi_i^p v_{\Sigma_{fj}} \} \quad [I]$$

for $j < i \leq G$, and

$$[L_{ij}] = (v_{\Sigma_{fj}} \beta_{i-G}) \quad [I]$$

for $j \leq G < i$.

$$[U] = \begin{bmatrix} [U_{11}] & \dots & [U_{1,G+I}] \\ \vdots & & \vdots \\ [U_{G+1,1}] & \dots & [U_{G+I,G+I}] \end{bmatrix} \quad (7)$$

where,

$$[U_{ij}] = [0]$$

for $j \leq i$,

and for $G < i < j$,

$$[U_{ij}] = v_i \{ \Sigma_{sij} + (1-\beta) \chi_i^p v_{\Sigma_{fj}} \} \quad [I]$$

for $i < j \leq G$, and

$$[U_{ij}] = (\chi_{i,j-G}^d \lambda_{j-G}) \quad [I]$$

for $i \leq G < j$.

Note that $[L] = [L(t)]$ is lower triangular, $[U] = [U(t)]$ is upper triangular, and $[U_{ij}]$ and $[L_{ij}]$ are diagonal (if non-zero).

For a reactor composed of more than one region, each with different properties, the non-zero elements of $[H_i]$, $[\Gamma_i]$, $[U_{ij}]$, and $[L_{ij}]$ are no longer identical but depend on the properties at that mesh point. For region interfaces, a more rigorous development yields the proper volume weighting of properties for that point. The band structure of the matrices involved is unchanged.

Finally, using the above definitions, the time dependent multigroup diffusion equations may be written

$$\frac{d}{dt} \underline{\psi}(t) = [B(t)] \underline{\psi}(t) + \underline{S}(t) \quad (8)$$

where

$$[B(t)] = [L(t)] + [U(t)] + [H(t)] + [\Gamma(t)].$$

2.3 Time Dependence

In this section, the temporal variable is discretized by approximating the neutron flux time dependence with an exponential. This approximation is exact when the flux behavior is asymptotic and is expected to be accurate in other cases.

Integration of equation (8) over the interval
 $h = t_{j+1} - t_j$ and rearranging yields:

$$\begin{aligned} & \underline{\psi}^{j+1} - \int_{t_j}^{t_{j+1}} [\Gamma(t)] \underline{\psi}(t) dt - \int_{t_j}^{t_{j+1}} [H(t)] \underline{\psi}(t) dt \\ &= \underline{\psi}^j + \int_{t_j}^{t_{j+1}} [L(t)] \underline{\psi}(t) dt + \int_{t_j}^{t_{j+1}} [U(t)] \underline{\psi}(t) dt \quad (9) \\ & \quad + \int_{t_j}^{t_{j+1}} \underline{S}(t) dt \end{aligned}$$

where,

$$\underline{\psi}^j = \underline{\psi}(t_j) = \text{Column } [\psi_{11}^j, \dots, \psi_{GP}^j]$$

It is reasonably accurate to approximate,

$$\psi_{gp}(t) \approx e^{\omega_{gp}(t-t_j)} \psi_{gp}^j \quad (10)$$

in the interval h .

Numerically, a more manageable approach is to use energy independent frequencies, ω_p , such that

$$\psi_{gp}(t) \approx e^{\omega_p(t-t_j)} \psi_{gp}^j \quad \text{for } g=1, \dots, G. \quad (11)$$

This approximation is physically justifiable if the test energy group for determination of the point dependent frequencies is judiciously chosen (e.g., for a thermal reactor, the behavior of the faster flux groups would be expected to closely follow that of a thermal energy group).

Then substitute

$$\underline{\psi}(t) = e^{(t-t_j)} \cdot [\Omega] \underline{\psi}^j, \quad (12a)$$

where

$$[\Omega] = \text{Diagonal } [\omega_1, \dots, \omega_p, \dots, \omega_1, \dots, \omega_p],$$

into the second integral on the right hand side of equation (9) and

$$\underline{\psi}(t) = e^{(t-t_{j+1})} \cdot [\Omega] \underline{\psi}^{j+1} \quad (12b)$$

into all other integrals involving $\underline{\psi}(t)$ in (9). These substitutions are performed to produce a stable numerical scheme implicit in all terms except the term involving [U]. Finally, approximation of [L], [U], [Γ], [H], and [Ω] by constants in the interval h yields the algorithm used in GAKIN II:

$$\begin{aligned}
\{[I] - [H+\Gamma][FF2]\} \underline{\psi}^{j+1} = \\
[L][FF2] \underline{\psi}^{j+1} + \{[I]+[U][FF1]\} \underline{\psi}^j \\
+ \int_{t_j}^{t_{j+1}} \underline{S}(t) dt
\end{aligned} \tag{13}$$

The elements of the diagonal matrices [FF1] and [FF2] are given by

$$FF1_p = \frac{e^{\omega_p \cdot h} - 1}{\omega_p} \quad \text{for all } g \tag{14a}$$

$$FF2_p = \frac{1 - e^{-\omega_p \cdot h}}{\omega_p} \quad \text{for all } g \tag{14b}$$

The fact that matrix factorization is performed one group at a time has been used to account for the slowing down source, [L] $\underline{\psi}$ implicitly. Since the external source term, $\underline{S}(t)$ is a known (in GAKIN II, linear) function of time, the final term in equation (13) is easily determined.

2.4 Proof of Consistency

A numerical scheme for solution of a properly posed set of equations must converge to the correct answer as successively smaller time steps are used. Assuming the time dependent multigroup diffusion equations are properly posed, consistency and stability imply

convergence (Reference 3). In this section we will show that the GAKIN II algorithm is consistent and that the truncation error is of order h^2 . The scheme will be proven stable in the next section. Note that these proofs are rigorous only for constant frequencies. However, experience has indicated that the scheme works provided the time step used is not too large.

Neglect the source term and rearrange equation (13) as follows,

$$\underline{\psi}^{j+1} - \underline{\psi}^j = [H+\Gamma+L][FF2] \underline{\psi}^{j+1} + [U][FF1] \underline{\psi}^j \quad (15)$$

or

$$\begin{aligned} \underline{\psi}^{j+1} - \underline{\psi}^j &= [H+\Gamma+L] \{h[I] - o(h^2)\} \underline{\psi}^{j+1} \\ &\quad + [U] \{h[I] + o(h^2)\} \underline{\psi}^j. \end{aligned} \quad (16)$$

Further rearrangements gives,

$$\frac{1}{h} \{\underline{\psi}^{j+1} - \underline{\psi}^j\} = [H+\Gamma+L] \underline{\psi}^{j+1} + [U] \underline{\psi}^j + o(h). \quad (17)$$

Taking the limit of this equation as $h \rightarrow 0$,

$$\frac{d}{dt} \underline{\psi} = [B] \underline{\psi}. \quad (18)$$

The numerical scheme proposed for GAKIN II is therefore consistent with the time dependent multi-group diffusion equations (spatially discretized) for any fixed h .

Equation (16) also shows that the truncation error is of order h^2 by comparison with

$$\underline{\psi}^{j+1} = e^{h[B]} \underline{\psi}^j.$$

2.5 Proof of Stability

In this section the GAKIN II algorithm is proven numerically stable. Unstable error modes cannot dominate the solution and the method will provide convergent results (since it is also consistent).

By ignoring the external source term in equation (13) and rearranging other terms, the GAKIN II algorithm may be written

$$[G_1] \underline{\psi}^{j+1} = [G_2] \underline{\psi}^j$$

where,

$$[G_1] = [I] - \{[H] + [\Gamma]\} \quad [FF2]$$

$$[G_2] = [I] + [U] [FF1] + [L] [FF2].$$

$[G_2]$ can be shown to be nonnegative for all fixed values of ω_p , h , $[U]$, and $[L]$.

For most physical problems

$$\Sigma_{tg} \geq (1-\beta) \chi_g^p v \Sigma_{fg} + \Sigma_{sgg} - 1/v_g \quad \text{for all } g.$$

Therefore, $[G_1]$ is a nonsingular matrix with positive diagonal elements and nonpositive off diagonal elements. Such a matrix can be shown to have a nonnegative inverse (Reference 4). Therefore, $[G_1]^{-1} [G_2]$ is nonnegative and irreducible and by the Perron-Frobenius Theorem has a single largest eigenvalue whose associated eigenvector has positive components. Consequently, the algorithm can be proven numerically stable for all real ω_p and any h (Reference 5).

3. Frequency Prediction

In order to solve for $\underline{\psi}$, some means of predicting the frequencies, ω_p , $p=1,2,\dots$, must be found. GAKIN II is in this sense a predictor-corrector type of algorithm. Three methods have been tested for use in GAKIN II. No completely satisfactory method universally applicable to all problems has been found. However, the method finally

chosen provides acceptable results for most problems. In any case, use of a sufficiently small time step will always provide correct results.

The first predictor tried (Reference 6) uses an approximation to the factors [FF1] and [FF2] (equations (14)). Expansion of the exponential terms in these factors,

$$[\text{FF1}] = h[\text{I}] + \frac{h^2}{2} [\Omega] + \dots \quad (21a)$$

$$[\text{FF2}] = h[\text{I}] - \frac{h^2}{2} [\Omega] + \dots, \quad (21b)$$

shows that they may be approximated (with error of order h^2) by $h[\text{I}]$. The predictor step for this method then consists of applying this approximation to the GAKIN II algorithm in the test energy group, g' ; solving for approximate flux values $\psi_{g',p}^{j+1}$; and computing frequencies, $\omega_p = \frac{1}{h} \ln(\psi_{g',p}^{j+1} / \psi_{g',p}^j)$. These predicted frequencies are then substituted and the corrector step (full GAKIN II algorithm) is carried out. If the designated test energy group is other than group one, it is necessary to approximate the slowing down source at step $j+1$ by $[\text{L}] \cdot e^{h \cdot [\Omega]} \cdot \psi^j$ (again with error of order h^2).

In the second predictor tried, the factors [FF1] and [FF2] are calculated explicitly using a frequency

$\omega_p = \frac{1}{h} \ln(\psi_{g',p}^j / \psi_{g',p}^{j-1})$ found from the results of the previous step. This predictor consists of using these values of [FF1] and [FF2] in the GAKIN II algorithm in test group, g' ; solving for approximate flux values $\psi_{g',p}^{j+1}$; and computing predicted frequencies, ω_p , as in the first method. These ω_p are then used in the corrector step. Again, series expansions of [FF1] and [FF2] show that neglecting the change in $[\Omega]$ should result in errors of order h^2 .

The third method tested and the one finally implemented in the current version of GAKIN II calculates frequencies, $\omega_p = \frac{1}{h} \ln(\psi_{g',p}^j / \psi_{g',p}^{j-1})$, from test energy groups, g' , fluxes. These frequencies are then used directly in the full GAKIN II algorithm to calculate the flux and precursor values at the end of time step $j+1$. As before, approximation of $[\Omega]$ should mean that the error is of order h^2 for this scheme.

Testing of the above prediction methods has been conducted using American Nuclear Society Benchmark Problems (Reference 7). Problem X-A3, a prompt supercritical excursion in a three region core and problem X-A2, a delayed supercritical transient in the same core have been solved using the various prediction schemes. In both problems, the initiating mechanism is a decrease in the absorption cross section in a non-central region of

the reactor. Results obtained using the frequency predictor incorporated in the present version of GAKIN II are listed in section 9.

Results for the prompt supercritical problem using all of the frequency predictors demonstrate substantial gains in time step size. Difficulties appear when the methods are applied to the slower transient. Relatively small time steps are necessary for converged solutions with all three methods and numerical instabilities occur when the same time step size is used in the second method.

The third method has been chosen for use in GAKIN II because it is the simplest and the other two methods do not result in savings worth the added computational effort. GAKIN II is an excellent means of solving rapid or moderately slow kinetics problems. However, for very slow transients there are other existing codes which may enable use of larger time step sizes.

4. Automatic Time Step Adjustment

GAKIN II incorporates an option by which the time step size may be automatically adjusted. The method used for this adjustment is based largely on a number of years of code use. Basically, tests are made to determine how rapidly the frequencies are changing in space and

time and the time step is increased or decreased accordingly. Figure 1 is a flow diagram of the time step adjustment logic.

For all space points, p , the maximum frequency $\bar{\omega}$ and the minimum frequency $\underline{\omega}$ are found. The ratio $R_s = \bar{\omega}/\underline{\omega}$ if $\bar{\omega}$ is greater than or equal to zero, or $R_s = \underline{\omega}/\bar{\omega}$ if $\bar{\omega}$ is less than zero is used to define

$$\epsilon_s = \frac{\epsilon_2}{1 - R_s} .$$

a quantity indicative of how rapidly the frequencies are varying in space (ϵ_2 is an input parameter).

In a similar fashion, at each test point, n , (WPT on input card #6), the ratio $R_{nj} = \omega_{nj}/\omega_{nj-1}$ for $|\omega_{nj}| \leq |\omega_{nj-1}|$, or $R_{nj} = \omega_{nj-1}/\omega_n$ for $|\omega_{nj}| > |\omega_{nj-1}|$, where subscript j refers to the time step, is used to define

$$\epsilon_{Tn} = \frac{\epsilon_1}{1 - R_{nj}}$$

(ϵ_1 is an input parameter). The quantity ϵ_T , the maximum over all n of ϵ_{Tn} is then used as an indication of how rapidly the frequencies are changing in time. E_x' the maximum of ϵ_s and ϵ_T (but not less than ϵ_1) and T_6 , the largest $|\omega_p \cdot h|$ are compared to determine if time step

adjustment is necessary. If $E_x \geq 2T_6$ the time step size, h , is increased according to the input parameter TSTINC. If $T_6 > E_x$ and $T_6 > \epsilon_3$ (ϵ_3 is another input parameter) the time step size, h , is decreased.

Recommended values for input constants (card 12) are:

$$\epsilon_1 = 2 \times 10^{-4} \quad (\text{EP1}),$$

$$\epsilon_2 = 1.6 \times 10^{-2} \quad (\text{EP2}),$$

$$\epsilon_3 = 5 \times 10^{-3} \quad (\text{EP3}),$$

$$\text{TSTINC} = 1.05.$$

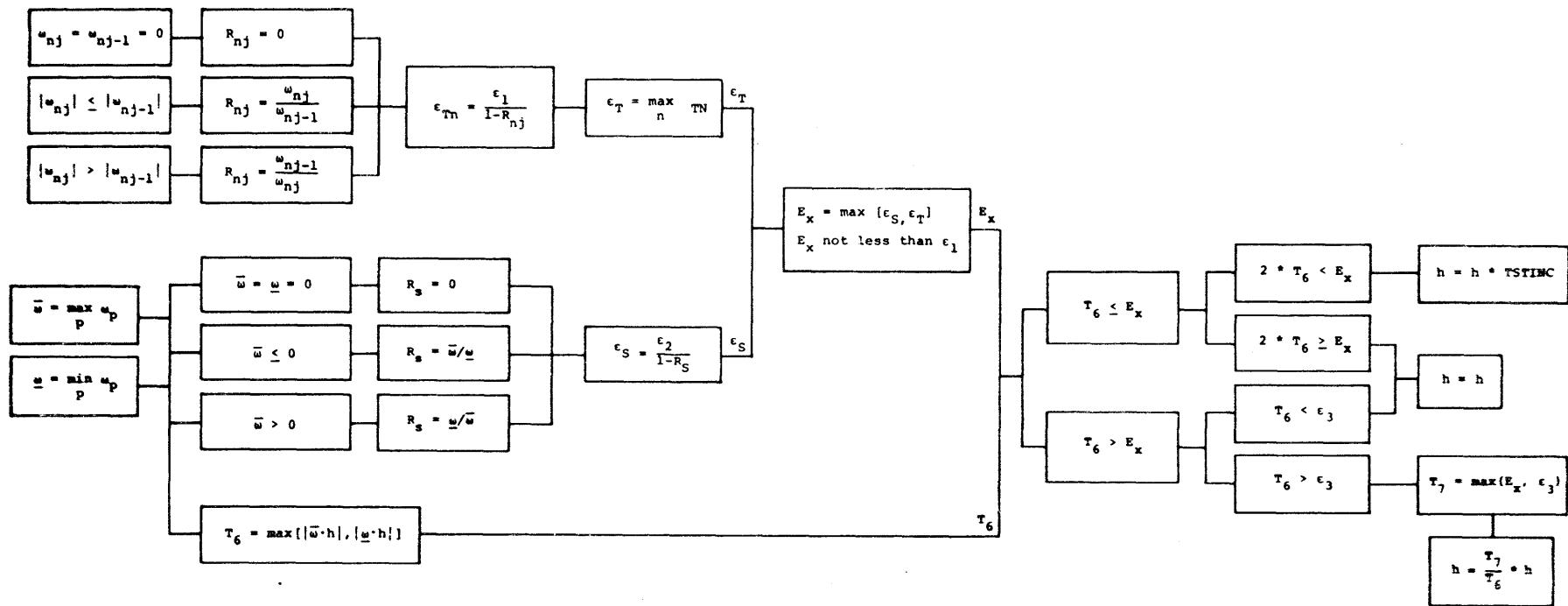


Figure 1 Automatic Time Step Adjustment Logic

5. Steady State Calculation

The initial flux-precursor vector used in GAKIN II must be the converged solution to a steady state calculation for the initial cross sections. These values may be input by the user (STEADY = 0 on Card 3) or they may be determined by the code (STEADY = 1,2). The method used to search for the steady state $\underline{\psi}$ is a simple power iteration and is discussed in this section.

Neglecting the derivative and source terms in equation (1) and using the associated precursor concentration equations (2) to define,

$$\bar{\lambda} = (1-\beta) \lambda_p + \sum_{i=1}^I \beta_i \lambda_i, \quad (22)$$

the group diffusion equations become

$$-\nabla \cdot [D(r)] \nabla \underline{\phi}(r) + [A(r)] \underline{\phi}(r) = \frac{1}{K_{\text{eff}}} \bar{\lambda} \underline{\nu \Sigma_f(r)}^T \cdot \underline{\phi}(r). \quad (23)$$

Discretizing the spatial variable as in section 2.2.1 and splitting [A] such that

$$[A] = [R] - [T],$$

where [R] contains all of the diagonal elements of [A], (23) becomes

$$\{[R] - [v]^{-1}[H]\} \underline{\phi} = [T] \underline{\phi} + \frac{1}{K_{\text{eff}}} \bar{\chi} \underline{v} \Sigma_f^T \cdot \underline{\phi}. \quad (24)$$

The terms involving the precursors are not considered since they have been accounted for implicitly in $\bar{\chi}$. Also the division by K_{eff} is actually performed and v is replaced by a new "equilibrium" value. Therefore, K_{eff} is unity after the steady state solution of equation (24) is completed.

$\{[R] - [v]^{-1}[H]\}$ is a nonsingular matrix with positive diagonal elements and nonpositive off diagonal elements. $[T] + \frac{1}{K_{\text{eff}}} \bar{\chi} \underline{v} \Sigma_f^T$ is nonnegative. Consequently, the Perron-Frobenius theorem applies and the solution, $\underline{\phi}$, corresponding to the largest eigenvalue K_{eff} has positive components.

6. Cross Sections and Input Parameters

6.1 Definitions

In terms of input parameters the variables used in Section 2 are defined in each region, R, as follows.

$$\Sigma_{\text{tr}G} = \text{SIGT}(R,G) \quad = \text{Transport cross section.}$$

$$D_G = 1/3 \Sigma_{\text{tr}G} \quad = \text{Diffusion coefficient.}$$

$$\Sigma_{\text{f}G} = \text{SIGF}(R,G) \quad = \text{Fission cross section.}$$

$$\Sigma_{\text{c}G} = \text{SIGC}(R,G) \quad = \text{Capture cross section.}$$

$$\Sigma_{\text{s}GG'} = \text{SIGX}(R,G,G') \quad = \text{Transfer cross section from group } G' \text{ to } G.$$

$$\Sigma_{\text{t}G'} = \Sigma_{\text{f}G'} + \Sigma_{\text{c}G'} + \sum_{G=1}^{\text{GRP}} \Sigma_{\text{s}GG'} \quad = \text{SIGX}(R,G',G')$$

= Total interaction cross section in group G' (GRP is the number of neutron groups).

$$\nu_G = \text{NU}(G) \quad = \text{Neutrons per fission.}$$

$$v_G = V(G) \quad = \text{Group speed.}$$

$$\chi_G^{\text{p}} = \text{CHI}(G) \quad = \text{Prompt neutron yield into group } G.$$

$$\chi_{\text{IG}}^{\text{d}} = \text{SDIN}(G,I) \quad = \text{Delayed neutron yield from delayed group } I \text{ into neutron group } G.$$

$\beta_I = \text{BETA}(I) = \text{Delay neutron fraction for delayed group } I.$

$\lambda_I = \text{DECAY}(I) = \text{Decay constant for delayed group } I.$

For each space point $P = 1, \dots, PT$

$\phi_{PG} = \text{PSI}(P, G); G=1, \dots, \text{GRP}$

$c_{PI} = \text{PSI}(P, G'); G'=\text{GRP}+I; I=1, \dots, \text{DEL}$

(DEL is the number of delayed neutron groups).

6.2 Xenon Feedback

The time rate of change of xenon can be expressed in the following form

$$\frac{d\chi}{dt} = \gamma_x \sum_{g=1}^G \Sigma_{fg} \phi_g + \lambda_I \underline{I} - \sum_{g=1}^G \sigma_{xg} \phi_g \chi \quad (25)$$

where

- χ : space point vector of xenon concentrations
- ϕ_g : the vector of pointwise fluxes for group g
- σ_{xg} : capture cross section for Xe-135 in group g
- Σ_{fg} : macroscopic fission gross section
- λ_x : xenon decay constant = $2.874 \times 10^{-5} \text{ sec}^{-1}$

- λ_I : iodine decay constant = $2.093 \times 10^{-5} \text{ sec}^{-1}$
 γ_x : cumulative yield for Xe-135
 γ_I : cumulative yield for I-135
 \underline{I} : space point vector of iodine concentration
 whose rate of change is of the form

$$\frac{d\underline{I}}{dt} = \lambda_I \sum_{g=1}^G \Sigma_{fg} \phi_g \underline{I} \quad (26)$$

For each region, r , the vectors $\underline{\chi}_{j+1}$ and \underline{I}_{j+1} can be computed for space points in r using the results of the previous step.

$$\begin{aligned} \underline{\chi}_{j+1} = & e^{\alpha_x h} \underline{\chi}_j + \frac{\lambda_I}{\alpha_x - \lambda_I} (e^{-\lambda_I h} - e^{-\alpha_x h}) \underline{I}_j \quad (27) \\ & + \left(\frac{\gamma_x + \gamma_I}{\alpha_x} \right) (1 - e^{-\alpha_x h}) - \left(\frac{\gamma_I}{\alpha_x - \lambda_I} \right) (e^{-\lambda_I h} - e^{-\alpha_x h}) \bar{S}_f \end{aligned}$$

$$\underline{I}_{j+1} = e^{-\lambda_I h} \underline{I}_j + \left(\frac{1 - e^{-\lambda_I h}}{\lambda_I} \right) \gamma_I \bar{S}_f \quad (28)$$

where

$$\alpha_x = \sum_{g=1}^G \sigma_{xg} \bar{\phi}_{gj+1} + \lambda_x$$

$\bar{\phi}_{g,j}$ is the volume averaged flux over region r for group g and step j .

$$\bar{S}_f = \sum_{g=1}^G [\Sigma_{fg} \left(\frac{\bar{\phi}_{g,j} - \bar{\phi}_{g,j+1}}{2} \right)]$$

In GAKIN II the xenon concentration, XENON(R) is calculated for each region, R, and the iodine concentration, IODINE(R), is calculated for each region, R.

6.3 Time Dependent Cross Section Variation

The time variation in the cross sections may be either linear or quadratic at the users choice. As assumed in equation (9), the cross sections are constant over the interval of integration. Thus, the cross sections are time dependent step functions calculated in the following manner for each region R:

$$\text{SIGX}(R, G, G')_{j+1} = \text{SIGX}(R, G, G')_0 + \text{CXL}(R) \tau + \text{CXQ}(R) \tau^2$$

$$\text{SIGT}(R, G)_{j+1} = \text{SIGT}(R, G)_0 + \text{CTL}(R, G) \tau + \text{CTQ}(R, G) \tau^2$$

$$\text{SIGC}(R, G)_{j+1} = \text{SIGC}(R, G)_0 + \text{CCL}(R, G) \tau + \text{CCQ}(R, G) \tau^2 +$$

$$\text{XABS}(R, G) \cdot \text{XENON}(R)$$

$$\text{SIGF}(R,G)_{j+1} = \text{SIGF}(R,G)_0 + \text{CFL}(R,G) \tau + \text{CFQ}(R,G) \tau^2$$

where:

$$\tau = \frac{t - t_z}{\Delta \text{TZ}}$$

t_z : time at the beginning of the time zone.

t : time at step j .

ΔTZ : length of the time zone.

$\text{CXL}(R)$, $\text{CXQ}(R)$, $\{\text{CTL}(R,G)$, $\text{CTQ}(R,G)$, $\text{CCL}(R,G)$, $\text{CCQ}(R,G)$, $\text{CFL}(R,G)$, $\text{CFQ}(R,G) \mid G=1, \dots, \text{GRP}\}$, are constants specified for each time zone.

$\text{XENON}(R)$ is the xenon build-up in region R as calculated in equation (27).

$\text{SIGX}(R,G,G')$, $\text{SIGT}(R,G)$, $\text{SIGC}(R,G)$, $\text{SIGF}(R,G)$ are defined as in Section 6.1.

$\text{XABS}(R,G)$ is σ_{xg} in Section 6.2, the xenon capture cross section in group G and region R .

7. Summary of Changes to GAKIN

The most significant change in the original code, GAKIN, as described in Reference 1 is the replacement of the iterative scheme for frequency prediction by an explicit, order h^2 method. The algorithm itself has been altered to account for the slowing down source implicitly. The steady state calculation has been changed to account for the precursor concentrations implicitly and to eliminate calculation of them during flux iteration. A minor alteration has been made to more formally account for the effect of xenon buildup on cross-sections in that the xenon capture cross section has been made group dependent.

A number of programming changes have been made. The present version of GAKIN II has been programmed for use on the IBM-370 model 165 computer with Fortran G or H compiler. Several subroutines have been unified or eliminated in addition to those eliminated pursuant to the changes discussed above. The code has been restructured and object time dimensioning has been incorporated. Consequently, recompilation of only a short MAIN sub-program results in minimal storage costs for a class of problems to be solved. Changes in input format are detailed in Section 8.4.

8. User Information

8.1 General

GAKIN II is presently in load module form compiled in FORTRAN H(opt=2). The current dimensions can accomodate problems with 10 regions (M1), 10 neutron energy groups (M2), 6 delayed neutron groups (M4), 50 test points (M7), and 100 space points (M5). The number of edits for each time zone is limited to fifty. To increase or decrease the dimensions, the user need only recompile the short MAIN program with appropriate dimensions. The number of bytes of core storage necessary for use of the code can be approximated by

$$100,000 + 8[P(G+D) + 2GD + 9G + G(G+1) + 26R + 19RG + RG^2 + 11P + 4PG + 2N + 50]$$

where,

R is the number of regions,

G is the number of neutron energy groups,

D is the number of delayed groups,

P is the number of space points, and

N is the number of test points.

Computation time per step is roughly approximated by $2 \times 10^{-4} [P(G + .3D)]$ seconds.

Input data is checked extensively for errors and execution is prevented if any are found. Problems may be stacked, i.e., the code automatically seeks new input data after completion of a problem. Sections 8.2 and 8.3 describe the input format in detail.

8.2 Detailed Input Specifications

CARD #1 - Problem Title. Printed at the head of each output sequence. (12A6)

CARD #2 - Problem Dimensions and Internal Controls.

{GRP, THG, GF, DEL, REG, NUM, NCOMP, GEOM, BCL, BCR, MTZ, XEN}, (12I6)

GRP: Total number of neutron groups. ($0 < \text{GRP} \leq M2^*$)

THG: Number of the group for which the frequencies are to be calculated and tested. ($0 < \text{THG} < \text{GRP}$). For two group problems the last group is taken to be the thermal group and it is recommended that $\text{THG}=\text{GRP}=2$. In systems with more than one thermal group some experimentation may be required in the selection of THG.

GF: Number of fast groups. GF is used in the standard cross section input card #16. If the fast transfer matrix option, card #16, is not desired enter a zero or blank for GF. ($0 \leq \text{GF} \leq \text{GRP}$).

* See Section 8.1 for dimension limits

DEL: Total number of delayed neutron groups.
($0 \leq \text{DEL} \leq \text{M4}^*$)

REG: Total number of homogeneous regions.
($0 < \text{REG} \leq \text{M1}^*$)

NUM: Total number of space points at which the frequencies are to be computed and tested. These points are referred to as "test points".
($0 < \text{NUM} \leq \text{M7}^*$, $\text{NUM} \geq \text{REG}$).

NCOMP: Total number of compositions. ($0 < \text{NCOMP}$).

GEOM: Geometry control
0 - Slab; 1 - Cylinder; 2 - Sphere

BCL: Left (or bottom) boundary condition = 0 - zero flux

BCR: Right (or top) boundary condition = 1 - zero gradient

MTZ: (a) If $\text{MTZ} > 0$ punch restart information
(b) $|\text{MTZ}| = \text{NTZ} =$ total number of time zones. Each time zone can have unique properties of time dependent cross sections, external sources, time steps and print-out control.

XEN: Is feedback from the buildup in xenon to be computed?
0 - No, 1 - Yes.

CARD #3 - Steady State Calculation and number of space points {STEADY, PUNBAL, TIGHT1, TIGHT2, TIGHT3, PT}, (2I6,3E12.6, I6)

STEADY: Is there is to be a search for the flux distribution and v which match the initial cross sections?

* See Section 8.1 for dimension limits.

- 0 - No,
- 1 - Yes, initial estimate entered on card #20,
- 2 - Yes, flat flux initial estimate,
- 3 - No, but initial precursor concentrations are to be calculated from the fluxes entered on card #20.

PUNBAL: If an initializing calculation is to be done ($STEADY \geq 1$) should the resulting flux and precursor distribution (steady state distribution) be punched?

0 - No, 1 - Yes,

TIGHT1

TIGHT2 Convergence criterion for the steady state solution.

TIGHT3

In order for the $j+1$ steady state iteration to be acceptable it is necessary that the following be satisfied.

$$0 < |K_{\text{eff}}^{j+1}/K_{\text{eff}}^j - 1.0| < \text{TIGHT1}$$

$$0 < |K_{\text{eff}}^{j+1} - 1.0| < \text{TIGHT2}$$

$$0 < |\psi_q^{j+1}/\psi_q^j - 1.0| < \text{TIGHT3} \text{ for all test points } q.$$

where K_{eff}^j is the K-effective at iteration j and ψ_q^j is the THG group flux at point q and iteration j .

PT: Number of space points (The left hand boundary of the problem is mesh point number one).

CARD #4 - Region boundaries. {PB(R) | R = 1, ..., REG}, (12I6).

PB(R): Number of the mesh point at the right hand boundary of region R. The left hand boundary of region one is assumed to be mesh point number one. (Note that PB(REG) = PT)

CARD #5 - Region Lengths. {LR(R) | R = 1, ..., REG}, (6E12.5).

LR(R): The length of region R (cm).

CARD #6 - Test Points. {WPT(N) | N = 1, NUM}, (12I6)

WPT(N): Space point to be used as test points in the calculation and checking of the frequencies and in testing convergence of the steady state solution.

If DEL = 0 then cards #7, #8, and #9 are not to be included.

CARD #7 - Delay Fraction, {BETA(G') | G' = 1, ..., DEL}, (6E12.5).

BETA(G'): Delay fraction from fission into delay group G'.

CARD #8 - Yield Fraction. {SDIN(G,G') | G' = 1, ..., DEL, G=1, ..., GRP}, (6E12.5) (Start a new card for each neutron group G).

SDIN(G,G'): Fractional yield in group G from delayed group G'.

CARD #9 - Decay Constant. {DECAY(G') | G' = 1, ..., DEL}, (6E12.5).

DECAY(G'): Decay constant for delayed group G'.

CARD #10 - Fission Yield. {CHI(G) | G = 1, ..., GRP}

CHI(G): Yield from fission in group G.

CARD #11 - Neutron Speed. {V(G) | G = 1, ..., GRP}.

V(G): Average neutron speed for group G (cm/sec). This array should be in descending order with largest value first. All subsequent reference to group indexes assume the same ordering.

CARD #12 - Frequency Prediction and Time Step Adjustment Controls {EP1, EP2, EP3, IEP4, IEP6, TSTINC}, (3E12.5, 2I12, E12.5)

EP1, EP2, EP3: These parameters are explained in Section 4 and are used for testing related to time step adjustment. Recommended values:

$$EP1 = .2 \times 10^{-3}$$

$$EP2 = .16 \times 10^{-1}$$

$$EP3 = .5 \times 10^{-2}$$

IEP4: Set IEP4 = 0 unless the frequencies are to be set to zero and the frequency prediction is to be bypassed (IEP4 = 1).

IEP6: = 0 auto. time step adjustment to be used.

= 1 no time step adjustment

TSTINC: Increase in time step size per time step (Recommended value 1.05).

CARD #13 - Composition Assignments. {NCMP(R) | R = 1, ..., REG}, (12I6).

NCMP(R): Number of the composition assigned to region R. One value for each region. $NCMP(R) \leq NCOMP$ for all R.

The sequence of cards #14 thru #18 is repeated for each composition. The ordering of compositions in this set of cards must be consistent with the numbers used to identify the compositions on card #13.

GAKIN makes no use of the $(n, 2n)$, (n, α) , or (n, p) reaction rates or self-shielding factors, hence these terms are not included in the input.

CARD #14 - Composition I.D. and Transfer Matrix Control. {NUCNAM, I1, I2, I3}, (15A4, 3I4).

NUCNAM: Composition name used as identification during edit.

I1: Not used.

I2: = 0 - No fast and no full transfer matrix available. Do not include cards #16 and #17.

= 1 - Only fast transfer matrix available (i.e., only transfer from G into G' where $G=1, \dots, GRP$ and $G'=G+1, \dots, GF+1$).

= 2 - Full transfer matrix is to be read.

I3: Not used.

Repeat card #15 for each neutron group $G=1, \dots, GRP$.

CARD #15 - Composition Macroscopic Cross Sections. $\{v(G), \Sigma^f(G), \Sigma^c(G), \Sigma^{tr}(G), \Sigma(n, 2n)(G), \Sigma(G \rightarrow G+1)\}$, (5E12.5).

- $\nu(G)$: Neutrons per fission.
 $\Sigma^f(G)$: Macroscopic fission cross section.
 $\Sigma^c(G)$: Macroscopic capture cross section.
 $\Sigma^{tr}(G)$: Macroscopic transport cross section.
 $\Sigma^{(n,2n)}(G)$: Not used in GAKIN.
 $\Sigma(G \rightarrow G+1)$: Sum of elastic and inelastic macroscopic scattering cross sections for energy transfer from group G to G+1.

After the data for composition M has been read, then all regions specified, on card #13, to contain composition M (i.e., all R such that $M = \text{NCMP}(R)$) receive the following storage instruction:

- $\nu(G) \rightarrow \text{NU}(R,G)$
 $\Sigma^f(G) \rightarrow \text{SIGF}(R,G)$
 $\Sigma^{tr}(G) \rightarrow \text{SIGT}(R,G)$
 $\Sigma^c(G) \rightarrow \text{SIGC}(R,G)$
 $\Sigma(G \rightarrow G') \rightarrow \text{SIGX}(R,G',G)$

CARD #16 - Fast Transfer Matrix (supply this card only if $I2=1$ and $GF \neq 0$). $\{\Sigma(G \rightarrow G') \mid G'=G+1, \dots, GF+1; G=1, \dots, GF\}$, (6E12.5) (Start a new card for each G).

$\Sigma(G \rightarrow G')$: Sum of elastic and inelastic macroscopic scattering cross sections for energy transfer from G to G'.

If $GF=GRP$ then enter a zero for $\Sigma(GF \rightarrow GF+1)$.

CARD #17 - Full Transfer Matrix (supply this card only if I2=2).
 $\{\Sigma(G \rightarrow G') \mid G'=1, \dots, \text{GRP}; G=1, \dots, \text{GRP}\}$, (6E12.5)
 (Start a new card for each group G).
 $\Sigma(G \rightarrow G')$: Same definition as for card #16.

Supply cards #18 and #19 only if XEN \neq 0.

CARD #18 - Fission Yields. {GAMAX, GAMAI}, (2E12.5)

GAMAX: Fission Yield for Xe-135

GAMAI: Fission Yield for I-135.

CARD #19 - Xenon and Iodine Parameters
 $\{\text{XENON}(R), \text{IODINE}(R), \text{XABS}(R,G), G=1, \dots, \text{GRP}\}$.

XENON(R): Initial Xenon concentration in region R, atoms/cm³. The initial cross sections must reflect the effect of this concentration.

IODINE(R): Initial Iodine concentration in region R atoms/cm³.

XABS(R,G): Xenon capture cross section in region R in group G, barns.

(Start a new card for each region).

CARD #20 - Initial Flux Distribution. $\{\text{PSI}(P,G) \mid P=1, \dots, \text{PT}; G=1, \text{GRP}\}$, (6E12.5).

The initial flux distribution is read in point-wise for each group (start a new card for each group).

If a steady state calculation is not performed (i.e., STEADY=0) then the initial precursor concentrations are read in immediately following the fluxes.

$\{\text{PSI}(P,G) \mid P=1, \dots, \text{PT}; G=\text{GRP}+1, \dots, \text{GRP}+\text{DEL}\}$, (6E12.5).

Omit Card #20 if STEADY=2.

The sequence of cards #21 thru #33 must be repeated for each time zone. Start with the first zone and arrange in increasing order. The problem will terminate at the end of time zone NTZ.

CARD #21 - Time Zone Control Card {HBEGIN, IH, TZ, IPRN, NUM2, NTAG, SORCE, IEP4, IEP6}
(E12.5, I12, E12.5 6I6)
IEP4 & IEP6 are repeated here for possible alteration in each time zone (see Card #12).

HBEGIN: Initial time step size (Sec.).

IH: = 0 Time step is kept the same as at the end of the preceding time zone.

= 1 Step size set equal to HBEGIN.

TZ: |TZ| = Time at the end of this zone.
TZ > 0 precursor concentrations printed at each edit time.
TZ < 0 precursor concentrations printed at end of time zone only.

IPRN: In this time zone every IPRNth step will be edited. If IPRN=0 this edit criterion is ignored.

NUM2: (a) If NUM2 < 0 then NUM2 is the number of print times to be read in on card #22.

(b) If NUM2 > 0 then print-outs will occur at NUM2 evenly spaced intervals throughout the time zone. Do not supply card #22.

(c) If NUM2=0 this output option is ignored. Do not supply card #22.

$$(|\text{NUM2}| \leq 50)$$

NTAG: Time dependent cross section control index.

(a) If NTAG=0 then there are no time dependent cross sections in this time zone. Do not supply cards #23 thru #30.

(b) If $NTAG = -1$ then the same time dependent cross section parameters are used for this time zone as in the previous zone. Do not supply cards #23 thru #30.

(c) If $NTAG > 0$ then the time dependent cross section parameters are to be read in for $NTAG$ regions. Only regions with changing cross sections need be considered. The omitted regions will be assumed to have zero change in their cross section.

SORCE: External source control index.

(a) If $SORCE = 0$ then there are no external sources in this time zone. Do not supply cards #31, #32 or #33.

(b) If $SORCE = -1$ then the external source parameters are the same for this time zone as for the previous zone. Do not supply cards #31, #32 or #33.

(c) If $SORCE > 0$ then the external source parameters are to be read in for $SORCE$ regions. Only regions with nonzero sources need be considered. The omitted regions will be assumed to have zero external sources.

CARD #22 - Print Timing (Do not use this card if $NUM2 \geq 0$).
{STPRN(N) | $N=1, -NUM2$ }.

STPRN(N): The program will automatically adjust the time step so that a solution is calculated and printed at the time STPRN(N).

$TZ_0 < STPRN(N) < STPRN(N+1) < TZ_1$, $N=1, \dots, -NUM2$
where TZ_0 is the time at the beginning of the time zone and $TZ_1 = TZ$ is the time at the end of the zone.

The sequence of cards #23 thru #30 should be repeated $NTAG$ times. Supply this sequence of cards only if $NTAG > 0$.

CARD #23 - Time Dependent Cross Section Control Card.
 {R, TAGX(R), TAGT(R), TAGC(R), TAGF(R)},
 (516).

R: Region number for which the following data applies.

TAGX(R): Is the transfer cross section changing with time.

TAGT(R): Is the transport cross section changing with time.

TAGC(R): Is the capture cross section changing with time.

TAGF(R): Is the fission cross section changing with time.

= 0 No.

= 1 Yes - linear change only.

= 2 Yes - linear and quadratic variation with time.

If t_j is the time at step j , TZ_0 and TZ_1 are respectively the time at the beginning and end of the time zone, then the time dependent changes in the cross sections can be expressed as follows:

$$\Delta TZ = TZ_1 - TZ_0 \quad \tau = (t_j - TZ_0) / \Delta TZ$$

$$SIGX(R, G, G')_{j+1} = SIGX(R, G, G')_0 + CXL(R) \tau + CXQ(R) \tau^2$$

$$SIGT(R, G)_{j+1} = SIGT(R, G)_0 + CTRL(R, G) \tau + CTRQ(R, G) \tau^2$$

$$SIGC(R, G)_{j+1} = SIGC(R, G)_0 + CCL(R, G) \tau + CCQ(R, G) \tau^2$$

$$SIGF(R, G)_{j+1} = SIGF(R, G)_0 + CFL(R, G) \tau + CFQ(R, G) \tau^2$$

- CARD #24 - Time Variations in the Transfer Cross Section. Supply this card if TAGX(R) = 1 or 2. CXL(R), CXQ(R), (2E12.5).
- CXL(R): Total linear change in SIGX(R,G,G') over the time interval $\Delta T Z$.
- CXQ(R): Total quadratic change in SIGX(R,G,G') over the time interval $\Delta T Z$.
- CARD #25 - Linear Variations in the Transport Cross Section. Supply this card if TAGT(R) = 1 or 2. CTRL(R,G)/G=1,...,GRP, (6E12.5).
- CTRL(R,G): Total linear change in SIGT(R,G) within the time interval $\Delta T Z$.
- CARD #26 - Quadratic Variations in the Transport Cross Section. Supply this card only if TAGT(R) = 2. CTRQ(R,G)/G=1,...,GRP, (6E12.5).
- CTRQ(R,G): Total quadratic change in SIGT(R,G) in the time interval $\Delta T Z$.
- CARD #27 - Linear Variations in the Capture Cross Section. Supply this card if TAGC(R) = 1 or 2. CCL(R,G)/G=1,...,GRP, (6E12.5).
- CCL(R,G): Total linear change in SIGC(R,G) in the time interval $\Delta T Z$.
- CARD #28 - Quadratic Variations in the Capture Cross Section. Supply this card only if TAGC(R) = 2. CCQ(R,G)/G=1,...,GRP, (6E12.5).
- CCQ(R,G): Total quadratic change in SIGC(R,C) in the time interval $\Delta T Z$.
- CARD #29 - Linear Variation in the Fission Cross Section. Supply this card if TAGF(R) = 1 or 2. CFL(R,G)/G=1,...,GRP, (6E12.5).

CCQ(R,G): Total linear change in SIGF(R,G) in the time interval ΔT_Z .

CARD #30 - Quadratic Variation in the Fission Cross Section. Supply this card only if TAGF(R) = 2. {CFQ(R,G)/G=1,GRP}, (6E12.5).

CFQ(R,G): Total quadratic change in SIGF(R,G) in the time interval ΔT_Z .

The sequence of cards #31 thru #33 is repeated SORCE times. Supply this sequence of cards only if SORCE > 0. The sequence need not be repeated for any region with a zero external source. All omitted regions are assumed to have zero source.

CARD #31 - External Source Input Control Card. {R, SOR(R)}, (2I6).

R: Region for which the following data applies.

SOR(R): = 0 No external source for this region (equivalent to the omission of the sequence for this region).

= 1 Source input for each group and each interior point of the region.

= 2 Source input for each group. The one value is taken to be constant over the interior of the region.

CARD #32 - Pointwise External Source Input. Supply this card only if SOR(R) = 1. {SRCEO(P,G), SRCE1(P,G)/P interior to R in increasing order, G=1,...,GRP}, (6E12.5). (Start a new card for each group).

SRCEO(P,G): Initial external source space point P, group G.

SRCE1(P,G): Total linear change in SRCEO(P,G) in the time interval ΔT_Z .

CARD #33 - Region Constant External Source. Supply this card only if $SOR(R) = 2$. { $SRCEO(R,G)$, $SRCE1(R,G)/G=1,\dots,GRP$ }, (6E12.5). (Three sets of two numbers per card, i.e., three groups per card).

$SRCEO(P,G) = SRCEO(R,G)$, and $SRCE1(P,G) = SRCE1(R,G)$ for all P interior to R.

$SRCEO(P,G) =$ and $SRCE1(P,G)$ are the same as defined on card #32.

Card 1	
Word	1
Column	2-72
Format	Alpha-Numeric
	Title Card
Symbol	

Card 2						
Word	1	2	3	4	5	6
Column	1-6	7-12	13-18	19-24	25-30	31-36
Format	Integer	Integer	Integer	Integer	Integer	Integer
	Number of neutron groups	Test group	Total number of fast groups	Number of delayed groups	Number of regions	Number of test points
Symbol	GRP	THG	GF	DEL	REG	NUM

Card 2
(cont.)

Word	7	8	9	10	11	12
Column	37-42	43-48	49-54	55-60	61-66	67-72
Format	Integer	Integer	Integer	Integer	Integer	Integer
	Number of compositions	Geometry 0 - Slab 1 - Cylinder 2 - Sphere	Left (or bottom) boundary 0 - Zero flux 1 - Zero gradient	Right (or top) boundary	Number of time zones <0 no punch >0 punched output	Xenon feedback 0 - no 1 - yes
Symbol	NCOMP	GEOM	BCL	BCR	MTZ	XEN

Card 3

Word	1	2	3	4	5	6
Column	1-6	7-12	13-24	25-36	37-48	49-54
Format	Integer	Integer	Decimal	Decimal	Decimal	Integer
	Steady state calculation 0 - no 1 - yes 2 - yes 3 - no	Punch steady state fluxes 0 - no 1 - yes	Convergence criterion for steady state calculation			Number of space mesh points
Symbol	STEADY	PUNBAL	TIGHT1	TIGHT2	TIGHT3	PT

Card 4 Twelve words per card.

Word	1	2				REG
Column	1-6	7-12				
Format	Integer	Integer				Integer
	Right hand boundary, first region	Right hand boundary, second region	. . .			Right hand boundary, last region PB (REG)=PT
Symbol	PB(1)	PB(2)				PB (REG)

Card 5 Six words per card.

Word	1	2				REG
Column	1-12	13-24				
Format	Decimal	Decimal				Decimal
	Length of first region (cm)	Length of second region, (cm)	. . .			Length of last region, (cm)
Symbol	LR(1)	LR(2)				LR (REG)

Card 6 Twelve words per card.

Word	1	2		NUM
Column	1-6	7-12		
Format	Integer	Integer		Integer
	First test point	Second test point	...	Last test point WPT(NUM) ≤ PT
Symbol	WPT(1)	WPT(2)		WPT(NUM)

Card 7 Supply this card only if DEL>0, six words per card.

Word	1	2		DEL
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Delay fraction first delay group	Delay fraction second delay group	...	Delay fraction last group
Symbol	BETA(1)	BETA(2)		BETA(DEL)

Supply this card only if DEL > 0, six words per card. Start a new card for each neutron group G. (G = 1,2,...,GRP)

Card 8

Word	1	2		DEL
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Yield fraction in group G from delayed group 1.	Yield fraction in group G from delayed group 2.	...	Yield fraction in group G from delayed group DEL.
Symbol	SDIN(G,1)	SDIN(G,2)		SDIN(G,DEL)

Card 9

Supply this card only if DEL>0, six words per card.

Word	1	2		DEL
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Decay const. for first delayed group	Decay const. for second delayed group	...	Decay const. for last delayed group
Symbol	DECAY(1)	DECAY(2)		DECAY(DEL)

Card 10 Six words per card.

Word	1	2		GRP
Column	1-12	13-24		
Format				Decimal
	Fission yield first group	Fission yield second group	. . .	Fission yield last group
Symbol	CHI(1)	CHI(2)		CHI(GRP)

Card 11 Six words per card.

Word	1	2		GRP
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Neutron speed first group (cm/sec)	Neutron speed second group (cm/sec)	. . .	Neutron speed last group (cm/sec)
Symbol	V(1)	V(2)		V(GRP)

Card 12

Word	1	2	3	4	5	6
Column	1-12	13-24	25-36	37-48	149-60	61-72
Format	Decimal	Decimal	Decimal	Integer	Integer	Decimal
	Adjustable time step parameters.			Frequency Prediction: 0 - used 1 - by-passed	Time step: 0 - Adjusted 1 - Constant	Rate of time step increase
Symbol	EP1	EP2	EP3	IEP4	IEP6	TSTINC

Card 13 Twelve words per card.

Word	1	2		REG
Column	1-6	7-12		
Format	Integer	Integer		Integer
	Number of the composition assigned to first region	Number of the composition assigned to second region		Number of the composition assigned to the last region
Symbol	NCMP (1)	NCMP (2)		NCMP (REG)

Card 14 Repeat the sequence #14 thru #18 for each composition.

Word	1		2	3	4
Column	1-6	7-60	61-64	65-68	69-72
Format	A6	Alpha-Numeric	Integer	Integer	Integer
	Composition I.D.	Additional I.D.	Not used	0 - No tran. matrix 1 - Only fast tran. matrix 2 - Full tran. matrix	
Symbol	NUCNAM		I1	I2	I3

Card 15 Supply this card for each group G, (G = 1, 2, ..., GRP)

Word	1	2	3	4	5	6
Column	1-12	13-24	25-36	37-48	49-60	61-72
Format	Decimal	Decimal	Decimal	Decimal	Decimal	Decimal
	Neutrons per fission	Macroscopic fission	Macroscopic capture	Macroscopic transport	Not used	Macroscopic transfer from G to G+1
Symbol	$\nu(G)$	$\Sigma^f(G)$	$\Sigma^c(G)$	$\Sigma^{tr}(G)$	$\Sigma^{(n, 2n)}(G)$	$\Sigma(G \rightarrow G+1)$

Card 16 Supply this card only if I2 = 1. Six words per card. Start a new card for each group G. (G = 1, 2, ..., GRP).

Word	1	2		
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Macroscopic transfer	Macroscopic transfer	...	Macroscopic transfer
Symbol	$\Sigma(G \rightarrow G+1)$	$\Sigma(G \rightarrow G+2)$		$\Sigma(G \rightarrow GF+1)$

Card 17 Full Transfer Matrix. Supply this card only if I2 = 2. Six words per card. Start a new card for each group G. (G = 1, 2, ..., GRP).

Work	1	2		GRP
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
			...	
Symbol	$\Sigma(G \rightarrow 1)$	$\Sigma(G \rightarrow 2)$		$\Sigma(G \rightarrow GRP)$

Card 18 Supply this card only if XEN = 1.

Word	1	2	
Column	1-12	13-24	
Format	Decimal	Decimal	
	Fission yield for ^{135}Xe	Fission yield for ^{135}I	
Symbol	GAMAX	GAMAI	

Card 19 Supply this card only if XEN = 1. Six words per card. Start a new card for each region R. (R = 1, 2, ..., REG).

Word	1	2	3	4		GRP
Column	1-12	13-24	25-36	37-48		
Format	Decimal	Decimal	Decimal	Decimal		Decimal
	Initial ^{135}Xe concentration	Initial ^{135}I concentration	Xenon capture cross section	. . .		
Symbol	XENON (R)	IODINE (R)	XABS (R, 1)			XABS (R, GRP)

Six words per card. Start a new card for each group G. (G = 1,2,...,K).

Card 20 K = GRP if STEADY=1,3; K = GRP+DEL if STEADY = 0; Omit card 20 if STEADY=2.

Word	1	2		PT
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Initial flux group G, point 1	Initial flux group G, point 2	. . .	Initial flux group G point PT
Symbol	PSI(1,G)	PSI(2,G)		PSI(PT,G)

Card 21 Repeat the sequence of cards #21 thru #33 once for each time zone.

Word	1	2	3	4	5	6
Column	1-12	13-24	25-36	37-42	43-48	49-54
Format	Decimal	Integer	Decimal	Integer	Integer	Integer
	Initial time step	Initial time step control 0 - H = HP 1-H=HBEGIN	Time at the end of the time zone. Precursor conc. printed >0, each edit <0, at TZ only	Print every IPRN th step	Number of pring times > 0 Calcul- ate < 0 Read card #22	# of regions with chang- ing cross sections (-1 if same as last time zone.)
Symbol	HBEGIN	IH	TZ	IPRN	NUM2	NTAG

Card 21 (cont.)

Word	7	8	9	
Column	55-60	61-66	67-72	
Format	Integer	Integer	Integer	
	External source control index 0 - No 1 - Yes	See Card #12	See Card #12	
Symbol	SORCE	IEP4	IEP6	

Card 22 Supply this card only if NUM2 < 0. Six words per card.

Word	1	2		NUM2
Column	1-12	13-24		
Format	Decimal	Decimal		
	Print time number one	Print time number two	. . .	Last print time for this time zone
Symbol	STPRN (1)	STPRN (2)		STPRN (NUM2)

Card 23 Repeat the card sequence #23 through #30 NTAG times. If $NTAG \leq 0$ omit the entire sequence.

Word	1	2	3	4	5	
Column	1-6	1-12	13-18	19-24	25-30	
Format	Integer	Integer	Integer	Integer	Integer	
	Region for which the following data applies	Time variation in SIGX(R)?	Time variation in SIGT(R)?	Time variation in SIGC(R)?	Time variation in SIGF(R)?	
		0 - no time dependent change; 1 - linear change with time; 2 - quadratic change with time.				
Symbol	R	TAGX(R)	TAGT(R)	TAGC(R)	TAGF(R)	

Card 24 Supply this card only if TAGX(R) = 1 or 2

Word	1	2	
Column	1-12	13-24	
Format	Decimal	Decimal	
	Total linear change in the transfer cross section	Total quadratic change in the transfer cross section	
Symbol	CXL(R)	CXQ(R)	

Card 25 Supply this card only if TAGT(R) = 1 or 2. Six words per card.

Word	1	2		GRP
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Total linear change in the transport cross section.			
	Group #1	Group #2		Last Group, GRP
Symbol	CTRL(R,1)	CTRL(R,2)	. . .	CTRL(R,GRP)

Card 26 Supply this card only if TAGT(R) = 2. Six words per card.

Word	1	2		GRP
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Total quadratic change in the transport cross section.			
	Group #1	Group #2		Last Group, GRP
Symbol	CTRQ(R,1)	CTRQ(R,2)	. . .	CTRQ(R,GRP)

Card 27 Supply this card only if TAGC(R) = 1 or 2. Six words per card.

Word	1	2		GRP
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Total linear change in the capture cross section.			
	Group #1	Group #2		Last Group, #GRP
Symbol	CCL(R,1)	CCL(R,2)	. . .	CCL(R,GRP)

Card 28 Supply this card only if TAGC(R) = 2. Six words per card.

Word	1	2		GRP
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Total quadratic change in the capture cross section.			
	Group #1	Group #2		Last Group, #GRP
Symbol	CCQ(R,1)	CCQ(R,2)	. . .	CCQ(R,GRP)

Card 29 Supply this card only if TAGF(R) = 1 or 2. Six words per card.

Word	1	2		GRP
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Total linear change in the fission cross section.			
	Group #1	Group #2		Last Group, #GRP
Symbol	CFL(R,1)	CFL(R,2)	. . .	CFL(R,GRP)

Card 30 Supply this card only if TAGF(R) = 2. Six words per card.

Word	1	2		GRP
Column	1-12	13-24		
Format	Decimal	Decimal		Decimal
	Total quadratic change in the fission cross section.			
	Group #1	Group #2		Last Group, #GRP
Symbol	CFQ(R,1)	CFQ(R,2)	. . .	CFQ(R,GRP)

Card 31 Repeat the card sequence #31 thru #33 SORCE times. If SORCE = 0 omit the entire sequence.

Word	1	2
Column	1-6	7-12
Format	Integer	Integer
	Region for which the following data applies	= 0: no source for region R = 1: pointwise source read in (Card #32) = 2: constant source for region R (Card #33)
Symbol	R	SOR(R)

Card 32 Supply this card only if SOR(R) = 1. Six words per card.
 $K = PB(R-1) + 1.$

Word	1	2	3	4
Column	1-12	13-24	25-36	37-48
Format	Decimal	Decimal	Decimal	Decimal
	Initial external source point K group G	Total linear change in source point K group G	Initial external source point K+1 group G	Total linear change in the source point K+1 group G
Symbol	SRCEO(K,G)	SRCEL(K,G)	SRCEO(K+1,G)	SRCEL(K+1,G)

Card 32 (cont.) Repeat card #32 once for each group G. ($G = 1, 2, \dots, GRP$)

Word				
Column				
Format		Decimal	Decimal	
	. . .	Initial external source point PB(R)-1, group G	Total linear change in the source point PB(R)-1, group G	
Symbol		SRCEO(PB(R)-1,G)	SRCEL(PB(R)-1,G)	

Card 33 Supply this card only if $SOR(R) = 2$. Two words per card. Repeat the card once for each group G. ($G = 1, 2, \dots, GRP$)

Word	1	2	
Column	1-12	13-24	
Format	Decimal	Decimal	
	Initial external source for region R, group G	Total linear change in source region R, group G	
Symbol	SRCEO(R,G)	SRCEL(R,G)	

8.4 Edit Description

At the intervals specified on Card 21 or 22 the following information will be printed.

- 1) Problem Title.
- 2) Step Number and Time Zone Number.
- 3) Time.
- 4) Time step size (this number will not reflect adjustments made in the time step size necessary to accomodate edit times or time zone endings).
- 5) Frequencies, ω , and $e^{\omega \cdot h}$ at each test point.
- 6) Neutron fluxes at each point in each energy group.
- 7) Precursor concentrations at each point in each group (this output may be suppressed except at the end of time zones by specifying a negative TZ on card 21).
- 8) Region averaged fluxes for each group.
- 9) Region averaged power normalized to initial power in each region.
- 10) Total core averaged power normalized to initial power.

8.5 How to Alter Previous GAKIN Input Decks

Input decks from the original GAKIN (Reference 1) must be altered as follows before use in GAKIN II.

Card 3; Word 6; Columns 49-54; should be PT, an integer, the total number of mesh points.

Card 12; Words 1, 2, and 3; Columns 1-12, 13-24, and 25-36; EP1, EP2, and EP3 are now decimal numbers chosen in accordance with Section 4 for time step adjustment criteria.

Word 4; Columns 37-48; IEP4 should be a 0 or 1 in column 48:

0 - Frequency prediction used

1 - Frequency prediction bypassed (all frequencies set equal to zero).

Word 5; Columns 49-60; IEP6 should be a 0 or 1 in column 60:

0 - Time step adjusted automatically

1 - Time step kept constant.

Card 19; Word 1; Columns 1-12; is now XENON(R) a decimal number equal to the initial Xe^{135} concentration (atoms/cm³) in region R.

Word 2; Columns 13-24; is now IODINE(R) the initial I^{135} concentration (atoms/cm³) in region R.

Word 3; 4, ..., GRP+2; Columns 25-36, 37-48, ...; are now the Xenon capture cross sections in region R for each group, XABS(1), XABS(2), ..., XABS(GRP).

Card 21; Word 1; Columns 1-12; is now HBEGIN (decimal),
the initial time step size in seconds.

Word 2; Columns 13-24; IH should be a 0 or 1
in column 24:

0 - Time step size (H) at the start of
this time zone is equal to the time
step size at the end of the previous
time zone

1 - Time step size, $H = \text{HBEGIN}$.

Word 3; Columns 25-36; TZ may be specified
with a minus sign in order to suppress
printing of precursor concentrations
except at the end of each time zone.

8.6 List of Subprograms

- MAIN: Provides absolute dimensions for all
arrays and calls three subroutines.
- DIRECT: Called by MAIN and with the subroutines
called by it comprises the code. Directs
code execution.
- CALC: Performs one time step calculation.
- AVRAGE: Computes core and region averaged flux
and power values.
- COEF1: Calculates invariant matrix coefficients.
- COEF2: Calculates those matrix elements which
may vary from step to step.
- DEN: Calculates the precursor concentrations
from flux values at a point.

EQPREC: Calculates the steady state precursor concentrations.

ERR: Prints error messages.

FEDBKX: Calculates the xenon concentrations.

FREQ: Predicts the frequencies at each time step and adjusts the time step size.

INEDA: Edits initial input data.

INEDB: Edits input data initially and at each time zone.

INPTA1: Reads cards 1-3. Called by MAIN to provide dimension variables.

INPTA2: Reads cards 4-20. Called only once for each problem.

INPUTB: Reads cards 21-33 (each time zone).

ITER: Performs one steady state iteration.

LHS: Calculates the left hand side (Equation 13) of the GAKIN algorithm.

MATINV: Inverts the left hand side of the steady state and time dependent equations and solves for $[\psi]$.

PREC: Calculates the precursor concentrations at each step.

PRINTA: Prints output edit information.

PROD: Calculates the source (right hand side of equation (24)) for the steady state calculation.

PUN: Punches restart input cards.

RHS: Computes the right hand side of the GAKIN algorithm (Equation 13).

RESCAL: Rescales flux values to keep flux norm constant.

SCALE: Computes flux norm.

SETUP: Directs steady state calculation.

SOURCE: Computes the external source term at each time step.

TEST: Tests for time zone ending, edit times and problem end.

TITLE: Prints problem title and end of problem note.

UPDATE: Recalculates time dependent cross sections before each time step.

9. Sample Problems

9.1 Prompt Supercritical Transient

This is problem X-A3 of the ANS Benchmark Series (Reference 7). The core analyzed consists of one central and two outer regions. The transient is initiated by decreasing the absorption cross section in region 1 (an outer region) by 5% in .01 seconds. Analysis is done with two energy groups and six delayed groups.

CARD 01
 BENCHMARK PROBLEM PROMPT SUPERCRITICAL TRANSIENT

CARD 02 2 2 1 6 3 5 2 C C C -1 C

CARD 03 1 00.10CCCCD-06C.1CCCC0C-060.1C0000C-06 97

CARD 04, 17 81 97

CARD 05 0.40CCCCD 020.160000D 03C.4CCCC0C 02

CARD 06 9 33 49 65 89

CARD 07 0.25CCCCD-030.164C00D-02C.147C00D-02C.296C00D-02C.86CCCCD-030.32CCCCD-C3

CARD 08 0.1CCCCD 010.10C000D 010.1C0C00D 01C.1CCCCD 010.1CCCCD C1C.1CCCCD C1

CARD 08 0.0 0.0 C.C C.C 0.C C.C

CARD 09 0.124CCCD-010.305C00D-010.111C00D 00C.301CCD C0C.114CCD C1C.301CCD C1

CARD 10 0.1CCCCD 010.0

CARD 11 0.10CCCCD 080.30000D 06

CARD 12 0.2CCCCD-030.16CCCCD-01C.5CCCC0C 05 0 CC.1C5CCCC C1

CARD 13 1 2 1

CARD 14 CUTER CORE C 1 0

CARD 15 0.25CCCCD 010.400C00D-02C.7C0C00D-02C.222222C CCC.C C.C

CARD 15 0.25CCCCD 010.80CCCCD-01C.1CCCC0D CCC.666667D CCC.C C.C

CARD 16 0.15CCCCD-01

CARD 14 INNER CORE C 1 C

CARD 15 0.25CCCCD 010.20CCCCD-02C.8CCCC0D-02C.333333C CCC.C C.C

CARD 15 0.25CC00D 010.396CC0D-01C.4C4CCD-C1C.666667D CCC.C C.C

CARD 16 0.100000D-01

CARD 20

0.0	0.296339D	000.588292D	000.871539D	000.114189D	C1C.139534C	C1
0.162813D	010.183684D	01C.201835D	01C.217000D	010.228553D	C1C.237517C	C1
0.242561D	010.244001D	01C.241765C	01C.235688D	01C.225038C	C1C.207080C	C1
0.192509D	010.179716D	01C.168085C	010.157359C	010.147417C	C1C.138184C	C1
0.129608D	010.121645D	01C.114256D	01C.107406D	010.101062D	01C.951949C	C0
0.897765D	000.847813D	000.801858D	000.759683D	000.721089C	000.685895C	CC
0.653934D	000.625056D	000.599124C	000.576017C	000.555625C	000.537853C	CC
0.522616D	000.509843D	000.499474C	000.491459D	000.485761C	000.482352C	CC
0.481218D	000.482352D	000.485761D	000.491459D	000.499474C	000.509843C	CC
0.522616D	000.537853D	000.555625C	000.576017C	000.599124C	000.625056C	CC
0.653934D	000.685895D	000.721089C	000.759683C	000.801858C	000.847813C	CC
0.897765D	000.951949D	000.101062D	01C.107406D	01C.114256C	C1C.121645C	C1
0.129608D	010.138184D	010.147417C	01C.157359C	010.168085C	C1C.179716C	C1
0.192509D	010.207080D	01C.225038C	01C.235688D	010.241765C	C1C.244001C	C1
0.242561D	010.237517D	01C.228953D	01C.217000D	01C.201835C	C1C.183684C	C1
0.162813D	010.139534D	010.114189C	01C.871539D	000.588292D	000.296339C	CC
0.0						

CARD 20

0.0	0.245335D-01C.487C40D-01C.721536D-010.945354C-01C.115518C	CC				
0.134791D	000.152070D	000.167098D	000.179653D	000.189554D	000.196664C	CC
0.200924D	000.202462D	000.202036C	000.202884C	000.218305C	000.236848C	CC
0.233388D	000.222680D	000.210007C	000.197236D	000.185001C	000.173497C	CC
0.162759D	000.152770D	000.143494C	000.134892D	000.126926C	000.119557C	CC
0.112752D	000.106479D	000.100707C	000.954101C-010.905631C-01C.861429C-01			
0.821289D-010.785020D-01C.752452C-01C.723432C-010.697821C-010.675501C-01						
0.656365D-010.640323D-010.627299D-01C.617233D-010.610077C-01C.617233C-010.627299D-01C.640323D-01						
0.604372D-010.605796D-010.610077C-01C.617233C-010.627299D-01C.640323D-01						
0.656365D-010.675501D-010.697821C-010.723432C-01C.752452C-010.785020D-010.821289D-010.861429D-01C.905631D-01C.954101D-01C.100707C						
0.112752D	000.119557D	000.126926C	000.134892D	000.143494C	000.152770C	CC
0.162759D	000.173497D	000.185001C	000.197236D	000.210007C	000.222680C	CC
0.233388D	000.236848D	000.218305C	000.202884D	000.202036C	000.202462C	CC
0.200924D	000.196664D	000.189554C	000.179653D	000.167098D	000.152070C	CC
0.134791D	000.115518D	000.945354C-01C.721536C-010.487C40C-01C.245335C-01				
0.0						

*** INPUT EDIT FOR TIME ZONE 1 ***

CARD 21 0.100000D-04 1-.100000C-01 C -2 1 0 C 0

CARD 22 0.100000D-020.500000D-02

CARD 23 1 0 0 1 C

CARD 27 0.0 -.900000D-02

BENCHMARK PROBLEM PROMPT SUPERCRITICAL TRANSIENT

*** INPUT ECIT ***

2 NEUTRON GROUP(S) , 6 DELAYED GROUP(S) , 3 REGION(S) , 2 COMPOSITION(S)
 SLAB GEOMETRY , LEFT BOUNDARY ZERO RIGHT BOUNDARY ZERO
 IS THERE TO BE END OF PROBLEM PUNCHED OUTPUT NO ,
 ARE THE STEADY STATE FLUXES TO BE PUNCHED NO
 TEST POINTS FOR FREQUENCY CALCULATION 9 33 49 65 89
 GROUP 2 IS SPECIFIED AS THE TEST GROUP FOR THE FREQUENCY CALCULATION

REGION NUMBER	MESH POINT BOUNDARIES	
	LEFT	RIGHT
1	1	17
2	17	81
3	81	97

REGION NUMBER	LENGTH (CM)	MESH SPACING (CM)
1	40.0000	2.5000
2	160.0000	2.5000
3	40.0000	2.5000

GROUP	FRACTIONAL YIELD FROM DELAYED GROUP I INTO NEUTRON GROUP G					
	I= 1	I= 2	I= 3	I= 4	I= 5	I= 6
1	0.01240	0.03050	0.11100	0.30100	1.14000	3.01000
2	0.0	0.0	0.0	0.0	0.0	0.0

GROUP NUMBER	AVERAGE NEUTRON SPEED (CM/SEC)	NEUTRONS PER FISSION	FISSION YIELD
1	0.100000 08	0.250000 01	0.100000 01
2	0.300000 06	0.250000 01	0.0

CCMPCSTION 1
 GRCLP DIFFUSION GROUP DEPENDENT CROSS SECTIONS
 NUMBER COEFFICIENT (CAPTURE) (FISSION)
 1 0.150000D 01 0.700000E-02 0.400000D-02
 2 0.500000D 00 0.100000E 00 0.800000E-01

SCATTERING MATRIX GP INTO G (THE TOTAL REMOVAL IS COMPUTED AND STORED AS THE DIAGONAL ELEMENTS)
 (G) GP= 1 GP= 2
 1 0.260000D-010.0
 2 0.150000D-010.180000D 00

CCMPCSTION 2
 GRCLP DIFFUSION GROUP DEPENDENT CROSS SECTIONS
 NUMBER COEFFICIENT (CAPTURE) (FISSION)
 1 0.100000D 01 0.800000E-02 0.200000D-02
 2 0.500000D 00 0.400000E-01 0.396000D-01

SCATTERING MATRIX GP INTO G (THE TOTAL REMOVAL IS COMPUTED AND STORED AS THE DIAGONAL ELEMENTS)
 (G) GP= 1 GP= 2
 1 0.200000D-010.0
 2 0.100000D-010.800000D-01

CCMPCSTION ASSIGNMENT TO REGIONS
 REGION CCMPCSTION
 1 1
 2 2
 3 1

NO XENON BUILDUP CONSIDERED IN THIS PROBLEM

ARE STEADY STATE CONDITIONS TO BE CALCULATED ? YES

INPLT FLLX DISTRIBUTION

(1) 0.0	(2) 2.963389C-C1	(3) 5.882921D-01	(4) 8.715388C-C1	(5) 1.141887D CC	(6) 1.395336D CC
(7) 1.628134C CC	(8) 1.836836D CC	(9) 2.018354D CC	(10) 2.170000C CC	(11) 2.289529D CC	(12) 2.375165D CC
(13) 2.425611C CC	(14) 2.440005D CC	(15) 2.417649D CC	(16) 2.356881C CC	(17) 2.250384C CC	(18) 2.070800C CC
(19) 1.925089D CC	(20) 1.797160D CC	(21) 1.680847C CC	(22) 1.573593C CC	(23) 1.474167D CC	(24) 1.381839C CC
(25) 1.296079C CC	(26) 1.216448D CC	(27) 1.142558D CC	(28) 1.074057D CC	(29) 1.010621D CC	(30) 9.519489C-C1
(31) 8.977647C-01	(32) 8.478128D-C1	(33) 8.018577D-C1	(34) 7.596828C-C1	(35) 7.210891D-01	(36) 6.858947C-C1
(37) 6.539338D-01	(38) 6.250557D-01	(39) 5.991242D-01	(40) 5.760171D-C1	(41) 5.556254D-C1	(42) 5.378531C-C1
(43) 5.226163D-01	(44) 5.098432D-C1	(45) 4.994736D-01	(46) 4.914587C-C1	(47) 4.857605D-01	(48) 4.823524D-C1
(49) 4.812181C-01	(50) 4.823524D-C1	(51) 4.857605D-01	(52) 4.914587C-C1	(53) 4.994736D-01	(54) 5.098432C-01
(55) 5.226163D-01	(56) 5.378531D-C1	(57) 5.556254D-01	(58) 5.760171D-C1	(59) 5.991242D-01	(60) 6.250557C-01
(61) 6.539338D-01	(62) 6.858947D-C1	(63) 7.210891D-01	(64) 7.596828C-C1	(65) 8.018577D-C1	(66) 8.478128D-C1
(67) 8.977647D-01	(68) 9.519489D-C1	(69) 1.010621D CC	(70) 1.074057D CC	(71) 1.142558D CC	(72) 1.216448C CC
(73) 1.296079C CC	(74) 1.381839C CC	(75) 1.474167D CC	(76) 1.573593D CC	(77) 1.680847C CC	(78) 1.797160C CC
(79) 1.925089D CC	(80) 2.070800D CC	(81) 2.250384D CC	(82) 2.356881D CC	(83) 2.417649D CC	(84) 2.440005D CC
(85) 2.425611D CC	(86) 2.375165D CC	(87) 2.289529D CC	(88) 2.170000C CC	(89) 2.018354D CC	(90) 1.836836C CC
(91) 1.628134D CC	(92) 1.395336D CC	(93) 1.141887D CC	(94) 8.715388C-C1	(95) 5.882921D-01	(96) 2.963389D-C1
(97) 0.0	(98) 0.0	(99) 0.0	(100) 0.0	(101) 0.0	(102) 0.0
(1) 0.0	(2) 2.453354D-C2	(3) 4.870399D-02	(4) 7.215364C-C2	(5) 9.453544D-C2	(6) 1.155182C-C1
(7) 1.347913D-C1	(8) 1.520695D-01	(9) 1.670975D-01	(10) 1.796533C-C1	(11) 1.895539D-C1	(12) 1.966639C-C1
(13) 2.009241C-01	(14) 2.024615D-C1	(15) 2.020363D-C1	(16) 2.028838C-C1	(17) 2.183045D-C1	(18) 2.368475C-C1
(19) 2.333879C-01	(20) 2.226800D-C1	(21) 2.100072D-C1	(22) 1.972358D-C1	(23) 1.850011D-C1	(24) 1.734965C-C1
(25) 1.627586D-C1	(26) 1.527695D-C1	(27) 1.434938D-01	(28) 1.348922D-C1	(29) 1.269256D-C1	(30) 1.195571D-C1
(31) 1.127521D-01	(32) 1.064786D-C1	(33) 1.007070D-01	(34) 9.541012C-C2	(35) 9.056306C-C2	(36) 8.614293C-C2
(37) 8.212890D-C2	(38) 7.850204D-C2	(39) 7.524524D-C2	(40) 7.234317D-C2	(41) 6.978214D-02	(42) 6.755008C-C2
(43) 6.563646C-C2	(44) 6.403226D-C2	(45) 6.272593C-C2	(46) 6.172331C-C2	(47) 6.100767D-C2	(48) 6.057963C-C2
(49) 6.043717D-C2	(50) 6.057963D-C2	(51) 6.100767D-02	(52) 6.172331C-C2	(53) 6.272593D-C2	(54) 6.403226D-C2
(55) 6.563646C-C2	(56) 6.755008D-C2	(57) 6.978214D-C2	(58) 7.234317C-C2	(59) 7.524524D-02	(60) 7.850204C-C2
(61) 8.212890C-C2	(62) 8.614293D-C2	(63) 9.056306D-02	(64) 9.541012C-C2	(65) 1.007070D-C1	(66) 1.064786C-C1
(67) 1.127521D-01	(68) 1.195571D-C1	(69) 1.269256D-01	(70) 1.348922C-C1	(71) 1.434938D-01	(72) 1.527695D-C1
(73) 1.627586C-01	(74) 1.734965D-C1	(75) 1.850011D-01	(76) 1.972358C-C1	(77) 2.100072D-01	(78) 2.226800C-C1
(79) 2.333879D-01	(80) 2.368475D-C1	(81) 2.183045D-01	(82) 2.028838C-C1	(83) 2.020363D-C1	(84) 2.024615C-C1
(85) 2.009241D-01	(86) 1.966639D-C1	(87) 1.895539D-01	(88) 1.796533C-C1	(89) 1.670975D-C1	(90) 1.520695D-C1
(91) 1.347913D-01	(92) 1.155182D-C1	(93) 9.453544D-C2	(94) 7.215364C-C2	(95) 4.870399C-C2	(96) 2.453354D-C2
(97) 0.0	(98) 0.0	(99) 0.0	(100) 0.0	(101) 0.0	(102) 0.0

THE INITIAL PRECURSOR CONCENTRATIONS ARE CALCULATED FROM THE STEADY STATE FLLX DISTRIBUTION

ARE THERE ANY TIME DEPENDENT CHANGES IN THE
CRSS SECTION DATA YES

TIME	CRSS SECTION	GRUP	REGION	TOTAL LINEAR	TOTAL QUADRATIC
ZONE				CHANGE	CHANGE
1	CAPTURE	2	1	-9.99999D-C2	0.0

ARE THERE ANY TIME DEPENDENT SOURCES ? NO

EQUILIBRIUM NU(G) (1) 0.277307CD C1(2) C.277307CD 01(

EQUILIBRIUM FLUXES

1)C.0 (2)0.2862154D 00(3)0.5683025D 00(4)0.8421926C CC(5)C.1103935D C1(6)C.1349755D C1
7)C.1576107D 01(8)0.1779726D 01(9)C.1957674D C1(10)C.2107386C C1(11)C.2226699C C1(12)C.2313890C 01
13)C.2367680D 01(14)0.2387212D 01(15)C.2371878D C1(16)C.2320555D C1(17)C.2228526C C1(18)C.2070561C 01
19)C.1937223D C1(20)0.1817865D 01(21)0.1708274D C1(22)0.1606625D C1(23)C.1511952D C1(24)C.1423753D C1
25)C.1341590D C1(26)0.1265016D 01(27)C.1193741D 01(28)C.1127462C C1(29)C.1065902C 01(30)C.1008802C 01
31)C.9559232D 00(32)0.9070443D 00(33)C.8619608D CC(34)C.8204835C CC(35)C.7824402C CC(36)C.7476705C CC
37)C.7160292D CC(38)0.6873840D 00(39)0.6616150C CC(40)C.6286144C CC(41)C.6182860C CC(42)C.6005446C CC
43)C.5853161D CC(44)0.5725367D 00(45)0.5621530D 00(46)0.5541215C CC(47)C.5484085C CC(48)C.5445903C CC
49)0.5438525D CC(50)0.544903D CC(51)C.5484085D CC(52)C.5541215C CC(53)C.5621530C CC(54)0.5725367C CC
55)C.5853161D 00(56)0.6005446D 00(57)0.6182860D 00(58)C.6286144C CC(59)C.6616150C CC(60)C.6873840C CC
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79)C.1937223D C1(80)0.2070561D 01(81)0.2228526C 01(82)0.2320555C C1(83)C.2371878C C1(84)C.2387212C 01
85)0.2367680D 01(86)0.2313890D 01(87)C.2226699D C1(88)0.2107386C C1(89)C.1957674C C1(90)C.1779726C 01
91)C.1576107D 01(92)0.1349755D 01(93)C.1103935D C1(94)C.8421926C CC(95)C.5683025C CC(96)C.2862154C CC
57)C.C (1)C.0 (2)0.2369936D-01(3)C.4705688D-C1(4)0.6973568E-C1(5)C.9140864D-01(6)C.1117632D CC
7)0.1305057D CC(8)0.1473659D 00(9)C.1621008D CC(10)C.1744985C CC(11)C.1843833C 00(12)C.1916242C CC
13)C.1961651D CC(14)0.1981376D 00(15)C.1983172C 00(16)C.1999832C CC(17)C.2165068C CC(18)C.2366467C CC
19)0.2346132D CC(20)C.2250399D 00(21)C.2132734C 00(22)C.2012460C CC(23)C.1856364C CC(24)C.1786642C CC
25)0.1683822D CC(26)0.1587837D 00(27)C.1498417D CC(28)C.1415235C CC(29)C.1337972C 00(30)0.1266300C CC
31)C.1199924D 00(32)0.1138569D 00(33)C.1081978D CC(34)C.1029914C CC(35)C.9821599D-C1(36)C.9385151C-01
37)C.8987974D-C1(38)0.8628404D-01(39)0.8304938C-01(40)C.8016223C-C1(41)C.7761049C-C1(42)C.7538350C-01
43)0.7347194D-01(44)0.7186780D-01(45)C.7056438D-C1(46)C.6955623C-C1(47)C.6883911C-01(48)C.6841004C-01
49)0.6826721D-01(50)0.6841004D-01(51)C.6883911D-C1(52)C.6955623D-C1(53)C.7056438C-C1(54)C.7186780C-01
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1)0.0 (2)0.1700076D-03(3)0.3375631D-C3(4)C.5002498D-C3(5)C.6557210D-03(6)0.8017345C-03
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 13)C.1406882D-C2(14)0.1420072D-02(15)0.1417446D-02(16)0.1413421C-C2(17)C.1057637D-C2(18)C.7554563D-C3
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 25)C.5228085D-03(26)0.4929951D-03(27)C.4652280D-03(28)C.4354013D-C3(29)C.4154111C-C3(30)C.3931581C-03
 31)C.3725500D-C3(32)0.3535006D-03(33)0.3359303D-C3(34)0.3197656D-C3(35)C.3045395D-C3(36)C.2913882D-C3
 37)0.2790567D-03(38)0.2678929D-03(39)C.2578500D-C3(40)C.2488860D-C3(41)C.2409634D-C3(42)0.2340491C-03
 43)0.2281141D-03(44)0.2231336D-03(45)0.2190868D-C3(46)C.2159567D-C3(47)C.2137302D-C3(48)C.2123980D-03
 49)C.2119546D-C3(50)0.2123980D-03(51)0.2137302D-03(52)0.2159567D-C3(53)C.2150868D-C3(54)C.2231336D-C3
 55)C.2281141D-03(56)0.2340491D-03(57)C.2409634D-C3(58)0.2488860D-C3(59)C.2578500D-C3(60)C.2678929D-C3
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 67)C.3725500D-C3(68)0.3931581D-03(69)0.4154111C-C3(70)C.4354013D-C3(71)C.4652280D-C3(72)C.4529951D-C3
 73)C.5228085D-03(74)0.5547643D-03(75)0.5889187D-C3(76)0.6252038D-C3(77)0.6631983D-C3(78)C.7015033D-C3
 79)0.7360447D-C3(80)0.7554563D-03(81)0.1097637D-C2(82)C.1413421C-C2(83)C.1417446C-C2(84)0.1420072C-C2
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 91)C.9361841D-C3(92)0.8017345D-03(93)0.6557210D-03(94)0.5002498D-C3(95)C.3375631D-03(96)C.1700076D-C3
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 19)0.1963043D-02(20)0.1870921D-02(21)C.1768761D-C2(22)C.1667429D-C2(23)C.1570656C-C2(24)C.1479565C-02
 25)C.1394339D-C2(26)0.1314826D-02(27)C.1240771D-02(28)0.1171891C-C2(29)C.1107908C-C2(30)C.1048559D-C2
 31)C.9935970D-C3(32)0.9427919D-03(33)C.8959317C-C3(34)C.8528202C-C3(35)C.8132772C-C3(36)C.7771371C-C3
 37)0.7442488D-03(38)0.7144747D-03(39)C.6876901D-C3(40)C.6637830D-C3(41)C.6426534C-03(42)C.6242128C-C3
 43)C.6083841D-03(44)0.5951011D-03(45)0.5843081D-C3(46)C.5759601C-C3(47)C.5700220D-C3(48)C.5664691D-C3
 49)C.5652864D-C3(50)0.5664691D-03(51)C.5700220D-03(52)C.5759601C-C3(53)C.5843081C-03(54)C.5951011C-C3
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 13)C.9241311D-03(14)0.9327954D-03(15)C.93107C6D-C3(16)C.9284267D-C3(17)C.7209994C-03(18)C.4562327C-03
 19)C.4834819D-C3(20)0.4607929D-03(21)C.4356316C-03(22)C.4106744C-03(23)C.3868400D-03(24)C.3644052C-C3
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 57)C.C (1)C.0 (2)0.8292306D-04(3)C.16465C1D-C3(4)0.244CC22C-C3(5)C.3198350D-03(6)0.3910546D-C3
 7)C.4566339D-03(8)0.5156270D-03(9)C.5671833D-C3(10)C.61056C9C-C3(11)C.6451402C-03(12)0.6704478C-03
 13)C.6862217D-C3(14)0.6926555D-03(15)0.6913747C-03(16)C.6894115C-03(17)C.5353845D-03(18)C.3684820D-C3
 19)C.3590138D-C3(20)0.3421658D-03(21)C.3234821D-03(22)C.3049499C-03(23)C.2872515C-03(24)C.2705923C-C3
 25)0.2550055D-03(26)0.2404637D-03(27)C.2269200D-C3(28)C.2143227C-03(29)C.2026212C-03(30)0.1917671D-03
 31)C.1817153D-03(32)0.1724237D-03(33)0.1638536D-C3(34)C.1555691C-03(35)C.1487373D-C3(36)C.1421277C-C3
 37)C.1361129D-03(38)0.1306676D-03(39)0.1257691D-03(40)0.1213968C-03(41)C.1175325C-03(42)C.1141600D-C3
 43)C.1112651D-03(44)0.1088358D-03(45)C.1068620D-C3(46)C.1053352C-03(47)C.1042492C-03(48)0.1035994C-C3
 49)C.1033831D-03(50)0.1035994D-03(51)C.1042492D-C3(52)C.1053352D-C3(53)C.1068620C-03(54)C.1088358C-C3
 55)C.1112651D-C3(56)0.1141600D-03(57)0.1175325C-03(58)C.1213968C-03(59)C.1257691C-03(60)C.1206676D-C3
 61)0.1361129D-03(62)0.1421277D-03(63)C.1487373D-C3(64)C.1555691C-03(65)C.1638536C-03(66)0.1724237D-03
 67)0.1817153D-03(68)0.1917671D-03(69)C.2026212D-C3(70)C.2143227D-C3(71)C.2269200D-C3(72)C.2404637C-03
 73)C.2550055D-C3(74)C.2705923D-03(75)C.2872515C-03(76)C.3049499C-03(77)C.3234821C-03(78)C.3421658D-C3
 79)C.3590138D-C3(80)C.3684820D-C3(81)C.5353845C-03(82)0.6894115C-03(83)C.6913747C-03(84)C.6926555D-C3
 85)0.6862217D-03(86)0.6704478D-03(87)C.6451402D-C3(88)C.61056C9C-03(89)C.5671833D-03(90)C.5156270D-C3
 91)C.4566339D-C3(92)0.3910546D-03(93)C.3198350D-C3(94)C.244CC22C-C3(95)C.16465C1D-C3(96)C.8292306C-C4
 57)C.0 (

1)0.0 (2)0.6361268D-05(3)C.1263078D-C4(4)C.1871812C-C4(5)C.2453547C-04(6)C.2999893C-04
 7)C.3502971D-C4(8)0.3955524D-04(9)0.4351028D-C4(10)C.468379C-C4(11)C.4949C5ED-C4(12)C.5143199C-C4
 13)C.52642C5D-C4(14)0.5313561D-04(15)C.5303736D-04(16)0.5288675C-C4(17)C.41C7C89C-C4(18)C.2826732D-C4
 19)0.2754099D-04(20)0.2624853D-04(21)C.2481525D-C4(22)C.2339359C-C4(23)C.22C3589C-04(24)0.2075792C-04
 25)0.1956221D-04(26)0.1844667D-04(27)C.1740769D-04(28)C.1644132D-C4(29)C.1554366C-04(30)C.14711C1C-04
 31)C.1393991D-C4(32)0.1322712D-04(33)C.1256969C-04(34)0.1196485D-C4(35)C.1141CC7D-C4(36)C.1C9C3C3D-C4
 37)C.1044162D-04(38)0.1C02389D-04(39)C.9648113D-C5(40)C.93127C3C-05(41)C.9C1626CC-05(42)C.8757543D-05
 43)0.8535471D-05(44)0.8349113D-05(45)0.819769C-D-05(46)C.8C8C57CC-C5(47)C.799726CC-C5(48)C.7947413C-05
 49)C.7930821D-C5(50)0.7947413D-05(51)C.799726CC-05(52)0.808057CC-C5(53)C.819769C-D-05(54)C.8349113D-C5
 55)C.8535471D-C5(56)C.8757543D-05(57)C.9C1626CC-05(58)C.93127C3C-05(59)0.9648113C-05(60)C.1CC2389C-C4
 61)0.1044162D-04(62)0.1090303D-04(63)C.1141CC7D-C4(64)C.1196485D-C4(65)C.1256969C-04(66)0.1322712C-04
 67)C.1393991D-C4(68)0.1471101D-04(69)0.1554366C-04(70)C.1644132C-C4(71)C.174C769D-C4(72)C.1844667C-04
 73)C.1956221D-C4(74)0.2075792D-04(75)C.2203589D-04(76)0.2339359C-04(77)C.2481525C-04(78)C.2624853C-04
 79)0.2754099D-C4(80)0.2826732D-04(81)C.4107C89D-C4(82)C.5288675C-C4(83)C.53C3736C-04(84)0.5313561C-04
 85)C.52642C5D-C4(86)0.5143199D-04(87)0.4949058D-C4(88)C.468379C-C4(89)C.4351C2ED-C4(90)C.3955524C-04
 91)C.35C2971D-C4(92)0.2999893D-04(93)C.2453547C-04(94)0.1871812C-C4(95)C.1263078C-04(96)0.6361268C-C5
 97)0.0 (1)C.0 (2)0.8964655D-06(3)C.1780CC1D-05(4)C.2637862C-C5(5)C.3457676C-C5(6)C.4227618C-05
 7)C.4936583D-C5(8)0.5574346D-05(9)0.6131712C-05(10)0.66C0659C-C5(11)C.6974489D-C5(12)C.7248C84C-C5
 13)0.7418613D-05(14)0.7488167D-05(15)C.7474321D-C5(16)C.7453C97C-C5(17)C.578794CC-05(18)0.3983589C-05
 19)0.3881230D-05(20)0.3699090D-05(21)C.34971C4D-C5(22)C.3296756D-C5(23)C.31C5421C-C5(24)C.2925322C-05
 25)C.2756816D-C5(26)0.2599607D-05(27)C.2453189C-05(28)0.2317CC3C-C5(29)C.219C5CCD-C5(30)C.2C73158C-C5
 31)C.1964490D-C5(32)0.1864040D-05(33)C.1771391D-05(34)C.1686153C-C5(35)C.16C797CC-05(36)C.1536516C-C5
 37)C.1471491D-05(38)0.1412623D-05(39)C.1359666D-C5(40)C.1312398C-C5(41)C.127C622C-05(42)0.1234162C-C5
 43)C.12C2866D-C5(44)0.1176604D-05(45)0.1155264C-C5(46)C.1138759C-C5(47)C.1127C19D-C5(48)C.1119994C-C5
 49)C.1117656D-C5(50)0.1119994D-05(51)C.1127019D-C5(52)C.1138759C-C5(53)C.1155264D-05(54)C.11766C4C-C5
 55)0.1202866D-C5(56)0.1234162D-05(57)C.127C622D-C5(58)C.1312398C-C5(59)C.1359666C-05(60)0.1412623C-05
 61)C.1471491D-C5(62)0.1536516D-05(63)C.1607970D-C5(64)C.1686153C-C5(65)C.1771391D-C5(66)C.1864C4CC-C5
 67)C.1964490D-C5(68)0.2073158D-05(69)0.21905CCD-05(70)0.2317CC3C-C5(71)C.2453189C-05(72)C.25996C7C-C5
 73)C.2756816D-05(74)0.2925322D-05(75)C.31C5421D-C5(76)C.3296756C-C5(77)C.34971C4C-05(78)C.3699C9CC-C5
 79)C.3881230D-05(80)0.3983589D-05(81)C.578794CC-05(82)C.7453C97C-C5(83)C.7474321D-C5(84)C.7488167C-C5
 85)C.7418613D-05(86)0.7248084D-05(87)C.6974489C-05(88)0.66C0659C-C5(89)C.6131712D-C5(90)C.5574346C-C5
 91)0.4936583D-05(92)0.4227618D-05(93)C.3457676D-C5(94)C.2637862C-C5(95)C.1780CC1C-05(96)0.8964655C-C6
 97)C.0 (

REGION FRACTICNAL PCWER

1 C.2789988C CC
 2 0.442C024C CC
 3 C.2789988C CC

TOTAL NORMALIZED POWER = C.1CCCCCD C1

BENCHMARK PROBLEM PROMPT SUPERCRITICAL TRANSIENT

TIME ZCNE= 1 STEP NUMBER= 80 TIME=C.100000D-C2 TIME STEP=C.127628D-C4

TEST POINT	MESH POINT	FREQUENCY	EXP(W*F)
1	9	1.0086D C2	1.000030D CC
2	33	4.5460D C1	1.000013D CC
3	49	0.0	1.000000D CC
4	65	0.0	1.000000D CC
5	89	0.0	1.000000D CC

POINT-WISE FLUXES FOR GROUP 1

(1) 0.0 (2) 3.029636D-C1(3) 6.015166D-01(4) 8.913127D-C1(5) 1.168123D CC(6) 1.427946D CC
 (7) 1.666968D CC(8) 1.881719D CC(9) 2.069070D CC(10) 2.226289D CC(11) 2.351084D CC(12) 2.441628D CC
 (13) 2.496576D CC(14) 2.515040D CC(15) 2.496402D CC(16) 2.439536D CC(17) 2.339610D CC(18) 2.169044D CC
 (19) 2.024854D CC(20) 1.895926D CC(21) 1.777814D CC(22) 1.668553D CC(23) 1.567111D CC(24) 1.472822D CC
 (25) 1.385176D CC(26) 1.303737D CC(27) 1.228116D CC(28) 1.157960D CC(29) 1.092942D CC(30) 1.032759D CC
 (31) 9.771345D-01(32) 9.258115D-C1(33) 8.785540D-C1(34) 8.351446D-C1(35) 7.953843D-01(36) 7.590909D-01
 (37) 7.260984D-C1(38) 6.962535D-C1(39) 6.694238D-01(40) 6.454840D-C1(41) 6.242248D-C1(42) 6.058492D-C1
 (43) 5.899721D-C1(44) 5.766204D-C1(45) 5.657319D-01(46) 5.572556D-C1(47) 5.511510D-C1(48) 5.473881D-C1
 (49) 5.459473D-01(50) 5.468188D-C1(51) 5.500032D-C1(52) 5.555110D-C1(53) 5.633626D-C1(54) 5.735887D-C1
 (55) 5.862301D-01(56) 6.013379D-C1(57) 6.189736D-01(58) 6.392098D-C1(59) 6.621297D-C1(60) 6.878283D-C1
 (61) 7.164120D-01(62) 7.479996D-C1(63) 7.827225D-01(64) 8.207252D-C1(65) 8.621659D-01(66) 9.072157D-C1
 (67) 9.560676D-01(68) 1.008924D CC(69) 1.066005D CC(70) 1.127549D CC(71) 1.193814D CC(72) 1.265077D CC
 (73) 1.341642D CC(74) 1.423835D CC(75) 1.512027D CC(76) 1.606655D CC(77) 1.708298D CC(78) 1.817885D CC
 (79) 1.937240D CC(80) 2.070574D CC(81) 2.228537D CC(82) 2.320568D CC(83) 2.371886D CC(84) 2.387219D CC
 (85) 2.367685D CC(86) 2.313894D CC(87) 2.226703D CC(88) 2.107389D CC(89) 1.957676D CC(90) 1.779727D CC
 (91) 1.576108D CC(92) 1.349756D CC(93) 1.103536D CC(94) 8.421931D-C1(95) 5.683028D-C1(96) 2.862155D-01
 (97) 0.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 1 = 0.703650D C2

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 1 = 0.166478D C3

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 1 = 0.666838D C2

POINT-WISE FLUXES FOR GROUP 2

(1) 0.0 (2) 2.516062D-02(3) 4.995501D-02(4) 7.402229D-02(5) 9.701212D-02(6) 1.185898E-01
 (7) 1.384412E-01(8) 1.562773E-01(9) 1.718385E-01(10) 1.848988E-01(11) 1.952707D-01(12) 2.028153E-01
 (13) 2.074725D-01(14) 2.093781D-01(15) 2.093351D-01(16) 2.107297E-01(17) 2.273334D-01(18) 2.473800E-01
 (19) 2.445604E-01(20) 2.340340E-01(21) 2.213260E-01(22) 2.084251E-01(23) 1.960233D-01(24) 1.843394E-01
 (25) 1.734205D-01(26) 1.632530E-01(27) 1.538035D-01(28) 1.450332E-01(29) 1.369036D-01(30) 1.293777E-01
 (31) 1.224212D-01(32) 1.160022E-01(33) 1.100914D-01(34) 1.046616E-01(35) 9.968796D-02(36) 9.514789D-02
 (37) 9.102061E-02(38) 8.728731D-02(39) 8.393099D-02(40) 8.093633E-02(41) 7.828968E-02(42) 7.597896E-02
 (43) 7.399358E-02(44) 7.232442D-02(45) 7.096377D-02(46) 6.990527E-02(47) 6.914391D-02(48) 6.867598E-02
 (49) 6.849905D-02(50) 6.861197D-02(51) 6.901484E-02(52) 6.970901E-02(53) 7.069709D-02(54) 7.198296D-02
 (55) 7.357175E-02(56) 7.546992D-02(57) 7.768522D-02(58) 8.022675E-02(59) 8.310501D-02(60) 8.633192E-02
 (61) 8.992086E-02(62) 9.388675D-02(63) 9.824610E-02(64) 1.030171D-01(65) 1.082196D-01(66) 1.138748E-01
 (67) 1.200076D-01(68) 1.266427D-01(69) 1.338080E-01(70) 1.415329E-01(71) 1.498493D-01(72) 1.587900E-01
 (73) 1.683875E-01(74) 1.786686D-01(75) 1.896400E-01(76) 2.012489E-01(77) 2.132758D-01(78) 2.250418E-01
 (79) 2.346147E-01(80) 2.366479D-01(81) 2.165077D-01(82) 1.999839E-01(83) 1.983177D-01(84) 1.981380E-01
 (85) 1.961655E-01(86) 1.916245D-01(87) 1.843835E-01(88) 1.744987E-01(89) 1.621009D-01(90) 1.473660E-01
 (91) 1.305057D-01(92) 1.117632D-01(93) 9.140867E-02(94) 6.973570E-02(95) 4.705689D-02(96) 2.369936E-02
 (97) 0.0

TOTAL INTEGRATED FLUX FOR REGION 1 GRUP 2 = 0.591216D 01

TOTAL INTEGRATED FLUX FOR REGION 2 GRUP 2 = 0.205262D 02

TOTAL INTEGRATED FLUX FOR REGION 3 GRUP 2 = 0.558751D 01

REGION	NORMALIZED POWER
1	0.1057022E 01
2	0.1013323E 01
3	0.1000002E 01

TOTAL NORMALIZED POWER = 0.1021758D 01

BENCHMARK PROBLEM PROMPT SUPERCRITICAL TRANSIENT

TIME ZCNE= 1 STEP NUMBER= 288 TIME=C.500000D-C2 TIME STEP=C.252695D-C4

TEST POINT	MESH POINT	FREQUENCY	EXP(W*F)
1	9	3.2554D C2	1.005006D CC
2	33	2.6144D C2	1.004018D CC
3	49	1.5368D C2	1.002360D CC
4	65	3.8046D C1	1.000584D CC
5	89	1.1413D C1	1.000175D CC

POINT-WISE FLUXES FOR GROUP 1

(1) C.0	(2) 7.125541D-C1	(3) 1.414306D CC	(4) 2.094616D CC	(5) 2.742170D CC	(6) 3.350134D CC
(7) 3.906302D CC	(8) 4.403237D CC	(9) 4.833399D CC	(10) 5.190255D CC	(11) 5.468382D CC	(12) 5.663539D CC
(13) 5.772705D CC	(14) 5.794024D CC	(15) 5.726411D CC	(16) 5.567876D CC	(17) 5.30E726D CC	(18) 4.874881D CC
(19) 4.504931D CC	(20) 4.174256D CC	(21) 3.872669D CC	(22) 3.595352D CC	(23) 3.335540D CC	(24) 3.103291D CC
(25) 2.885041D CC	(26) 2.683428D CC	(27) 2.497226D CC	(28) 2.325313D CC	(29) 2.166662D CC	(30) 2.020324D CC
(31) 1.885427D CC	(32) 1.761168D CC	(33) 1.646806D CC	(34) 1.541661D CC	(35) 1.445107D CC	(36) 1.356570D CC
(37) 1.275520D CC	(38) 1.201475D CC	(39) 1.133591D CC	(40) 1.072665D CC	(41) 1.017126D CC	(42) 9.670382E-C1
(43) 9.220980D-01	(44) 8.820293D-C1	(45) 8.465840D-01	(46) 8.155400D-C1	(47) 7.886993D-01	(48) 7.658873D-C1
(49) 7.469510D-01	(50) 7.317585D-C1	(51) 7.201979D-01	(52) 7.121764D-C1	(53) 7.076195D-01	(54) 7.064709D-01
(55) 7.086914D-01	(56) 7.142589D-C1	(57) 7.231680D-01	(58) 7.354296D-C1	(59) 7.510710D-C1	(60) 7.701358D-C1
(61) 7.926838D-01	(62) 8.187912D-C1	(63) 8.485508D-01	(64) 8.820723D-C1	(65) 9.194827D-01	(66) 9.609264D-C1
(67) 1.006566D CC	(68) 1.056584D CC	(69) 1.111180D CC	(70) 1.170577D CC	(71) 1.235017D CC	(72) 1.304766D CC
(73) 1.380115D CC	(74) 1.461386D CC	(75) 1.548942D CC	(76) 1.643217D CC	(77) 1.744754D CC	(78) 1.854608D CC
(79) 1.974507D CC	(80) 2.108769D CC	(81) 2.268213D CC	(82) 2.361064D CC	(83) 2.412578D CC	(84) 2.427578D CC
(85) 2.407209D CC	(86) 2.352097D CC	(87) 2.263117D CC	(88) 2.141567D CC	(89) 1.989201D CC	(90) 1.808213D CC
(91) 1.601205D CC	(92) 1.371158D CC	(93) 1.121380D CC	(94) 8.554664D-C1	(95) 5.772429D-C1	(96) 2.907131D-C1
(97) C.0	(

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 1 = C.163238D C3

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 1 = C.254271D C3

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 1 = C.677847D C2

POINT-WISE FLUXES FOR GROUP 2

(1) 0.0 (2) 6.010576D-C2(3) 1.193C05D-C1(4) 1.766868D-C1(5) 2.313949D-01(6) 2.825954D-C1
 (7) 3.295118D-01(8) 3.714326D-C1(9) 4.077224D-01(10) 4.378318D-C1(11) 4.6131C3D-C1(12) 4.778278D-C1
 (13) 4.872422D-01(14) 4.898506D-C1(15) 4.873938D-01(16) 4.871CC0C-C1(17) 5.18CC21D-01(18) 5.534876D-C1
 (19) 5.403078D-01(20) 5.112783D-C1(21) 4.782678D-C1(22) 4.454875D-C1(23) 4.143547D-01(24) 3.852738D-01
 (25) 3.582870D-01(26) 3.333122D-C1(27) 3.102293D-01(28) 2.88911CC-C1(29) 2.692342D-01(30) 2.51C834D-C1
 (31) 2.343509D-01(32) 2.189376D-C1(33) 2.047519D-01(34) 1.917096D-C1(35) 1.797332D-01(36) 1.687516D-C1
 (37) 1.586993D-01(38) 1.495166D-C1(39) 1.411486D-01(40) 1.335452D-C1(41) 1.266607D-01(42) 1.204535D-C1
 (43) 1.148861D-01(44) 1.099242D-C1(45) 1.055372D-01(46) 1.018977D-C1(47) 9.838123D-C2(48) 9.556616D-C2
 (49) 9.323368D-C2(50) 9.136751D-C2(51) 8.995390D-C2(52) 8.898145D-C2(53) 8.8441C5D-C2(54) 8.832585D-C2
 (55) 8.863114D-C2(56) 8.935430D-C2(57) 9.049484D-C2(58) 9.2C5428D-C2(59) 9.403618D-C2(60) 9.644614D-C2
 (61) 9.929177D-C2(62) 1.025828D-C1(63) 1.063309D-C1(64) 1.1C5459D-C1(65) 1.152559D-C1(66) 1.2C4670D-C1
 (67) 1.262C38D-C1(68) 1.324891D-C1(69) 1.393480D-C1(70) 1.468081D-C1(71) 1.548992D-C1(72) 1.636527D-C1
 (73) 1.730997D-C1(74) 1.832659D-C1(75) 1.941566D-C1(76) 2.057170D-C1(77) 2.177229D-C1(78) 2.294840D-C1
 (79) 2.390354D-C1(80) 2.409414D-C1(81) 2.203223D-C1(82) 2.034344D-C1(83) 2.016793D-C1(84) 2.014468D-C1
 (85) 1.993997D-C1(86) 1.947491D-01(87) 1.873613D-01(88) 1.772936D-C1(89) 1.646788D-C1(90) 1.496952D-C1
 (91) 1.325579D-01(92) 1.135132D-C1(93) 9.283505D-C2(94) 7.0821C3D-C2(95) 4.778791D-02(96) 2.4C6712D-C2
 (97) 0.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 2 = 0.139158D C2

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 2 = 0.311389D C2

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 2 = 0.567870D C1

REGION	NORMALIZED POWER
1	0.247461D C1
2	0.154027D C1
3	0.1016394D C1

TOTAL NORMALIZED POWER = 0.1654793D C1

BENCHMARK PROBLEM PRCMPT SUPERCRITICAL TRANSIENT

TIME ZONE= 1 STEP NUMBER= 486 TIME=C.100000D-C1 TIME STEP=C.252695D-C4

TEST PCINT	MESH PCINT	FREQUENCY	EXP(W*F)
1	9	7.7692E 02	1.017167D 00
2	33	7.16C4C C2	1.C15811D CC
3	49	6.3323C C2	1.C1397CD CC
4	65	3.7774C C2	1.C0831CC CC
5	89	1.5345C C2	1.003367D 00

PCINT-WISE FLUXES FOR GROUP 1

(1) 0.0	(2) 9.960839D CC	(3) 1.976312D 01	(4) 2.52508CC C1	(5) 3.827284D 01	(6) 4.668561D C1
(7) 5.435517D 01	(8) 6.115937C C1	(9) 6.698986D 01	(10) 7.175372C C1	(11) 7.5375C1D 01	(12) 7.7755E1D C1
(13) 7.897690D 01	(14) 7.889704D C1	(15) 7.754818D 01	(16) 7.4915CC C1	(17) 7.C89311D 01	(18) 6.43C270C 01
(19) 5.864968D 01	(20) 5.361523D C1	(21) 4.905974D 01	(22) 4.491C68C C1	(23) 4.112181D 01	(24) 3.765815C C1
(25) 3.449C37D C1	(26) 3.159264C C1	(27) 2.894170C 01	(28) 2.651644C C1	(29) 2.429759D C1	(30) 2.226757C C1
(31) 2.041033D 01	(32) 1.871118D C1	(33) 1.715672D 01	(34) 1.573469C 01	(35) 1.443390C 01	(36) 1.324410C 01
(37) 1.215595C 01	(38) 1.116089D C1	(39) 1.025113D C1	(40) 9.419516C CC	(41) 8.659541D C0	(42) 7.965249C C0
(43) 7.331201D CC	(44) 6.752434D C0	(45) 6.224416C 00	(46) 5.743011C CC	(47) 5.3C4446D C0	(48) 4.9C52E3D CC
(49) 4.542385D CC	(50) 4.212899D CC	(51) 3.914227D CC	(52) 3.644CC7C CC	(53) 3.4CC094D C0	(54) 3.18C545C CC
(55) 2.983599C 00	(56) 2.807663D CC	(57) 2.651305D CC	(58) 2.513235D CC	(59) 2.392298D CC	(60) 2.287465C CC
(61) 2.197822D CC	(62) 2.122565D CC	(63) 2.06C991C CC	(64) 2.C12491C CC	(65) 1.97655CD CC	(66) 1.952734C CC
(67) 1.940694D CC	(68) 1.940157D CC	(69) 1.95C926C CC	(70) 1.972876C CC	(71) 2.C05952D 00	(72) 2.C5C171C CC
(73) 2.105621C CC	(74) 2.172464D CC	(75) 2.25C951D CC	(76) 2.34146CC CC	(77) 2.444590D 00	(78) 2.561438C CC
(79) 2.694323D CC	(80) 2.848781D CC	(81) 3.038985C CC	(82) 3.148976C CC	(83) 3.2C537CD CC	(84) 3.2148C0C CC
(85) 3.178938D CC	(86) 3.09871CD CC	(87) 2.975328C 00	(88) 2.81C526C CC	(89) 2.606596D 00	(90) 2.366370D CC
(91) 2.093190C CC	(92) 1.790855D CC	(93) 1.463574D CC	(94) 1.1159C4C CC	(95) 7.526873C-01	(96) 3.789838C-01
(97) 0.0	(

TOTAL INTEGRATED FLUX FOR REGION 1 GRUP 1 = 0.224286C 04

TOTAL INTEGRATED FLUX FOR REGION 2 GRUP 1 = C.208C22D 04

TOTAL INTEGRATED FLUX FOR REGION 3 GRUP 1 = C.893CC7D C2

POINT-WISE FLUXES FOR GROUP 2

(1) C.0 (2) 8.542783D-C1(3) 1.694960D CC(4) 2.508666D CC(5) 3.282443D C0(6) 4.003976D 00
 (7) 4.661778D 00(8) 5.245378D CC(9) 5.745487D CC(10) 6.154161D CC(11) 6.464972D CC(12) 6.673303D CC
 (13) 6.777180D CC(14) 6.780350D CC(15) 6.704384D CC(16) 6.636956D CC(17) 6.924807D CC(18) 7.221613D CC
 (19) 6.932234D CC(20) 6.463639D CC(21) 5.960859D CC(22) 5.473963D CC(23) 5.018731D C0(24) 4.598687D CC
 (25) 4.213091D C0(26) 3.859825D CC(27) 3.536433D CC(28) 3.240477D CC(29) 2.969662D C0(30) 2.721864D CC
 (31) 2.495134D CC(32) 2.287685D CC(33) 2.097886D CC(34) 1.924243D CC(35) 1.765292D CC(36) 1.620084D CC
 (37) 1.487182D C0(38) 1.365642D CC(39) 1.254513D C0(40) 1.152926D CC(41) 1.060085D C0(42) 9.752651D-C1
 (43) 8.978031D-01(44) 8.270937D-C1(45) 7.625843D-01(46) 7.037707D-C1(47) 6.501928D-01(48) 6.014311D-C1
 (49) 5.571035D-01(50) 5.168618D-C1(51) 4.803893D-01(52) 4.473980D-C1(53) 4.176265D-C1(54) 3.908377D-C1
 (55) 3.668170D-01(56) 3.453704D-C1(57) 3.263234D-01(58) 3.095188D-C1(59) 2.948161D-01(60) 2.820901D-C1
 (61) 2.712295D-01(62) 2.621368D-C1(63) 2.547265D-01(64) 2.489250D-C1(65) 2.446698D-01(66) 2.419089D-01
 (67) 2.406000D-01(68) 2.407107D-C1(69) 2.422175D-01(70) 2.451058D-C1(71) 2.493688D-C1(72) 2.550070D-C1
 (73) 2.620251D-C1(74) 2.704249D-C1(75) 2.801861D-C1(76) 2.912133D-C1(77) 3.031929D-C1(78) 3.152015D-C1
 (79) 3.246392D-01(80) 3.243222D-C1(81) 2.945593D-C1(82) 2.706846D-C1(83) 2.672876D-01(84) 2.661025D-01
 (85) 2.626657D-01(86) 2.559286D-C1(87) 2.457158D-C1(88) 2.321031D-C1(89) 2.152634D-C1(90) 1.954266D-C1
 (91) 1.728677D-C1(92) 1.479040D-C1(93) 1.208722D-01(94) 9.215970D-C2(95) 6.216278D-C2(96) 3.125951D-C2
 (97) C.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 2 = 0.194127D C3

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 2 = 0.249632D C3

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 2 = 0.746430D 01

PRECURSOR CONCENTRATION FOR DELAYED GROUP 1

(1) C.0 (2) 1.701128D-C4(3) 3.377719D-04(4) 5.005587D-C4(5) 6.561253D-C4(6) 8.022277D-C4
 (7) 9.367584D-04(8) 1.057777D-C3(9) 1.163539D-03(10) 1.252522D-C3(11) 1.323454D-C3(12) 1.375366D-C3
 (13) 1.407718D-03(14) 1.420905D-C3(15) 1.418272D-03(16) 1.414233D-C3(17) 1.098251D-03(18) 7.558629D-04
 (19) 7.364296D-04(20) 7.018606D-C4(21) 6.635274D-04(22) 6.255061D-C4(23) 5.891960D-C4(24) 5.550186D-04
 (25) 5.230417D-04(26) 4.932090D-C4(27) 4.654240D-04(28) 4.395811D-C4(29) 4.155759D-C4(30) 3.933093D-C4
 (31) 3.726886D-04(32) 3.536277D-C4(33) 3.360469D-C4(34) 3.198726D-C4(35) 3.050370D-C4(36) 2.914782D-04
 (37) 2.791392D-04(38) 2.679686D-C4(39) 2.579194D-C4(40) 2.489497D-C4(41) 2.410219D-C4(42) 2.341028D-04
 (43) 2.281634D-04(44) 2.231788D-C4(45) 2.191283D-04(46) 2.159948D-C4(47) 2.137652D-C4(48) 2.124302D-C4
 (49) 2.119841D-C4(50) 2.124252D-C4(51) 2.137552D-04(52) 2.159796D-C4(53) 2.191079D-C4(54) 2.231531D-C4
 (55) 2.281320D-04(56) 2.340656D-C4(57) 2.409787D-C4(58) 2.489001D-C4(59) 2.578630D-04(60) 2.679049D-04
 (61) 2.790679D-C4(62) 2.913986D-C4(63) 3.049486D-04(64) 3.197747D-C4(65) 3.359388D-C4(66) 3.535086D-C4
 (67) 3.725575D-C4(68) 3.931653D-C4(69) 4.154178D-04(70) 4.394078D-C4(71) 4.652342D-04(72) 4.930012D-C4
 (73) 5.228144D-04(74) 5.547701D-C4(75) 5.889244D-C4(76) 6.252095D-C4(77) 6.632040D-04(78) 7.015091D-04
 (79) 7.360505D-C4(80) 7.554621D-C4(81) 1.097645D-C3(82) 1.413431D-C3(83) 1.417456D-C3(84) 1.420082D-C3
 (85) 1.406891D-03(86) 1.374552D-C3(87) 1.322666D-03(88) 1.251771D-C3(89) 1.162839D-03(90) 1.057138D-C3
 (91) 9.361903D-04(92) 8.017398D-C4(93) 6.557254D-C4(94) 5.002531D-C4(95) 3.375654D-04(96) 1.700087D-04
 (97) C.0 (

PRECURSOR CONCENTRATION FOR DELAYED GROUP 2

(1) 0.0	(2) 4.541032D-04	(3) 5.016557D-04	(4) 1.336201D-03	(5) 1.751471D-03	(6) 2.141475D-03
(7) 2.500586D-03	(8) 2.823625D-03	(9) 3.105935D-03	(10) 3.343450D-03	(11) 3.532779D-03	(12) 3.671328D-03
(13) 3.757663D-03	(14) 3.792845D-03	(15) 3.785772D-03	(16) 3.774941D-03	(17) 2.921440D-03	(18) 2.017482D-03
(19) 1.965568D-03	(20) 1.873264D-03	(21) 1.770920D-03	(22) 1.669412D-03	(23) 1.572475D-03	(24) 1.481234D-03
(25) 1.395869D-03	(26) 1.316229D-03	(27) 1.242057D-03	(28) 1.173070D-03	(29) 1.108990D-03	(30) 1.049551D-03
(31) 9.545064D-04	(32) 9.436259D-04	(33) 8.966965D-04	(34) 8.535217D-04	(35) 8.139206D-04	(36) 7.777273D-04
(37) 7.447902D-04	(38) 7.149713D-04	(39) 6.881457D-04	(40) 6.642010D-04	(41) 6.430369D-04	(42) 6.245647D-04
(43) 6.087071D-04	(44) 5.953975D-04	(45) 5.845802D-04	(46) 5.762099D-04	(47) 5.702514D-04	(48) 5.666798D-04
(49) 5.654800D-04	(50) 5.666470D-04	(51) 5.701856D-04	(52) 5.761105D-04	(53) 5.844466D-04	(54) 5.952285D-04
(55) 6.085016D-04	(56) 6.243211D-04	(57) 6.427533D-04	(58) 6.638753D-04	(59) 6.877755D-04	(60) 7.145538D-04
(61) 7.443222D-04	(62) 7.772054D-04	(63) 8.133408D-04	(64) 8.528796D-04	(65) 8.959873D-04	(66) 9.428442D-04
(67) 9.936463D-04	(68) 1.048606D-03	(69) 1.107953D-03	(70) 1.171923D-03	(71) 1.240812D-03	(72) 1.314866D-03
(73) 1.394378D-03	(74) 1.479604D-03	(75) 1.570693D-03	(76) 1.667466D-03	(77) 1.768798D-03	(78) 1.870959D-03
(79) 1.963081D-03	(80) 2.014852D-03	(81) 2.927470D-03	(82) 3.769685D-03	(83) 3.780418D-03	(84) 3.787421D-03
(85) 3.752240D-03	(86) 3.665988D-03	(87) 3.527607D-03	(88) 3.238528D-03	(89) 3.101340D-03	(90) 2.819432D-03
(91) 2.496859D-03	(92) 2.138274D-03	(93) 1.748847D-03	(94) 1.334196D-03	(95) 9.003010D-04	(96) 4.534205D-04
(97) 0.0					

PRECURSOR CONCENTRATION FOR DELAYED GROUP 3

(1) 0.0	(2) 1.122905D-04	(3) 2.229605D-04	(4) 2.304129D-04	(5) 4.230970D-04	(6) 5.295310D-04
(7) 6.183232D-04	(8) 6.981924D-04	(9) 7.679864D-04	(10) 8.267002D-04	(11) 8.734948D-04	(12) 9.077292D-04
(13) 9.290487D-04	(14) 9.377154D-04	(15) 9.359280D-04	(16) 9.331973D-04	(17) 7.246054D-04	(18) 4.986232D-04
(19) 4.857447D-04	(20) 4.628932D-04	(21) 4.375665D-04	(22) 4.124516D-04	(23) 3.884706D-04	(24) 3.659005D-04
(25) 3.447857D-04	(26) 3.250884D-04	(27) 3.067447D-04	(28) 2.896843D-04	(29) 2.738382D-04	(30) 2.591406D-04
(31) 2.455300D-04	(32) 2.329496D-04	(33) 2.213463D-04	(34) 2.106715D-04	(35) 2.008803D-04	(36) 1.919316D-04
(37) 1.837877D-04	(38) 1.764145D-04	(39) 1.697809D-04	(40) 1.638591D-04	(41) 1.586241D-04	(42) 1.540540D-04
(43) 1.501296D-04	(44) 1.468343D-04	(45) 1.441543D-04	(46) 1.420783D-04	(47) 1.405975D-04	(48) 1.397057D-04
(49) 1.393990D-04	(50) 1.396763D-04	(51) 1.405385D-04	(52) 1.419892D-04	(53) 1.440345D-04	(54) 1.466829D-04
(55) 1.499454D-04	(56) 1.538357D-04	(57) 1.583700D-04	(58) 1.635672D-04	(59) 1.694491D-04	(60) 1.760403D-04
(61) 1.833683D-04	(62) 1.914638D-04	(63) 2.003607D-04	(64) 2.100960D-04	(65) 2.207107D-04	(66) 2.322490D-04
(67) 2.447592D-04	(68) 2.582937D-04	(69) 2.729088D-04	(70) 2.886655D-04	(71) 3.056287D-04	(72) 3.238668D-04
(73) 3.434493D-04	(74) 3.644393D-04	(75) 3.868737D-04	(76) 4.107079D-04	(77) 4.356652D-04	(78) 4.608267D-04
(79) 4.835159D-04	(80) 4.962664D-04	(81) 7.210469D-04	(82) 9.284868D-04	(83) 9.311299D-04	(84) 9.328541D-04
(85) 9.241885D-04	(86) 9.029440D-04	(87) 8.688599D-04	(88) 8.222889D-04	(89) 7.638687D-04	(90) 6.944336D-04
(91) 6.149830D-04	(92) 5.266624D-04	(93) 4.307456D-04	(94) 3.286159D-04	(95) 2.217464D-04	(96) 1.116786D-04
(97) 0.0					

PRECURSOR CONCENTRATION FOR DELAYED GROUP 4

(1) 0.0	(2) 8.416804D-C5	(3) 1.671203D-C4	(4) 2.476587D-C4	(5) 3.246198D-C4	(6) 3.968920D-C4
(7) 4.634314D-C4	(8) 5.232770D-C4	(9) 5.755648D-C4	(10) 6.155411D-C4	(11) 6.545771D-C4	(12) 6.801922D-C4
(13) 6.961210D-C4	(14) 7.025594D-C4	(15) 7.011527D-C4	(16) 6.990147D-C4	(17) 5.426433D-C4	(18) 3.732939D-C4
(19) 3.635687D-C4	(20) 3.463937D-C4	(21) 3.273770D-C4	(22) 3.085274D-C4	(23) 2.905338D-C4	(24) 2.736024D-C4
(25) 2.577656D-C4	(26) 2.429945D-C4	(27) 2.292405D-C4	(28) 2.164505D-C4	(29) 2.045723D-C4	(30) 1.935563D-C4
(31) 1.833560D-C4	(32) 1.739283D-C4	(33) 1.652335D-C4	(34) 1.572347D-C4	(35) 1.498980D-C4	(36) 1.431924D-C4
(37) 1.370895D-C4	(38) 1.315635D-C4	(39) 1.265910D-C4	(40) 1.221509D-C4	(41) 1.182244D-C4	(42) 1.147949D-C4
(43) 1.118478D-C4	(44) 1.093706D-C4	(45) 1.073529D-C4	(46) 1.057859D-C4	(47) 1.046631D-C4	(48) 1.039796D-C4
(49) 1.037324D-C4	(50) 1.039204D-C4	(51) 1.045443D-C4	(52) 1.056066D-C4	(53) 1.071117D-C4	(54) 1.090658D-C4
(55) 1.114770D-C4	(56) 1.143553D-C4	(57) 1.177128D-C4	(58) 1.215634D-C4	(59) 1.259231D-C4	(60) 1.308103D-C4
(61) 1.362453D-C4	(62) 1.422508D-C4	(63) 1.488519D-C4	(64) 1.560763D-C4	(65) 1.639540D-C4	(66) 1.725181D-C4
(67) 1.818043D-C4	(68) 1.918515D-C4	(69) 2.027016D-C4	(70) 2.143997D-C4	(71) 2.269940D-C4	(72) 2.405354D-C4
(73) 2.550754D-C4	(74) 2.706609D-C4	(75) 2.873193D-C4	(76) 3.050174D-C4	(77) 3.235497D-C4	(78) 3.422338D-C4
(79) 3.590821D-C4	(80) 3.685497D-C4	(81) 3.854802D-C4	(82) 4.095324D-C4	(83) 4.349410D-C4	(84) 4.627735D-C4
(85) 4.863373D-C4	(86) 5.055960D-C4	(87) 5.242465D-C4	(88) 5.436611D-C4	(89) 5.632758D-C4	(90) 5.831066D-C4
(91) 4.567076D-C4	(92) 3.911175D-C4	(93) 3.198863D-C4	(94) 2.440413D-C4	(95) 1.646764D-C4	(96) 8.293629D-C5
(97) 0.0	(

PRECURSOR CONCENTRATION FOR DELAYED GROUP 5

(1) 0.0	(2) 6.722517D-C6	(3) 1.334756D-C5	(4) 1.977508D-C5	(5) 2.592383D-C5	(6) 3.169271D-C5
(7) 3.700209D-C5	(8) 4.177500D-C5	(9) 4.594227D-C5	(10) 4.944362D-C5	(11) 5.222880D-C5	(12) 5.425945D-C5
(13) 5.551445D-C5	(14) 5.600934D-C5	(15) 5.587457D-C5	(16) 5.567323D-C5	(17) 4.317713D-C5	(18) 2.966356D-C5
(19) 2.886265D-C5	(20) 2.747530D-C5	(21) 2.594538D-C5	(22) 2.442165D-C5	(23) 2.298829D-C5	(24) 2.163135D-C5
(25) 2.036309D-C5	(26) 1.918100D-C5	(27) 1.808101D-C5	(28) 1.700587D-C5	(29) 1.610978D-C5	(30) 1.523014D-C5
(31) 1.441596D-C5	(32) 1.366370D-C5	(33) 1.297007D-C5	(34) 1.233205D-C5	(35) 1.174686D-C5	(36) 1.121195D-C5
(37) 1.072498D-C5	(38) 1.028383D-C5	(39) 9.886583D-C6	(40) 9.531491D-C6	(41) 9.217008D-C6	(42) 8.941757D-C6
(43) 8.704530D-C6	(44) 8.504284D-C6	(45) 8.340134D-C6	(46) 8.211351D-C6	(47) 8.117357D-C6	(48) 8.057723D-C6
(49) 8.032167D-C6	(50) 8.040553D-C6	(51) 8.082887D-C6	(52) 8.159323D-C6	(53) 8.270156D-C6	(54) 8.415831D-C6
(55) 8.596938D-C6	(56) 8.814216D-C6	(57) 9.068560D-C6	(58) 9.361020D-C6	(59) 9.692805D-C6	(60) 1.006529D-C5
(61) 1.048003D-C5	(62) 1.093874D-C5	(63) 1.144334D-C5	(64) 1.199593D-C5	(65) 1.259881D-C5	(66) 1.325450D-C5
(67) 1.396574D-C5	(68) 1.473550D-C5	(69) 1.556698D-C5	(70) 1.646364D-C5	(71) 1.742917D-C5	(72) 1.846748D-C5
(73) 1.958250D-C5	(74) 2.077783D-C5	(75) 2.205557D-C5	(76) 2.341318D-C5	(77) 2.483487D-C5	(78) 2.626827D-C5
(79) 2.756083D-C5	(80) 2.828698D-C5	(81) 4.109866D-C5	(82) 5.292185D-C5	(83) 5.307201D-C5	(84) 5.316986D-C5
(85) 5.267560D-C5	(86) 5.146444D-C5	(87) 4.952154D-C5	(88) 4.686698D-C5	(89) 4.353712D-C5	(90) 3.957951D-C5
(91) 3.505110D-C5	(92) 3.001719D-C5	(93) 2.455035D-C5	(94) 1.872545D-C5	(95) 1.263842D-C5	(96) 6.365108D-C6
(97) 0.0	(

PRECURSOR CONCENTRATION FOR DELAYED GROUP 6

(1) 0.0	(2) 1.030495D-06	(3) 2.045939D-06	(4) 3.031500D-06	(5) 3.972782D-06	(6) 4.856039D-06
(7) 5.668371E-06	(8) 6.397915D-06	(9) 7.034024D-06	(10) 7.567428D-06	(11) 7.990415D-06	(12) 8.297120D-06
(13) 8.484318D-06	(14) 8.554367D-06	(15) 8.526971D-06	(16) 8.486921D-06	(17) 6.569384D-06	(18) 4.501609D-06
(19) 4.371582D-06	(20) 4.154232D-06	(21) 3.916393D-06	(22) 3.681883D-06	(23) 3.458767D-06	(24) 3.249369D-06
(25) 3.053948E-06	(26) 2.872050D-06	(27) 2.702993D-06	(28) 2.546056D-06	(29) 2.400532D-06	(30) 2.265756E-06
(31) 2.141106E-06	(32) 2.026009D-06	(33) 1.919931E-06	(34) 1.822385E-06	(35) 1.732921D-06	(36) 1.651124E-06
(37) 1.576619D-06	(38) 1.509061D-06	(39) 1.448138E-06	(40) 1.393568E-06	(41) 1.345099D-06	(42) 1.302505D-06
(43) 1.265587E-06	(44) 1.234171D-06	(45) 1.208110E-06	(46) 1.187278E-06	(47) 1.171574D-06	(48) 1.160918E-06
(49) 1.155255D-06	(50) 1.154548D-06	(51) 1.158786E-06	(52) 1.167976E-06	(53) 1.182149D-06	(54) 1.201356E-06
(55) 1.225671D-06	(56) 1.255188D-06	(57) 1.290260E-06	(58) 1.330324E-06	(59) 1.376247D-06	(60) 1.427983D-06
(61) 1.485743E-06	(62) 1.549766D-06	(63) 1.620316D-06	(64) 1.697686E-06	(65) 1.782197E-06	(66) 1.874200E-06
(67) 1.974077D-06	(68) 2.082244D-06	(69) 2.199152D-06	(70) 2.325284E-06	(71) 2.461161D-06	(72) 2.607329E-06
(73) 2.764344D-06	(74) 2.932712D-06	(75) 3.112726E-06	(76) 3.304026E-06	(77) 3.504385D-06	(78) 3.706415D-06
(79) 3.888594D-06	(80) 3.990885D-06	(81) 5.798247D-06	(82) 7.466124E-06	(83) 7.487181E-06	(84) 7.500881D-06
(85) 7.431064E-06	(86) 7.260129D-06	(87) 6.985980E-06	(88) 6.611452D-06	(89) 6.141676E-06	(90) 5.583354E-06
(91) 4.944524D-06	(92) 4.234393D-06	(93) 3.463200E-06	(94) 2.642067E-06	(95) 1.782833D-06	(96) 8.978907D-07
(97) 0.0					

REGION	NORMALIZED POWER
1	0.3432872E-02
2	0.1242193E-02
3	0.1337118E-01

TOTAL NORMALIZED POWER = 0.1544125E-02

BENCHMARK PROBLEM PROMPT SUPERCRITICAL TRANSIENT
END OF PROBLEM

9.2 Delayed Supercritical Transient

This problem (Problem X-A1 of Reference 7) involves the same core as in Section 9.1, but with initiation from a 1% decrease in the absorption cross section in region 1 occurring in 1.0 seconds.

BENCHMARK PROBLEM DELAYED SUPERCRITICAL TRANSIENT

*** INPUT EDIT ***

2 NEUTRON GROUP(S) , 6 DELAYED GROUP(S) , 3 REGION(S) , 2 COMPOSITION(S)
 SLAB GEOMETRY , LEFT BOUNDARY ZERO RIGHT BOUNDARY ZERO
 IS THERE TO BE END OF PROBLEM PUNCHED OUTPLT NO ,
 ARE THE STEADY STATE FLUXES TO BE PUNCHED NO
 TEST POINTS FOR FREQUENCY CALCULATION 9 33 49 65 89
 GROUP 2 IS SPECIFIED AS THE TEST GROUP FOR THE FREQUENCY CALCULATION

REGION NUMBER	MESH POINT LEFT	BOUNDARIES RIGHT
1	1	17
2	17	81
3	81	97

REGION NUMBER	LENGTH (CM)	MESH SPACING (CM)
1	40.0000	2.5000
2	160.0000	2.5000
3	40.0000	2.5000

FRACTIONAL YIELD FROM DELAYED GROUP I INTO NEUTRON GROUP G	I=1	I=2	I=3	I=4	I=5	I=6
GROUP 1	0.01240	0.03050	0.11100	0.30100	1.14000	3.01000
GROUP 2	C.C	0.0	0.0	0.0	C.C	C.C

GROUP NUMBER	AVERAGE NEUTRON SPEED (CM/SEC)	NEUTRONS PER FISSION	FISSION YIELD
1	0.100000 08	0.250000 01	0.100000 01
2	0.300000 06	0.250000 01	0.0

COMPOSITION 1

GROUP NUMBER	DIFFUSION COEFFICIENT	GROUP DEPENDENT CROSS SECTIONS	
		(CAPTURE)	(FISSION)
1	0.150000D 01	0.700000E-02	0.400000E-02
2	0.500000D 00	0.100000E 00	0.800000E-01

SCATTERING MATRIX GP INTO G (THE TOTAL REMOVAL IS COMPUTED AND STORED AS THE DIAGONAL ELEMENTS)

(G)	GP= 1	GP= 2
1	0.260000D-010.0	
2	0.150000D-C10.180000D 00	

COMPOSITION 2

GROUP NUMBER	DIFFUSION COEFFICIENT	GROUP DEPENDENT CROSS SECTIONS	
		(CAPTURE)	(FISSION)
1	0.100000D 01	0.800000E-02	0.200000E-02
2	0.500000D 00	0.404000E-01	0.396000E-01

SCATTERING MATRIX GP INTO G (THE TOTAL REMOVAL IS COMPUTED AND STORED AS THE DIAGONAL ELEMENTS)

(G)	GP= 1	GP= 2
1	0.200000D-010.0	
2	0.100000D-010.800000D-01	

COMPOSITION ASSIGNMENT TO REGIONS

REGION	COMPOSITION
1	1
2	2
3	1

NO XENON BUILDUP CONSIDERED IN THIS PROBLEM

ARE STEADY STATE CONDITIONS TO BE CALCULATED ? YES

INPUT FLUX DISTRIBUTION

(1) 0.0	(2) 2.963389D-C1	(3) 5.882921D-01	(4) 8.715388C-C1	(5) 1.141887C C0	(6) 1.395336C 00
(7) 1.628134D 00	(8) 1.836836D CC	(9) 2.018354C 0C	(10) 2.170000C CC	(11) 2.289529D CC	(12) 2.375165C 00
(13) 2.425611D 0C	(14) 2.440005D C0	(15) 2.417649C 0C	(16) 2.356881C CC	(17) 2.250384D CC	(18) 2.070800D CC
(19) 1.925089C 0C	(20) 1.797160D CC	(21) 1.680847D CC	(22) 1.573593C CC	(23) 1.474167C C0	(24) 1.381839D 00
(25) 1.296079C 0C	(26) 1.216448D CC	(27) 1.142558D CC	(28) 1.074057C CC	(29) 1.010621C CC	(30) 9.519489C-01
(31) 8.977647D-C1	(32) 8.478128D-C1	(33) 8.018577C-01	(34) 7.596828C-C1	(35) 7.210891D-C1	(36) 6.858947D-C1
(37) 6.539338D-01	(38) 6.250557D-C1	(39) 5.991242D-01	(40) 5.760171C-C1	(41) 5.556254C-C1	(42) 5.378531D-C1
(43) 5.226163C-01	(44) 5.098432D-01	(45) 4.994736C-01	(46) 4.914587D-C1	(47) 4.857605C-C1	(48) 4.823524C-01
(49) 4.812181C-01	(50) 4.823524D-01	(51) 4.857605C-01	(52) 4.914587C-C1	(53) 4.994736D-C1	(54) 5.098432C-01
(55) 5.226163D-01	(56) 5.378531D-C1	(57) 5.556254C-01	(58) 5.760171C-C1	(59) 5.991242D-01	(60) 6.250557D-C1
(61) 6.539338C-01	(62) 6.858947D-01	(63) 7.210891D-01	(64) 7.596828D-C1	(65) 8.018577C-01	(66) 8.478128C-01
(67) 8.977647D-01	(68) 9.519489D-01	(69) 1.010621C 0C	(70) 1.074057C CC	(71) 1.142558D CC	(72) 1.216448C CC
(73) 1.296079D CC	(74) 1.381839D C0	(75) 1.474167C 0C	(76) 1.573593C CC	(77) 1.680847D C0	(78) 1.797160D CC
(79) 1.925089C 0C	(80) 2.070800D CC	(81) 2.250384D CC	(82) 2.356881C CC	(83) 2.417649C C0	(84) 2.440005C 0C
(85) 2.425611C 0C	(86) 2.375165D C0	(87) 2.289529D 0C	(88) 2.170000C CC	(89) 2.018354D C0	(90) 1.836836C 00
(91) 1.628134D 0C	(92) 1.395336D C0	(93) 1.141887C 0C	(94) 8.715388C-C1	(95) 5.882921D-C1	(96) 2.963389D-C1
(97) 0.0	(
(1) 0.0	(2) 2.453354D-C2	(3) 4.870399D-02	(4) 7.215364C-C2	(5) 9.453544C-C2	(6) 1.155182C-01
(7) 1.347913D-C1	(8) 1.520695D-C1	(9) 1.670975D-01	(10) 1.796533C-C1	(11) 1.895539D-C1	(12) 1.966639D-C1
(13) 2.009241D-01	(14) 2.024615D-C1	(15) 2.020363D-C1	(16) 2.028838C-C1	(17) 2.183045C-C1	(18) 2.368475D-01
(19) 2.333879C-01	(20) 2.226800D-C1	(21) 2.100072D-C1	(22) 1.972358D-C1	(23) 1.850011C-C1	(24) 1.734965C-01
(25) 1.627586D-C1	(26) 1.527695D-C1	(27) 1.434938C-01	(28) 1.348922C-C1	(29) 1.269256D-C1	(30) 1.195571D-C1
(31) 1.127521D-01	(32) 1.064786D-C1	(33) 1.007070C-C1	(34) 9.541012C-C2	(35) 9.056306C-C2	(36) 8.614293D-C2
(37) 8.212890C-02	(38) 7.850204D-C2	(39) 7.524524C-C2	(40) 7.234317C-C2	(41) 6.978214C-C2	(42) 6.755008C-02
(43) 6.563646D-02	(44) 6.403226D-C2	(45) 6.272593C-02	(46) 6.172331C-C2	(47) 6.100767D-C2	(48) 6.057963C-C2
(49) 6.043717D-02	(50) 6.057963D-C2	(51) 6.100767C-C2	(52) 6.172331C-C2	(53) 6.272593D-C2	(54) 6.403226D-C2
(55) 6.563646C-02	(56) 6.755008D-C2	(57) 6.978214D-02	(58) 7.234317C-C2	(59) 7.524524D-02	(60) 7.850204C-02
(61) 8.212890C-02	(62) 8.614293D-02	(63) 9.056306C-02	(64) 9.541012C-C2	(65) 1.007070C-C1	(66) 1.064786C-C1
(67) 1.127521D-01	(68) 1.195571D-C1	(69) 1.269256C-01	(70) 1.348922C-C1	(71) 1.434938D-C1	(72) 1.527695D-C1
(73) 1.627586C-01	(74) 1.734965D-C1	(75) 1.850011D-C1	(76) 1.972358C-C1	(77) 2.100072C-01	(78) 2.226800C-01
(79) 2.333879D-01	(80) 2.368475D-C1	(81) 2.183045D-01	(82) 2.028838C-C1	(83) 2.024615C-01	(84) 2.009241D-01
(85) 2.009241D-01	(86) 1.966639D-C1	(87) 1.895539C-01	(88) 1.796533C-C1	(89) 1.670975D-C1	(90) 1.520695D-C1
(91) 1.347913D-01	(92) 1.155182D-C1	(93) 9.453544D-C2	(94) 7.215364C-C2	(95) 4.870399C-02	(96) 2.453354D-02
(97) 0.0	(

THE INITIAL PRECURSOR CONCENTRATIONS ARE CALCULATED FROM THE STEADY STATE FLUX DISTRIBUTION

ARE THERE ANY TIME DEPENDENT CHANGES IN THE CROSS SECTION DATA YES

TIME ZONE	CROSS SECTION	GROUP	REGION	TOTAL LINEAR CHANGE	TOTAL QUADRATIC CHANGE
1	CAPTURE	2	1	-.180000D-C2	C.C

ARE THERE ANY TIME DEPENDENT SOURCES ? NC

EQUILIBRIUM NU(G) (1) C.277307CC C1(2) C.277307CD C1(

EQUILIBRIUM FLUXES

1)C.0 (2)0.2862154D 00(3)0.5683025D 00(4)0.8421926D CC(5)C.1103935D 01(6)C.1349755D C1
7)C.1576107D 01(8)0.1779726D 01(9)C.1957674D C1(10)C.2107386D C1(11)C.2226699D 01(12)C.2313890D 01
13)C.2367680D 01(14)0.2387212D 01(15)C.2371878D C1(16)C.2320559D C1(17)C.2228526D C1(18)C.2070561D 01
19)C.1537223D C1(20)0.1817865D 01(21)C.1708274D C1(22)0.1606625D C1(23)C.1511992D 01(24)C.1423793D C1
25)0.1341590D 01(26)0.1265016D 01(27)C.1193741D C1(28)C.1127462D C1(29)C.1065902D 01(30)0.1008802D 01
31)C.9559232D 00(32)0.9070443D 00(33)C.8619608D CC(34)C.8204839D CC(35)C.7824402D CC(36)C.7476705D CC
37)C.7160292D CC(38)0.6873840D 00(39)C.6616150D 00(40)0.6386144D CC(41)C.6182860D CC(42)C.6005446D CC
43)C.5853161D CC(44)0.5725367D 00(45)C.5621530D CC(46)0.5541215D CC(47)C.5484085D CC(48)C.5449903D CC
49)C.5438525D 00(50)0.5449903D 00(51)C.5484085D CC(52)C.5541215D CC(53)C.5621530D 00(54)C.5725367D CC
55)C.5853161D CC(56)0.6005446D 00(57)0.6182860D CC(58)C.6386144D CC(59)C.6616150D CC(60)C.6873840D CC
61)C.7160292D CC(62)0.7476705D 00(63)C.7824402D CC(64)C.8204839D CC(65)C.8619608D 00(66)C.9070443D CC
67)0.9559232D 00(68)0.1008802D 01(69)C.1065902D C1(70)C.1127462D C1(71)C.1193741D 01(72)0.1265016D 01
73)C.1341590D C1(74)0.1423793D 01(75)0.1511992D C1(76)C.1606625D C1(77)C.1708274D C1(78)C.1817865D C1
79)C.1537223D C1(80)0.2070561D 01(81)C.2228526D 01(82)0.2320559D C1(83)C.2371878D 01(84)C.2387212D C1
85)0.2367680D 01(86)C.2313890D 01(87)C.2226699D C1(88)C.2107386D C1(89)C.1957674D 01(90)0.1779726D 01
91)C.1576107D 01(92)0.1349755D 01(93)0.1103935D 01(94)C.8421926D CC(95)C.5683025D CC(96)C.2862154D CC
97)C.0 (2)0.2369936D-01(3)C.4705688D-C1(4)C.6973568D-C1(5)C.9140864D-01(6)0.1117632D 00
7)C.1305057D 00(8)0.1473659D 00(9)C.1621008D CC(10)C.1744985D CC(11)C.1843832D CC(12)0.1916242D 00
13)C.1961651D CC(14)0.1981376D 00(15)C.1983172D 00(16)0.1999832D CC(17)C.2165068D CC(18)C.2266467D CC
19)C.2346132D 00(20)0.2250399D 00(21)C.2132734D CC(22)0.2012460D CC(23)C.1896364D 00(24)C.1786642D 00
25)C.1683822D 00(26)0.1587817D 00(27)C.1498417D CC(28)C.1415239D CC(29)C.1227972D CC(30)C.1266300D CC
31)C.1199924D CC(32)0.1138569D 00(33)C.1081978D CC(34)C.1029914D CC(35)C.9821599D-01(36)C.9385151D-C1
37)C.8987974D-C1(38)0.8628404D-01(39)C.8304938D-C1(40)C.8016223D-C1(41)C.7761049D-01(42)C.7538350D-C1
43)0.7347194D-01(44)0.7186780D-01(45)C.7056438D-C1(46)C.6955623D-C1(47)C.6883911D-01(48)0.6841004D-C1
49)C.6826721D-C1(50)0.6841004D-01(51)0.6883911D-C1(52)C.6955623D-C1(53)C.7056438D-C1(54)C.7186780D-C1
55)C.7347194D-C1(56)0.7538350D-01(57)C.7761049D-01(58)0.8016223D-C1(59)C.8304938D-C1(60)C.8628404D-C1
61)C.8987974D-01(62)0.9385151D-01(63)C.9821599D-C1(64)C.1029914D CC(65)C.1081978D 00(66)0.1138569D CC
67)C.1199924D 00(68)0.1266300D 00(69)0.1337972D 00(70)C.1415239D CC(71)C.1498417D CC(72)C.1587817D CC
73)C.1683822D CC(74)C.1786642D 00(75)0.1896364D 00(76)0.2012460D CC(77)C.2132734D 00(78)0.2250399D CC
79)C.2346132D 00(80)0.2366467D 00(81)C.2165068D CC(82)C.1999832D CC(83)C.1983172D 00(84)0.1981376D 00
85)C.1961651D 00(86)0.1916242D 00(87)C.1843833D 00(88)0.1744985D CC(89)C.1621008D CC(90)C.1473659D CC
91)C.1305057D CC(92)0.1117632D 00(93)C.9140864D-01(94)0.6973568D-C1(95)C.4705688D-C1(96)C.2369936D-C1
97)C.0 (

1)O.0 (2)O.1700076D-03(3)C.3375631D-C3(4)C.50C2498D-C2(5)C.6557210C-03(6)C.8C17345C-03
7)C.9361841D-C3(8)O.1057131D-02(9)O.1162831C-02(10)O.1251763C-C2(11)C.1322657D-C2(12)C.1374542D-C2
13)C.1406882D-C2(14)O.142C072D-02(15)C.1417446D-C2(16)O.1413421C-C2(17)C.1C97637C-02(18)C.7554563D-C3
19)C.7360447D-03(20)O.7015033D-03(21)O.6631983D-C3(22)C.6252C38D-C3(23)C.5889187C-03(24)C.5547643C-03
25)C.5228085D-C3(26)O.4929951D-03(27)O.4652280C-C3(28)C.4354C13C-C3(29)C.4154111D-03(30)C.3931581C-C3
31)C.3725500D-C3(32)O.3535006D-03(33)O.3359303D-C3(34)O.3197656C-C3(35)O.3C4939C-03(36)O.2913E82C-C3
37)O.2790567D-03(38)O.2678929D-03(39)O.257850C-03(40)C.24E8E6C-C3(41)C.24C9634C-03(42)O.234C491C-03
43)C.2281141D-C3(44)O.2231336D-03(45)O.2190868D-C3(46)C.2159567C-C3(47)C.21373C2D-03(48)C.212398C-C3
49)C.2119546D-C3(50)O.2123980D-03(51)O.2137302D-03(52)O.2159567C-C3(53)O.219C868D-03(54)C.2231336D-C3
55)O.2281141D-03(56)O.2340491D-03(57)C.24C9634C-C3(58)O.24E8E6C-C3(59)C.257850C-03(60)O.2678929C-03
61)O.2790567D-03(62)O.2913882D-03(63)O.304939C-03(64)C.3197656D-C3(65)C.33593C3D-03(66)C.3535006C-03
67)O.3725500D-03(68)O.3931581D-03(69)O.4154111D-03(70)O.4394C13C-C3(71)C.465228C-03(72)O.4929951D-03
73)O.5228085D-03(74)O.5547643D-03(75)C.5889187D-C3(76)C.6252038C-C3(77)C.6631983C-03(78)O.7015033C-03
79)C.7360447D-03(80)O.7554563D-03(81)C.1C97637D-C2(82)O.1413421D-C2(83)C.1417446C-02(84)C.142C072C-02
85)C.14C6882D-C2(86)O.1374542D-02(87)C.1322657C-02(88)O.1251763C-C2(89)C.1162831D-02(90)C.1C57131D-C2
91)O.9361841D-03(92)O.8017345D-03(93)C.6557210D-03(94)C.50C2498C-C3(95)C.3375631C-03(96)O.17C0076C-03
97)C.0 (1)C.0 (2)O.4534131D-03(3)O.9C02864C-03(4)C.1334174D-C2(5)C.174E819D-02(6)C.213E239C-C2
7)C.2496818D-02(8)O.2819385D-02(9)O.3101289D-02(10)O.3338472C-C2(11)O.3527548D-02(12)C.3665926C-C2
13)O.3752176D-02(14)O.3787355D-02(15)C.3780352D-C2(16)C.3769E18C-C2(17)C.2927417C-02(18)O.2C14814C-02
19)C.1963043D-C2(20)O.1870921D-02(21)O.1768761D-C2(22)C.1E67429D-C2(23)C.157C656D-C2(24)C.1479565C-C2
25)C.1394339D-C2(26)O.1314826D-02(27)O.1240771D-02(28)O.1171891C-C2(29)C.11C79C8D-02(30)C.1C48559D-C2
31)O.9935970D-03(32)O.9427919D-03(33)C.8959317D-C3(34)C.852E2C2C-C3(35)C.8132772C-03(36)O.7771371C-03
37)O.7442488D-03(38)O.7144747D-03(39)O.68769C1D-03(40)C.6E37E3C-03(41)C.6426534D-03(42)C.6242128C-03
43)C.6C83841D-03(44)O.5951011D-03(45)O.5843081C-03(46)O.5759601C-C3(47)C.57C22C-03(48)C.5E64691C-03
49)O.5652864D-03(50)O.5664691D-03(51)C.57C022C-03(52)C.57596C1C-C3(53)C.5843081C-03(54)O.5951011C-03
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61)C.7442488D-C3(62)O.7771371D-03(63)O.8132772C-03(64)O.852E2C2C-C3(65)C.8959317D-C3(66)C.9427919D-C3
67)C.9935970D-03(68)O.1048559D-02(69)C.11C79C8C-02(70)O.1171891C-C2(71)O.124C771C-02(72)C.1314826C-02
73)O.1394339D-02(74)O.1479565D-02(75)C.1570656D-C2(76)C.1E67429D-C2(77)C.176E761C-02(78)C.1E7C921C-02
79)C.1963043D-C2(80)O.2014814D-02(81)C.2927417D-C2(82)O.3769E18C-C2(83)C.378C352D-C2(84)C.3787355D-C2
85)C.3752176D-02(86)O.3665926D-02(87)C.3527548D-C2(88)O.3338472C-02(89)C.31C1289C-02(90)C.2E19385D-C2
91)O.2496818D-02(92)O.2138239D-02(93)C.174E819D-C2(94)C.1334174D-C2(95)C.9C02864C-03(96)O.4534131C-03
57)C.0 (

1)C.0 (2)0.1116720D-03(3)0.2217334D-03(4)0.3285965C-C3(5)C.43C72C1D-03(6)0.5266312D-C3
7)0.6149464D-03(8)0.6943921D-03(9)C.7638228D-C3(10)C.8222351C-C3(11)C.8688069C-03(12)0.9028884C-03
13)C.9241311D-03(14)0.9327954D-03(15)0.9310706D-03(16)C.9284267C-C3(17)C.72C9954D-03(18)C.4962327C-03
19)C.4834819D-C3(20)0.4607929D-03(21)C.4356316D-03(22)0.4106744C-C3(23)C.3884400D-C3(24)C.3644052D-C3
25)0.3434145D-C3(26)0.3238312D-03(27)C.3055915D-C3(28)C.2886273C-C3(29)C.2728689C-03(30)0.2582518C-03
31)C.2447150D-03(32)0.2322021D-03(33)C.2206608D-C3(34)C.2100428C-C3(35)C.2003037C-03(36)C.1914027C-03
37)C.1823026D-C3(38)0.1759694D-03(39)0.1693726D-03(40)0.1634845C-C3(41)C.1582804D-03(42)C.1537386D-C3
43)0.1498402D-03(44)0.1465687D-03(45)C.1439104D-C3(46)C.1418544C-C3(47)C.1403915C-03(48)0.1395168C-03
49)C.1392255D-03(50)0.1395168D-03(51)C.1403915D-C3(52)C.1418544C-C3(53)C.1439104C-03(54)C.1465687C-03
55)C.1498402D-C3(56)0.1537386D-03(57)C.1582804D-03(58)0.1634845C-C3(59)C.1693726D-C3(60)C.1759694D-C3
61)C.1823026D-C3(62)0.1914027D-03(63)C.2003037D-C3(64)0.2100428C-C3(65)C.2206608C-03(66)C.2322021D-C3
67)C.2447150D-03(68)0.2582518D-03(69)C.2728689D-C3(70)C.2886273C-C3(71)C.3055915C-03(72)C.3238312C-03
73)C.3434145D-C3(74)0.3644052D-03(75)0.3868400D-03(76)C.4106744C-C3(77)C.4356316D-C3(78)C.4607929C-03
79)C.4834819D-C3(80)0.4962327D-03(81)C.5284267C-C3(82)C.5284267C-C3(83)0.5310706D-03(84)0.5327954C-03
85)0.9241311D-03(86)0.9028884D-03(87)C.8688069D-C3(88)C.8222351C-C3(89)C.7638228C-03(90)0.6943921C-03
91)C.6149464D-03(92)0.5266312D-03(93)0.4307201D-C3(94)C.3285965C-C3(95)C.2217334C-03(96)C.1116720C-C3
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1)0.0 (2)0.8292306D-04(3)C.1646501D-C3(4)C.2440022C-C3(5)C.3198350C-03(6)0.3910546C-03
7)0.4566339D-03(8)0.5156270D-03(9)C.5671833D-03(10)C.6105609D-C3(11)C.6451402C-03(12)0.6704478C-03
13)C.6862217D-C3(14)0.6926555D-03(15)0.6913747D-03(16)0.6894115C-C3(17)C.5252845D-C3(18)C.3684820D-C3
19)0.3590138D-03(20)0.3421658D-03(21)C.3234821D-C3(22)C.3049459C-C3(23)C.2872515C-03(24)0.2705923D-03
25)0.2550055D-03(26)0.2404637D-03(27)C.2269200D-C3(28)C.2143227C-C3(29)C.2026212D-03(30)0.1917671C-03
31)C.1817153D-C3(32)0.1724237D-03(33)C.1638536D-03(34)0.1559691C-C3(35)C.1487373D-C3(36)C.1421277D-C3
37)C.1361129D-C3(38)0.1306676D-03(39)C.1257691D-C3(40)C.1213968C-C3(41)C.1175325C-03(42)C.1141600D-C3
43)C.1112651D-03(44)0.1088358D-03(45)C.1068620D-C3(46)C.1053352D-C3(47)C.1042492C-03(48)C.1035994C-03
49)C.1033831D-C3(50)0.1035994D-03(51)C.1042492C-03(52)C.1053352C-03(53)C.1068620D-03(54)C.1088358C-03
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61)0.1361129D-03(62)0.1421277D-03(63)C.1487373D-C3(64)C.1559691C-C3(65)C.1638536C-03(66)0.1724237C-03
67)C.1817153D-03(68)0.1917671D-03(69)0.2026212D-03(70)C.2143227C-C3(71)C.2269200D-C3(72)C.2404637C-03
73)C.2550055D-C3(74)0.2705923D-03(75)0.2872515D-03(76)0.3049459C-C3(77)C.3234821C-03(78)C.3421658D-C3
79)0.3590138D-03(80)0.3684820D-03(81)C.353845D-C3(82)C.6894115C-C3(83)C.6913747C-03(84)0.6926555C-03
85)C.6862217D-03(86)C.6704478D-03(87)C.6451402D-03(88)C.6105609D-C3(89)C.5671833D-03(90)C.5156270C-03
91)C.4566339D-03(92)0.3910546D-03(93)0.3198350D-03(94)0.2440022C-C3(95)C.1646501D-C3(96)C.8292306D-C4
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1)C.0 (2)0.6361268D-05(3)C.1263078D-04(4)C.1871812D-C4(5)C.2453547D-C4(6)C.2999893C-04
 7)C.35C2971D-C4(8)0.3955524D-04(9)C.4351028D-04(10)0.468379C-C4(11)C.4949C58D-C4(12)C.5143199D-C4
 13)0.5264205D-04(14)0.5313561D-04(15)C.53C3736D-C4(16)C.5288675C-C4(17)C.41C7089C-04(18)0.2826732C-04
 19)0.2754099D-04(20)0.2624853D-04(21)C.2481525D-C4(22)C.2339359D-C4(23)C.22C3589C-04(24)C.2C75792C-04
 25)C.1956221D-C4(26)0.1844667D-04(27)C.1740769C-04(28)0.1644132C-C4(29)C.1554366D-C4(30)C.14711C1D-C4
 31)C.1393991D-C4(32)C.1322712D-04(33)C.1256969D-C4(34)0.1196485C-C4(35)C.1141C07D-04(36)0.1C9C3C3D-C4
 37)0.1044162D-04(38)0.1002389D-04(39)C.9648113D-C5(40)C.93127C3D-C5(41)C.9C1626C-C5(42)0.8757543C-05
 43)C.8535471D-C5(44)0.8349113D-05(45)0.819769C-C5(46)C.8C8C57C-C5(47)C.799726C-C5(48)C.7947413C-C5
 49)C.7930821D-C5(50)0.7947413D-05(51)C.799726C-C5(52)0.808C57C-C5(53)0.819769C-C5(54)C.8349113C-C5
 55)0.8535471D-05(56)0.8757543D-05(57)C.901626C-C5(58)C.93127C3C-C5(59)C.9648113C-05(60)0.1C02389C-04
 61)C.1C44162D-C4(62)0.109C303D-04(63)0.1141C07D-04(64)C.1196485C-C4(65)C.1256969D-C4(66)C.1222712C-04
 67)C.1393991D-C4(68)0.1471101D-04(69)C.1554366D-04(70)0.1644132C-C4(71)0.174C769C-04(72)C.1844667D-C4
 73)0.1956221D-04(74)0.2C75792D-04(75)C.22C3589D-C4(76)C.2339359C-C4(77)C.2481525C-04(78)0.2624853C-04
 79)C.2754099D-04(80)0.2826732D-04(81)C.4107089D-C4(82)C.5288675D-C4(83)C.53C3736D-C4(84)C.5313561C-04
 85)C.52642C5D-04(86)0.5143199D-04(87)C.4949058D-04(88)0.468379C-C4(89)C.4351C28C-C4(90)C.3955524D-C4
 91)0.3502971D-C4(92)0.2999893D-04(93)C.2453547D-C4(94)0.1871812C-04(95)C.1263078C-04(96)0.6361268D-05
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 7)C.4936583D-C5(8)0.5574346D-05(9)C.6131712D-05(10)C.66C0659C-C5(11)C.6974489C-05(12)0.7248C84C-C5
 13)C.7418613C-05(14)0.7488167D-05(15)C.7474321D-C5(16)C.7453C97D-C5(17)C.578794C-C5(18)C.3983589C-05
 19)C.388123C-C5(20)0.3699090D-05(21)0.34971C4C-05(22)C.3296756D-C5(23)C.31C5421D-C5(24)C.2925322C-C5
 25)C.2756816D-C5(26)0.2599607D-05(27)0.2453189D-C5(28)0.2317C03C-C5(29)C.219C5C0C-C5(30)C.2C73158D-C5
 31)C.1964490D-05(32)0.1864040D-05(33)C.1771391D-C5(34)C.1686153C-C5(35)C.16C797C-C5(36)0.1536516C-05
 37)C.1471491D-C5(38)0.1412623D-05(39)C.1359666D-C5(40)C.1312398C-C5(41)C.127C622D-C5(42)C.1234162C-C5
 43)C.12C2866D-C5(44)0.1176604D-05(45)C.1155264D-05(46)0.1138759C-C5(47)C.1127019D-05(48)C.1119994D-C5
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 73)C.2756816D-05(74)0.2925322D-05(75)C.3105421D-C5(76)C.3296756C-C5(77)C.34971C4C-C5(78)C.3699C9C-C5
 79)C.388123C-C5(80)0.3983589D-05(81)C.578794C-C5(82)0.7453C97C-C5(83)C.7474321D-C5(84)C.7488167D-C5
 85)C.7418613D-05(86)0.7248084D-C5(87)C.6974489D-C5(88)0.66C0659C-C5(89)C.6131712D-05(90)C.5574346D-05
 91)C.4936583D-05(92)0.4227618D-05(93)C.3457676D-C5(94)C.2637862C-C5(95)C.178C0C1C-C5(96)0.8964655D-06
 97)C.C (1)C.C (2)C.C (3)C.C (4)C.C (5)C.C (6)C.C (7)C.C (8)C.C (9)C.C (10)C.C (11)C.C (12)C.C (13)C.C (14)C.C (15)C.C (16)C.C (17)C.C (18)C.C (19)C.C (20)C.C (21)C.C (22)C.C (23)C.C (24)C.C (25)C.C (26)C.C (27)C.C (28)C.C (29)C.C (30)C.C (31)C.C (32)C.C (33)C.C (34)C.C (35)C.C (36)C.C (37)C.C (38)C.C (39)C.C (40)C.C (41)C.C (42)C.C (43)C.C (44)C.C (45)C.C (46)C.C (47)C.C (48)C.C (49)C.C (50)C.C (51)C.C (52)C.C (53)C.C (54)C.C (55)C.C (56)C.C (57)C.C (58)C.C (59)C.C (60)C.C (61)C.C (62)C.C (63)C.C (64)C.C (65)C.C (66)C.C (67)C.C (68)C.C (69)C.C (70)C.C (71)C.C (72)C.C (73)C.C (74)C.C (75)C.C (76)C.C (77)C.C (78)C.C (79)C.C (80)C.C (81)C.C (82)C.C (83)C.C (84)C.C (85)C.C (86)C.C (87)C.C (88)C.C (89)C.C (90)C.C (91)C.C (92)C.C (93)C.C (94)C.C (95)C.C (96)C.C (97)C.C (98)C.C (99)C.C (100)C.C

REGION FRACTIONAL POWER

1 0.278998C CC
 2 C.442C024C CC
 3 0.278998C CC

TCTAL NORMALIZED POWER = C.1CCCCC0D C1

BENCHMARK PROBLEM DELAYED SUPERCRITICAL TRANSIENT

TIME ZCNE= 1 STEP NUMBER= 65 TIME=0.100000 CO TIME STEP=C.242726D-C2

TEST POINT	MESH POINT	FREQUENCY	EXP(W*F)
1	9	4.4585D-C1	1.CC0875D CC
2	33	3.3967D-01	1.C00666D CC
3	49	1.7308D-01	1.000339D 00
4	65	3.446D-C2	1.CCCC68D CC
5	89	0.0	1.CCCCCD CC

POINT-WISE FLUXES FOR GRUP 1

(1) C.0 (2) 3.016838D-C1(3) 5.99C086D-01(4) 8.876786D-C1(5) 1.163523D C0(6) 1.422556D 00
 (7) 1.661034D 00(8) 1.875513D C0(9) 2.062892D CC(10) 2.22C465D CC(11) 2.345953D C0(12) 2.437536D 00
 (13) 2.493873D CC(14) 2.514062D 00(15) 2.497467D CC(16) 2.442918D CC(17) 2.345456D CC(18) 2.178325D CC
 (19) 2.037179D CC(20) 1.910817D CC(21) 1.794802D CC(22) 1.6872C9D CC(23) 1.587C54D C0(24) 1.493719D CC
 (25) 1.406738D 00(26) 1.325716D CC(27) 1.25C301D CC(28) 1.18C169D CC(29) 1.115023D 00(30) 1.054586D 00
 (31) 5.986C26D-01(32) 9.468352D-C1(33) 8.99C647D-01(34) 8.55C888D-C1(35) 8.147213D-C1(36) 7.777913D-C1
 (37) 7.441422D-01(38) 7.136314D-C1(39) 6.861297D-01(40) 6.615204D-01(41) 6.396991D-01(42) 6.2C5730D-C1
 (43) 6.040611D-01(44) 5.9C0929D-C1(45) 5.786C9CD-01(46) 5.6556C4D-C1(47) 5.629C82D-01(48) 5.586238D-C1
 (49) 5.566885D-01(50) 5.570933D-C1(51) 5.598395D-01(52) 5.645377D-C1(53) 5.724C88D-C1(54) 5.822835D-01
 (55) 5.946C27D-01(56) 6.094174D-C1(57) 6.267892D-01(58) 6.4679C5D-C1(59) 6.655C45D-01(60) 6.95C262D-C1
 (61) 7.234618D-01(62) 7.549303D-C1(63) 7.895631D-01(64) 8.275C48D-C1(65) 8.689141D-01(66) 9.139642D-01
 (67) 9.628433D-01(68) 1.015756D CC(69) 1.072924D CC(70) 1.134586D CC(71) 1.2C1CC1D CC(72) 1.272447D CC
 (73) 1.349229D CC(74) 1.431674D CC(75) 1.520155D 00(76) 1.615110D CC(77) 1.717122D C0(78) 1.827122D CC
 (79) 1.946943D 00(80) 2.080819D CC(81) 2.239437D CC(82) 2.331851D CC(83) 2.383361D 00(84) 2.398719D 00
 (85) 2.379049D 00(86) 2.324965D CC(87) 2.237327D CC(88) 2.11742CD CC(89) 1.966976D C0(90) 1.788167D C0
 (91) 1.583572D CC(92) 1.356140D CC(93) 1.109152D 00(94) 8.461696D-C1(95) 5.7C9846D-C1(96) 2.875658D-C1
 (97) C.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GRUP 1 = C.7C2472D 02

TOTAL INTEGRATED FLUX FOR REGION 2 GRUP 1 = C.168493D 03

TOTAL INTEGRATED FLUX FOR REGION 3 GRUP 1 = C.670028D 02

POINT-WISE FLUXES FOR GROUP 2

(1) 0.0 (2) 2.500405D-C2(3) 4.964683D-02(4) 7.357227D-C2(5) 9.643469D-C2(6) 1.179038D-C1
 (7) 1.376693D-C1(8) 1.554457D-C1(9) 1.709764D-01(10) 1.840376D-C1(11) 1.944437D-01(12) 2.020568D-C1
 (13) 2.068176D-01(14) 2.088644D-C1(15) 2.090125D-01(16) 2.107064D-C1(17) 2.279811D-01(18) 2.489996D-01
 (19) 2.467321D-01(20) 2.365539D-C1(21) 2.240816D-01(22) 2.113448D-C1(23) 1.990555D-C1(24) 1.874434D-01
 (25) 1.765631D-01(26) 1.664066D-01(27) 1.569450D-01(28) 1.481423D-C1(29) 1.399663D-C1(30) 1.323800D-C1
 (31) 1.253526D-01(32) 1.188543D-C1(33) 1.128577D-01(34) 1.073375D-C1(35) 1.022702D-01(36) 9.763441D-02
 (37) 9.341047D-02(38) 8.958048D-02(39) 8.612821D-02(40) 8.303901D-C2(41) 8.029978D-C2(42) 7.789890D-02
 (43) 7.582614D-02(44) 7.407271D-02(45) 7.263112D-02(46) 7.149522D-C2(47) 7.066015D-C2(48) 7.012229D-C2
 (49) 6.987930D-02(50) 6.993008D-C2(51) 7.027474D-C2(52) 7.091466D-C2(53) 7.185244D-C2(54) 7.309193D-C2
 (55) 7.463826D-02(56) 7.649786D-C2(57) 7.867844D-C2(58) 8.118908D-C2(59) 8.404025D-C2(60) 8.724385D-C2
 (61) 9.081323D-02(62) 9.476331D-02(63) 9.911058D-02(64) 1.038732D-C1(65) 1.090711D-C1(66) 1.147260D-C1
 (67) 1.208616D-01(68) 1.275034D-C1(69) 1.346791D-C1(70) 1.424186D-C1(71) 1.507535D-C1(72) 1.597170D-C1
 (73) 1.693415D-01(74) 1.796539D-C1(75) 1.906610D-C1(76) 2.023096D-C1(77) 2.143790D-01(78) 2.261872D-C1
 (79) 2.357923D-01(80) 2.378218D-C1(81) 2.175697D-C1(82) 2.009576D-C1(83) 1.992779D-C1(84) 1.990930D-C1
 (85) 1.971074D-01(86) 1.925416D-C1(87) 1.852636D-01(88) 1.753297D-C1(89) 1.628712D-C1(90) 1.480651D-C1
 (91) 1.311240D-01(92) 1.122920D-C1(93) 9.184074D-02(94) 7.006508D-C2(95) 4.727904D-02(96) 2.381121D-02
 (97) 0.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 2 = 0.589146D 01

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 2 = 0.207988D 02

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 2 = 0.561426D 01

REGION	NORMALIZED POWER
1	0.105404D 01
2	0.102643D 01
3	0.100478D 01

TOTAL NORMALIZED POWER = 0.102809D 01

BENCHMARK PROBLEM DELAYED SUPERCRITICAL TRANSIENT

TIME ZONE= 1 STEP NUMBER= 177 TIME=0.500000 C0 TIME STEP=C.523461D-C2

TEST POINT	MESH POINT	FREQUENCY	EXP(W*F)
1	9	8.0829D-01	1.003201D CC
2	33	6.8191D-C1	1.002700D CC
3	49	4.1025D-C1	1.001623D CC
4	65	1.3500D-01	1.000534D CC
5	89	6.7972D-C2	1.000269D CC

POINT-WISE FLUXES FOR GROUP 1

(1) C.0	(2) 4.001681D-C1	(3) 7.945125D-C1	(4) 1.177294D CC	(5) 1.542943D C0	(6) 1.886137D CC
(7) 2.201882D 00	(8) 2.485581D CC	(9) 2.733107D CC	(10) 2.940855D CC	(11) 3.105799D C0	(12) 3.225531D 00
(13) 3.298281D 00	(14) 3.322875D CC	(15) 3.298502D CC	(16) 3.223667D CC	(17) 3.091939D C0	(18) 2.866845D 00
(19) 2.676319D CC	(20) 2.505642D 00	(21) 2.348957D 00	(22) 2.203695D CC	(23) 2.068522D CC	(24) 1.942588D CC
(25) 1.825242D CC	(26) 1.715932D CC	(27) 1.614162D 00	(28) 1.519477D 00	(29) 1.431459D C0	(30) 1.349716D CC
(31) 1.273888D 00	(32) 1.203639D CC	(33) 1.138658D CC	(34) 1.078658D CC	(35) 1.023373D C0	(36) 9.725594D-C1
(37) 9.259907D-C1	(38) 8.834608D-C1	(39) 8.447808D-C1	(40) 8.097787D-C1	(41) 7.782987D-C1	(42) 7.502003D-C1
(43) 7.253577D-C1	(44) 7.036595D-C1	(45) 6.850079D-C1	(46) 6.693182D-C1	(47) 6.565189D-C1	(48) 6.465507D-C1
(49) 6.393667D-C1	(50) 6.349322D-C1	(51) 6.332241D-C1	(52) 6.342311D-C1	(53) 6.379539D-C1	(54) 6.444045D-C1
(55) 6.536067D-C1	(56) 6.655961D-C1	(57) 6.804204D-C1	(58) 6.981391D-C1	(59) 7.188243D-C1	(60) 7.425606D-C1
(61) 7.694456D-C1	(62) 7.995903D-C1	(63) 8.331196D-C1	(64) 8.701727D-C1	(65) 9.109037D-C1	(66) 9.554822D-C1
(67) 1.004094D 00	(68) 1.056943D CC	(69) 1.114250D CC	(70) 1.176254D CC	(71) 1.243216D 00	(72) 1.315417D CC
(73) 1.393164D 00	(74) 1.476792D CC	(75) 1.566678D 00	(76) 1.663269D CC	(77) 1.767161D CC	(78) 1.879310D CC
(79) 2.001594D 00	(80) 2.138359D CC	(81) 2.300594D 00	(82) 2.395072D CC	(83) 2.447582D C0	(84) 2.463014D CC
(85) 2.442527D 00	(86) 2.386757D CC	(87) 2.296588D CC	(88) 2.173341D CC	(89) 2.018793D 00	(90) 1.835173D CC
(91) 1.625124D 00	(92) 1.391672D CC	(93) 1.138178D CC	(94) 8.682929D-C1	(95) 5.859035D-C1	(96) 2.950765D-C1
(97) C.0	(

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 1 = C.929578D C2

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 1 = C.196132D C3

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 1 = C.687835D C2

POINT-WISE FLUXES FOR GROUP 2

(1) 0.0 (2) 3.329665D-C2(3) 6.610873D-C2(4) 9.795874D-C2(5) 1.283831D-01(6) 1.569392D-01
 (7) 1.832112D-01(8) 2.068170D-01(9) 2.274132D-01(10) 2.447010D-01(11) 2.584327D-01(12) 2.684248D-01
 (13) 2.745987D-01(14) 2.771362D-01(15) 2.771069D-01(16) 2.790150D-01(17) 3.011626D-01(18) 3.279117D-01
 (19) 3.242287D-01(20) 3.102455D-01(21) 2.933127D-01(22) 2.760827D-01(23) 2.594824D-01(24) 2.438077D-01
 (25) 2.291251D-01(26) 2.154196D-01(27) 2.026492D-01(28) 1.907640D-01(29) 1.797142D-01(30) 1.694517D-01
 (31) 1.599315D-01(32) 1.511117D-01(33) 1.429534D-01(34) 1.354203D-01(35) 1.284793D-01(36) 1.220995D-01
 (37) 1.162527D-01(38) 1.109130D-01(39) 1.060566D-01(40) 1.016619D-01(41) 9.770947D-02(42) 9.418154D-02
 (43) 9.106237D-02(44) 8.833795D-02(45) 8.599600D-02(46) 8.402591D-02(47) 8.241868D-02(48) 8.116686D-02
 (49) 8.026459D-02(50) 7.970747D-02(51) 7.949262D-02(52) 7.961864D-02(53) 8.008558D-02(54) 8.089495D-02
 (55) 8.204975D-02(56) 8.355445D-02(57) 8.541502D-02(58) 8.763894D-02(59) 9.023525D-02(60) 9.321458D-02
 (61) 9.658917D-02(62) 1.003730D-01(63) 1.045816D-01(64) 1.092326D-01(65) 1.143453D-01(66) 1.199410D-01
 (67) 1.260430D-01(68) 1.326767D-01(69) 1.398699D-01(70) 1.476523D-01(71) 1.560559D-01(72) 1.651129D-01
 (73) 1.748594D-01(74) 1.853193D-01(75) 1.965001D-01(76) 2.083469D-01(77) 2.206326D-01(78) 2.326564D-01
 (79) 2.424236D-01(80) 2.444159D-01(81) 2.235300D-01(82) 2.064132D-01(83) 2.046508D-01(84) 2.044314D-01
 (85) 2.023683D-01(86) 1.976604D-01(87) 1.901722D-01(88) 1.799614D-01(89) 1.671621D-01(90) 1.519584D-01
 (91) 1.345656D-01(92) 1.152350D-01(93) 9.424483D-02(94) 7.189748D-02(95) 4.851472D-02(96) 2.443329D-02
 (97) 0.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 2 = 0.782531D 01

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 2 = 0.242103D 02

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 2 = 0.576359D 01

REGION NORMALIZED POWER

1 0.1398077D 01
 2 0.1194797D 01
 3 0.1031505D 01

TOTAL NORMALIZED POWER = 0.1205954D 01

BENCHMARK PROBLEM DELAYED SUPERCRITICAL TRANSIENT

TIME ZONE= 1 STEP NUMBER= 272 TIME=C.1CCCCOD C1 TIME STEP=C.355353D-C2

TEST POINT	MESH POINT	FREQUENCY	EXP(W*F)
1	9	1.6015C C0	1.001812D 00
2	33	1.4628D CC	1.CC1655D CC
3	49	1.0743D C0	1.CC1215D CC
4	65	5.0491C-01	1.CC0571D CC
5	89	3.1852D-01	1.000360D 00

POINT-WISE FLUXES FOR GROUP 1

(1) 0.0 (2) 6.921405D-01(3) 1.374115D 00(4) 2.C259C6D CC(5) 2.667793D C0(6) 3.26C495D CC
 (7) 3.805305D C0(8) 4.294220D C0(9) 4.720058D 00(10) 5.076561C CC(11) 5.358489D C0(12) 5.561687D CC
 (13) 5.683121D 00(14) 5.720813D CC(15) 5.673434D CC(16) 5.538536C CC(17) 5.305359D C0(18) 4.908603D 00
 (19) 4.571807D 00(20) 4.269854D CC(21) 3.992677D CC(22) 3.735795D CC(23) 3.496856D C0(24) 3.274306C 00
 (25) 3.066958D CC(26) 2.873789D C0(27) 2.693882D 00(28) 2.526393C CC(29) 2.37C542D CC(30) 2.2256C3D CC
 (31) 2.090904C 00(32) 1.965817D CC(33) 1.849762D CC(34) 1.742198C CC(35) 1.642626C 00(36) 1.550583C 00
 (37) 1.465638C 00(38) 1.387397D CC(39) 1.315494D CC(40) 1.249594D CC(41) 1.189387D C0(42) 1.134592C 00
 (43) 1.084951D CC(44) 1.040230D C0(45) 1.000218C 00(46) 9.647246C-C1(47) 9.2358C6D-C1(48) 9.C66362D-C1
 (49) 8.837607D-C1(50) 8.648417D-C1(51) 8.49785CC-01(52) 8.385132C-C1(53) 8.3C9664D-C1(54) 8.271010D-C1
 (55) 8.268899C-01(56) 8.303224D-C1(57) 8.374C38D-C1(58) 8.461555D-C1(59) 8.626153D-C1(60) 8.8C8372C-01
 (61) 9.028915C-01(62) 9.288657D-C1(63) 9.58864CC-01(64) 9.930083C-C1(65) 1.C31439D C0(66) 1.C74314C CC
 (67) 1.121811D CC(68) 1.174128D CC(69) 1.231483C 00(70) 1.294118C C0(71) 1.362295D C0(72) 1.4363C3D CC
 (73) 1.516457C 00(74) 1.603106D CC(75) 1.696643D CC(76) 1.797539D CC(77) 1.906425D 00(78) 2.024320D 00
 (79) 2.153234C CC(80) 2.297821D C0(81) 2.469865C CC(82) 2.569957C CC(83) 2.625144D CC(84) 2.64C7C2C CC
 (85) 2.617894D CC(86) 2.557411D CC(87) 2.460207C 00(88) 2.3277C0C C0(89) 2.161795D 00(90) 1.964873D CC
 (91) 1.739760C 00(92) 1.489685D CC(93) 1.218236D CC(94) 9.293C88C-C1(95) 6.270475C-01(96) 3.157892D-01
 (97) 0.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GRUP 1 = C.160288C 03

TOTAL INTEGRATED FLUX FOR REGION 2 GRUP 1 = C.277738D C3

TOTAL INTEGRATED FLUX FOR REGION 3 GRUP 1 = C.737011D C2

POINT-WISE FLUXES FOR GROUP 2

(1) 0.0	(2) 5.787691D-C2((3) 1.149C37D-C1((4) 1.7C2428D-C1((5) 2.230813D-C1((6) 2.726431D-C1
(7) 3.182C03D-01((8) 3.590836D-C1((9) 3.946929D-01((10) 4.245C68D-C1((11) 4.48C942D-C1((12) 4.651365D-01
(13) 4.754977D-C1((14) 4.794891D-C1((15) 4.789348D-C1((16) 4.814834D-C1((17) 5.181C45D-C1((18) 5.618953D-C1
(19) 5.540441D-01((20) 5.287981D-C1((21) 4.986538D-C1((22) 4.681118D-C1((23) 4.387378D-C1((24) 4.110234D-01
(25) 3.850712D-01((26) 3.608456D-C1((27) 3.382654D-C1((28) 3.172274D-C1((29) 2.97668D-C1((30) 2.794680D-01
(31) 2.625533D-C1((32) 2.468457D-C1((33) 2.32272D-C1((34) 2.187648D-C1((35) 2.06261D-C1((36) 1.947C25D-C1
(37) 1.840355D-C1((38) 1.742102D-C1((39) 1.6518C8D-C1((40) 1.569C52D-C1((41) 1.493444D-C1((42) 1.424633D-C1
(43) 1.362293D-C1((44) 1.306131D-C1((45) 1.255881D-C1((46) 1.2113C6D-C1((47) 1.172191D-C1((48) 1.138350D-C1
(49) 1.109618D-C1((50) 1.085853D-C1((51) 1.066938D-C1((52) 1.052775D-C1((53) 1.043289D-C1((54) 1.038426D-C1
(55) 1.038150D-C1((56) 1.042449D-C1((57) 1.051329D-C1((58) 1.064817D-C1((59) 1.082961D-01((60) 1.105828D-C1
(61) 1.133506D-01((62) 1.166105D-C1((63) 1.203757D-C1((64) 1.246613D-C1((65) 1.294850D-01((66) 1.348667D-C1
(67) 1.408286D-01((68) 1.473955D-C1((69) 1.545549D-01((70) 1.624564D-C1((71) 1.71C125D-C1((72) 1.8C2971D-C1
(73) 1.903439D-01((74) 2.011804D-C1((75) 2.128124D-01((76) 2.251796D-C1((77) 2.38C375D-C1((78) 2.5C6331D-C1
(79) 2.608257D-01((80) 2.626935D-C1((81) 2.4CC311D-C1((82) 2.215C62D-C1((83) 2.195C66D-01((84) 2.191853D-C1
(85) 2.169023D-01((86) 2.117973D-C1((87) 2.037247D-01((88) 1.927466D-C1((89) 1.79CC75D-01((90) 1.627C10D-01
(91) 1.44C605D-C1((92) 1.233531D-C1((93) 1.008758D-01((94) 7.695122D-C2((95) 5.192253D-C2((96) 2.614886D-C2
(97) 0.0	(

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 2 = 0.135573D C2

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 2 = 0.342823D C2

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 2 = 0.617601D C1

PRECURSOR CONCENTRATION FOR DELAYED GROUP 1

(1) 0.0	(2) 1.710523D-C4((3) 3.39637C-C4((4) 5.03322D-C4((5) 6.597458D-C4((6) 8.06652D-C4
(7) 9.419212D-C4((8) 1.063602D-C3((9) 1.16994C-C3((10) 1.2594C5D-C3((11) 1.33C717D-C3((12) 1.3829C1D-C3
(13) 1.415417D-C3((14) 1.428664D-C3((15) 1.425993D-C3((16) 1.4219C4D-C3((17) 1.104172D-C3((18) 7.599C27D-C4
(19) 7.403379D-C4((20) 7.055599D-C4((21) 6.669998D-C4((22) 6.287549D-C4((23) 5.922319D-C4((24) 5.57854C-C4
(25) 5.256894D-C4((26) 4.956812D-C4((27) 4.677325D-C4((28) 4.417367D-C4((29) 4.175888D-C4((30) 3.951890D-C4
(31) 3.744441D-C4((32) 3.552674D-C4((33) 3.375785D-C4((34) 3.213C34D-C4((35) 3.063739D-C4((36) 2.927274D-C4
(37) 2.803069D-C4((38) 2.690602D-C4((39) 2.5894C2D-C4((40) 2.499C46D-C4((41) 2.419154D-C4((42) 2.349392D-C4
(43) 2.289468D-C4((44) 2.239129D-C4((45) 2.198166D-C4((46) 2.1664C7D-C4((47) 2.143717D-C4((48) 2.13CC3D-C4
(49) 2.125205D-C4((50) 2.129305D-C4((51) 2.142318D-C4((52) 2.164299D-C4((53) 2.195340D-C4((54) 2.235571D-C4
(55) 2.285159D-C4((56) 2.344311D-C4((57) 2.413276D-C4((58) 2.492342D-C4((59) 2.581839D-C4((60) 2.682142D-C4
(61) 2.79367D-C4((62) 2.916890D-C4((63) 3.052318D-C4((64) 3.2C0519D-C4((65) 3.362115D-C4((66) 3.537780D-C4
(67) 3.728251D-C4((68) 3.934322D-C4((69) 4.156855D-C4((70) 4.396775D-C4((71) 4.655C72D-C4((72) 4.932788D-C4
(73) 5.230981D-C4((74) 5.550611D-C4((75) 5.892242D-C4((76) 6.255194D-C4((77) 6.635251D-C4((78) 7.018419D-C4
(79) 7.363936D-C4((80) 7.558089D-C4((81) 1.098143D-C3((82) 1.414C66D-C3((83) 1.418C89D-C3((84) 1.42C712D-C3
(85) 1.407513D-C3((86) 1.375156D-C3((87) 1.323246D-C3((88) 1.252318D-C3((89) 1.163345D-C3((90) 1.057597D-C3
(91) 9.365966D-C4((92) 8.020872D-C4((93) 6.56CC91D-C4((94) 5.0C4694D-C4((95) 3.377112D-C4((96) 1.7C0822D-C4
(97) 0.0	(

PRECURSOR CONCENTRATION FOR DELAYED GROUP 2

(1) 0.0	(2) 4.602329D-04((3) 9.138245D-04((4) 1.354229C-03((5) 1.775092C-03((6) 2.170340C-03
(7) 2.534270D-03((8) 2.861630D-03((9) 3.147698D-03((10) 3.388356D-03((11) 3.580164D-03((12) 3.720495C-03
(13) 3.807896D-03((14) 3.843440D-03((15) 3.836143C-03((16) 3.824993C-03((17) 2.970074D-03((18) 2.043840C-03
(19) 1.991069D-03((20) 1.897402D-03((21) 1.793577D-03((22) 1.690611C-03((23) 1.592284C-03((24) 1.499735C-03
(25) 1.413145D-03((26) 1.332361D-03((27) 1.257120D-03((28) 1.187136D-03((29) 1.122124D-03((30) 1.061817C-03
(31) 1.005962D-03((32) 9.543255D-04((33) 9.066910C-04((34) 8.628586C-04((35) 8.226444D-04((36) 7.858797D-04
(37) 7.524101C-04((38) 7.220951D-04((39) 6.948075C-04((40) 6.704327C-04((41) 6.488683D-04((42) 6.300237D-04
(43) 6.138199C-04((44) 6.001887D-04((45) 5.890727D-04((46) 5.804254D-04((47) 5.742101D-04((48) 5.704008C-04
(49) 5.689812D-04((50) 5.699453D-04((51) 5.732969C-04((52) 5.790498C-04((53) 5.872281D-04((54) 5.976658D-04
(55) 6.110072D-04((56) 6.267073D-04((57) 6.450317C-04((58) 6.660569C-04((59) 6.898708C-04((60) 7.165731D-04
(61) 7.462753C-04((62) 7.791017D-04((63) 8.151896D-04((64) 8.546899D-04((65) 8.977680C-04((66) 9.446039C-04
(67) 9.953936D-04((68) 1.050349D-03((69) 1.109701C-03((70) 1.173695C-03((71) 1.242595D-03((72) 1.316610C-03
(73) 1.396231C-03((74) 1.481505D-03((75) 1.572652C-03((76) 1.669491C-03((77) 1.770896D-03((78) 1.873133D-03
(79) 1.965323C-03((80) 2.017119D-03((81) 2.930720D-03((82) 3.773834C-03((83) 3.784551D-03((84) 3.791538C-03
(85) 3.756300D-03((86) 3.669938D-03((87) 3.531395D-03((88) 3.342102C-03((89) 3.104652D-03((90) 2.822435C-03
(91) 2.499514D-03((92) 2.140544D-03((93) 1.750702D-03((94) 1.335609C-03((95) 9.012541D-04((96) 4.539003D-04
(97) 0.0	(

PRECURSOR CONCENTRATION FOR DELAYED GROUP 3

(1) 0.0	(2) 1.176542D-04((3) 2.336086C-04((4) 3.461883C-04((5) 4.537667D-04((6) 5.547898D-04
(7) 6.477982C-04((8) 7.314482D-04((9) 8.045321D-04((10) 8.659960C-04((11) 9.149609C-04((12) 9.507551C-04
(13) 9.730074C-04((14) 9.819921D-04((15) 9.800094C-04((16) 9.770015C-04((17) 7.584180C-04((18) 5.216941C-04
(19) 5.080661D-04((20) 4.840223D-04((21) 4.574008C-04((22) 4.310100C-04((23) 4.058131D-04((24) 3.820988D-04
(25) 3.599124C-04((26) 3.392136D-04((27) 3.195347C-04((28) 3.020013C-04((29) 2.852403C-04((30) 2.698824D-04
(31) 2.555625C-04((32) 2.423203D-04((33) 2.300999D-04((34) 2.188495D-04((35) 2.085217D-04((36) 1.990728C-04
(37) 1.904628C-04((38) 1.826552D-04((39) 1.756172C-04((40) 1.693188C-04((41) 1.637234D-04((42) 1.588373C-04
(43) 1.546098C-04((44) 1.510329D-04((45) 1.480914C-04((46) 1.457728C-04((47) 1.440673D-04((48) 1.429673D-04
(49) 1.424683C-04((50) 1.425679D-04((51) 1.432664D-04((52) 1.445666C-04((53) 1.464739D-04((54) 1.489959C-04
(55) 1.521433C-04((56) 1.559291D-04((57) 1.603691C-04((58) 1.654817C-04((59) 1.712882D-04((60) 1.778130C-04
(61) 1.850832D-04((62) 1.931292D-04((63) 2.019847C-04((64) 2.116866C-04((65) 2.222755D-04((66) 2.337957D-04
(67) 2.462954C-04((68) 2.598268D-04((69) 2.744464D-04((70) 2.902150C-04((71) 3.071977C-04((72) 3.254630C-04
(73) 3.450804C-04((74) 3.661132D-04((75) 3.885984D-04((76) 4.124909D-04((77) 4.375129D-04((78) 4.627417C-04
(79) 4.854904D-04((80) 4.982630D-04((81) 7.239107C-04((82) 9.321423C-04((83) 9.347709D-04((84) 9.364815D-04
(85) 9.277654C-04((86) 9.064245D-04((87) 8.721973D-04((88) 8.254379C-04((89) 7.667865C-04((90) 6.970803C-04
(91) 6.173226C-04((92) 5.286629D-04((93) 4.323797D-04((94) 3.298614D-04((95) 2.225863D-04((96) 1.121014C-04
(97) 0.0	(

PRECURSOR CONCENTRATION FOR DELAYED GROUP 4

(1) 0.0 (2) 9.438311D-05(3) 1.873997D-04(4) 2.777031D-04(5) 3.639858D-04(6) 4.449986E-04
 (7) 5.195686E-04(8) 5.866162D-04(9) 6.451711E-04(10) 6.943872E-04(11) 7.235589D-04(12) 7.621476E-04
 (13) 7.798562D-04(14) 7.869040D-04(15) 7.851296E-04(16) 7.824695E-04(17) 6.070706D-04(18) 4.172615E-04
 (19) 4.061134E-04(20) 3.866704D-04(21) 3.651895D-04(22) 3.439114E-04(23) 3.236029D-04(24) 3.044929E-04
 (25) 2.866155E-04(26) 2.699370D-04(27) 2.544015D-04(28) 2.399485E-04(29) 2.26518E-04(30) 2.140533E-04
 (31) 2.025013D-04(32) 1.918127D-04(33) 1.819416E-04(34) 1.728458E-04(35) 1.644862D-04(36) 1.568271D-04
 (37) 1.498355E-04(38) 1.434815D-04(39) 1.377378D-04(40) 1.325797E-04(41) 1.279849D-04(42) 1.239338E-04
 (43) 1.204087E-04(44) 1.173946D-04(45) 1.148783E-04(46) 1.128488E-04(47) 1.112974D-04(48) 1.102171E-04
 (49) 1.096031D-04(50) 1.094525D-04(51) 1.097644E-04(52) 1.105398E-04(53) 1.117818D-04(54) 1.134953D-04
 (55) 1.156873E-04(56) 1.183668D-04(57) 1.215448D-04(58) 1.252344E-04(59) 1.294511E-04(60) 1.342122E-04
 (61) 1.395376E-04(62) 1.454495D-04(63) 1.519726D-04(64) 1.591341D-04(65) 1.669638D-04(66) 1.754945E-04
 (67) 1.847618D-04(68) 1.948046D-04(69) 2.056646E-04(70) 2.173870E-04(71) 2.300203D-04(72) 2.436155D-04
 (73) 2.582241D-04(74) 2.738935D-04(75) 2.906509E-04(76) 3.084627E-04(77) 3.271210D-04(78) 3.459363D-04
 (79) 3.629003E-04(80) 3.724114D-04(81) 5.410198E-04(82) 6.966044E-04(83) 6.985385D-04(84) 6.997922E-04
 (85) 6.932585D-04(86) 6.772947D-04(87) 6.517055E-04(88) 6.167553E-04(89) 5.729226D-04(90) 5.208329D-04
 (91) 4.612356E-04(92) 3.949893D-04(93) 3.230491E-04(94) 2.464519E-04(95) 1.663020D-04(96) 8.375468D-05
 (97) 0.0 (

PRECURSOR CONCENTRATION FOR DELAYED GROUP 5

(1) 0.0 (2) 9.082536D-06(3) 1.803285E-05(4) 2.672064E-05(5) 3.501943D-05(6) 4.280840D-05
 (7) 4.997417E-05(8) 5.641241D-05(9) 6.202943D-05(10) 6.674361E-05(11) 7.048698D-05(12) 7.320777E-05
 (13) 7.487749E-05(14) 7.551717D-05(15) 7.530206E-05(16) 7.498648E-05(17) 5.809593D-05(18) 3.985292E-05
 (19) 3.872816E-05(20) 3.681981D-05(21) 3.472258E-05(22) 3.264908E-05(23) 3.067179D-05(24) 2.881199E-05
 (25) 2.707249E-05(26) 2.544968D-05(27) 2.393785D-05(28) 2.253088E-05(29) 2.122274E-05(30) 2.000772E-05
 (31) 1.888046E-05(32) 1.783599D-05(33) 1.686969E-05(34) 1.597727D-05(35) 1.515478D-05(36) 1.439858E-05
 (37) 1.370531D-05(38) 1.307188D-05(39) 1.249549E-05(40) 1.197357E-05(41) 1.150379D-05(42) 1.108406D-05
 (43) 1.071248E-05(44) 1.038740D-05(45) 1.010734D-05(46) 9.871037E-06(47) 9.677407E-06(48) 9.525556D-06
 (49) 9.414769E-06(50) 9.344511D-06(51) 9.314420D-06(52) 9.324309D-06(53) 9.374161E-06(54) 9.464135E-06
 (55) 9.594558D-06(56) 9.765932D-06(57) 9.978935E-06(58) 1.023442E-05(59) 1.053343D-05(60) 1.087719D-05
 (61) 1.126710E-05(62) 1.170477D-05(63) 1.219203E-05(64) 1.273088E-05(65) 1.332358D-05(66) 1.397259E-05
 (67) 1.468062E-05(68) 1.545062D-05(69) 1.628580E-05(70) 1.718965E-05(71) 1.816588E-05(72) 1.921845E-05
 (73) 2.035136E-05(74) 2.156826D-05(75) 2.287125E-05(76) 2.425765E-05(77) 2.571111D-05(78) 2.717751E-05
 (79) 2.849924E-05(80) 2.923671D-05(81) 4.246185E-05(82) 5.46628E-05(83) 5.480673D-05(84) 5.489869E-05
 (85) 5.438079E-05(86) 5.312410D-05(87) 5.111330E-05(88) 4.836916E-05(89) 4.492919D-05(90) 4.084241E-05
 (91) 3.616757E-05(92) 3.097193D-05(93) 2.533032E-05(94) 1.922995E-05(95) 1.303933D-05(96) 6.566946E-06
 (97) 0.0 (

PRECURSOR CONCENTRATION FOR DELAYED GROUP 6

(1) 0.0 (2) 1.601972D-06(3) 3.180524D-06(4) 4.712577D-06(5) 6.175733D-06(6) 7.548599D-06
 (7) 8.811105D-06(8) 9.944792D-06(9) 1.093309D-05(10) 1.176158D-05(11) 1.241826D-05(12) 1.289400D-05
 (13) 1.318381D-05(14) 1.329137D-05(15) 1.324738D-05(16) 1.318359D-05(17) 1.020286D-05(18) 6.988265D-06
 (19) 6.782801D-06(20) 6.441118D-06(21) 6.067101D-06(22) 5.697845D-06(23) 5.345948D-06(24) 5.015067D-06
 (25) 4.705633D-06(26) 4.416955D-06(27) 4.147988D-06(28) 3.897609D-06(29) 3.664718D-06(30) 3.448273D-06
 (31) 3.247298D-06(32) 3.060884D-06(33) 2.888185D-06(34) 2.728419D-06(35) 2.580860D-06(36) 2.444838D-06
 (37) 2.319736D-06(38) 2.204982D-06(39) 2.100056D-06(40) 2.004478D-06(41) 1.917812D-06(42) 1.839660D-06
 (43) 1.769664D-06(44) 1.707502D-06(45) 1.652885D-06(46) 1.605561D-06(47) 1.565307D-06(48) 1.531933D-06
 (49) 1.505280D-06(50) 1.485216D-06(51) 1.471642D-06(52) 1.464484D-06(53) 1.463698D-06(54) 1.469266D-06
 (55) 1.481201D-06(56) 1.499541D-06(57) 1.524352D-06(58) 1.555730D-06(59) 1.593796D-06(60) 1.638704D-06
 (61) 1.690634D-06(62) 1.749798D-06(63) 1.816439D-06(64) 1.890832D-06(65) 1.973283D-06(66) 2.064137D-06
 (67) 2.163769D-06(68) 2.272597D-06(69) 2.391073D-06(70) 2.519691D-06(71) 2.658982D-06(72) 2.809508D-06
 (73) 2.971842D-06(74) 3.146507D-06(75) 3.333801D-06(76) 3.533327D-06(77) 3.742706D-06(78) 3.954068D-06
 (79) 4.144509D-06(80) 4.250162D-06(81) 6.170733D-06(82) 7.942123D-06(83) 7.961708D-06(84) 7.973983D-06
 (85) 7.897861D-06(86) 7.714596D-06(87) 7.421968D-06(88) 7.022996D-06(89) 6.523123D-06(90) 5.929466D-06
 (91) 5.250544D-06(92) 4.496116D-06(93) 3.677029D-06(94) 2.805064D-06(95) 1.892759D-06(96) 9.532337D-07
 (97) 0.0 (

REGION NORMALIZED POWER

1 0.2417898D 01
 2 0.1691876D 01
 3 0.1105293D 01

TOTAL NORMALIZED POWER = 0.1730779D 01

*** INPUT EDIT FOR TIME ZONE 2 ***

CARD 21 0.25000D-C2 1-.30000D 01 0 -2 0 0 0 1

CARD 22 0.15000D C10.20000D 01

ARE THERE ANY TIME DEPENDENT CHANGES IN THE
 CROSS SECTION DATA NO

ARE THERE ANY TIME DEPENDENT SOURCES ? NO

BENCHMARK PROBLEM DELAYED SUPERCRITICAL TRANSIENT

TIME ZONE= 2 STEP NUMBER= 200 TIME=0.150000 G1 TIME STEP=0.250000-02

TEST POINT	MESH POINT	FREQUENCY	EXP(W*H)
1	9	2.3870D-01	1.000597D 00
2	33	2.3162D-01	1.000579D 00
3	49	1.8913D-01	1.000473D 00
4	65	1.1109D-01	1.000278D 00
5	89	8.2628D-02	1.000207D 00

POINT-WISE FLUXES FOR GROUP 1

(1) 0.0 (2) 8.150433D-01(3) 1.618111D 00(4) 2.397402D 00(5) 3.141468D 00(6) 3.839373D 00
 (7) 4.480863D 00(8) 5.056512D 00(9) 5.557860D 00(10) 5.977538D 00(11) 6.309375D 00(12) 6.548478D 00
 (13) 6.691279D 00(14) 6.735450D 00(15) 6.679431D 00(16) 6.520348D 00(17) 6.245545D 00(18) 5.777987D 00
 (19) 5.380977D 00(20) 5.024948D 00(21) 4.698052D 00(22) 4.395019D 00(23) 4.113065D 00(24) 3.850376D 00
 (25) 3.605547D 00(26) 3.377376D 00(27) 3.164781D 00(28) 2.966766D 00(29) 2.782411D 00(30) 2.610860D 00
 (31) 2.451318D 00(32) 2.303045D 00(33) 2.165353D 00(34) 2.037604D 00(35) 1.919204D 00(36) 1.809604D 00
 (37) 1.708294D 00(38) 1.614804D 00(39) 1.528699D 00(40) 1.449577D 00(41) 1.377070D 00(42) 1.310838D 00
 (43) 1.250573D 00(44) 1.195991D 00(45) 1.146835D 00(46) 1.102874D 00(47) 1.063900D 00(48) 1.029727D 00
 (49) 1.000190D 00(50) 9.751485D-01(51) 9.544785D-01(52) 9.380776D-01(53) 9.258621D-01(54) 9.177674D-01
 (55) 9.137470D-01(56) 9.137728D-01(57) 9.178346D-01(58) 9.259402D-01(59) 9.381152D-01(60) 9.544032D-01
 (61) 9.748660D-01(62) 9.995838D-01(63) 1.028655D 00(64) 1.062198D 00(65) 1.100350D 00(66) 1.143268D 00
 (67) 1.191131D 00(68) 1.244137D 00(69) 1.302510D 00(70) 1.366494D 00(71) 1.436359D 00(72) 1.512402D 00
 (73) 1.594948D 00(74) 1.684357D 00(75) 1.781038D 00(76) 1.885478D 00(77) 1.998336D 00(78) 2.120674D 00
 (79) 2.254592D 00(80) 2.404959D 00(81) 2.584094D 00(82) 2.688270D 00(83) 2.745525D 00(84) 2.761391D 00
 (85) 2.737195D 00(86) 2.673664D 00(87) 2.571800D 00(88) 2.433086D 00(89) 2.259513D 00(90) 2.053568D 00
 (91) 1.818203D 00(92) 1.556789D 00(93) 1.273071D 00(94) 9.711140D-01(95) 6.552437D-01(96) 3.299857D-01
 (97) 0.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 1 = 0.188728D 03

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 1 = 0.314975D 03

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 1 = 0.770512D 02

PCINT-WISE FLUXES FOR GROUP 2

(1) 0.0 (2) 6.815568D-02(3) 1.353099D-01(4) 2.004760D-01(5) 2.626963D-01(6) 3.210566D-01
 (7) 3.746995D-01(8) 4.228367D-01(9) 4.647613D-01(10) 4.998593D-01(11) 5.276229D-01(12) 5.476772D-01
 (13) 5.598620D-01(14) 5.645441D-01(15) 5.638710D-01(16) 5.668471D-01(17) 6.099298D-01(18) 6.614340D-01
 (19) 6.521300D-01(20) 6.223402D-01(21) 5.867779D-01(22) 5.507426D-01(23) 5.160777D-01(24) 4.833625D-01
 (25) 4.527174D-01(26) 4.241005D-01(27) 3.974163D-01(28) 3.725544D-01(29) 3.494049D-01(30) 3.278621D-01
 (31) 3.078269D-01(32) 2.892067D-01(33) 2.719152D-01(34) 2.558722D-01(35) 2.410033D-01(36) 2.272395D-01
 (37) 2.145168D-01(38) 2.027760D-01(39) 1.919626D-01(40) 1.820261D-01(41) 1.729203D-01(42) 1.646025D-01
 (43) 1.570339D-01(44) 1.501790D-01(45) 1.440055D-01(46) 1.384843D-01(47) 1.335893D-01(48) 1.292971D-01
 (49) 1.255872D-01(50) 1.224416D-01(51) 1.198450D-01(52) 1.177844D-01(53) 1.162494D-01(54) 1.152317D-01
 (55) 1.147257D-01(56) 1.147276D-01(57) 1.152364D-01(58) 1.162528D-01(59) 1.177801D-01(60) 1.198239D-01
 (61) 1.223918D-01(62) 1.254940D-01(63) 1.291427D-01(64) 1.333528D-01(65) 1.381415D-01(66) 1.435286D-01
 (67) 1.495364D-01(68) 1.561900D-01(69) 1.635171D-01(70) 1.715481D-01(71) 1.803161D-01(72) 1.898561D-01
 (73) 2.002027D-01(74) 2.113842D-01(75) 2.234059D-01(76) 2.362046D-01(77) 2.495241D-01(78) 2.625764D-01
 (79) 2.731218D-01(80) 2.749659D-01(81) 2.511569D-01(82) 2.317140D-01(83) 2.295778D-01(84) 2.292066D-01
 (85) 2.267902D-01(86) 2.214282D-01(87) 2.129685D-01(88) 2.014760D-01(89) 1.871016D-01(90) 1.700478D-01
 (91) 1.505581D-01(92) 1.289114D-01(93) 1.054179D-01(94) 8.041401D-02(95) 5.425807D-02(96) 2.732478D-02
 (97) C.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 2 = 0.159631D 02

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 2 = 0.388800D 02

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 2 = 0.645693D 01

REGION	NORMALIZED POWER
1	0.2846943D 01
2	0.1918759D 01
3	0.1155555D 01

TOTAL NORMALIZED POWER = 0.1964788D 01

BENCHMARK PROBLEM DELAYED SUPERCRITICAL TRANSIENT

TIME ZONE= 2 STEP NUMBER= 400 TIME=0.20000000 C1 TIME STEP=0.2500000-02

TEST POINT	MESH POINT	FREQUENCY	EXP(W*H)
1	9	2.2986D-01	1.000575D 00
2	33	2.2262D-01	1.000557D 00
3	49	1.8154D-01	1.000454D 00
4	65	1.0172D-01	1.000254D 00
5	89	7.1430D-02	1.000179D 00

POINT-WISE FLUXES FOR GROUP 1

(1) 0.0 (2) 9.194184D-01(3) 1.825324D 00(4) 2.704401D 00(5) 3.543730D 00(6) 4.330974D 00
 (7) 5.054563D 00(8) 5.703860D 00(9) 6.269321D 00(10) 6.742633D 00(11) 7.116834D 00(12) 7.386408D 00
 (13) 7.547328D 00(14) 7.596972D 00(15) 7.533584D 00(16) 7.353926D 00(17) 7.043731D 00(18) 6.515997D 00
 (19) 6.067810D 00(20) 5.665826D 00(21) 5.296681D 00(22) 4.954431D 00(23) 4.635937D 00(24) 4.339151D 00
 (25) 4.062488D 00(26) 3.804590D 00(27) 3.564236D 00(28) 3.340303D 00(29) 3.131749D 00(30) 2.937607D 00
 (31) 2.756980D 00(32) 2.589029D 00(33) 2.432976D 00(34) 2.288099D 00(35) 2.153726D 00(36) 2.029234D 00
 (37) 1.914044D 00(38) 1.807623D 00(39) 1.709476D 00(40) 1.619146D 00(41) 1.536213D 00(42) 1.460290D 00
 (43) 1.391023D 00(44) 1.328087D 00(45) 1.271188D 00(46) 1.220059D 00(47) 1.174457D 00(48) 1.134167D 00
 (49) 1.098997D 00(50) 1.068778D 00(51) 1.043365D 00(52) 1.022632D 00(53) 1.006476D 00(54) 9.948142D-01
 (55) 9.875838D-01(56) 9.847420D-01(57) 9.862654D-01(58) 9.921503D-01(59) 1.002412D 00(60) 1.017086D 00
 (61) 1.036226D 00(62) 1.059507D 00(63) 1.088222D 00(64) 1.121286D 00(65) 1.159235D 00(66) 1.202224D 00
 (67) 1.250434D 00(68) 1.304064D 00(69) 1.363341D 00(70) 1.428514D 00(71) 1.499858D 00(72) 1.577677D 00
 (73) 1.662306D 00(74) 1.754114D 00(75) 1.853522D 00(76) 1.961034D 00(77) 2.077332D 00(78) 2.203515D 00
 (79) 2.341762D 00(80) 2.497123D 00(81) 2.682382D 00(82) 2.790085D 00(83) 2.849133D 00(84) 2.865275D 00
 (85) 2.839893D 00(86) 2.773746D 00(87) 2.667877D 00(88) 2.523824D 00(89) 2.343653D 00(90) 2.129942D 00
 (91) 1.885752D 00(92) 1.614575D 00(93) 1.320293D 00(94) 1.007116D 00(95) 6.795260D-01(96) 3.422117D-01
 (97) 0.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 1 = 0.212878D 03

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 1 = 0.346607D 03

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 1 = 0.799352D C2

POINT-WISE FLUXES FOR GROUP 2

(1) 0.0 (2) 7.688361D-02(3) 1.526372D-01(4) 2.261474D-01(5) 2.963338D-01(6) 3.621647D-01
 (7) 4.226727D-01(8) 4.765684D-01(9) 5.242544D-01(10) 5.638378D-01(11) 5.951458D-01(12) 6.177558D-01
 (13) 6.314868D-01(14) 6.367528D-01(15) 6.359758D-01(16) 6.393100D-01(17) 6.878687D-01(18) 7.459076D-01
 (19) 7.353619D-01(20) 7.017088D-01(21) 6.615429D-01(22) 6.208413D-01(23) 5.816829D-01(24) 5.447208D-01
 (25) 5.100910D-01(26) 4.777459D-01(27) 4.475776D-01(28) 4.194616D-01(29) 3.932735D-01(30) 3.688939D-01
 (31) 3.462109D-01(32) 3.251197D-01(33) 3.055225D-01(34) 2.873288D-01(35) 2.704540D-01(36) 2.548201D-01
 (37) 2.403544D-01(38) 2.269898D-01(39) 2.146642D-01(40) 2.033203D-01(41) 1.929052D-01(42) 1.833704D-01
 (43) 1.746714D-01(44) 1.667675D-01(45) 1.596217D-01(46) 1.532002D-01(47) 1.474729D-01(48) 1.424127D-01
 (49) 1.379953D-01(50) 1.341997D-01(51) 1.310074D-01(52) 1.284028D-01(53) 1.263729D-01(54) 1.249074D-01
 (55) 1.239982D-01(56) 1.236401D-01(57) 1.238301D-01(58) 1.245676D-01(59) 1.258548D-01(60) 1.276958D-01
 (61) 1.300977D-01(62) 1.330696D-01(63) 1.366233D-01(64) 1.407733D-01(65) 1.455366D-01(66) 1.509327D-01
 (67) 1.565841D-01(68) 1.637160D-01(69) 1.711567D-01(70) 1.793370D-01(71) 1.882907D-01(72) 1.980535D-01
 (73) 2.086611D-01(74) 2.201423D-01(75) 2.325022D-01(76) 2.456750D-01(77) 2.593943D-01(78) 2.728423D-01
 (79) 2.836940D-01(80) 2.855205D-01(81) 2.607280D-01(82) 2.404972D-01(83) 2.382448D-01(84) 2.378315D-01
 (85) 2.353010D-01(86) 2.297186D-01(87) 2.209262D-01(88) 2.089913D-01(89) 1.940703D-01(90) 1.763733D-01
 (91) 1.561526D-01(92) 1.336574D-01(93) 1.093289D-01(94) 8.339576D-02(95) 5.626919D-02(96) 2.833736D-02
 (97) 0.0 (

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 2 = 0.180057D 02

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 2 = 0.427845D 02

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 2 = 0.665875D 01

REGION	NORMALIZED POWER
1	0.3211227D 01
2	0.2111448D 01
3	0.1198822D 01

TOTAL NORMALIZED POWER = 0.2163664D 01

BENCHMARK PROBLEM DELAYED SUPERCRITICAL TRANSIENT

TIME ZCNE= 2 STEP NUMBER= 800 TIME=0.300000 01 TIME STEP=0.250000-02

TEST POINT	MESH POINT	FREQUENCY	EXP(W*H)
1	9	2.1020D-01	1.000526D 00
2	33	2.0531D-01	1.000513D 00
3	49	1.7534D-01	1.000438D 00
4	65	1.1004D-01	1.000275D 00
5	89	8.2413D-02	1.000206D 00

POINT-WISE FLUXES FOR GROUP 1

(1) 0.0	(2) 1.149721D 00	(3) 2.282538D 00	(4) 3.381793D 00	(5) 4.431324D 00	(6) 5.415700D 00
(7) 6.320445D 00	(8) 7.132257D 00	(9) 7.839198D 00	(10) 8.430870D 00	(11) 8.898570D 00	(12) 9.235398D 00
(13) 9.436324D 00	(14) 9.498073D 00	(15) 9.418454D 00	(16) 9.193428D 00	(17) 8.805172D 00	(18) 8.144696D 00
(19) 7.583631D 00	(20) 7.080289D 00	(21) 6.617962D 00	(22) 6.189222D 00	(23) 5.790140D 00	(24) 5.418156D 00
(25) 5.071287D 00	(26) 4.747834D 00	(27) 4.446267D 00	(28) 4.165178D 00	(29) 3.903264D 00	(30) 3.659312D 00
(31) 3.432194D 00	(32) 3.220859D 00	(33) 3.024331D 00	(34) 2.841700D 00	(35) 2.672121D 00	(36) 2.514808D 00
(37) 2.369035D 00	(38) 2.234125D 00	(39) 2.109452D 00	(40) 1.994440D 00	(41) 1.888553D 00	(42) 1.791299D 00
(43) 1.702226D 00	(44) 1.620919D 00	(45) 1.546999D 00	(46) 1.480120D 00	(47) 1.419967D 00	(48) 1.366259D 00
(49) 1.318742D 00	(50) 1.277190D 00	(51) 1.241405D 00	(52) 1.211215D 00	(53) 1.186473D 00	(54) 1.167057D 00
(55) 1.152869D 00	(56) 1.143833D 00	(57) 1.139898D 00	(58) 1.141036D 00	(59) 1.147240D 00	(60) 1.158527D 00
(61) 1.174935D 00	(62) 1.196527D 00	(63) 1.223387D 00	(64) 1.255623D 00	(65) 1.293368D 00	(66) 1.336776D 00
(67) 1.386029D 00	(68) 1.441334D 00	(69) 1.502924D 00	(70) 1.571059D 00	(71) 1.646029D 00	(72) 1.728155D 00
(73) 1.817792D 00	(74) 1.915334D 00	(75) 2.021232D 00	(76) 2.136027D 00	(77) 2.260454D 00	(78) 2.395700D 00
(79) 2.544126D 00	(80) 2.711206D 00	(81) 2.910805D 00	(82) 3.026774D 00	(83) 3.090046D 00	(84) 3.106879D 00
(85) 3.078783D 00	(86) 3.006588D 00	(87) 2.891431D 00	(88) 2.734979D 00	(89) 2.539473D 00	(90) 2.307705D 00
(91) 2.042984D 00	(92) 1.749091D 00	(93) 1.430221D 00	(94) 1.090928D 00	(95) 7.360571D-01	(96) 3.706751D-01
(97) 0.0					

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 1 = 0.266167D 03

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 1 = 0.416870D 03

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 1 = 0.866450D 02

PCINT-WISE FLUXES FOR GROUP 2

(1) 0.0	(2) 9.614179D-02	(3) 1.908700D-01	(4) 2.827917D-01	(5) 3.705554D-01	(6) 4.528707D-01
(7) 5.285272D-01	(8) 5.964127D-01	(9) 6.555296D-01	(10) 7.050114D-01	(11) 7.441421D-01	(12) 7.723928D-01
(13) 7.895378D-01	(14) 7.960947D-01	(15) 7.950908D-01	(16) 7.992188D-01	(17) 8.598661D-01	(18) 9.323328D-01
(19) 9.190535D-01	(20) 8.768818D-01	(21) 8.265634D-01	(22) 7.755704D-01	(23) 7.265018D-01	(24) 6.801738D-01
(25) 6.367562D-01	(26) 5.961894D-01	(27) 5.583380D-01	(28) 5.230461D-01	(29) 4.901577D-01	(30) 4.595234D-01
(31) 4.310023D-01	(32) 4.044632D-01	(33) 3.797832D-01	(34) 3.568485D-01	(35) 3.355527D-01	(36) 3.157974D-01
(37) 2.974910D-01	(38) 2.805489D-01	(39) 2.648924D-01	(40) 2.504488D-01	(41) 2.371513D-01	(42) 2.249379D-01
(43) 2.137518D-01	(44) 2.035409D-01	(45) 1.942575D-01	(46) 1.858583D-01	(47) 1.783038D-01	(48) 1.715585D-01
(49) 1.655906D-01	(50) 1.603717D-01	(51) 1.558771D-01	(52) 1.520849D-01	(53) 1.489769D-01	(54) 1.465376D-01
(55) 1.447547D-01	(56) 1.436187D-01	(57) 1.431233D-01	(58) 1.432648D-01	(59) 1.440424D-01	(60) 1.454581D-01
(61) 1.475169D-01	(62) 1.502265D-01	(63) 1.535976D-01	(64) 1.576437D-01	(65) 1.623813D-01	(66) 1.678300D-01
(67) 1.740126D-01	(68) 1.809548D-01	(69) 1.886859D-01	(70) 1.972382D-01	(71) 2.066471D-01	(72) 2.169504D-01
(73) 2.281856D-01	(74) 2.403832D-01	(75) 2.535481D-01	(76) 2.676080D-01	(77) 2.822734D-01	(78) 2.966567D-01
(79) 3.082352D-01	(80) 3.100344D-01	(81) 2.829684D-01	(82) 2.609140D-01	(83) 2.583970D-01	(84) 2.578903D-01
(85) 2.550981D-01	(86) 2.490057D-01	(87) 2.394418D-01	(88) 2.264795D-01	(89) 2.102884D-01	(90) 1.910958D-01
(91) 1.691748D-01	(92) 1.448382D-01	(93) 1.184333D-01	(94) 9.033722D-02	(95) 6.095116D-02	(96) 3.069474D-02
(97) 0.0					

TOTAL INTEGRATED FLUX FOR REGION 1 GROUP 2 = 0.225128D 02

TOTAL INTEGRATED FLUX FOR REGION 2 GROUP 2 = 0.514575D 02

TOTAL INTEGRATED FLUX FOR REGION 3 GROUP 2 = 0.726131D 01

PRECURSOR CONCENTRATION FOR DELAYED GROUP 1

(1) 0.0	(2) 1.803788D-04	(3) 3.581517D-04	(4) 5.307505D-04	(5) 6.956817D-04	(6) 8.505627D-04
(7) 9.931559D-04	(8) 1.121402D-03	(9) 1.233448D-03	(10) 1.327679D-03	(11) 1.402748D-03	(12) 1.457625D-03
(13) 1.491740D-03	(14) 1.505514D-03	(15) 1.502474D-03	(16) 1.497864D-03	(17) 1.162755D-03	(18) 7.998326D-04
(19) 7.789400D-04	(20) 7.420754D-04	(21) 7.012570D-04	(22) 6.607910D-04	(23) 6.221540D-04	(24) 5.857889D-04
(25) 5.517652D-04	(26) 5.200211D-04	(27) 4.904529D-04	(28) 4.629466D-04	(29) 4.373903D-04	(30) 4.136774D-04
(31) 3.917084D-04	(32) 3.713907D-04	(33) 3.526384D-04	(34) 3.353725D-04	(35) 3.195200D-04	(36) 3.050138D-04
(37) 2.917927D-04	(38) 2.798007D-04	(39) 2.689872D-04	(40) 2.593065D-04	(41) 2.507174D-04	(42) 2.431838D-04
(43) 2.366736D-04	(44) 2.311592D-04	(45) 2.266173D-04	(46) 2.230284D-04	(47) 2.203774D-04	(48) 2.186527D-04
(49) 2.178470D-04	(50) 2.179567D-04	(51) 2.189819D-04	(52) 2.209269D-04	(53) 2.237994D-04	(54) 2.276115D-04
(55) 2.323788D-04	(56) 2.381213D-04	(57) 2.448627D-04	(58) 2.526313D-04	(59) 2.614593D-04	(60) 2.713837D-04
(61) 2.824459D-04	(62) 2.946922D-04	(63) 3.081737D-04	(64) 3.229467D-04	(65) 3.390731D-04	(66) 3.566204D-04
(67) 3.756617D-04	(68) 3.962769D-04	(69) 4.185520D-04	(70) 4.425795D-04	(71) 4.684588D-04	(72) 4.962942D-04
(73) 5.261916D-04	(74) 5.582477D-04	(75) 5.925184D-04	(76) 6.289355D-04	(77) 6.670750D-04	(78) 7.055304D-04
(79) 7.402049D-04	(80) 7.596703D-04	(81) 1.103691D-03	(82) 1.421156D-03	(83) 1.425157D-03	(84) 1.427759D-03
(85) 1.414465D-03	(86) 1.381925D-03	(87) 1.329740D-03	(88) 1.258448D-03	(89) 1.169027D-03	(90) 1.062753D-03
(91) 9.411546D-04	(92) 8.055854D-04	(93) 6.591940D-04	(94) 5.028971D-04	(95) 3.393485D-04	(96) 1.709065D-04
(97) 0.0					

PRECURSOR CONCENTRATION FOR DELAYED GROUP 2

(1) 0.0 (2) 5.202140D-04(3) 1.032898D-03(4) 1.530631D-03(5) 2.006207D-03(6) 2.452744D-03
 (7) 2.863777D-03(8) 3.233357D-03(9) 3.556137D-03(10) 3.827455D-03(11) 4.043421D-03(12) 4.201067D-03
 (13) 4.298755D-03(14) 4.337696D-03(15) 4.328029D-03(16) 4.313528D-03(17) 3.346854D-03(18) 2.300653D-03
 (19) 2.239344D-03(20) 2.132259D-03(21) 2.013911D-03(22) 1.896660D-03(23) 1.784739D-03(24) 1.679410D-03
 (25) 1.580864D-03(26) 1.488915D-03(27) 1.403259D-03(28) 1.323560D-03(29) 1.249491D-03(30) 1.180738D-03
 (31) 1.117011D-03(32) 1.058036D-03(33) 1.003563D-03(34) 9.533580D-04(35) 9.072072D-04(36) 8.649130D-04
 (37) 8.262944D-04(38) 7.911862D-04(39) 7.594381D-04(40) 7.309139D-04(41) 7.054914D-04(42) 6.830614D-04
 (43) 6.635275D-04(44) 6.468056D-04(45) 6.328235D-04(46) 6.215206D-04(47) 6.128478D-04(48) 6.067670D-04
 (49) 6.032510D-04(50) 6.022838D-04(51) 6.038598D-04(52) 6.079844D-04(53) 6.146737D-04(54) 6.239546D-04
 (55) 6.358649D-04(56) 6.504537D-04(57) 6.677811D-04(58) 6.879190D-04(59) 7.109509D-04(60) 7.369727D-04
 (61) 7.660927D-04(62) 7.984325D-04(63) 8.341269D-04(64) 8.733250D-04(65) 9.161906D-04(66) 9.629030D-04
 (67) 1.013657D-03(68) 1.068666D-03(69) 1.128158D-03(70) 1.192382D-03(71) 1.261602D-03(72) 1.336098D-03
 (73) 1.416154D-03(74) 1.502027D-03(75) 1.593868D-03(76) 1.691493D-03(77) 1.793760D-03(78) 1.896890D-03
 (79) 1.989872D-03(80) 2.041990D-03(81) 2.966455D-03(82) 3.819502D-03(83) 3.830079D-03(84) 3.836930D-03
 (85) 3.801086D-03(86) 3.713542D-03(87) 3.573225D-03(88) 3.381587D-03(89) 3.141249D-03(90) 2.855642D-03
 (91) 2.528875D-03(92) 2.165655D-03(93) 1.771217D-03(94) 1.351248D-03(95) 9.118008D-04(96) 4.592101D-04
 (97) 0.0 (

PRECURSOR CONCENTRATION FOR DELAYED GROUP 3

(1) 0.0 (2) 1.669688D-04(3) 3.315071D-04(4) 4.912201D-04(5) 6.437829D-04(6) 7.869747D-04
 (7) 9.187114D-04(8) 1.037075D-03(9) 1.140345D-03(10) 1.227019D-03(11) 1.295849D-03(12) 1.345883D-03
 (13) 1.376598D-03(14) 1.388380D-03(15) 1.384455D-03(16) 1.378700D-03(17) 1.068238D-03(18) 7.328779D-04
 (19) 7.122372D-04(20) 6.771659D-04(21) 6.386074D-04(22) 6.004748D-04(23) 5.641021D-04(24) 5.298817D-04
 (25) 4.978663D-04(26) 4.679896D-04(27) 4.401475D-04(28) 4.142275D-04(29) 3.901191D-04(30) 3.677175D-04
 (31) 3.469245D-04(32) 3.276485D-04(33) 3.098047D-04(34) 2.933144D-04(35) 2.781048D-04(36) 2.641088D-04
 (37) 2.512646D-04(38) 2.395153D-04(39) 2.288091D-04(40) 2.190984D-04(41) 2.103402D-04(42) 2.024955D-04
 (43) 1.955294D-04(44) 1.894108D-04(45) 1.841123D-04(46) 1.796100D-04(47) 1.758834D-04(48) 1.729157D-04
 (49) 1.706929D-04(50) 1.692046D-04(51) 1.684433D-04(52) 1.684049D-04(53) 1.690882D-04(54) 1.704952D-04
 (55) 1.726311D-04(56) 1.755039D-04(57) 1.791251D-04(58) 1.835092D-04(59) 1.886740D-04(60) 1.946408D-04
 (61) 2.014340D-04(62) 2.090817D-04(63) 2.176157D-04(64) 2.270715D-04(65) 2.374883D-04(66) 2.489097D-04
 (67) 2.613833D-04(68) 2.749613D-04(69) 2.897005D-04(70) 3.056621D-04(71) 3.229121D-04(72) 3.415203D-04
 (73) 3.615575D-04(74) 3.830884D-04(75) 4.061500D-04(76) 4.306948D-04(77) 4.564325D-04(78) 4.824023D-04
 (79) 5.058079D-04(80) 5.188490D-04(81) 7.534894D-04(82) 9.699449D-04(83) 9.724587D-04(84) 9.740579D-04
 (85) 9.648415D-04(86) 9.425220D-04(87) 9.068278D-04(88) 8.581271D-04(89) 7.970855D-04(90) 7.245729D-04
 (91) 6.416308D-04(92) 5.494526D-04(93) 4.493651D-04(94) 3.428091D-04(95) 2.313182D-04(96) 1.164976D-04
 (97) 0.0 (

PRECURSOR CONCENTRATICN FOR DELAYED GROUP 4

(1) 0.0 (2) 1.762669D-04(3) 3.499543D-04(4) 5.185206D-04(5) 6.794989D-04(6) 8.305336D-04
 (7) 9.694144D-04(8) 1.094109D-03(9) 1.202794D-03(10) 1.293880D-03(11) 1.366050D-03(12) 1.418298D-03
 (13) 1.450074D-03(14) 1.461787D-03(15) 1.456808D-03(16) 1.449618D-03(17) 1.121670D-03(18) 7.680740D-04
 (19) 7.453076D-04(20) 7.075710D-04(21) 6.662817D-04(22) 6.255158D-04(23) 5.866574D-04(24) 5.501077D-04
 (25) 5.159133D-04(26) 4.839976D-04(27) 4.542447D-04(28) 4.265305D-04(29) 4.007333D-04(30) 3.767377D-04
 (31) 3.544355D-04(32) 3.337258D-04(33) 3.145147D-04(34) 2.967153D-04(35) 2.802466D-04(36) 2.650341D-04
 (37) 2.510085D-04(38) 2.381061D-04(39) 2.262682D-04(40) 2.154408D-04(41) 2.055747D-04(42) 1.966246D-04
 (43) 1.885496D-04(44) 1.813126D-04(45) 1.748803D-04(46) 1.692230D-04(47) 1.643143D-04(48) 1.601313D-04
 (49) 1.566543D-04(50) 1.538666D-04(51) 1.517547D-04(52) 1.503080D-04(53) 1.495189D-04(54) 1.493824D-04
 (55) 1.498969D-04(56) 1.510631D-04(57) 1.528849D-04(58) 1.553689D-04(59) 1.585247D-04(60) 1.623646D-04
 (61) 1.669041D-04(62) 1.721617D-04(63) 1.781587D-04(64) 1.849199D-04(65) 1.924734D-04(66) 2.008505D-04
 (67) 2.100861D-04(68) 2.202188D-04(69) 2.312910D-04(70) 2.433488D-04(71) 2.564422D-04(72) 2.706243D-04
 (73) 2.859490D-04(74) 3.024657D-04(75) 3.202024D-04(76) 3.391206D-04(77) 3.589920D-04(78) 3.790626D-04
 (79) 3.971398D-04(80) 4.071088D-04(81) 5.908811D-04(82) 7.603349D-04(83) 7.620803D-04(84) 7.631499D-04
 (85) 7.557759D-04(86) 7.381648D-04(87) 7.101038D-04(88) 6.718819D-04(89) 6.240200D-04(90) 5.671984D-04
 (91) 5.022315D-04(92) 4.300519D-04(93) 3.516960D-04(94) 2.682892D-04(95) 1.810292D-04(96) 9.116927D-05
 (97) 0.0 (

PRECURSOR CONCENTRATICN FOR DELAYED GROUP 5

(1) 0.0 (2) 2.104079D-05(3) 4.177242D-05(4) 6.189025D-05(5) 8.109869D-05(6) 9.911549D-05
 (7) 1.156759D-04(8) 1.305366D-04(9) 1.434793D-04(10) 1.543143D-04(11) 1.628837D-04(12) 1.690679D-04
 (13) 1.728016D-04(14) 1.741331D-04(15) 1.734624D-04(16) 1.725023D-04(17) 1.333391D-04(18) 9.117195D-05
 (19) 8.836489D-05(20) 8.379432D-05(21) 7.881093D-05(22) 7.389645D-05(23) 6.921388D-05(24) 6.480993D-05
 (25) 6.068941D-05(26) 5.684254D-05(27) 5.325496D-05(28) 4.991136D-05(29) 4.679677D-05(30) 4.389697D-05
 (31) 4.119863D-05(32) 3.868931D-05(33) 3.635741D-05(34) 3.419218D-05(35) 3.218359D-05(36) 3.032235D-05
 (37) 2.859986D-05(38) 2.700813D-05(39) 2.553979D-05(40) 2.418803D-05(41) 2.294658D-05(42) 2.180965D-05
 (43) 2.077197D-05(44) 1.982869D-05(45) 1.897540D-05(46) 1.820810D-05(47) 1.752318D-05(48) 1.691742D-05
 (49) 1.638794D-05(50) 1.593220D-05(51) 1.554803D-05(52) 1.523353D-05(53) 1.498716D-05(54) 1.480767D-05
 (55) 1.469409D-05(56) 1.464577D-05(57) 1.466235D-05(58) 1.474374D-05(59) 1.489016D-05(60) 1.510211D-05
 (61) 1.538037D-05(62) 1.572601D-05(63) 1.614043D-05(64) 1.662529D-05(65) 1.718258D-05(66) 1.781461D-05
 (67) 1.852401D-05(68) 1.931373D-05(69) 2.0187C9D-05(70) 2.114774D-05(71) 2.219968D-05(72) 2.334719D-05
 (73) 2.459466D-05(74) 2.594609D-05(75) 2.740368D-05(76) 2.896405D-05(77) 3.060770D-05(78) 3.227059D-05
 (79) 3.376670D-05(80) 3.457745D-05(81) 5.014022D-05(82) 6.448000D-05(83) 6.459725D-05(84) 6.466282D-05
 (85) 6.401706D-05(86) 6.250782D-05(87) 6.011713D-05(88) 5.686948D-05(89) 5.280895D-05(90) 4.799304D-05
 (91) 4.249052D-05(92) 3.638005D-05(93) 2.974907D-05(94) 2.269244D-05(95) 1.531112D-05(96) 7.710721D-06
 (97) 0.0 (

PRECURSOR CONCENTRATION FOR DELAYED GROUP 6

(1) 0.0 (2) 3.389853D-06(3) 6.729870D-06(4) 9.970947D-06(5) 1.306543D-05(6) 1.596783D-05
 (7) 1.863548D-05(8) 2.102915D-05(9) 2.311368D-05(10) 2.485846D-05(11) 2.623810D-05(12) 2.723331D-05
 (13) 2.783357D-05(14) 2.804667D-05(15) 2.7937C1D-05(16) 2.778023D-05(17) 2.147059D-05(18) 1.467811D-05
 (19) 1.422397D-05(20) 1.348609D-05(21) 1.268187D-05(22) 1.188883D-05(23) 1.113319D-05(24) 1.042246D-05
 (25) 9.757400D-06(26) 9.136421D-06(27) 8.557201D-06(28) 8.017264D-06(29) 7.514188D-06(30) 7.045673D-06
 (31) 6.609563D-06(32) 6.203845D-06(33) 5.826641D-06(34) 5.476208D-06(35) 5.150923D-06(36) 4.849280D-06
 (37) 4.565881D-06(38) 4.311432D-06(39) 4.072732D-06(40) 3.852675D-06(41) 3.650237D-06(42) 3.464478D-06
 (43) 3.294531D-06(44) 3.139605D-06(45) 2.998974D-06(46) 2.871982D-06(47) 2.758030D-06(48) 2.656583D-06
 (49) 2.567160D-06(50) 2.489336D-06(51) 2.422737D-06(52) 2.367C42D-06(53) 2.321979D-06(54) 2.287321D-06
 (55) 2.262892D-06(56) 2.248560D-06(57) 2.244237D-06(58) 2.249881D-06(59) 2.265495D-06(60) 2.291126D-06
 (61) 2.326865D-06(62) 2.372848D-06(63) 2.429256D-06(64) 2.496316D-06(65) 2.574303D-06(66) 2.663539D-06
 (67) 2.764395D-06(68) 2.877293D-06(69) 3.002707D-06(70) 3.141163D-06(71) 3.293238D-06(72) 3.45953D-06
 (73) 3.640743D-06(74) 3.837392D-06(75) 4.049816D-06(76) 4.277507D-06(77) 4.517590D-06(78) 4.760624D-06
 (79) 4.979199D-06(80) 5.096911D-06(81) 7.388660D-06(82) 9.499793D-06(83) 9.515526D-06(84) 9.523926D-06
 (85) 9.427764D-06(86) 9.204620D-06(87) 8.851849D-06(88) 8.373061D-06(89) 7.774745D-06(90) 7.065362D-06
 (91) 6.255028D-06(92) 5.355315D-06(93) 4.379077D-06(94) 3.340263D-06(95) 2.253719D-06(96) 1.134969D-06
 (97) 0.0 (

REGION NCRMALIZED POWER

1 0.4015066D 01
 2 0.2539472D 01
 3 0.1299482D 01

TOTAL NORMALIZED POWER = 0.2605205D 01

BENCHMARK PROBLEM DELAYED SUPERCRITICAL TRANSIENT
 END OF PROBLEM

IHC900I EXECUTION TERMINATING DUE TO ERROR CCUNT FOR ERROR NUMBER 217

IHC217I FIOCS - END OF DATA SET ON UNIT 5

Appendix Code Listing

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C MAIN PROGRAM
  IMPLICIT REAL*8 (A-H,O-Z)
  INTEGER RTAG
  INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,
1     UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GC,GL,GU,GRP,GPU,CUT,
2     P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,
3     SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT
  REAL*8 ICDINE
  REAL*8 LR,NU,NUSIGF,NX
  COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL
  COMMON /A2/NUM,NCCMP,BCL,BCR,MTZ,NTZ,XEN,STEADY
  COMMON /A3/PUNBAL,SORCE,GEOM,NTAG,NUM2,PUNFRS
  COMMON /A4/TIGHT1,TIGHT2,TIGHT3
  COMMON/A5/IN,OUT,NERR
  COMMON/C1/M1,M2,M4,M5,M7
C FOR CONSERVATION OF CORE RECOMPILE MAIN WITH THE FOLLOWING DIMENSIONS
C ALTERED TO ACCOMODATE THE MAXIMUM EXPECTED PROBLEM SIZE. THE VARIABLE
C IN ( ) INDICATE THE DIMENSION INFORMATION TO BE PUNCHED ON SUBSEQUENT
C CARDS, WHERE,
C   GRP IS THE # OF NEUTRON GROUPS
C   REG IS THE # OF REGIONS
C   DEL IS THE # OF DELAYED GROUP
C   PT IS THE # OF SPACE POINTS
C   NUM IS THE # OF TEST POINTS
C   (PT,GRP+DEL)
  DIMENSION PSI(100,16)
C   (GRP,DEL) ***** IF DEL EQUALS 0: (GRP,1) *****
  DIMENSION SD(10,6),SDIN(10,6)
C   (GRP)
  DIMENSION CHI(10),NU(10),NX(10),TD(10),V(10),VINV(10)
  DIMENSION SIGCIN(10),SIGFIN(10),SIGTIN(10)
C   (GRP+1,GRP)
  DIMENSION SIGXIN(11,10)
C   (REG)
  DIMENSION POWREG(10),POWORG(10),REGFR(10),WCOEFL(10),WCOEFR(10)
  DIMENSION NCMP(10),FUEL(10),CHANGE(10),SCR(10),CXL(10),CXQ(10),

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MAINCC01
MAINCCC2
MAINCC03
MAINCC04
MAINCC05
MAINCC06
MAINCC07
MAINCC08
MAINCC09
MAIN0010
MAINCC11
MAINCC12
MAINCC13
MAINCC14
MAINCC15
MAINCC16
MAINCC17
MAINCC18
MAINCC19
MAINCC20
MAINCC21
MAINCC22
MAINCC23
MAINCC24
MAINCC25
MAINCC26
MAINCC27
MAINCC28
MAINCC29
MAINCC30
MAINCC31
MAINCC32
MAINCC33
MAINCC34
MAINCC35
MAINCC36

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	1DR(10),LR(10),PB(10),IPL(10),IPR(10),XL(10),XR(10),RTAG(10),	MAIN037
	2TAGC(10),TAGF(10),TAGT(10),TAGX(10),TI1(10),IODINE(10),XENON(10)	MAIN038
C	(REG,GRP)	MAIN039
	DIMENSION CCL(10,10),CCQ(10,10),CFL(10,10),CFQ(10,10),CTRL(10,10),	MAIN040
	1CTRQ(10,10),SIGC(10,10),SIGF(10,10),SIGT(10,10),NUSIGF(10,10),	MAIN041
	2DNSCAT(10,10),UPSCAT(10,10),SORG(10,10),D(10,10),XABS(10,10),	MAIN042
	3PSIBAR(10,10),PSITCT(10,10),PSIB1(10,10),PCWER(10,10)	MAIN043
C	(REG,GRP,GRP)	MAIN044
	DIMENSION SIGX(10,10,10)	MAIN045
C	(PT)	MAIN046
	DIMENSION WHZ(100),WZ(100),FF1(100),FF2(100),WCOEF(100)	MAIN047
	DIMENSION DPSI(100),DD(100),DL(100),DU(100),WA(100),GA(100)	MAIN048
C	(PT,GRP)	MAIN049
	DIMENSION SRCEO(100,10),SRCE1(100,10),CM(100,10),CP(100,10)	MAIN050
C	(NUM)	MAIN051
	DIMENSION WPT(50),PSISTO(50)	MAIN052
C	(NUM2)	MAIN053
	DIMENSION STPRN(50)	MAIN054
C	MAXIMUM # OF PRINT TIMES (NUM2) IS FIXED AT 50	MAIN055
C	M1= MAX # OF REGIONS	MAIN056
	M1=10	MAIN057
C	M2= MAX # OF NEUTRON GROUPS	MAIN058
	M2=10	MAIN059
C	M4= MAX # OF DELAYED GROUPS	MAIN060
	M4=6	MAIN061
C	M5= MAX # OF SPACE POINTS	MAIN062
	M5=100	MAIN063
C	M7= MAX # OF TEST POINTS (NUM)	MAIN064
	M7=50	MAIN065
	IN=5	MAIN066
	OUT=6	MAIN067
100	NERR=0	MAIN068
	CALL INPTA1	MAIN069
	CALL DIRECT(PSI,SIGC,SIGF,SIGT,SIGX,NU,SD,SDIN,CHI,NCMP,	MAIN070
	1FUEL,XABS,XENON,IODINE,LR,IPL,IPR,PB,XL,XR,DR,WHZ,WZ,WPT,NX,	MAIN071
	2NUSIGF,DNSCAT,UPSCAT,REGFR,WCOEF,WCOEFL,WCOEFR,D,CHANGE,CM,CP,	MAIN072

3SOR, SORG, SRCEO, SRCE1, STPRN, RTAG, TAGC, TAGF, TAGT, TAGX, CCL, CCC, CFL,
4CFQ, CTRL, CTRQ, CXL, CXQ, V, VINV, PSITOT, POWREG, POWORG, POWER, PSISTC,
5DD, DL, DU, FF1, FF2, T11, SIGCIN, SIGFIN, SIGTIN, SIGXIN, PSIB1, TD,
6WA, GA, DPSI, PSIBAR)
CALL TITLE(4)
GO TO 100
END

MAIN073
MAIN074
MAIN075
MAIN076
MAIN077
MAIN078
MAIN079

	SUBROUTINE AVRAGE(PSI,PSIBAR,PSITOT,POWER,WCOEF,WCEFL,WCEFR,	AVRGCC01
	IREFR, IPL, IPR, SIGF, POWREG, POWORG)	AVRGCC02
	IMPLICIT REAL*8 (A-H,O-Z)	AVRGCC03
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	AVRGCC04
1	UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CLT,	AVRGCC05
2	P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	AVRGCC06
3	SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	AVRGCC07
	INTEGER RBOUND , RINT	AVRGCC08
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	AVRGCC09
	COMMON /A9/POWTOT,PCWBAR	AVRGCC10
	COMMON /B2/NPRT,NZ,ISX,STEP,NZSAVE,PRBEND,IPRN	AVRGCC11
	DIMENSION PSI(PT,GU)	AVRGCC12
	DIMENSION PSIBAR(REG,GRP)	AVRGCC13
	DIMENSION PSITOT(REG,GRP)	AVRGCC14
	DIMENSION PCWREG(REG)	AVRGCC15
	DIMENSION POWORG(REG)	AVRGCC16
	DIMENSION POWER(REG,GRP)	AVRGCC17
	DIMENSION IPL(REG),IPR(REG)	AVRGCC18
	DIMENSION REGFR(REG),WCOEF(PT),WCEFL(REG),WCEFR(REG)	AVRGCC19
	DIMENSION SIGF(REG,GRP)	AVRGCC20
	DC 120 R=1,REG	AVRGCC21
	RINT=IPR(R)	AVRGCC22
	LINT=IPL(R)	AVRGCC23
	RBOUND=RINT+1	AVRGCC24
	LBOUND=LINT-1	AVRGCC25
	DC 120 G=1,GRP	AVRGCC26
	X=C.0	AVRGCC27
	DO 110 P=LINT,RINT	AVRGCC28
110	X=X+PSI(P,G)*WCOEF(P)	AVRGCC29
	X=X+PSI(LBOUND,G)*WCEFL(R)+PSI(RBOUND,G)*WCEFR(R)	AVRGCC30
	PSITOT(R,G)=X	AVRGCC31
	PSIBAR(R,G)=X/REGFR(R)	AVRGCC32
	POWER(R,G)=SIGF(R,G)*X	AVRGCC33
120	CONTINUE	AVRGCC34
	POWTOT=0.0D0	AVRGCC35
	DC 130 R=1,REG	AVRGCC36

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POWREG(R)=0.0DC
DO 125 G=1,GRP
PCWREG(R)=PCWREG(R)+POWER(R,G)
125 CCNTINUE
POWTCT=POWTOT+POWREG(R)
IF(PCWCRG(R).EQ.0.0DC) GO TO 130
PCWREG(R)=PCWREG(R)/PCWCRG(R)
130 CONTINUE
IF(PCWBAR.EQ.0.0DC) GO TO 140
POWTCT=PCWTCT/PCWBAR
140 RETURN
END
```

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AVRG0037
AVRG0038
AVRG0039
AVRG0040
AVRG0041
AVRG0042
AVRG0043
AVRG0044
AVRG0045
AVRG0046
AVRG0047
AVRG0048
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SUBROUTINE CALC(PSI,WHZ,WZ,NX,NUSIGF,SIGX,SD,SDIN,STPRN,FUEL,WPT,	CALCC001
IXL,XR,PB,IPL,IPR,VINV,UPSCAT,DNSCAT,SORG,SOR,SRCEC,SRCE1,CP,CM,	CALCC002
2FF1,FF2,TI1,DU,DL,DC,TD,WA,GA,DPSI)	CALCC003
IMPLICIT REAL*8 (A-H,O-Z)	CALCC004
REAL*8 LR,NU,NUSIGF,NX	CALCC005
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	CALCC006
1 UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	CALCC007
2 P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	CALCC008
3 SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	CALCC009
COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	CALCC010
COMMON /A2/NUM,NCCMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	CALCC011
COMMON /A3/PUNBAL,SORCE,GEOM,NTAG,NUM2,PUNFRS	CALCC012
COMMON /A7/BETA(6),DECAY(6),BETDCY(6),DECH(6)	CALCC013
COMMON /B1/H,HP,TIME,TZ,ZERC,TZO,TIMZ	CALCC014
DIMENSION PSI(PT,GU)	CALCC015
DIMENSION WHZ(PT)	CALCC016
DIMENSION SIGX(REG,GRP,GRP)	CALCC017
DIMENSION NX(GRP),NUSIGF(REG,GRP)	CALCC018
DIMENSION SD(GRP,IDEL)	CALCC019
DIMENSION SDIN(GRP,IDEL)	CALCC020
DIMENSION STPRN(50)	CALCC021
DIMENSION FUEL(REG)	CALCC022
DIMENSION WPT(NUM)	CALCC023
DIMENSION IPL(REG),IPR(REG),PB(REG),XL(REG),XR(REG)	CALCC024
DIMENSION VINV(GRP)	CALCC025
DIMENSION SOR(REG),SORG(REG,GRP),SRCEC(PT,GRP),SRCE1(PT,GRP)	CALCC026
DIMENSION CM(PT,GRP),CP(PT,GRP)	CALCC027
DIMENSION FF1(PT)	CALCC028
DIMENSION FF2(PT)	CALCC029
DIMENSION TI1(REG)	CALCC030
DIMENSION DD(PT),DL(PT),DU(PT)	CALCC031
DIMENSION DNSCAT(REG,GRP),UPSCAT(REG,GRP)	CALCC032
DIMENSION WZ(PT),WA(PT),GA(PT),TD(GRP)	CALCC033
DIMENSION DPSI(PT)	CALCC034
CALL FREQ(PSI,WHZ,WZ,FF1,FF2,STPRN,WPT,DPSI,PB)	CALCC035
IGONE=0	CALCC036


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        IF (DEL.EQ.0) GC TC 24
        DO 23 II=1,DEL
23      DECF (II)=DEXP (DECAY (II)*H)
        24 DC 150 G=1,GRP
          DO 115 R=1,REG
            TII (R)=NX (G)*NUSIGF (R,G)-SIGX (R,G,G)
            IF (GRP.EQ.1) TII (R)=-SIGX (R,G,G)
115     CONTINUE
          CALL      RHS (G,PSI,FF1,FF2,TII,NX,NUSIGF,VINV,SIGX ,FUEL,SD,
            1XL,XR,PB,IPL,IPR)
        120 IF (SORCE) 130,140,130
130     CALL      SOURCE (G,PSI,SORG,SOR,SRCEC,SRCE1,XL,XR,PB,IPL,IPR)
140     CALL      LHS (G,DU,DL,DD,CP,CM,TII,VINV,FF2,XL,XR,IPL,IPR,PB)
          CALL      MATINV (G,PT,GRP,PSI,DU,DL,DD,WA,GA)
        150 CONTINUE
          IF (DEL) 160,180,160
160     DC 170 G=GL,GU
          CALL      PREC (G,PSI,NUSIGF,FF2,FUEL,XL,XR,PB,IPL,IPR,TD)
        170 CONTINUE
        180 CCNTINUE
          RETURN
          END

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CALCC037
CALCC038
CALCC039
CALCC040
CALCC041
CALCC042
CALCC043
CALCC044
CALCC045
CALCC046
CALCC047
CALCC048
CALCC049
CALCC050
CALCC051
CALCC052
CALCC053
CALCC054
CALCC055
CALCC056
CALCC057
CALCC058

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	SUBROUTINE COEF1(NX,NUSIGF,CHI,NU,SIGF,SIGC,SIGX,PB,DR,LR,XL,XR,	CF1 CC01
	1 IPL,IPR,DNSCAT,UPSCAT,WCOEF,WCOEFL,WCOEFR,REGFR)	CF1 CC02
	IMPLICIT REAL*8 (A-F,O-Z)	CF1 CCC3
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	CF1 CC04
	1 UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	CF1 C005
	2 P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	CF1 CC06
	3 SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	CF1 C007
	REAL*8 IODINE	CF1 C008
	REAL*8 LR,NU,NUSIGF,NX	CF1 CCC9
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	CF1 C010
	COMMON /A3/PUNBAL,SORCE,GEOM,NTAG,NUM2,PUNFRS	CF1 C011
	COMMON /A7/BETA(6),DECAY(6),BETDCY(6),DECH(6)	CF1 CC12
C	CF1 CC13
	DIMENSION LR(REG),IPL(REG),IPR(REG),PB(REG),XL(REG),XR(REG)	CF1 C014
	DIMENSION REGFR(REG),WCOEF(PT),WCOEFL(REG),WCOEFR(REG)	CF1 CC15
	DIMENSION CHI(GRP)	CF1 CC16
	DIMENSION DNSCAT(REG,GRP),UPSCAT(REG,GRP)	CF1 C017
	DIMENSION NU(GRP)	CF1 C018
	DIMENSION NX(GRP),NUSIGF(REG,GRP)	CF1 C019
	DIMENSION SIGC(REG,GRP),SIGF(REG,GRP),SIGX(REG,GRP,GRP)	CF1 C020
	DIMENSION DR(REG)	CF1 C021
	FLOAT(I)=DFLOAT(I)	CF1 C022
C		CF1 C023
	DO 120 G=1,GRP	CF1 C024
	X=0.0	CF1 CC25
	IF(DEL.EQ.0) GO TO 111	CF1 CC26
	DO 110 GP=1,DEL	CF1 C027
	X=X+BETA(GP)	CF1 C028
	110 CONTINUE	CF1 C029
	111 NX(G)=CHI(G)*(1.0-X)	CF1 CC30
	120 CONTINUE	CF1 C031
	IF(DEL.EQ.0) GO TO 131	CF1 CC32
	DO 130 K=1,DEL	CF1 CC33
	130 BETDCY(K)=BETA(K)/DABS(DECAY(K))	CF1 C034
C		CF1 C035
	131 DO 150 R=1,REG	CF1 CC36

	DC 150 G=1,GRP	CF1 C037
	NUSIGF(R,G)=NU(G)*SIGF(R,G)	CF1 C038
	SIGX(R,G,G)=SIGC(R,G)+SIGF(R,G)	CF1 C039
	X=0.0	CF1 C040
	DC 140 GP=1,GRP	CF1 C041
140	X=X+SIGX(R,GP,G)	CF1 C042
	SIGX(R,G,G)=X	CF1 C043
150	CONTINUE	CF1 C044
C		CF1 C045
C	CALCULATION OF SPATIAL INVARIANT IN REGION R	CF1 C046
C		CF1 C047
	N=1	CF1 C048
	DO 160 R=1,REG	CF1 C049
	X=PB(R)-N	CF1 C050
	DR(R)=LR(R)/X	CF1 C051
	N=PB(R)	CF1 C052
160	CONTINUE	CF1 C053
	NL=2	CF1 C054
	IF(REG.EQ.1) DR(2)=0.0	CF1 C055
	N=REG-1	CF1 C056
	IF(GEOM-1) 181,182,186	CF1 C057
181	CONTINUE	CF1 C058
C		CF1 C059
C	REGION INTERFACE WEIGHTING FACTORS, SLAB GEOMETRY	CF1 C060
	DO 190 R=1,N	CF1 C061
	XL(R)=DR(R)/(DR(R)+DR(R+1))	CF1 C062
	XR(R)=DR(R+1)/(DR(R)+DR(R+1))	CF1 C063
190	CONTINUE	CF1 C064
C		CF1 C065
	GO TO 191	CF1 C066
182	CCONTINUE	CF1 C067
C		CF1 C068
C	REGION INTERFACE WEIGHTING FACTORS, CYLINDRICAL GEOMETRY	CF1 C069
C		CF1 C070
	RAD=LR(1)	CF1 C071
	DC 183 R=1,N	CF1 C072

CFI C073
 CFI C074
 CFI C075
 CFI C076
 CFI C077
 CFI C078
 CFI C079
 CFI C080
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 CFI C082
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 CFI C102
 CFI C103
 CFI C104
 CFI C105
 CFI C106
 CFI C107
 CFI C108

X1=1/(CR(R)+DR(R+1))
 X2=1/(4*RAD)
 XL(R)=CR(R)*X1*(1-DR(R))*X2
 XR(R)=CR(R+1)*X1*(1+DR(R+1))*X2
 RAD=RAC+LR(R+1)
 183 C C C
 183 CCONTINUE
 GO TO 191
 REGION INTERFACE WEIGHTING FACTORS, SPHERICAL GEOMETRY
 RAC=LR(1)
 DC 184 R=1,N
 X1=1/(DR(R)+DR(R+1))
 X2=1/(2*RAD)
 X3=1/(12*RAC**2)
 XL(R)=DR(R)*X1*(1-DR(R))*X2+(DR(R))*X3
 XR(R)=DR(R+1)*X1*(1+DR(R+1))*X2+(DR(R+1))*X3
 184 CCONTINUE
 191 CCONTINUE
 XL(REG)=1.0
 IPL(1)=2
 IPR(1)=PB(1)-1
 IF (REG.EQ.1) GO TO 210
 DC 200 R=2,REG
 IPL(R)=PB(R-1)+1
 IPR(R)=PB(R)-1
 200 CCONTINUE
 210 CCONTINUE
 THE ENERGY GROUP BOUNDARIES FOR UP AND DOWN SCATTERING ARE SET
 DC 330 R=1,REG
 DO 310 G=1,GRP
 IZ=G-1
 IF (I2) 220,22C,230
 220 DNSCAT(R,G)=0
 GO TO 260
 230 DC 240 I=1,I2
 IF (SIGX(R,G,I)) 240,240,250

240	CCONTINUE	CF1 0109
	I=0	CF1 0110
250	DNSCAT(R,G)=I	CF1 0111
260	IF (G-GRP) 280,270,270	CF1 0112
270	UPSCAT(R,G)=0	CF1 0113
	GO TO 310	CF1 0114
280	I2=G+1	CF1 0115
	I1=0	CF1 0116
	DO 300 I=I2,GRP	CF1 0117
	IF (SIGX(R,G,I)) 300,300,290	CF1 0118
290	I1=I	CF1 0119
300	CONTINUE	CF1 0120
	UPSCAT(R,G)=I1	CF1 0121
310	CCONTINUE	CF1 0122
	KK=0	CF1 0123
	DO 320 G=1,GRP	CF1 0124
320	KK=MAX0(KK,DNSCAT(R,G))	CF1 0125
	IF(GRP.EQ.1) GO TO 330	CF1 0126
	IF (KK.EQ.0) CALL EXIT	CF1 0127
330	CONTINUE	CF1 0128
	IF (GECM-1) 340,370,400	CF1 0129
340	DO 360 R=1,REG	CF1 0130
	PR=IPR(R)	CF1 0131
	PL=IPL(R)	CF1 0132
	WCDEF(LR)=DR(R)*0.5	CF1 0133
	DO 350 P=PL,PR	CF1 0134
350	WCDEF(P)=CR(R)	CF1 0135
	WCDEFR(R)=DR(R)*0.5	CF1 0136
	REGFR(R)=LR(R)	CF1 0137
360	CCONTINUE	CF1 0138
	GO TO 430	CF1 0139
370	RAD=C.0	CF1 0140
	DO 390 R=1,REG	CF1 0141
	PR=IPR(R)	CF1 0142
	PL=IPL(R)	CF1 0143
	WCDEF(LR)=DR(R)*RAD	CF1 0144

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DC 380 P=PL,PR
RAD=RAC+DR(R)
380 WCCEF(P)=2.0*RAC*DR(R)
WCCEFR(R)=DR(R)*RAD
RAD=RAC+DR(R)
390 REGFR(R)=2.0*RAC*LR(R)-LR(R)**2
GC TO 430
400 RAD=0.0
DO 420 R=1,REG
PR=IPR(R)
PL=IPL(R)
WCCEFL(R)=2.0*CR(R)*RAD**2
DO 410 P=PL,PR
RAD=RAC+CR(R)
410 WCCEF(P)=4.0*CR(R)*RAD**2
RAD=RAC+DR(R)
WCCEFR(P)=2.0*CR(R)*RAD**2
420 REGFR(R)=(RAD**3-(RAD-LR(R))**3)*4.0/3.0
430 CONTINUE
RETURN
END

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CF1 0145
CF1 0146
CF1 0147
CF1 0148
CF1 0149
CF1 0150
CF1 0151
CF1 0152
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CF1 0158
CF1 0159
CF1 0160
CF1 0161
CF1 0162
CF1 0163
CF1 0164
CF1 0165

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	SUBROUTINE COEF2(D,SIGT,CHANGE,PB,DR,LR,CM,CP)	CF2 0001
	IMPLICIT REAL*8 (A-H,O-Z)	CF2 0002
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	CF2 0003
1	UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	CF2 0004
2	P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	CF2 0005
3	SCRCE , SCRG , SCZ , STEADY , STEP , TACC , TAGF , TAGT	CF2 0006
	REAL*8 IODINE	CF2 0007
	REAL*8 LR,NU,NUSIGF,NX	CF2 0008
	INTEGER PFIRST,PLAST	CF2 0009
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	CF2 0010
	COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	CF2 0011
	COMMON /A3/PUNBAL,SORCE,GEOM,NTAG,NUM2,PUNFRS	CF2 0012
	DIMENSION PB(REG),DR(REG),LR(REG)	CF2 0013
	DIMENSION CM(PT,GRP),CP(PT,GRP)	CF2 0014
	DIMENSION CHANGE(REG)	CF2 0015
	DIMENSION D(REG,GRP)	CF2 0016
	DIMENSION SIGT(REG,GRP)	CF2 0017
	FLOAT(I)=DFLOAT(I)	CF2 0018
	DO 120 R=1,REG	CF2 0019
	IF (CHANGE(R).EQ.0) GO TO 120	CF2 0020
	DO 110 G=1,GRP	CF2 0021
110	D(R,G)=1.0/(3.0*SIGT(R,G))	CF2 0022
120	CONTINUE	CF2 0023
C		CF2 0024
C	CALCULATION OF DIFFERENCE COEFFICIENTS - CP AND CM	CF2 0025
C		CF2 0026
	IF (GEOM-1) 130,170,220	CF2 0027
C		CF2 0028
C	SLAB GEOMETRY	CF2 0029
C		CF2 0030
130	CONTINUE	CF2 0031
	PFIRST=2	CF2 0032
	DO 160 R=1,REG	CF2 0033
	IF (CHANGE(R).EQ.0) GO TO 160	CF2 0034
C		CF2 0035
C	NON BOUNDARY POINTS - SLAB	CF2 0036

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C
  PLAST=PB(R)-1
  DO 140 P=PFIRST,PLAST
  DC 140 G=1,GRP
  CM(P,G)=D(R,G)/DR(R)**2
  CP(P,G)=CM(P,G)
140 CONTINUE
  IF(R.EQ.1) GO TO 144
  IF(R.NE.REG) GC TC 143
157 IF(BCR.EQ.1) GC TO 151
  DC 152 G=1,GRP
  CP(PT,G)=0.0
152 CM(PT,G)=0.0
  GO TO 160
151 DC 154 G=1,GRP
  CP(PT,G)=0.0
154 CM(PT,G)=2*D(REG,G)/(DR(REG)**2)
153 GC TC 160

C
C   LEFT BOUNDARY
C
144 IF(BCL.EQ.1) GC TC 145
  DO 146 G=1,GRP
  CP(1,G)=0.
146 CM(1,G)=0.
  IF(R.EQ.REG) GC TO 157
  GO TO 143
145 DC 148 G=1,GRP
  CP(1,G)=2*D(1,G)/(DR(1)**2)
148 CM(1,G)=0.
  IF(R.EQ.REG) GC TO 157
  GO TO 143

C
C   INTERFACE POINTS  SLAB GEOM.
C
143 P=PB(R)

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CF2 C037
CF2 C038
CF2 C039
CF2 C040
CF2 C041
CF2 C042
CF2 C043
CF2 C044
CF2 C045
CF2 C046
CF2 C047
CF2 C048
CF2 C049
CF2 C050
CF2 C051
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CF2 C067
CF2 C068
CF2 C069
CF2 C070
CF2 C071
CF2 C072

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	X=(DR(R+1)+DR(R))*0.5	CF2 C073
	DO 150 G=1,GRP	CF2 C074
	CP(P,G)=D(R+1,G)/(DR(R+1)*X)	CF2 C075
	CM(P,G)=D(R,G)/(DR(R)*X)	CF2 C076
150	CCONTINUE	CF2 C077
160	PFIRST=PB(R)+1	CF2 C078
	GC TO 270	CF2 0079
C		CF2 C080
C	CYLINDRICAL GEOMETRY	CF2 C081
C		CF2 0082
170	RAD=0.0	CF2 C083
	PFIRST=2	CF2 C084
	IF(CHANGE(1).EQ.0) GO TO 173	CF2 C085
	IF(BCL.EQ.1) GC TO 171	CF2 C086
	DO 172 G=1,GRP	CF2 C087
	CM(1,G)=0.	CF2 C088
172	CP(1,G)=0.	CF2 C089
	GC TO 173	CF2 C090
171	DO 174 G=1,GRP	CF2 C091
	CM(1,G)=0.	CF2 C092
174	CP(1,G)=4*D(1,G)/(DR(1)**2)	CF2 C093
173	CCONTINUE	CF2 C094
	DO 210 R=1,REG	CF2 C095
	IF (CHANGE(R).EQ.1) GO TO 180	CF2 0096
	RAD=RAD+LR(R)	CF2 C097
	GO TO 210	CF2 C098
C		CF2 0099
C	NCN BOUNDARY PCINTS - CYLINDER	CF2 C100
C		CF2 0101
180	PLAST=PB(R)-1	CF2 0102
	DO 190 P=PFIRST,PLAST	CF2 0103
	RAD=RAD+DR(R)	CF2 0104
	X=1.0/(DR(R)**2)	CF2 0105
	Y=1.0/(2.0*RAD*DR(R))	CF2 0106
	DO 190 G=1,GRP	CF2 0107
	CM(P,G)=D(R,G)*(X-Y)	CF2 0108

	CP(P,G)=D(R,G)*(X+Y)	CF2 0109
190	CCONTINUE	CF2 0110
C		CF2 0111
C	BOUNDARY POINT - CYLINDER	CF2 0112
C		CF2 0113
	IF(R.EQ.REG) GO TO 201	CF2 0114
	P=PB(R)	CF2 0115
	RAD=RAC+DR(R)	CF2 0116
	RADP=RAD+0.5*DR(R)	CF2 0117
	RADM=RAD-0.5*DR(R)	CF2 0118
	X=RAD*(DR(R+1)+DR(R))*0.5	CF2 0119
	DO 200 G=1,GRP	CF2 0120
	CP(P,G)=D(R+1,G)*RADP/(DR(R+1)*X)	CF2 0121
	CM(P,G)=D(R,G)*RADM/(DR(R)*X)	CF2 0122
200	CCONTINUE	CF2 0123
	GO TO 210	CF2 0124
201	IF(BCR.EQ.1) GO TO 202	CF2 0125
	DO 203 G=1,GRP	CF2 0126
	CM(PT,G)=0.0	CF2 0127
203	CP(PT,G)=0.0	CF2 0128
	GO TO 210	CF2 0129
202	RAD=RAC+DR(REG)	CF2 0130
	X=2/(DR(REG)**2)*(1-DR(REG)/(2*RAD))/(1-DR(REG)/(4*RAD))	CF2 0131
	DO 204 G=1,GRP	CF2 0132
	CP(PT,G)=0	CF2 0133
204	CM(PT,G)=D(REG,G)*X	CF2 0134
210	PFIRST=PB(R)+1	CF2 0135
	GO TO 270	CF2 0136
C		CF2 0137
C	SPHERICAL GEOMETRY	CF2 0138
C		CF2 0139
220	RAD=0.0	CF2 0140
	PFIRST=2	CF2 0141
	DO 260 R=1,REG	CF2 0142
	IF (CHANGE(R).EQ.1) GO TO 230	CF2 0143
	RAD=RAC+LR(R)	CF2 0144

```

GC TO 260
C
C   NCN BOUNDARY POINTS - SPHERE
C
230 PLAST=PB(R)-1
    DO 240 P=PFIRST,PLAST
    RAD=RAC+DR(R)
    X=1.0/(DR(R)**2)
    Y=1.0/(RAD*DR(R))
    X1=1/(1+.083333*(DR(R)/RAD)**2)
    DO 241 G=1,GRP
    CM(P,G)=D(R,G)*(X-Y)*X1
241 CP(P,G)=D(R,G)*(X+Y)*X1
240 CCONTINUE
    IF(R.EC.REG) GC TO 251
C
C   BOUNDARY POINTS - SPHERE
C
    P=PB(R)
    RAD=RAC+DR(R)
    X=RAD**2*(DR(R)+DR(R+1))*0.5
    RADP2=(RAD+0.5*DR(R))**2
    RADM2=(RAD-0.5*DR(R))**2
    DO 250 G=1,GRP
    CP(P,G)=D(R+1,G)*RADP2/(DR(R+1)*X)
    CM(P,G)=D(R,G)*RADM2/(DR(R)*X)
250 CONTINUE
    GO TO 260
251 IF(BCR.EQ.1) GO TO 252
    DO 253 G=1,GRP
    CP(PT,G)=0.
253 CM(PT,G)=0.
    GO TO 260
252 RAD=RAC+DR(REG)
    X1=DR(REG)/RAD
    X2=(DR(REG)/(2*RAD))**2

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CF2 0145
CF2 0146
CF2 0147
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CF2 0178
CF2 0179
CF2 0180

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X3=(1-X1+X2)/(1-C.5*X1+X2)
X4=2*X3/(DR(REG)**2)
DC 254 G=1,GRP
CP(PT,G)=0.
254 CM(PT,G)=D(REG,G)*X4
260 PFIRST=PB(R)+1
270 CCONTINUE
RETURN
END

CF2 0181
CF2 0182
CF2 0183
CF2 0184
CF2 0185
CF2 0186
CF2 0187
CF2 0188
CF2 0189

	FUNCTION DEN(M,N,K,PSI,NUSIGF)	DEN C001
	IMPLICIT REAL*8 (A-H,O-Z)	DEN C002
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	DEN C003
1	UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	DEN C004
2	P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	DEN C005
3	SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	DEN C006
	REAL*8 LR,NU,NUSIGF,NX	DEN C007
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	DEN C008
	COMMON /A7/BETA(6),DECAY(6),BETDCY(6),DECH(6)	DEN C009
	DIMENSION PSI(PT,GRP)	DEN C010
	DIMENSION NUSIGF(REG,GRP)	DEN C011
C	THIS FUNCTION CALCULATES THE PRECURSOR CONCENTRATION AT PCINT M,	DEN C012
C	IN REGION N, AND GROUP K AND TIME CT	DEN C013
	T1=0.0	DEN C014
	DC 110 I=1,GRP	DEN C015
110	T1=T1+NUSIGF(N,I)*PSI(M,I)	DEN C016
	DEN=T1*BETDCY(K)	DEN C017
	RETURN	DEN C018
	END	DEN C019

SUBROUTINE DIRECT(PSI,SIGC,SIGF,SIGT,SIGX,NU,SD,SDIN,CHI,NCMP,	DIRTCC01
1FUEL,XABS,XENON,IODINE,LR,IPL,IPR,PB,XL,XR,CR,WHZ,WZ,WPT,NX,	DIRTCC02
2NUSIGF,DNSCAT,UPSCAT,REGFR,WCOEF,WCOEFL,WCOEFR,D,CHANGE,CM,CP,	DIRTCC03
3SCR,SORG,SRCEO,SRCE1,STPRN,RTAG,TAGC,TAGF,TAGT,TAGX,CCL,CCQ,CFL,	DIRTCC04
4CFQ,CTRL,CTRQ,CXL,CXQ,V,VINV,PSITOT,POWREG,POWCRG,POWER,PSISTO,	DIRTCC05
5DC,DL,DU,FF1,FF2,T11,SIGCIN,SIGFIN,SIGTIN,SIGXIN,PSIB1,TD,	DIRTCC06
6WA,GA,DPSI,PSIBAR)	DIRTCC07
IMPLICIT REAL*8 (A-F,O-Z)	DIRTCC08
REAL*8 IODINE	DIRTCC09
REAL*8 LR,NU,NUSIGF,NX	DIRTCC10
INTEGER GF,GRPLUS	DIRTCC11
INTEGER RTAG	DIRTCC12
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	DIRTCC13
1 UPSCAT,WPT,FUEL,G,GECM,GP,CPL,GPR,GC,GL,GU,GRP,GPU,CUT,	DIRTCC14
2P,PL,PR,PB,PRBEND,PT,PUNBAL,PUNFRS,R,REG,SCR,	DIRTCC15
3 SORCE , SORG , SCZ , STEADY , STEP , TAGC , TAGF , TAGT	DIRTCC16
COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	DIRTCC17
COMMON /A2/NUM,NCMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	DIRTCC18
COMMON /A3/PUNBAL,SORCE,GECM,NTAG,NUM2,PUNFRS	DIRTCC19
COMMON /A4/TIGHT1,TIGHT2,TIGHT3	DIRTCC20
COMMON/A5/IN,OUT,NERR	DIRTCC21
COMMON/A6/EP1,EP2,EP3,TSTINC,IEP4,IEP6	DIRTCC22
COMMON /A7/BETA(6),DECAY(6),BETDCY(6),DECH(6)	DIRTCC23
COMMON /A8/GAMAX,GAMAI	DIRTCC24
COMMON /A9/POWTGT,POWBAR	DIRTCC25
COMMON /B1/H,HP,TIME,TZ,ZERO,TZO,TIMZ	DIRTCC26
COMMON /B2/NPRT,NZ,ISX,STEP,NZSAVE,PRBEND,IPRN	DIRTCC27
COMMON /C2/GF,GRPLUS	DIRTCC28
DIMENSION PSI(PT,GU)	DIRTCC29
DIMENSION SIGC(REG,GRP),SIGF(REG,GRP),SIGT(REG,GRP),	DIRTCC30
1SIGX(REG,GRP,GRP)	DIRTCC31
DIMENSION NU(GRP)	DIRTCC32
DIMENSION SD(GRP,IDEL)	DIRTCC33
DIMENSION SDIN(GRP,IDEL)	DIRTCC34
DIMENSION CHI(GRP)	DIRTCC35
DIMENSION NCMP(REG)	DIRTCC36

DIMENSION FUEL(REG)	DIRTC037
DIMENSION XABS(REG,GRP)	DIRTC038
DIMENSION XENCN(REG),ICDINE(REG)	DIRTC039
DIMENSION LR(REG),IPL(REG),IPR(REG),PB(REG),XL(REG),XR(REG)	DIRTC040
DIMENSION WHZ(PT)	DIRTC041
DIMENSION WZ(PT)	DIRTC042
DIMENSION WPT(NUM)	DIRTC043
DIMENSION NX(GRP),NUSIGF(REG,GRP)	DIRTC044
DIMENSION DNSCAT(REG,GRP),UPSCAT(REG,GRP)	DIRTC045
DIMENSION REGFR(REG),WCOEF(PT),WCOEFL(REG),WCOEFR(REG)	DIRTC046
DIMENSION D(REG,GRP)	DIRTC047
DIMENSION CHANGE(REG)	DIRTC048
DIMENSION CM(PT,GRP),CP(PT,GRP)	DIRTC049
DIMENSION SOR(REG),SORG(REG,GRP),SRCEO(PT,GRP),SRCEI(PT,GRP)	DIRTC050
DIMENSION STPRN(50)	DIRTC051
DIMENSION RTAG(REG)	DIRTC052
DIMENSION TAGC(REG),TAGF(REG),TAGT(REG),TAGX(REG)	DIRTC053
DIMENSION CCL(REG,GRP),CCQ(REG,GRP),CFL(REG,GRP),CFQ(REG,GRP), ICTRL(REG,GRP),CTRQ(REG,GRP),CXL(REG),CXQ(REG)	DIRTC054
DIMENSION V(GRP)	DIRTC055
DIMENSION VINV(GRP)	DIRTC056
DIMENSION PSIBAR(REG,GRP)	DIRTC057
DIMENSION PSITOT(REG,GRP)	DIRTC058
DIMENSION POWREG(REG)	DIRTC059
DIMENSION PCWER(REG,GRP)	DIRTC060
DIMENSION DR(REG)	DIRTC061
DIMENSION POWORG(REG)	DIRTC062
DIMENSION PSISTC(NUM)	DIRTC063
DIMENSION DD(PT),DL(PT),DU(PT)	DIRTC064
DIMENSION FF1(PT),FF2(PT)	DIRTC065
DIMENSION TII(REG)	DIRTC066
DIMENSION SIGCIN(GRP),SIGFIN(GRP),SIGTIN(GRP)	DIRTC067
DIMENSION SIGXIN(GRPLUS,GRP)	DIRTC068
DIMENSION PSIB1(REG,GRP)	DIRTC069
DIMENSION TD(GRP)	DIRTC070
DIMENSION WA(PT),GA(PT),DPSI(PT)	DIRTC071
	DIRTC072

```

TIME=0.0
TIMZ=0.
TZ=0.0
TZ0=0.0
STEP=0
NZ=1
NZSAVE=1
ZERC=1.0D-10
PRBEND=0
POWBAR=0.0D0
DC 30 R=1,REG
30 POWCRG(R)=0.0D0
DO 50 P=1,PT
WZ(P)=0.0
WHZ(P)=1.0
DO 50 G=1,GU
50 PSI(P,G)=1.0D0
CALL      INPTA2(PSI,SIGF,SIGC,SIGT,SIGX,NU,SD,SDIN,CHI,VINV,V,
INCMP,FUEL,XABS,XENON,IODINE,PB,LR,WPT,SIGCIN,SIGFIN,SIGTIN,SIGXIN)
CALL      COEF1(NX,NUSIGF,CHI,NU,SIGF,SIGC,SIGX,PB,DR,LR,XL,XR,
1 IPL,IPR,DNSCAT,UPSCAT,WCOEF,WCOEFL,WCOEFR,REGFR)
DO 120 I=1,REG
120 CHANGE(I)=1
CALL      COEF2(D,SIGT,CHANGE,PB,DR,LR,CM,CP)
CALL      INPUTB(SCR,SORG,SRCEO,SRCE1,STPRN,IPL,IPR,RTAG,TAGX,
1TAGT,TAGF,TAGC,CXL,CXQ,CTRL,CTRQ,CCL,CCQ,CFL,CFQ)
CALL      INECA(PSI,WPT,PB,LR,DR,V,NU,CHI,SD,NCMP,D,SIGC,SIGF,
1SIGX,XENON,IODINE)
CALL      INEDB(TAGX,TAGT,TAGC,TAGF,CXL,CXQ,CTRL,CTRQ,CCL,CCQ,
1CFL,CFQ,SOR,SORG,SRCEO,SRCE1,IPL,IPR)
IF (NERR.EQ.1) CALL EXIT
IF (STEADY.LT.1) GO TO 130
CALL      SETUP(PSI,WPT,NU,NUSIGF,CM,CP,SIGX,PB,IPR,IPL,XL,XR,
1FUEL,NX,SDIN,UPSCAT,DNSCAT,PSISTD,DD,DL,DU,WA,GA)
130 CONTINUE
DO 131 P=1,PT

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DIRTC073
DIRTC074
DIRTC075
DIRTC076
DIRTC077
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DIRTC106
DIRTC107
DIRTC108

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131	DPSI(P)=PSI(P,THG)	DIRTC1C9
	CALL AVRAGE(PSI,PSIBAR,PSITOT,POWER,WCOEF,WCOEFL,WCEFR,	CIRTO110
	1REGFR, IPL, IPR, SIGF, POWREG, POWORG)	CIRTO111
	DO 140 I=1,REG	CIRTC112
	POWORG(I)=POWREG(I)	CIRTO113
	IF(POWREG(I).EQ.0.000) GO TO 140	CIRTO114
	POWREG(I)=POWREG(I)/POWTOT	CIRTC115
140	CONTINUE	DIRTO116
	POWBAR=POWTOT	DIRTO117
	IF(POWTOT.NE.0.000) POWTOT=1.0	DIRTC118
	WRITE(CUT,121)	DIRTO119
	WRITE(CUT,122)(R,POWREG(R),R=1,REG)	CIRTO120
	WRITE(CUT,123)POWTOT	CIRTC121
121	FORMAT(1H0,10X,'REGION',10X,'FRACTIONAL POWER',/)	CIRTC122
122	FORMAT(13X,12,12X,E14.7)	CIRTO123
123	FORMAT(1H0,10X,'TOTAL NORMALIZED POWER = ',E14.7)	DIRTC124
	IF (STEADY.LT.1) GO TO 300	CIRTC125
	CALL UPDAT(TAGT,TAGX,TAGC,TAGF,CHANGE,NUSIGF,PSIBAR,ICDINE,	CIRTC126
	1XABS,XENON, CTRL,CTRQ,CXL,CXQ,CCL,CCQ,CFL,CFQ,SIGT,SIGX,SIGF,	CIRTC127
	2SIGC,PSIB1,NU,FUEL)	DIRTC128
	CALL COEF2(D,SIGT,CHANGE,PB,DR,LR,CM,CP)	CIRTC129
	GO TO 300	CIRTO130
200	IF((DABS(TIME-TZ)).GT.ZERO) GO TO 220	DIRTC131
	CALL INPUTB(SOR,SORG,SRCEO,SRCE1,STPRN,IPL,IPR,RTAG,TAGX,	CIRTO132
	1TAGT,TAGF,TAGC,CXL,CXQ,CTRL,CTRQ,CCL,CCQ,CFL,CFQ)	CIRTO133
	CALL INEDB(TAGX,TAGT,TAGC,TAGF,CXL,CXQ,CTRL,CTRQ,CCL,CCQ,	DIRTC134
	1CFL,CFQ,SCR,SCRG,SRCEO,SRCE1,IPL,IPR)	DIRTC135
220	CALL UPDAT(TAGT,TAGX,TAGC,TAGF,CHANGE,NUSIGF,PSIBAR,ICDINE,	CIRTC136
	1XABS,XENON, CTRL,CTRQ,CXL,CXQ,CCL,CCQ,CFL,CFQ,SIGT,SIGX,SIGF,	DIRTC137
	2SIGC,PSIB1,NU,FUEL)	DIRTC138
	CALL COEF2(D,SIGT,CHANGE,PB,DR,LR,CM,CP)	CIRTC139
	IF (NERR.EQ.1) CALL EXIT	DIRTC140
300	CALL CALC(PSI,WHZ,WZ,NX,NUSIGF,SIGX,SD,SDIN,STPRN,FUEL,WPT,	CIRTC141
	1XL,XR,PB,IPL,IPR,VINV,UPSCAT,DNSCAT,SORG,SCR,SRCEO,SRCE1,CP,CM,	CIRTC142
	2FF1,FF2,TI1,DU,CL,DD,TD,WA,GA,DPSI)	CIRTO143
	CALL AVRAGE(PSI,PSIBAR,PSITOT,POWER,WCOEF,WCOEFL,WCEFR,	CIRTC144

1REGFR, IPL, IPR, SIGF, POWREG, POWORG)
CALL TEST(STPRN, PSI, PSITOT, POWREG, WPT, WZ, WHZ)
IF (PRBEND.NE.1) GC TC 200
IF(PUNFRS.EQ.1) CALL PUN(PSI, NU, SIGF, SIGC, SIGT, SIGX, XENCN, ICCINE)
RETURN
END

CIRT0145
CIRT0146
CIRT0147
CIRT0148
CIRT0149
CIRT0150

	SUBROUTINE EQPREC(PSI,FUEL,NUSIGF,IPL,IPR,XL,XR)	EQPCC001
	IMPLICIT REAL*8 (A-H,O-Z)	EQPCC002
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	EQPCC003
1	UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	EQPCC004
2	P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	EQPCC005
3	SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	EQPCC006
	REAL*8 LR,NU,NUSIGF,NX	EQPCC007
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	EQPCC008
	DIMENSION PSI(PT,GU)	EQPCC009
	DIMENSION IPL(REG),IPR(REG),XL(REG),XR(REG)	EQPCC010
	DIMENSION FUEL(REG)	EQPCC011
	DIMENSION NUSIGF(REG,GRP)	EQPCC012
C	THIS ROUTINE CALCULATES THE EQUILIBRIUM PRECURSOR CONCENTRATIONS	EQPCC013
	DC 110 G=GL,GU	EQPCC014
	DC 110 P=1,PT	EQPCC015
110	PSI(P,G)=0.0	EQPCC016
120	DC 190 R=1,REG	EQPCC017
	IF (FUEL(R)) 190,190,130	EQPCC018
130	PL=IPL(R)	EQPCC019
	IF (R.EQ.1) PL=1	EQPCC020
	PR=IPR(R)	EQPCC021
	IF (R.EQ.REG) PR=PT	EQPCC022
	DC 180 G=GL,GU	EQPCC023
	JG=G-GRP	EQPCC024
	DC 140 P=PL,PR	EQPCC025
	PSI(P,G)=DEN(P,R,JG,PSI,NUSIGF)	EQPCC026
140	CONTINUE	EQPCC027
160	M=PL-1	EQPCC028
	IF(R.NE.1) PSI(M,G)=PSI(M,G)+DEN(M,R,JG,PSI,NUSIGF)*XR(R-1)	EQPCC029
170	M=PR+1	EQPCC030
	IF(R.NE.REG) PSI(M,G)=PSI(M,G)+DEN(M,R,JG,PSI,NUSIGF)*XL(R)	EQPCC031
180	CONTINUE	EQPCC032
190	CONTINUE	EQPCC033
200	CONTINUE	EQPCC034
	RETURN	EQPCC035
	END	EQPCC036

SUBROUTINE ERR(SUB,TYPE,N1,N2)	ERR C001
INTEGER SUB,TYPE	ERR C002
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	ERR C003
1 UPSCAT,WPT, FUEL,G,GECEM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	ERR C004
2 P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	ERR C005
3 SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	ERR C006
COMMON/A5/IN,CUT,NERR	ERR C007
NERR=1	ERR C008
GO TO (110,150,170), TYPE	ERR C009
110 WRITE(CUT,120)	ERR C010
120 FORMAT(25HOERRORR FOUND IN SUB INPUT)	ERR C011
130 WRITE (OUT,140) N1,N2	ERR C012
140 FORMAT (7HOCARD ,I3,9H WORD ,I3)	ERR C013
GO TO 220	ERR C014
150 WRITE (OUT,160) N1	ERR C015
160 FORMAT (15HO PT>MAXPT, PT=,I6)	ERR C016
GO TO 220	ERR C017
170 WRITE (OUT,180) N1,N2	ERR C018
180 FORMAT (23HOERRORR IN SIGX INPUT G=,I3,4H I=I3)	ERR C019
GO TO 220	ERR C020
220 RETURN	ERR C021
C	ERR C022
END	ERR C023

```

SUBROUTINE FEDBKX(PSIBAR,SIGF,XABS,XENON,IODINE,PSIB1,FUEL)
IMPLICIT REAL*8 (A-H,O-Z)
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,TFG,XEN,
1      UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GC,GL,GU,GRP,GPU,CUT,
2      P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SCR,
3      SORCE , SCRG , SCZ , STEADY , STEP , TAGC , TAGF , TAGT
REAL*8 IODINE
REAL*8 LR,NU,NUSIGF,NX
REAL LAMDAI,LAMDAX
COMMON /A1/GRP,REG,PT,CL,GU,DEL,TFG,IDEL
COMMON /A8/GAMAX,GAMAI
COMMON /B1/H,HP,TIME,TZ,ZERO,TZO,TIMZ
DIMENSION PSIBAR(REG,GRP)
DIMENSION PSIB1(REG,GRP)
DIMENSION XENON(REG),IODINE(REG)
DIMENSION XABS(REG,GRP)
DIMENSION FUEL(REG)
DIMENSION SIGF(REG,GRP)
EXP(X)=DEXP(X)
FLCAT(I)=DFLOAT(I)
DATA LAMDAI, LAMDAX / 2.874E-5, 2.093E-5/

THIS ROUTINE CALCULATES THE FEEDBACK, BY REGIONS, FOR XENON
CALCULATION OF VOLUME WEIGHTED, REGION AVERAGED FLUX

DO 130 R=1,REG
IF(FUEL(R).EQ.0) GO TO 130
SBAR=0.0
ALPHAX=LAMDAX
DO 120 G=1,GRP
SBAR=SBAR+SIGF(R,G)*(PSIB1(R,G)+PSIBAR(R,G))*0.5
ALPHAX=ALPHAX+XABS(R,G)*PSIBAR(R,G)
120 CONTINUE
Z1=ALPHAX-LAMDAI
Z2=(GAMAX+GAMAI)/ALPHAX

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FCBK001
FCBK002
FCBK003
FCBK004
FCBK005
FCBK006
FCBK007
FCBK008
FCBK009
FCBK010
FCBK011
FCBK012
FCBK013
FCBK014
FCBK015
FCBK016
FCBK017
FCBK018
FCBK019
FCBK020
FCBK021
FCBK022
FCBK023
FCBK024
FCBK025
FCBK026
FCBK027
FCBK028
FCBK029
FCBK030
FCBK031
FCBK032
FCBK033
FCBK034
FCBK035
FCBK036

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	Y1=(-LAMDAI)*H	FDBKC037
	X1=0.0	FDBKC038
	IF (Y1.GT.(-88.0)) X1=EXP(Y1)	FDBKC039
	Y2=(-ALPHAX)*H	FDBK0040
	X2=0.0	FDBKC041
	IF (Y2.GT.(-88.0)) X2=EXP(Y2)	FDBKC042
C		FDBK0043
	IODINE(R)=X1*IODINE(R)+((1.0-X1)/LAMDAI)*GAMAI*SBAR	FDBKC044
C		FDBKC045
	XENON(R)=X2*XENON(R)+((X1-X2)/Z1)*(LAMDAI*IODINE(R)-GAMAI*SBAR)+Z2	FDBKC046
	1*(1.0-X2)*SBAR	FDBKC047
130	CONTINUE	FDBKC048
	DO 110 R=1,REG	FDBKC049
	DO 110 G=1,GRP	FDBKC050
110	PSIB1(R,G)=PSIBAR(R,G)	FDBKC051
	RETURN	FDBKC052
	END	FDBKC053

SUBROUTINE FREQ(PST,WHZ,WZ,FF1,FF2,STPRN,WPT,DPSI,PB)	FRECC001
IMPLICIT REAL*8 (A-H,O-Z)	FRECC002
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	FRECC003
1 UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	FRECC004
2 P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	FRECC005
3 SCRCE , SCRG , SCZ , STEADY , STEP , TAGC , TAGF , TAGT	FRECC006
REAL*8 LR,NU,NUSIGF,NX	FRECC007
COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	FRECC008
COMMON /A2/NUM,NCCMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	FRECC009
COMMON /A3/PUNBAL,SORCE,GEOM,NTAG,NUM2,PUNFRS	FRECC010
COMMON/A6/EP1,EP2,EP3,TSTINC,IEP4,IEP6	FRECC011
COMMON /B1/H,HP,TIME,TZ,ZERO,TZO,TIMZ	FRECC012
COMMON /B2/NPRT,NZ,ISX,STEP,NZSAVE,PRBEND,IPRN	FRECC013
DIMENSION PSI(PT,GU)	FRECC014
DIMENSION DPSI(PT)	FRECC015
DIMENSION FF1(PT)	FRECC016
DIMENSION FF2(PT)	FRECC017
DIMENSION PB(REG)	FRECC018
DIMENSION WZ(PT)	FRECC019
DIMENSION WHZ(PT)	FRECC020
DIMENSION WPT(NUM)	FRECC021
DIMENSION STPRN(50)	FRECC022
ISY=0	FRECC023
IF(IEP4.EQ.1) GO TO 311	FRECC024
PL=1	FRECC025
IF(BCL.EQ.0) PL=2	FRECC026
PR= PB(REG)-1	FRECC027
IF(BCR.EQ.0) GO TO 277	FRECC028
PR=PB(REG)	FRECC029
277 DO 278 P=PL,PR	FRECC030
WHZ(P)=PSI(P,THG)/DPSI(P)	FRECC031
DPSI(P)=WZ(P)	FRECC032
WZ(P)=(DLOG(WHZ(P)))/H	FRECC033
278 CONTINUE	FRECC034
IF(BCL.EQ.0) WHZ(1)=1.0	FRECC035
IF(BCR.EQ.0) WHZ(PT)=1.0	FRECC036

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311  CCNTINUE
      H=HP
      TIMEP=TIME+H
      IF((TZ-TIMEP).GT.ZERO) GO TO 1
      H =TZ-TIME
      ISY=1
1    CCNTINUE
      IF(NUM2.EQ.0) GO TO 2
      TIMEP=TIME+H
      IF((STPRN(NPRT)-TIMEP).GT.ZERO) GO TO 2
      ISY=1
      H =STPRN(NPRT)-TIME
2    CONTINUE
      IF(ISY.EQ.1) GO TO 397
      IF(IEP6.EQ.1) GO TO 401
      T1=WZ(2)
      T2=WZ(2)
      PL=3
      PR=PT-1
      DO 300 P=PL,PR
      IF(WZ(P).GT.T1) T1=WZ(P)
      IF(WZ(P).LT.T2) T2=WZ(P)
300  CONTINUE
      T4=T1*H
      T5=T2*H
      IF(T1.NE.0.0.AND.T2.NE.0.0) GO TO 303
      ES=EP2
      GO TO 310
303  IF(T1.GT.0.0) GO TO 305
      T3=1.0-T1/T2
      IF(T3.EQ.0.0 ) T3=0.001D0
      ES=EP2/T3
      GO TO 310
305  T3=1.0-T2/T1
      IF(T3.EQ.0.0 ) T3=0.001D0
      ES=EP2/T3

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FRECC037
FRECC038
FRECC039
FRECC040
FRECC041
FRECC042
FRECC043
FRECC044
FRECC045
FRECC046
FRECC047
FRECC048
FRECC049
FRECC050
FRECC051
FRECC052
FRECC053
FRECC054
FRECC055
FRECC056
FRECC057
FRECC058
FRECC059
FRECC060
FRECC061
FRECC062
FRECC063
FRECC064
FRECC065
FRECC066
FRECC067
FRECC068
FRECC069
FRECC070
FRECC071
FRECC072

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310 T3=0.0
    DO 315 N=1,NUM
    P=WPT(N)
    T1=WZ(P)
    T2=DPSI(P)
    T8=T1
    T9=T2
    IF(T1.NE.0.0.AND.T2.NE.0.0) GO TO 319
    ET=EP1
    GO TO 339
319 IF(DABS(T1).GT.DABS(T2)) GC TO 321
    T2=1.0-T1/T2
    GO TO 323
321 T2=1.0-T2/T1
323 IF(T2.GT.T3) T3=T2
315 CONTINUE
    ET=EP1/T3
339 CCNTINUE
340 EX=CMIN1(ES,ET)
    EX=CMAX1(EX,EP1)
    T6=CMAX1(DABS(T4),DABS(T5))
    IF(T6.GT.EX) GC TO 370
    T1=2.0*T6
    IF(T1.LT.EX) GC TO 360
394 HP=H
    GO TO 398
360 HP=H*TSTINC
    GO TO 398
370 IF(T6.LT.EP3) GO TO 394
    T7=CMAX1(EX,EP3)
    H=T7*H/T6
401 HP=H
397 CONTINUE
398 CONTINUE
    DO 30 P=1,PT
    IF(DABS(WZ(P)*H).LT.1.0D-5) GO TO 10

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FRECC073
FRECC074
FRECC075
FRECC076
FRECC077
FRECC078
FRECC079
FRECC080
FRECC081
FRECC082
FRECC083
FRECC084
FRECC085
FRECC086
FRECC087
FRECC088
FRECC089
FRECC090
FRECC091
FRECC092
FRECC093
FRECC094
FRECC095
FRECC096
FRECC097
FRECC098
FRECC099
FRECC100
FRECC101
FRECC102
FRECC103
FRECC104
FRECC105
FRECC106
FRECC107
FRECC108

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```
WHZ(P)=DEXP(WZ(P)*H)
FF1(P)=(WHZ(P)-1.0)/WZ(P)
FF2(P)=FF1(P)/WHZ(P)
GC TC 30
10 FF1(P)=H
   FF2(P)=H
   WZ(P)=0.000
   WHZ(P)=1.000
30 CONTINUE
   DO 700 P=1,PT
700 DPSI(P)=PSI(P,THG)
602 RETURN
   END
```

```
FREQ0109
FREQ0110
FRECC111
FREQ0112
FREQ0113
FRECC114
FREQ0115
FREQ0116
FREQ0117
FRECC118
FREQ0119
FRECC120
FREQ0121
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SUBROUTINE INEDA(PSI,WPT,PB,LR,DR,V,NU,CHI,SD,NCMP,D,SIGC,SIGF,
1SIGX,XENON,IODINE)
IMPLICIT REAL*8 (A-H,O-Z)
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,
1      UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CLT,
2      P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,
3      SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT
INTEGER RBCND
REAL*8 IODINE
REAL*8 LR,NU,NUSIGF,NX
COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL
COMMON /A2/NUM,NCMP,BCL,BCR,MTZ,NTZ,XEN,STEADY
COMMON /A3/PUNBAL,SORCE,GEOM,NTAG,NUM2,PUNFRS
COMMON/A5/IN,OUT,NERR
COMMON /A8/GAMAX,GAMAI
DIMENSION PSI(PT,GU)
DIMENSION XENCN(REG),IODINE(REG)
DIMENSION V(GRP)
DIMENSION PB(REG),DR(REG),LR(REG)
DIMENSION CHI(GRP)
DIMENSION D(REG,GRP)
DIMENSION NCMP(REG)
DIMENSION SD(GRP,IDEL)
DIMENSION WPT(NUM)
DIMENSION NU(GRP)
DIMENSION SIGC(REG,GRP),SIGF(REG,GRP),SIGX(REG,GRP,GRP)
DIMENSION NCTE1(9),NOTE2(2),NCTE3(6)
DATA NCTE1/4H      ,4H      ,4HSLAB,4H CYL,4HINCR,4HICAL,
14H  S,4HPPER,4HICAL/
DATA NCTE4/4H  I=/
DATA NCTE2/4H  NC ,4H YES/
DATA NCTE3/4HZERO,4H      ,4H      ,4HSYMM,4HETRY,4H      /
DATA NCTE5/4H  GP=/

CALL TITLE (2)
WRITE (6,300) GRP,DEL,REG,NCMP

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IEDAC001
IEDAC002
IEDAC003
IEDAC004
IEDAC005
IEDAC006
IEDAC007
IEDAC008
IEDAC009
IEDAC010
IEDAC011
IEDAC012
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IEDAC014
IEDAC015
IEDAC016
IEDAC017
IEDAC018
IEDAC019
IEDAC020
IEDAC021
IEDAC022
IEDAC023
IEDAC024
IEDAC025
IEDAC026
IEDAC027
IEDAC028
IEDAC029
IEDAC030
IEDAC031
IEDAC032
IEDAC033
IEDAC034
IEDAC035
IEDAC036

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```

NG=GEOM*3+1
LBOND=1+3*BCL
RBOND=1+3*BCR
NPUN=1+PUNFRS
NBAL=1+PUNBAL
WRITE (6,310) NCTE1(NG),NOTE1(NG+1),NOTE1(NG+2),NOTE3(LBOND),
INCTE3(LBOND+1),NOTE3(LBOND+2),NOTE3(RBOND),NOTE3(RBCND+1),
2NOTE3(RBOND+2),NOTE2(NPUN),NOTE2(NBAL)
WRITE (6,320) (WPT(N),N=1,NUM)
WRITE (6,330) THG
WRITE (6,340)
N1=1
DO 110 R=1,REG
WRITE (6,350) R,N1,PB(R)
110 N1=PB(R)
WRITE (6,360)
WRITE (6,370) ( R,LR(R),DR(R) ,R=1,REG)
WRITE (6,290)
IF (DEL) 120,120,130
120 WRITE (6,380)
GO TO 150
130 WRITE (6,390) ( NOTE4,I ,I=1,DEL)
DO 140 G=1,GRP
WRITE (6,400) G,(SD(G,GP),GP=1,DEL)
140 CCNTINUE
WRITE (6,290)
150 WRITE (6,410)
WRITE (6,420) ( G,V(G),NU(G),CHI(G) ,G=1,GRP)
WRITE (6,290)
C
C CROSS SECTIONS BY COMPOSITION ORDER
C
N=1
160 DO 200 R=1,REG
IF (NCMP(R).NE.N) GO TO 200
WRITE (6,430) N

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IEDAC037
IEDAC038
IEDACC39
IEDACC40
IEDAC041
IEDAC042
IEDAC043
IEDACC44
IEDACC45
IEDACC46
IEDAC047
IEDACC48
IEDACC49
IEDACC50
IEDACC51
IEDACC52
IEDACC53
IEDACC54
IEDACC55
IEDACC56
IEDACC57
IEDACC58
IEDACC59
IEDACC60
IEDACC61
IEDACC62
IEDACC63
IEDACC64
IEDACC65
IEDACC66
IEDACC67
IEDACC68
IEDACC69
IEDACC70
IEDACC71
IEDACC72

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WRITE (6,440) ( G,D(R,G),SIGC(R,G),SIGF(R,G) ,G=1,GRP)
WRITE (6,290)
WRITE (6,450)
L1=1
L2=GRP
170 L3=GRP
IF (L2.LE.9) GO TO 180
L2=L2-9
L3=L1+8
180 WRITE (6,460) ( NCTE5,G ,G=L1,L3)
DO 190 GP=1,GRP
190 WRITE (6,520) GP,(SIGX(R,GP,G),G=L1,L3)
IF (L3.EQ.GRP) GO TO 210
L1=L3+1
GO TO 170
200 CONTINUE
CALL ERR (3,0,C,C)
210 IF (N.EQ.NCCMP) GO TO 220
N=N+1
GO TO 160
220 CCNTINUE
WRITE (6,290)
WRITE (6,470)
WRITE (6,480) ( R,NCMP(R) ,R=1,REG)
WRITE (6,290)
IF (XEN.NE.0) GO TO 230
WRITE (6,490)
GO TO 240
230 CCNTINUE
WRITE (6,500)
C
WRITE (6,510) ( R,XENCN(R),IODINE(R),GAMAX,GAMAI ,R=1,REG)
240 CONTINUE
WRITE (6,290)
N1=1
IF (STEADY.GT.C) N1=2

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IEDA0073
IEDACC74
IEDA0075
IEDACC76
IEDACC77
IEDACC78
IEDACC79
IEDACC80
IEDACC81
IEDACC82
IEDA0083
IEDACC84
IEDACC85
IEDACC86
IEDACC87
IEDACC88
IEDACC89
IEDACC90
IEDACC91
IEDACC92
IEDACC93
IEDACC94
IEDACC95
IEDACC96
IEDACC97
IEDACC98
IEDACC99
IEDA0100
IEDA0101
IEDA0102
IEDA0103
IEDA0104
IEDA0105
IEDA0106
IEDA0107
IEDA0108

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```

WRITE (6,530) NOTE2(N1)
IF (STEADY.EQ.2) GO TO 280
WRITE (6,540)
DO 250 G=1,GRP
250 WRITE (6,550) (P,PSI(P,G),P=1,PT)
IF (STEADY.EQ.C) GO TO 260
WRITE (6,560)
GO TO 280
260 WRITE (6,570)
DO 270 G=GL,GU
270 WRITE (6,550) (P,PSI(P,G),P=1,PT)
280 CONTINUE
C
C
290 FORMAT (1H0)
300 FORMAT (1H0/25X,18H*** INPUT EDIT ***//3X,12,19H NEUTRON GROUP(S)
1,,3X,12,19H DELAYED GROUP(S) ,,3X,12,12H REGION(S) ,,3X,12,15H COM
2POSITION(S)/)
310 FORMAT(2X,3A4,11H GEOMETRY ,,3X,14HLEFT BOUNDARY ,3A4,3X, 15HRIGHT
1 BOUNDARY ,3A4//2X,45HIS THERE TO BE END OF PROBLEM PUNCHED OUTPUT
2 ,A4,3X,1H,/43HOARE THE STEADY STATE FLUXES TO BE PUNCHED ,A4,2X)
320 FORMAT (38HOTEST POINTS FOR FREQUENCY CALCULATION,3X,15I5/(48X,15I
15))
330 FORMAT (8HOGROUP ,13,61H IS SPECIFIED AS THE TEST GROUP FOR THE F
1FREQUENCY CALCULATION/)
340 FORMAT (1H0/33H REGION MESH POINT BOUNDARIES/26H NUMBER
1 LEFT RIGHT)
350 FORMAT (4X,I3,8X,I3,4X,I3)
360 FORMAT (1H0/4X,6HREGION,4X,6HLENGTH,4X,12HMESH SPACING/4X,6HNUMBER
1,5X,4H(CM),9X,4H(CM))
370 FORMAT (5X,I3,4X,F10.4,4X,F8.4)
380 FORMAT (19H0 NO DELAYED GROUPS)
390 FORMAT (59HFRACTIONAL YIELD FROM DELAYED GROUP I INTO NEUTRON GRO
1UP G/2X,5HGROUP,3X,10(3X,A4,I2,1X))
400 FORMAT (3X,I3,4X,10(2X,F8.5))
410 FORMAT (4X,5HGRCUP,5X,15HAVERAGE NEUTRON,6X,12HNEUTRONS PER,6X,7HF

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IEDA0109
IEDAC110
IECA0111
IEDAC112
IEDAC113
IEDAC114
IEDA0115
IEDAC116
IEDAC117
IEDA0118
IEDAC119
IEDAC120
IEDAC121
IEDAC122
IEDAC123
IEDA0124
IEDA0125
IEDAC126
IEDA0127
IEDA0128
IEDAC129
IEDAC130
IEDAC131
IEDAC132
IEDAC133
IEDAC134
IEDA0135
IEDAC136
IEDAC137
IEDAC138
IEDAC139
IEDA0140
IECA0141
IEDAC142
IEDAC143
IEDA0144

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11	FISSION/4X,6HNUMBER,4X,14HSPEED (CM/SEC),8X,7HFISSION,11X,5HYIELD)	IEDA0145
420	FORMAT (5X,I3,6X,E12.6,7X,E12.6,5X,E12.6)	IEDA0146
430	FORMAT (14HOCOMPOSITION ,I2/6X,5HGROLP,4X,9HDIFFUSION,6X,3CHGRCLP	IEDA0147
	1 DEPENDENT CROSS SECTIONS/6X,19HNUMBER COEFFICIENT,6X,9H(CAPTURE)	IEDA0148
	2,4X,9H(FISSION))	IEDA0149
440	FORMAT (7X,I3,4X,E12.6,2X,E12.6,2X,E12.6)	IEDA0150
450	FORMAT (7X,97HSCATTERING MATRIX GP INTO G (THE TOTAL REMOVAL IS	IEDAC151
	1COMPUTED AND STORED AS THE DIAGONAL ELEMENTS))	IEDAC152
460	FORMAT (4H (G),1X,9(6X,A4,I2))	IEDA0153
470	FORMAT (34HOCOMPOSITION ASSIGNMENT TO REGIONS/22H REGION COMPCS	IEDA0154
	1ITICN)	IEDAC155
480	FORMAT (5X,I2,8X,I2)	IEDA0156
490	FORMAT (43HONO XENON BUILDUP CONSIDERD IN THIS PROBLEM)	IEDAC157
500	FORMAT (7HOREGICN,7X,14HCONCENTRATIONS,10X,13HFISSION YIELD/7H NUM	IEDAC158
	1BER,4X,5HXENON,8X,6HIODINE,7X,5HXENON,8X,6HIODINE)	IEDAC159
510	FORMAT (3X,I2,1X,4(3X,E10.5))	IEDAC160
520	FORMAT (2X,I2,3X,9E12.6)	IEDAC161
530	FORMAT (48HOARE STEADY STATE CONDITIONS TO BE CALCULATED ? ,A4)	IEDA0162
540	FORMAT (24HOINPUT FLUX DISTRIBUTION)	IECA0163
550	FORMAT ((2X,6(1H(,I3,2H) ,1PE12.6)))	IEDAC164
560	FORMAT (92HOTH THE INITIAL PRECURSOR CONCENTRATIONS ARE CALCULATED FR	IEDAC165
	1OM THE STEADY STATE FLUX DISTRIBUTION)	IECA0166
570	FORMAT (60HOTH THE INITIAL PRECURSOR CONCENTRATIONS ARE READ IN FRCP	IEDAC167
	1CARDS)	IEDAC168
	RETURN	IECA0169
	END	IEDAC170

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SUBROUTINE INECB(TAGX, TAGT, TAGC, TAGF, CXL, CXQ, CTRL, CTRQ, CCL, CCQ,
1CFL, CFQ, SOR, SORG, SRCE0, SRCE1, IPL, IPR)
  IMPLICIT REAL*8 (A-H, O-Z)
  INTEGER BCL, BCR, CHANGE, DEL, DNSCAT, TAGX, TESTS, THG, XEN,
1      UPSCAT, WPT, FUEL, G, GEOM, GP, GPL, GPR, GC, GL, GU, GRP, GPU, CUT,
2      P, PL, PR, PB, PRBEND, PT, PUNBAL, PUNFRS, R, REG, SOR,
3      SRCE, SCRG, SCZ, STEADY, STEP, TAGC, TAGF, TAGT
  REAL*8 IODINE
  REAL*8 LR, NU, NUSICF, NX
  COMMON /A1/GRP, REG, PT, GL, GU, DEL, THG, IDEL
  COMMON /A3/PUNBAL, SRCE, GEOM, NTAG, NUM2, PUNFRS
  COMMON /A5/IN, OUT, NERR
  COMMON /A6/EP1, EP2, EP3, TSTINC, IEP4, IEP6
  COMMON /B1/H, HP, TIME, TZ, ZERC, TZ0, TIMZ
  COMMON /B2/NPRT, NZ, ISX, STEP, NZSAVE, PRBEND, IPRN
  .....

  DIMENSION IPL(REG), IPR(REG)
  DIMENSION SOR(REG), SORG(REG, GRP), SRCE0(PT, GRP), SRCE1(PT, GRP)
  DIMENSION TAGC(REG), TAGF(REG), TAGT(REG), TAGX(REG)
  DIMENSION CCL(REG, GRP), CCQ(REG, GRP), CFL(REG, GRP), CFQ(REG, GRP),
1CTRL(REG, GRP), CTRQ(REG, GRP), CXL(REG), CXQ(REG)
  DIMENSION NOTE2(2)
  DATA NOTE2(1), NOTE2(2) /4H NO, 4H YES /
  N1=1
  IF (NTAG.NE.0) N1=2
  WRITE (6, 250) NOTE2(N1)
  IF (NTAG.EQ.0) GO TO 180
  WRITE (6, 300)
  DO 170 R=1, REG
  IF (TAGX(R).EQ.0) GO TO 110
  WRITE (OUT, 270) NZ, R, CXL(R), CXQ(R)
110 IF (TAGT(R).EQ.0) GO TO 130
  DO 120 G=1, GRP
  IF ((CTRL(R, G).NE.0).OR.(CTRQ(R, G).NE.0)) WRITE (OUT, 260) NZ, G, R, C
1TRL(R, G), CTRQ(R, G)

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IEDBCC01
IEDBCC02
IEDBCC03
IEDBCC04
IEDBCC05
IEDBCC06
IEDBCC07
IEDBCC08
IEDBCC09
IEDBCC10
IEDBCC11
IEDBCC12
IEDBCC13
IEDBCC14
IEDBCC15
IEDBCC16
IEDBCC17
IEDBCC18
IEDBCC19
IEDBCC20
IEDBCC21
IEDBCC22
IEDBCC23
IEDBCC24
IEDBCC25
IEDBCC26
IEDBCC27
IEDBCC28
IEDBCC29
IEDBCC30
IEDBCC31
IEDBCC32
IEDBCC33
IEDBCC34
IEDBCC35
IEDBCC36

```

C
C

120	CONTINUE	IECBC037
130	IF (TAGC(R).EQ.0) GO TO 150	IEDBC038
	DO 140 G=1,GRP	IEDBCC39
	IF ((CCL(R,G).NE.0.0).OR.(CCQ(R,G).NE.0.C)) WRITE (CUT,280) NZ,G,R	IECBC040
	1,CCL(R,G),CCQ(R,G)	IECBC041
140	CONTINUE	IEDBC042
150	IF (TAGF(R).EQ.0) GO TO 170	IEDBC043
	DO 160 G=1,GRP	IEDBC044
	IF ((CFL(R,G).NE.0.0).OR.(CFQ(R,G).NE.0.C)) WRITE (CUT,290) NZ,G,R	IEDBC045
	1,CFL(R,G),CFQ(R,G)	IEDBC046
160	CONTINUE	IEDBC047
170	CONTINUE	IEDBC048
180	CONTINUE	IEDBC049
C	EDIT OF SOURCE INPUT	IECBC050
	N1=1	IEDBC051
	IF (SORCE.NE.0) N1=2	IECBC052
	WRITE (6,310) NOTE2(N1)	IEDBC053
	IF (SORCE.EQ.0) GO TO 240	IEDBCC54
	WRITE (6,320)	IEDBC055
	WRITE (6,330)	IEDBC056
	DO 230 R=1,REG	IEDBCC57
	IF (SOR(R)-1) 230,210,190	IEDBC058
190	CONTINUE	IEDBC059
C	SPACE DEPENDENT SOURCE ACROSS THE REGION	IEDBC060
	PL=IPL(R)	IEDBCC61
	PR=IPR(R)	IECBC062
	DO 200 G=1,GRP	IECBC063
	IF (SORG(R,G).EQ.0) GO TO 200	IECBC064
	WRITE (6,340) NZ,R,G	IEDBCC65
	WRITE (6,350) (II,SRCEC(II,G),II=PL,PR)	IEDBC066
	WRITE (6,360) (II,SRCEL(II,G),II=PL,PR)	IEDBCC67
200	CONTINUE	IEDBC068
	GO TO 230	IEDBCC69
210	CONTINUE	IEDBC070
C	CONSTANT SOURCE FOR THE REGION	IEDBC071
	II=IPR(R)	IEDBC072

```

DO 220 G=1,GRP
IF (SORG(R,G).EQ.0) GO TO 220
WRITE (6,370) NZ,R,G,SRCEO(II,G),SRCE1(II,G)
220 CCNTINUE
230 CCNTINUE
240 CONTINUE
RETURN

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IECBC073
IECBC074
IECBC075
IECBC076
IECBC077
IECBC078
IECBC079
IECBC080
IECE0081
IECB0082
IECBC083
IECBC084
IECBC085
IECBC086
IECBC087
IECB0088
IECBC089
IECBC090
IECBC091
IECBC092
IECBC093
IECBC094
IECBC095
IECB0096
IECBC097
IECBC098
IECBC099
IECBC100
IECB0101

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C

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250 FORMAT (44HOARE THERE ANY TIME DEPENDENT CHANGES IN THE/21H CRSS
1SECTION DATA A4)
260 FORMAT (2X,I2,7X,9HTRANSPORT,5X,I2,6X,I2,8X,E11.5,4X,E11.5)
270 FORMAT (2X,I2,7X,9HTRANSFER ,13X,I2,8X,E11.5,4X,E11.5)
280 FORMAT (2X,I2,7X,9H CAPTURE ,5X,I2,6X,I2,8X,E11.5,4X,E11.5)
290 FORMAT (2X,I2,7X,9H FISSION ,5X,I2,6X,I2,8X,E11.5,4X,E11.5)
300 FORMAT (71HOTIME CROSS SECTION GRUP REGION TOTAL LINEAR
1 TOTAL QUADRATIC/5H ZONE,21X,1H ,7X,1H ,9X,6HCHANGE,8X,6HCHANGE)
310 FORMAT (40HOARE THERE ANY TIME DEPENDENT SOURCES ? ,A4)
320 FORMAT (21HO SCURCE DISTRIBUTION/61H A - UNIFCRM SOURCE FOR ALL
1 SPACE POINTS WITHIN THE REGION/49H B - SPACE DEPENDENT SCURCES
2 WITHIN THE REGION)
330 FORMAT (36HOTIME REGION GRUP DISTRIBUTION/5H ZONE)
340 FORMAT (2X,I2,6X,I2,5X,I2,8X,3H(A))
350 FORMAT (43X,14HINITIAL SOURCE4(1X,1H(,I2,1H),E10.5 )/(57X,4(1X,1H(
1,I2,1H),E10.5)))
360 FORMAT (38X,19HTIME RATE OF CHANGE,4(1X,1H(,I2,1H),E10.5)/(57X,4(1
1X,1H(,I2,1H),E10.5)))
370 FORMAT (2X,I2,6X,I2,5X,I2,8X,3H(B),17H INITIAL SOURCE=,E10.5/27X,
120HTIME RATE OF CHANGE=)
END

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SUBROUTINE INPTA1
IMPLICIT REAL*8 (A-H,O-Z)
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,
1      UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CLT,
2      P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,
3      SCRCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT
INTEGER GF,GRPLUS
REAL*8 LR,NU,NUSIGF,NX
REAL*8 ICDINE
COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL
COMMON /A2/NUM,NCCMP,BCL,BCR,MTZ,NTZ,XEN,STEADY
COMMON /A3/PUNBAL,SCRCE,GEOM,NTAG,NUM2,PUNFRS
COMMON /A4/TIGHT1,TIGHT2,TIGHT3
COMMON/A5/IN,OUT,NERR
COMMON/C1/M1,M2,M4,M5,M7
COMMON /C2/GF,GRPLUS
DIMENSION ID(14)
ABS(X)=DABS(X)
FLOAT(I)=DFLOAT(I)
C ***** CARD 1 *****
CALL TITLE (1)
WRITE (OUT,390)
CALL TITLE (3)
C ***** CARD 2 *****
READ (IN,350) GRP,THG,GF,DEL,REG,NUM,NCCMP,GEOM,BCL,BCR,MTZ,XEN
WRITE (OUT,400) GRP,THG,GF,DEL,REG,NUM,NCCMP,GEOM,BCL,BCR,MTZ,XEN
IF ((GRP.LT.1).OR.(GRP.GT.M2)) CALL ERR (1,1,2,1)
IF ((THG.LT.1).OR.(THG.GT.GRP)) CALL ERR (1,1,2,2)
IF ((GF.LT.0).OR.(GF.GT.GRP)) CALL ERR (1,1,2,3)
IF ((DEL.LT.0).OR.(DEL.GT.M4)) CALL ERR (1,1,2,4)
IF ((REG.LT.1).OR.(REG.GT.M1)) CALL ERR (1,1,2,5)
IF ((NUM.LT.1).OR.(NUM.GT.M7)) CALL ERR (1,1,2,6)
IF(NUM.LT.REG) CALL ERR(1,1,2,6)
IF (NCCMP.LT.1) CALL ERR (1,1,2,7)
IF ((GEOM.LT.0).OR.(GEOM.GT.2)) CALL ERR (1,1,2,8)
IF ((BCL.NE.0).AND.(BCL.NE.1)) CALL ERR (1,1,2,9)

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IPA1CC01
IPA1CCC2
IPA1CC03
IPA10004
IPA1C005
IPA1C006
IPA1C007
IPA1C008
IPA1CCC9
IPA1C010
IPA1C011
IPA1CC12
IPA1C013
IPA1C014
IPA1CC15
IPA1CC16
IPA1C017
IPA1C018
IPA1CC19
IPA1C020
IPA1C021
IPA1CC22
IPA1C023
IPA1C024
IPA1CC25
IPA1C026
IPA1C027
IPA1CC28
IPA1C029
IPA1C030
IPA1CC31
IPA1CC32
IPA1C033
IPA1C034
IPA1CC35
IPA1C036

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	IF ((BCR.NE.0).AND.(BCR.NE.1)) CALL ERR (1,1,2,10)	IPA1CC37
	IF (MTZ.EQ.0) CALL ERR (1,1,2,11)	IPA1C038
	IF ((XEN.NE.0).AND.(XEN.NE.1)) CALL ERR (1,1,2,12)	IPA1C039
C	PUNFRS=1	IPA1C040
	IF (MTZ.LT.0) PUNFRS=0	IPA1C041
	NTZ=IABS(MTZ)	IPA1C042
	GL=GRP+1	IPA1C043
	GU=DEL+GRP	IPA1C044
	GRPLUS=GRP+1	IPA1C045
	IDEL=DEL	IPA1C046
	IF(DEL.EQ.0)IDEL=1	IPA1C047
C	***** CARD 3 *****	IPA1C048
	READ (IN ,380) STEADY,PUNBAL,TIGHT1,TIGHT2,TIGHT3,PT	IPA1C049
	WRITE (OUT,410) STEADY,PUNBAL,TIGHT1,TIGHT2,TIGHT3,PT	IPA1CC50
	DO 1 I=1,4	IPA1C051
	IF (STEADY.EQ.(I-1)) GO TO 2	IPA1C052
1	CONTINUE	IPA1CC53
	CALL ERR(1,1,3,1)	IPA1CC54
2	CONTINUE	IPA1C055
	IF ((PUNBAL.NE.C).AND.(PUNBAL.NE.1)) CALL ERR (1,1,3,2)	IPA1C056
	IF (TIGHT1.LT.C) CALL ERR (1,1,3,3)	IPA1CC57
	IF (TIGHT2.LT.0) CALL ERR (1,1,3,4)	IPA1C058
	IF (TIGHT3.LT.0) CALL ERR (1,1,3,5)	IPA1C059
	RETURN	IPA1CC60
350	FORMAT (12I6)	IPA1C061
380	FORMAT (2I6,3E12.6,I6)	IPA1C062
390	FORMAT (10H1CARD 01)	IPA1C063
400	FORMAT (10HOCARD 02 ,2X,12I6)	IPA1C064
410	FORMAT (10HOCARD 03 ,2X,2I6,3E12.6,I6)	IPA1C065
	END	IPA1C066
		IPA1CC67

SUBROUTINE INPTA2(PSI,SIGF,SIGC,SIGT,SIGX,NU,SD,SDIN,CHI,VINV,V,	IPA2CC01
INCMP,FUEL,XABS,XENON,IODINE,PB,LR,WPT,SIGCIN,SIGFIN,SIGTIN,SIGXIN)	IPA2CC02
IMPLICIT REAL*8 (A-H,O-Z)	IPA2CC03
INTEGER GF,GPLUS,GFPLUS,GRPLUS	IPA2CC04
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	IPA2CC05
1 UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GL,GRP,GPU,CUT,	IPA2CC06
2 P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	IPA2CC07
3 SCRCE , SORG , SCZ , STEADY , STEP , TAGC , TAGF , TAGT	IPA2CC08
REAL*8 IODINE	IPA2CC09
REAL*8 LR,NU,NUSIGF,NX	IPA2CC10
COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	IPA2CC11
COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	IPA2CC12
COMMON /A4/TIGHT1,TIGHT2,TIGHT3	IPA2CC13
COMMON/A5/IN,OUT,NERR	IPA2CC14
COMMON/A6/EP1,EP2,EP3,TSTINC,IEP4,IEP6	IPA2CC15
COMMON /A7/BETA(6),DECAY(6),BETDCY(6),DECH(6)	IPA2CC16
COMMON /A8/GAMAX,GAMAI	IPA2CC17
COMMON /B1/H,HP,TIME,TZ,ZERC,TZO,TIMZ	IPA2CC18
COMMON /C2/GF,GRPLUS	IPA2CC19
DIMENSION PSI(PT,GU)	IPA2CC20
DIMENSION XABS(REG,GRP)	IPA2CC21
DIMENSION XENON(REG),IODINE(REG)	IPA2CC22
DIMENSION VINV(GRP)	IPA2CC23
DIMENSION V(GRP)	IPA2CC24
DIMENSION PB(REG),LR(REG)	IPA2CC25
DIMENSION CHI(GRP)	IPA2CC26
DIMENSION FUEL(REG)	IPA2CC27
DIMENSION NCMP(REG)	IPA2CC28
DIMENSION SD(GRP,IDEL)	IPA2CC29
DIMENSION SDIN(GRP,IDEL)	IPA2CC30
DIMENSION WPT(NUM)	IPA2CC31
DIMENSION NU(GRP)	IPA2CC32
DIMENSION SIGC(REG,GRP),SIGF(REG,GRP),SIGT(REG,GRP),	IPA2CC33
1SIGX(REG,GRP,GRP)	IPA2CC34
DIMENSION SIGCIN(GRP),SIGFIN(GRP),SIGTIN(GRP)	IPA2CC35
DIMENSION SIGXIN(GRPLUS,GRP)	IPA2CC36

IPAZC037
IPAZC038
IPAZC039
IPAZC040
IPAZC041
IPAZC042
IPAZC043
IPAZC044
IPAZC045
IPAZC046
IPAZC047
IPAZC048
IPAZC049
IPAZC050
IPAZC051
IPAZC052
IPAZC053
IPAZC054
IPAZC055
IPAZC056
IPAZC057
IPAZC058
IPAZC059
IPAZC060
IPAZC061
IPAZC062
IPAZC063
IPAZC064
IPAZC065
IPAZC066
IPAZC067
IPAZC068
IPAZC069
IPAZC070
IPAZC071
IPAZC072

```

DIMENSION IC(14)
ABS(X)=DABS(X)
FLCAT(I)=DFLOAT(I)
***** CARD 4 *****
READ (IN,350) (PB(R),R=1,REG)
WRITE (OUT,420) (PB(R),R=1,REG)
IF (REG.EQ.1) GO TO 120
N=REG-1
DC 110 R=1,N
IF (PB(R).GE.PB(R+1)) CALL ERR (1,1,4,R)
110 CONTINUE
120 IF (PT.NE.PB(REG).OR.PT.LT.1) CALL ERR(1,1, 3,6)
***** CARD 5 *****
READ (IN,360) (LR(R),R=1,REG)
WRITE (OUT,430) (LR(R),R=1,REG)
DC 130 R=1,REG
IF (LR(R).LE.0.0) CALL ERR (1,1,5,R)
130 CONTINUE
***** CARD 6 *****
READ (IN,350) (WPT(N),N=1,NUM)
WRITE (OUT,440) (WPT(N),N=1,NUM)
DO 140 N=1,NUM
140 IF (WPT(N).GT.PT) CALL ERR (1,2,WPT(N),0)
IF (DEL.EQ.0) GO TO 180
***** CARD 7 *****
READ (IN,360) (BETA(GP),GP=1,DEL)
WRITE (OUT,450) (BETA(GP),GP=1,DEL)
***** CARD 8 *****
DO 150 G=1,GRP
READ (IN,360) (SDIN(G,1),I=1,DEL)
WRITE (OUT,460) (SDIN(G,1),I=1,DEL)
150 CONTINUE

```

C	***** CARD 9 *****	IPA2C073
	READ (IN,360) (DECAY(GP),GP=1,DEL)	IPA2CC74
	WRITE (OUT,470) (DECAY(I),I=1,DEL)	IPA2C075
	DC 170 GP=1,DEL	IPA2C076
	DC 160 G=1,GRP	IPA2CC77
160	SD(G,GP)=ABS(SCIN(G,GP)*DECAY(GP))	IPA2C078
170	DECAY(GP)=-ABS(DECAY(GP))	IPA2C079
C		IPA2C080
180	CCONTINUE	IPA2C081
C	***** CARD 10 *****	IPA20082
	READ (IN,360) (CHI(G),G=1,GRP)	IPA2C083
	WRITE (OUT,480) (CHI(G),G=1,GRP)	IPA2C084
C		IPA20085
C	***** CARD 11 *****	IPA2CC86
	READ (IN,360) (V(G),G=1,GRP)	IPA2C087
	WRITE (OUT,490) (V(G),G=1,GRP)	IPA2C088
	DC 190 G=1,GRP	IPA20089
190	VINV(G)=1.0/V(G)	IPA2CC90
C	***** CARD 12 *****	IPA2C091
	READ (IN,660) EP1,EP2,EP3,IEP4,IEP6,TSTINC	IPA2C092
	WRITE (OUT,700) EP1,EP2,EP3,IEP4,IEP6,TSTINC	IPA2CC93
	IF(EP1.LE.0.0) CALL ERR (1,1,12,1)	IPA2CC94
	IF(EP2.LE.0.0) CALL ERR (1,1,12,2)	IPA2C095
	IF(IEP4.NE.0.AND.IEP4.NE.1) CALL ERR(1,1,12,5)	IPA2C096
	IF(IEP6.NE.0.AND.IEP6.NE.1) CALL ERR(1,1,12,6)	IPA2CC97
	GFPLUS=GF+1	IPA2C098
C	***** CARD 13 *****	IPA20099
	READ (IN,350) (NCMP(R),R=1,REG)	IPA2C100
	WRITE (OUT,510) (NCMP(R),R=1,REG)	IPA20101
	DC 310 I=1,NCOMP	IPA20102
	DC 200 G=1,GRP	IPA20103
	SIGCIN(G)=0.0	IPA2C104
	SIGFIN(G)=0.0	IPA2C105
	SIGTIN(G)=0.0	IPA2C106
	DC 200 GP=1,GRP	IPA2C107
200	SIGXIN(GP,G)=0.0	IPA20108

C	***** CARD 14 *****	IPA20109
	READ (IN,370) NUCNAM,(ID(K),K=1,14),I1,I2,I3	IPA20110
	WRITE (OUT,520) NUCNAM,(ID(K),K=1,14),I1,I2,I3	IPA20111
C	***** CARD 15 *****	IPA20112
	DC 210 G=1,GRP	IPA20113
	READ (IN,360) NU(G),SIGFIN(G),SIGCIN(G),SIGTIN(G),XX,SIGXIN(G+1,G)	IPA20114
	WRITE (OUT,530) NU(G),SIGFIN(G),SIGCIN(G),SIGTIN(G),XX,SIGXIN(G+1,	IPA20115
	1G)	IPA20116
210	CONTINUE	IPA20117
	INDX=I2+1	IPA20118
	GO TO (270,220,250), INDX	IPA20119
220	CONTINUE	IPA20120
C	FAST MATRIX	IPA20121
	IF (GF.EQ.0) GO TO 270	IPA20122
	DO 240 G=1,GF	IPA20123
	GPLUS=G+1	IPA20124
	IF (GPLUS.GT.GRP) GO TO 230	IPA20125
C	***** CARD 16 *****	IPA20126
	READ (IN,360) (SIGXIN(GP,G),GP=GPLUS,GFPLUS)	IPA20127
	WRITE (OUT,540) (SIGXIN(GP,G),GP=GPLUS,GFPLUS)	IPA20128
	GO TO 240	IPA20129
230	READ (IN,360) XX	IPA20130
240	CONTINUE	IPA20131
	GO TO 270	IPA20132
250	DO 260 G=1,GRP	IPA20133
C	***** CARD 17 *****	IPA20134
	READ (IN,360) (SIGXIN(GP,G),GP=1,GRP)	IPA20135
	WRITE (OUT,550) (SIGXIN(GP,G),GP=1,GRP)	IPA20136
260	CONTINUE	IPA20137
270	CONTINUE	IPA20138
C		IPA20139
C	ASSIGNMENT OF COMPOSITIONS TO REGIONS	IPA20140
C		IPA20141
	DO 300 R=1,REG	IPA20142
	IF (NCMP(R).NE.1) GO TO 300	IPA20143
	DO 290 G=1,GRP	IPA20144

	SIGF(R,G)=SIGFIN(G)	IPA20145
	SIGC(R,G)=SIGCIN(G)	IPA20146
	SIGT(R,G)=SIGTIN(G)	IPA20147
	DC 280 GP=1,GRP	IPA20148
280	SIGX(R,GP,G)=SIGXIN(GP,G)	IPA20149
290	CONTINUE	IPA20150
300	CONTINUE	IPA20151
310	CONTINUE	IPA20152
C		IPA20153
C	SET FUEL(R)=0 FOR NON FISSION REGIONS	IPA20154
C		IPA20155
	DO 311 R=1,REG	IPA20156
	FUEL(R)=0	IPA20157
	DO 311 G=1,GRP	IPA20158
	IF(ABS(SIGF(R,G)).GT.ZERO) FUEL(R)=1	IPA20159
311	CONTINUE	IPA20160
C		IPA20161
	IF (XEN.EQ.0) GO TO 330	IPA20162
C	***** CARD 18 *****	IPA20163
	READ (IN,360) GAMAX,GAMAI	IPA20164
	WRITE (OUT,560) GAMAX,GAMAI	IPA20165
C	***** CARD 19 *****	IPA20166
	DO 320 R=1,REG	IPA20167
	READ (IN,360) XENON(R),IODINE(R),(XABS(R,G),G=1,GRP)	IPA20168
	WRITE(OUT,570) XENON(R),IODINE(R),(XABS(R,G),G=1,GRP)	IPA20169
320	CONTINUE	IPA20170
330	CONTINUE	IPA20171
	IF (STEADY.EQ.2) GO TO 345	IPA20172
	IPP=GRP	IPA20173
	IF (STEADY.EQ.0) IPP=GU	IPA20174
	DO 340 G=1,IPP	IPA20175
C	***** CARD 20 *****	IPA20176
	READ (IN,360) (PSI(P,G),P=1,PT)	IPA20177
	WRITE (OUT,580) (PSI(P,G),P=1,PT)	IPA20178
340	CONTINUE	IPA20179
345	CONTINUE	IPA20180

RETURN

C

350 FORMAT (12I6)
360 FORMAT (6E12.5)
370 FORMAT (15A4,3I4)
420 FORMAT (10HOCARD 04,2X,12I6/(12X,12I6))
430 FORMAT (10HOCARD 05,2X,6E12.6/(12X,6E12.6))
440 FORMAT (10HOCARD 06,2X,12I6/(12X,12I6))
450 FORMAT (10HOCARD 07,2X,6E12.6/(12X,6E12.6))
460 FORMAT (10HOCARD 08,2X,6E12.6/(12X,6E12.6))
470 FORMAT (10HOCARD 09,2X,6E12.6/(12X,6E12.6))
480 FORMAT (10HOCARD 10,2X,6E12.6/(12X,6E12.6))
490 FORMAT (10HOCARD 11,2X,6E12.6/(12X,6E12.6))
510 FORMAT (10HOCARD 13,2X,12I6/(12X,12I6))
520 FORMAT (10HOCARD 14,2X,15A4,3I4)
530 FORMAT (10HOCARD 15,2X,6E12.6)
540 FORMAT (10HOCARD 16,2X,6E12.6/(12X,6E12.6))
550 FORMAT (10HOCARD 17,2X,6E12.6/(12X,6E12.6))
560 FORMAT (10HOCARD 18,2X,6E12.6)
570 FORMAT (10HOCARD 19,2X,6E12.6)
580 FORMAT (10HOCARD 20,2X,6E12.6/(12X,6E12.6))
660 FORMAT (3E12.5,2I12,E12.5)
700 FORMAT (10HOCARD 12,2X,3E12.6,2I12,E12.6)

C

END

IPA20181
IPA20182
IPA20183
IPA20184
IPA20185
IPA20186
IPA20187
IPA20188
IPA20189
IPA20190
IPA20191
IPA20192
IPA20193
IPA20194
IPA20195
IPA20196
IPA20197
IPA20198
IPA20199
IPA20200
IPA20201
IPA20202
IPA20203
IPA20204
IPA20205

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SUBROUTINE INPUTB(SOR,SORG,SRCEO ,SRCE1,STPRN,IPL,IPR,RTAG,TAGX,IN
1TAGT,TAGF,TAGC,CXL,CXQ,CTRL,CTRQ,CCL,CCQ,CFL,CFQ)      IN
  IMPLICIT REAL*8 (A-H,O-Z)                            IN
  INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,  IN
1      UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPL,CLT,
2      P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,IN
1      UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,
2      P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SCR,
3      SRCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT
  INTEGER RTAG
  REAL*8 IODINE
  REAL*8 LR,NU,NUSIGF,NX
  COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL
  COMMON /A3/PUNBAL,SRCE,GEOM,NTAG,NUM2,PUNFRS
  COMMON/A5/IN,OUT,NERR
  COMMON/A6/EP1,EP2,EP3,TSTINC,IEP4,IEP6
  COMMON /B1/H,HP,TIME,TZ,ZERC,TZO,TIMZ
  COMMON /B2/NPRT,NZ,ISX,STEP,NZSAVE,PRBEND,IPRN
  DIMENSION IPL(REG),IPR(REG)
  DIMENSION STPRN(50)
  DIMENSION SOR(REG),SORG(REG,GRP),SRCEO(PT,GRP),SRCE1(PT,GRP)
  DIMENSION RTAG(REG)
  DIMENSION TAGC(REG),TAGF(REG),TAGT(REG),TAGX(REG)
  DIMENSION CCL(REG,GRP),CCQ(REG,GRP),CFL(REG,GRP),CFQ(REG,GRP),
1CTRL(REG,GRP),CTRQ(REG,GRP),CXL(REG),CXQ(REG)
  FLGAT(I)=DFLOAT(I)
  TZO=TZ
  STEP=0
  NPRT=1
  DO 11 R=1,REG
  TAGX(R)=0
  TAGT(R)=0
  TAGC(R)=0
  TAGF(R)=0
  CXQ(R)=0.0
  DO 11 G=1,GRP

```

```

IPB C001
IPB C002
IPB C003
IPB C004
IPB C005
IPB C006
IPB C007
IPB C008
IPB C009
IPB C010
IPB C011
IPB C012
IPB C013
IPB C014
IPB C015
IPB C016
IPB C017
IPB C018
IPB C019
IPB C020
IPB C021
IPB C022
IPB C023
IPB C024
IPB C025
IPB C026
IPB C027
IPB C028
IPB C029
IPB C030
IPB C031
IPB C032
IPB C033
IPB C034
IPB C035
IPB C036

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	CTRQ(R,G)=0.0	IPB C037
	CCQ(R,G)=0.0	IPB C038
11	CFQ(R,G)=0.0	IPB C039
	WRITE (OUT,510) NZ	IPB C040
C	***** CARD 21 *****	IPB C041
	READ (IN,650) HBEGIN,IH,TZ,IPRN,NUM2,NTAG,SORCE,IEP4,IEP6	IPB C042
	WRITE(OUT,670) HBEGIN,IH,TZ,IPRN,NUM2,NTAG,SORCE,IEP4,IEP6	IPB C043
	IF(IH.NE.0.AND.IH.NE.1) CALL ERR(1,1,21,2)	IPB C044
	IF(NZ.EQ.1.AND.IH.NE.1) CALL ERR(1,1,21,2)	IPB C045
	IF(IH.EQ.0) GO TO 15	IPB C046
	H=HBEGIN	IPB C047
	HP=HBEGIN	IPB C048
15	CONTINUE	IPB C049
	ISX=0	IPB C050
	IF(TZ.LE.0.000) ISX=1	IPB C051
	TZ=DABS(TZ)	IPB C052
	IF (TZ.LT.TZ0) CALL ERR (1,1,21,3)	IPB C053
	IF (IPRN.LT.0) CALL ERR (1,1,21,4)	IPB C054
	IF(IABS(NUM2).GT.50) CALL ERR (1,1,21,5)	IPB C055
	IF ((NTAG.LT.-2).OR.(NTAG.GT.REG)) CALL ERR (1,1,21,6)	IPB C056
	IF ((SORCE.LT.-2).OR.(SORCE.GT.REG)) CALL ERR (1,1,21,7)	IPB C057
C		IPB C058
	IF (NUM2) 110,140,120	IPB C059
110	NUM2=-NUM2	IPB C060
C	***** CARD 22 *****	IPB C061
	READ (IN,490) (STPRN(N),N=1,NUM2)	IPB C062
	WRITE (OUT,530) (STPRN(N),N=1,NUM2)	IPB C063
	STPRN(NUM2+1)=TZ	IPB C064
	GO TO 160	IPB C065
120	X=(TZ-TZ0)/NUM2	IPB C066
	STPRN(1)=TZ0+X	IPB C067
	DO 130 N=2,NUM2	IPB C068
130	STPRN(N)=STPRN(N-1)+X	IPB C069
	GO TO 160	IPB C070
140	CONTINUE	IPB C071
	DO 150 N=1,50	IPB C072

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150 STPRN(N)=0.0
160 CONTINUE
DO 170 R=1,REG
170 RIAG(R)=1
IF (NTAG) 270,240,180
180 CONTINUE
DO 230 I=1,NTAG
***** CARD 23 *****
READ (IN,480) R,TAGX(R),TAGI(R),TAGC(R),TAGF(R)
WRITE (OUT,540) R,TAGX(R),TAGI(R),TAGC(R),TAGF(R)
RIAG(R)=-1
IF (TAGX(R).EQ.0) GO TO 190
IF (TAG(R).EQ.0) GO TO 200
***** CARD 24 *****
READ (IN,490) CXL(R),CXQ(R)
WRITE (OUT,550) CXL(R),CXQ(R)
***** CARD 25 *****
IF (TAGI(R).EQ.0) GO TO 200
IF (TAGI(R).EQ.3)GC TO 195
READ (IN,490) (CTRL(R,G),G=1,GRP)
WRITE (OUT,560) (CTRL(R,G),G=1,GRP)
***** CARD 26 *****
IF (TAGI(R).LT.2) GO TO 200
READ (IN,490) (CTRQ(R,G),G=1,GRP)
WRITE (OUT,570) (CTRQ(R,G),G=1,GRP)
***** CARD 27 *****
IF (TAGC(R).EQ.0) GO TO 210
IF (TAGC(R).EQ.3)GO TO 205
READ (IN,490) (CCL(R,G),G=1,GRP)
WRITE (OUT,580) (CCL(R,G),G=1,GRP)
***** CARD 28 *****
IF (TAGC(R).LT.2) GC TO 210
READ (IN,490) (CCQ(R,G),G=1,GRP)
WRITE (OUT,610) (CCQ(R,G),G=1,GRP)
***** CARD 29 *****
IF (TAGF(R).EQ.0) GO TO 220
IF (TAGF(R).EQ.3)GO TO 215

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IPB C073
IPB C074
IPB C075
IPB C076
IPB C077
IPB C078
IPB C079
IPB C080
IPB C081
IPB C082
IPB C083
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IPB C094
IPB C095
IPB C096
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IPB C098
IPB C099
IPB C100
IPB C101
IPB C102
IPB C103
IPB C104
IPB C105
IPB C106
IPB C107
IPB C108

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	READ (IN,490) (CFL(R,G),G=1,GRP)	IPB C109
	WRITE (OUT,620) (CFL(R,G),G=1,GRP)	IPB C110
C	***** CARD 30 *****	IPB C111
215	IF (TAGF(R).LT.2) GC TC 220	IPB C112
	READ (IN,490) (CFQ(R,G),G=1,GRP)	IPB C113
	WRITE (OUT,630) (CFQ(R,G),G=1,GRP)	IPB C114
220	CONTINUE	IPB C115
230	CONTINUE	IPB C116
240	DO 260 R=1,REG	IPB C117
	IF (RTAG(R).LT.0) GC TC 260	IPB C118
	TAGX(R)=0	IPB C119
	TAGT(R)=0	IPB C120
	TAGC(R)=0	IPB C121
	TAGF(R)=0	IPB C122
	CXL(R)=0.0	IPB C123
	CXQ(R)=0.0	IPB C124
	DO 250 G=1,GRP	IPB C125
	CTRL(R,G)=0.0	IPB C126
	CTRQ(R,G)=0.0	IPB C127
	CCL(R,G)=0.0	IPB C128
	CCQ(R,G)=0.0	IPB C129
	CFL(R,G)=0.0	IPB C130
	CFQ(R,G)=0.0	IPB C131
250	CONTINUE	IPB C132
260	CONTINUE	IPB C133
270	CONTINUE	IPB C134
	DO 280 R=1,REG	IPB C135
280	RTAG(R)=1	IPB C136
	IF (SORCE) 430,440,290	IPB C137
290	DO 400 N=1,SORCE	IPB C138
C	***** CARD 31 *****	IPB C139
	READ (IN,480) R,SCR(R)	IPB C140
	WRITE (OUT,640) R,SCR(R)	IPB C141
	RTAG(R)=-1	IPB C142
	PL=IPL(R)	IPB C143
	PR=IPR(R)	IPB C144

	IF (SOR(R)-1) 340,300,320	IPB 0145
C	***** CARD 32 *****	IPB 0146
300	DO 310 G=1,GRP	IPB 0147
	READ (IN,490) (SRCEO(P,G),SRCE1(P,G) ,P=PL,PR)	IPB 0148
	WRITE (OUT,590) (SRCEO(P,G),SRCE1(P,G) ,P=PL,PR)	IPB 0149
310	CONTINUE	IPB 0150
	GO TO 370	IPB 0151
320	K=PL	IPB 0152
C	***** CARD 33 *****	IPB 0153
	READ (IN,490) (SRCEO(K,G),SRCE1(K,G) ,G=1,GRP)	IPB 0154
	WRITE (OUT,600) (SRCEC(K,G),SRCE1(K,G) ,G=1,GRP)	IPB 0155
	DO 330 P=PL,PR	IPB 0156
	DO 330 G=1,GRP	IPB 0157
	SRCEO(P,G)=SRCEO(K,G)	IPB 0158
	SRCE1(P,G)=SRCE1(K,G)	IPB 0159
330	CONTINUE	IPB 0160
	GO TO 370	IPB 0161
340	CONTINUE	IPB 0162
	DO 350 P=PL,PR	IPB 0163
	DO 350 G=1,GRP	IPB 0164
350	SRCE1(P,G)=0.0	IPB 0165
	DO 360 G=1,GRP	IPB 0166
360	SORG(R,G)=0.0	IPB 0167
	GO TO 400	IPB 0168
370	DO 390 G=1,GRP	IPB 0169
	SGRG(R,G)=0.0	IPB 0170
	DO 380 P=PL,PR	IPB 0171
380	IF ((SRCEO(P,G).NE.0).OR.(SRCE1(P,G).NE.C)) SORG(R,G)=1	IPB 0172
390	CONTINUE	IPB 0173
400	CONTINUE	IPB 0174
	DO 420 R=1,REG	IPB 0175
	IF (RTAG(R).LT.0) GO TO 420	IPB 0176
	PL=IPL(R)	IPB 0177
	PR=IPR(R)	IPB 0178
	DO 410 G=1,GRP	IPB 0179
	SGRG(R,G)=0	IPB 0180

DO 410 P=PL,PR	IPB 0181
SRCEO(P,G)=0.0	IPB 0182
410 SRCEL(P,G)=0.0	IPB 0183
420 CCNTINUE	IPB 0184
430 RETURN	IPB 0185
440 DO 470 G=1,GRP	IPB 0186
DO 450 P=1,PT	IPB 0187
SRCEO(P,G)=0.0	IPB 0188
450 SRCEL(P,G)=0.0	IPB 0189
DO 460 R=1,REG	IPB 0190
460 SCRG(R,G)=0	IPB 0191
470 CCNTINUE	IPB 0192
RETURN	IPB 0193
C	IPB 0194
480 FORMAT (12I6)	IPB 0195
490 FORMAT (6E12.5)	IPB 0196
510 FORMAT (1H1,24X,28H*** INPUT EDIT FOR TIME ZONE,I2,4H ***)	IPB 0197
530 FORMAT (10HOCARD 22 ,2X,6E12.6/(12X,6E12.6))	IPB 0198
540 FCRMAT (10HOCARC 23 ,2X,12I6)	IPB 0199
550 FORMAT (10HOCARC 24 ,2X,2E12.6)	IPB 0200
560 FORMAT (10HOCARD 25 ,2X,6E12.6/(12X,6E12.6))	IPB 0201
570 FORMAT (10HOCARD 26 ,2X,6E12.6/(12X,6E12.6))	IPB 0202
580 FORMAT (10HOCARD 27 ,2X,6E12.6/(12X,6E12.6))	IPB 0203
590 FORMAT (10HOCARD 32 ,2X,6E12.6/(12X,6E12.6))	IPB 0204
600 FORMAT (10HOCARD 33 ,2X,2E12.6/(12X,2E12.6))	IPB 0205
610 FORMAT (10HOCARD 28 ,2X,6E12.6/(12X,6E12.6))	IPB 0206
620 FORMAT (10HOCARD 29 ,2X,6E12.6/(12X,6E12.6))	IPB 0207
630 FORMAT (10HOCARD 30 ,2X,6E12.6/(12X,6E12.6))	IPB 0208
640 FORMAT (10HOCARD 31 ,2X,2I6)	IPB 0209
650 FORMAT (E12.5,I12,E12.5,6I6)	IPB 0210
670 FORMAT (10HOCARD 21 ,2X,E12.6,I12,E12.6,6I6)	IPB 0211
END	IPB 0212

	SUBROUTINE ITER(PSI,CM,CP,SIGX,PB,IPL,IPR,XL,XR,SDIN,FUEL,	ITERCC01
	INX,NUSIGF,UPSCAT,DNSCAT,DD,DL,DU,WA,GA)	ITERCC02
	IMPLICIT REAL*8 (A-F,O-Z)	ITERCC03
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	ITERCC04
1	UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GC,GL,GU,GRP,GPU,CUT,	ITERCC05
2	P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	ITERCC06
3	SORCE , SORG , SCZ , STEADY , STEP , TAGC , TAGF , TAGT	ITERCC07
	REAL*8 LR,NU,NUSIGF,NX	ITERCC08
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	ITERCC09
	COMMON /A2/NUM,NCCMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	ITERCC10
	COMMON /A7/BETA(6),DECAY(6),BETDCY(6),DECH(6)	ITERCC11
	COMMON /B2/NPRT,NZ,ISX,STEP,NZSAVE,PRBEND,IPRN	ITERC012
	DIMENSION PSI(PT,GRP)	ITERC013
	DIMENSION IPL(REG),IPR(REG),PB(REG),XL(REG),XR(REG)	ITERC014
	DIMENSION CM(PT,GRP),CP(PT,GRP)	ITERC015
	DIMENSION DC(PT),DL(PT),DU(PT)	ITERC016
	DIMENSION SIGX(REG,GRP,GRP)	ITERCC17
	DIMENSION FUEL(REG),NX(GRP)	ITERC018
	DIMENSION SCIN(GRP,IDEL)	ITERC019
	DIMENSION NUSIGF(REG,GRP),UPSCAT(REG,GRP),DNSCAT(REG,GRP)	ITERCC20
	DIMENSION WA(PT),GA(PT)	ITERCC21
C	THIS ROUTINE PERFORMS 1 FLUX ITERATION	ITERC022
	DO 500 G=1,GRP	ITERCC23
200	BAR=0.0	ITERC024
	IF(DEL.EQ.0) GO TO 204	ITERC025
	DO 203 I=1,DEL	ITERC026
203	BAR=BAR+BETA(I)*SCIN(G,I)	ITERCC27
204	BAR=BAR+NX(G)	ITERC028
	DO 110 P=1,PT	ITERC029
	DD(P)=CM(P,G)+CP(P,G)	ITERCC30
	DU(P)=-CP(P,G)	ITERC031
110	DL(P)=-CM(P,G)	ITERC032
	IF(BCL.EQ.1) GO TO 120	ITERC033
	DD(1)=1.000	ITERCC34
	DU(1)=0.0	ITERC035
	GO TO 130	ITERC036

120	DD(1)=CD(1)+SIGX(1,G,G)	ITERC037
130	Z=SIGX(1,G,G)	ITERC038
	PL=2	ITERCC39
	PR=IPR(1)	ITERC040
	DC 140 P=PL,PR	ITERC041
140	DD(P)=CD(P)+Z	ITERC042
	I2=PB(1)	ITERC043
	DC(I2)=CD(I2)+Z*XL(1)	ITERC044
	IF(REG-1) 190,190,150	ITERC045
150	DC 170 R=2,REG	ITERC046
	Z=SIGX(R,G,G)	ITERC047
	I1=PB(R-1)	ITERC048
	CD(I1)=CD(I1)+Z*XR(R-1)	ITERCC49
	I1=PB(R)	ITERCC50
	CD(I1)=CD(I1)+Z*XL(R)	ITERC051
	PL=IPL(R)	ITERC052
	PR=IPR(R)	ITERC053
	DC 160 P=PL,PR	ITERC054
160	DD(P)=CD(P)+Z	ITERC055
170	CCONTINUE	ITERC056
	IF(BCR.EQ.1) GO TO 180	ITERC057
	DD(PT)=1.000	ITERC058
	DL(PT)=0.0	ITERCC59
	GO TO 190	ITERC060
180	CD(PT)=CD(PT)+SIGX(REG,G,G)	ITERC061
190	CCONTINUE	ITERCC62
	PL=1	ITERC063
	IF(BCL.EQ.0) PL=2	ITERC064
	DC 450 R=1,REG	ITERC065
	PR=IPR(R)	ITERC066
	IF((R.EQ.REG).AND.(BCR.EQ.1)) PR=PT	ITERC067
	DC 400 P=PL,PR	ITERC068
	PSI(P,G)=PRCD(P, R ,G,PSI,NUSIGF,SIGX,FUEL,UPSCAT,DNSCAT,BAR)	ITERC069
400	CONTINUE	ITERC070
	PL=PR+2	ITERCC71
450	CCONTINUE	ITERCC72

```
IF(REG.EQ.1) GO TO 460
DC 455 R=2,REG
P=PB(R-1)
JR1=R-1
455 PSI(P,G)=PRCD(P,JR1,G,PSI,NUSIGF,SIGX,FUEL,UPSCAT,DNSCAT,BAR)
1*XL(R-1)+PRCD(P,R,G,PSI,NUSIGF,SIGX,FUEL,UPSCAT,DNSCAT,BAR)*
2XR(R-1)
460 CCNTINUE
IF(BCL.EQ.0) PSI(1,G)=0.0
IF(BCR.EQ.0) PSI(PT,G)=0.0
CALL MATINV(G,PT,GRP,PSI,DU,DL,DD,WA,GA)
500 CCNTINUE
RETURN
END
```

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ITERC073
ITERC074
ITERC075
ITERC076
ITERC077
ITERC078
ITERC079
ITERC080
ITERC081
ITERC082
ITERC083
ITERC084
ITERC085
ITERC086
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	SUBROUTINE LHS(G,DU,DL,DC,CP,CM,TI1,VINV,FF2,XL,XR,IPL,IPR,PB)	LHS C001
C	THIS ROUTINE EVALUATES THE TRI-DIAGONAL MATRIX FOR THE LEFT-HAND	LHS C002
C	SIDE OF THE ALGORITHM FOR GROUP G	LHS C003
	IMPLICIT REAL*8 (A-F,G-Z)	LHS C004
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	LHS C005
1	UPSCAT,WPT,FUEL,G,GEOM,GP,GPL,GPR,GC,GL,GU,GRP,GPU,CUT,	LHS C006
2	P,PL,PR,PB,PRBEND,PT,PUNBAL,PUNFRS,R,REG,SOR,	LHS C007
3	SCRCE,SCRG,SCZ,STEADY,STEP,TAGC,TAGF,TAGT	LHS C008
	REAL*8 LR,NU,NLSIGF,NX	LHS C009
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	LHS C010
	COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	LHS C011
	DIMENSION FF2(PT)	LHS C012
	DIMENSION VINV(GRP)	LHS C013
	DIMENSION TI1(REG)	LHS C014
	DIMENSION IPL(REG),IPR(REG),XL(REG),XR(REG)	LHS C015
	DIMENSION PB(REG)	LHS C016
	DIMENSION CM(PT,GRP),CP(PT,GRP)	LHS C017
	DIMENSION DC(PT),DL(PT),DL(PT)	LHS C018
	PL=2	LHS C019
	DC 1 R=1,REG	LHS C020
	PR=IPR(R)	LHS C021
	T1=TI1(R)	LHS C022
	DC 2 P=PL,PR	LHS C023
	DU(P)=-CP(P,G)*FF2(P+1)	LHS C024
	DL(P)=-CM(P,G)*FF2(P-1)	LHS C025
	DD(P)=VINV(G)+(CM(P,G)+CP(P,G)-T1)*	LHS C026
	1FF2(P)	LHS C027
2	CONTINUE	LHS C028
1	PL=PR+2	LHS C029
	DC 3 R=1,REG	LHS C030
	IF(R-1) 5,4,5	LHS C031
4	IF(BCL.EQ.1) GO TO 65	LHS C032
	DD(1)=VINV(G)	LHS C033
	DU(1)=0.0	LHS C034
	GO TO 5	LHS C035
65	DD(1)=VINV(G)+(CM(1,G)+CP(1,G)-	LHS C036

	1TI1(1))*FF2(1)	LHS C037
	DU(1)=-CP(1,G)*FF2(2)	LHS C038
5	IF(R.EQ.REG) GO TO 3	LHS C039
	P=PB(R)	LHS C040
	T1=TI1(R)*XL(R)+TI1(R+1)*XR(R)	LHS C041
	DD(P)=VINV(G)+(CM(P,G)+CP(P,G)-T1)*FF2(P)	LHS C042
	DU(P)=-CP(P,G)*FF2(P+1)	LHS C043
	DL(P)=-CM(P,G)*FF2(P-1)	LHS C044
3	CONTINUE	LHS C045
	IF(BCR.EQ.1) GO TO 33	LHS C046
	DD(PT)=VINV(G)	LHS C047
	DL(PT)=0.0	LHS C048
	GO TO 605	LHS C049
33	DD(PT)=VINV(G)+(CP(PT,G)+CM(PT,G)-	LHS C050
	1TI1(REG))*FF2(PT)	LHS C051
	DL(PT)=-CM(PT,G)*FF2(PT)	LHS C052
605	CONTINUE	LHS C053
	RETURN	LHS C054
	END	LHS C055

	SUBROUTINE MATINV(G,PT,GRP,PSI,DU,DL,DD,WA,GA)	MINVCC01
	IMPLICIT REAL*8 (A-H,O-Z)	MINVCC02
	INTEGER P,G,PT,GRP,PL	MINVCC03
	DIMENSION PSI(PT,GRP)	MINVCC04
	DIMENSION DD(PT),DL(PT),DU(PT)	MINV0005
	DIMENSION WA(PT),GA(PT)	MINVCCC6
C	THIS ROUTINE EVALUATES THE FUNCTION AT THE NEW TIME BY INVERTING	MINVCC07
C	THE LEFT-HAND SIDE MATRIX. MATRIX FACTORIZATION IS USED.	MINVCC08
C	FIRST THE FORWARD ELIMINATION	MINVCCC9
	WA(1)=DU(1)/DD(1)	MINVCC10
	GA(1)=PSI(1,G)/DD(1)	MINVCC11
	DO 110 P=2,PT	MINVCC12
	T1=1.000/(DD(P)-DL(P)*WA(P-1))	MINVCC13
	IF(P.EQ.PT)GO TO 150	MINVCC14
	WA(P)=DU(P)*T1	MINV0015
150	GA(P)=(PSI(P,G)-DL(P)*GA(P-1))*T1	MINVCC16
110	CONTINUE	MINVCC17
C	NOW THE BACK SUBSTITUTION	MINVCC18
	PSI(PT,G)=GA(PT)	MINVCC19
	PL=PT-1	MINVCC20
	DO 120 J=1,PL	MINVCC21
	P=PT-J	MINVCC22
	PSI(P,G)=GA(P)-WA(P)*PSI(P+1,G)	MINVCC23
120	CONTINUE	MINVCC24
	RETURN	MINVCC25
	END	MINVCC26

	SUBROUTINE PREC(G,PSI,NUSIGF,FF2,FUEL,XL,XR,PB,IPL,IPR,TD)	PRECCCC1
	IMPLICIT REAL*8 (A-H,O-Z)	PRECC002
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	PRECC003
1	UPSCAT,WPT, FUEL,G,GECM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CLT,	PRECC004
2	P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	PRECC005
3	SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	PRECC006
	REAL*8 LR,NU,NUSIGF,NX	PRECC007
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	PRECC008
	COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	PRECC009
	COMMON /A7/BETA(6),DECAY(6),BETDCY(6),DECH(6)	PRECC010
	DIMENSION PSI(PT,GU)	PRECC011
	DIMENSION FF2(PT)	PRECC012
	DIMENSION IPL(REG),IPR(REG),PB(REG),XL(REG),XR(REG)	PRECC013
	DIMENSION FUEL(REG)	PRECC014
	DIMENSION TD(GRP)	PRECC015
	DIMENSION NUSIGF(REG,GRP)	PRECC016
C	THIS ROUTINE CALCULATES THE PRECURSOR CONCENTRATIONS IN THE	PRECC017
C	INTERIOR OF EACH REGION FOR PRECURSOR GROUP G	PRECC018
	J=G-GRP	PRECC019
	X5=DECAY(J)	PRECC020
	X6=DECH(J)	PRECC021
	DO 17 R=1,REG	PRECC022
	PL=IPL(R)	PRECC023
	IF (R.EQ.1) PL=1	PRECC024
	PR=IPR(R)	PRECC025
	IF (R.EQ.REG) PR=PT	PRECC026
	IF(FUEL(R)) 13,11,13	PRECC027
11	DO 12 P=PL,PR	PRECC028
	PSI(P,G)=0.0	PRECC029
12	CONTINUE	PRECC030
	GO TO 17	PRECC031
13	DO 14 GP=1,GRP	PRECC032
14	TD(GP)=NUSIGF(R,GP)*BETA(J)	PRECC033
	DO 16 P=PL,PR	PRECC034
	T1=0.0	PRECC035
	T2=0.0	PRECC036

	DC 15 GP=1,GRP	PRECC037
	Y=FF2(P)	PRECC038
	T2=T2+TD(GP)*PSI(P,GP)*Y	PRECC039
15	CONTINUE	PRECC040
	PSI(P,G)=X6*PSI(P,G)+T2	PRECC041
16	CONTINUE	PRECC042
17	CONTINUE	PRECC043
	IF(BCL.EQ.0) PSI(1,G)=0.0	PRECC044
	IF(BCR.EQ.0) PSI(PT,G)=0.0	PRECC045
C	THIS ROUTINE CALCULATES THE PRECURSOR CONCENTRATIONS AT THE	PRECC046
C	BOUNDARY POINTS OF THE REGIONS IN PRECURSOR GROUP G	PRECC047
	X8=BETA(J)	PRECC048
	IP=REG-1	PRECC049
	DO 160 R=1,IP	PRECC050
	P=PB(R)	PRECC051
	IF (FUEL(R)) 130,110,130	PRECC052
110	IF (FUEL(R+1)) 130,120,130	PRECC053
120	PSI(P,G)=0.0	PRECC054
	GO TO 160	PRECC055
130	X1=XL(R)	PRECC056
	X2=XR(R)	PRECC057
	DO 140 GP=1,GRP	PRECC058
	TD(GP)=(NUSIGF(R,GP)*X1+NUSIGF(R+1,GP)*X2)*X8	PRECC059
140	CONTINUE	PRECC060
	T1=0.0	PRECC061
	T2=0.0	PRECC062
	Y=FF2(P)	PRECC063
	DO 150 GP=1,GRP	PRECC064
	T2=T2+TD(GP)*PSI(P,GP)*Y	PRECC065
150	CONTINUE	PRECC066
	PSI(P,G)=X6*PSI(P,G)+T2	PRECC067
160	CONTINUE	PRECC068
	RETURN	PRECC069
	END	PRECC070

	SUBROUTINE PRINTA(PSI,PSITCT,POWREG,WPT,WZ,WHZ)	PRINCC01
	IMPLICIT REAL*8 (A-F,C-Z)	PRINCC02
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	PRINCC03
1	UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	PRINCC04
2	P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SCR,	PRINCC05
3	SORCE , SORG , SCZ , STEADY , STEP , TAGC , TAGF , TAGI	PRINCC06
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	PRINCC07
	COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	PRINCC08
	COMMON/A5/IN,CUT,NERR	PRINCC09
	COMMON /A9/POWTCT,POWBAR	PRINCC10
	COMMON /B1/H,HP,TIME,TZ,ZERG,TZO,TIMZ	PRINCC11
	COMMON /B2/NPRT,NZ,ISX,STEP,NZSAVE,PRBEND,IPRN	PRINCC12
	DIMENSION PSI(PT,GU)	PRINCC13
	DIMENSION PSITCT(REG,GRP)	PRINCC14
	DIMENSION POWREG(REG)	PRINCC15
	DIMENSION WHZ(PT)	PRINCC16
	DIMENSION WZ(PT)	PRINCC17
	DIMENSION WPT(NUM)	PRINCC18
	WRITE (CUT,140)	PRINCC19
	CALL TITLE (2)	PRINCC20
	WRITE (CUT,130) NZ,STEP,TIME,HP	PRINCC21
	TPRT=TIME	PRINCC22
	WRITE (OUT,150)	PRINCC23
	DO 110 N=1,NUM	PRINCC24
	P=WPT(N)	PRINCC25
109	WRITE (OUT,240) N,P,WZ(P),WHZ(P)	PRINCC26
110	CONTINUE	PRINCC27
	IGPT=GU	PRINCC28
	IF((DABS(TIME-TZ)).LE.ZERO) GO TO 2	PRINCC29
	IF(ISX.GT.0) IGPT=GRP	PRINCC30
2	CONTINUE	PRINCC31
	DO 120 G=1,IGPT	PRINCC32
	IF(G.LE.GRP) GO TO 111	PRINCC33
	IG9=G-GRP	PRINCC34
	WRITE (CUT,221) IG9	PRINCC35
	GO TO 112	PRINCC36

111	WRITE (OUT,220) G	PRINC037
112	WRITE (OUT,230) (P,PSI(P,G),P=1,PT)	PRINC038
	IF(G.GT.GRP) GO TO 120	PRINC039
	WRITE (OUT,222) (R,G,PSITOT(R,G),R=1,REG)	PRINCC40
120	CONTINUE	PRINCC41
	WRITE(OUT,121)	PRINC042
	WRITE(CUT,122)(R,POWREG(R),R=1,REG)	PRINC043
	WRITE(CUT,123)PCWTCT	PRINCC44
121	FORMAT(1H0,10X,'REGION',10X,'NORMALIZED POWER',/)	PRINC045
122	FORMAT(13X,I2,12X,E14.7)	PRINC046
123	FORMAT(1H0,10X,'TOTAL NORMALIZED POWER = ',E14.7)	PRINC047
130	FORMAT (12H0 TIME ZONE=I2,14H STEP NUMBER=I4,7H TIME=,E12.6,12H	PRINC048
	1 TIME STEP=,E12.6)	PRINC049
140	FORMAT (1H0)	PRINCC50
150	FORMAT (1H0/11H TEST POINT,6X,10H MESH POINT,6X,9H FREQUENCY,9X,8HEX	PRINC051
	1P(W*H),1H)	PRINC052
220	FORMAT (30HOPPOINT-WISE FLUXES FOR GROUP ,I3)	PRINC053
221	FORMAT(44HOPRECURSOR CONCENTRATION FOR DELAYED GROUP ,I2)	PRINCC54
222	FORMAT(34HOTOTAL INTEGRATED FLUX FOR REGION ,I2,7H GROUP ,I2,	PRINC055
	13H = ,E12.6)	PRINC056
230	FORMAT ((2X,6(1H(,I3,2H) ,1PE12.6)))	PRINCC57
240	FORMAT(4X,I3,13X,I3,9X,1PE11.4,6X,1PE13.6,14X,I3)	PRINC058
	RETURN	PRINC059
	END	PRINCC60

	FUNCTION PROD(P, R ,G,PSI,NUSIGF,SIGX,FUEL,UPSCAT,DNSCAT,BAR)	PRDCCC01
	IMPLICIT REAL*8 (A-H,O-Z)	PRDCCC02
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	PRDCCC03
1	UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	PRDCCC04
2	P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SCR,	PRDCCC05
3	SORCE , SORG , SCZ , STEADY , STEP , TAGC , TAGF , TAGT	PRDCCC06
	REAL*8 LR,NUSIGF	PRDCCC07
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	PRDCCC08
	DIMENSION PSI(PT,GRP)	PRDCCC09
	DIMENSION DNSCAT(REG,GRP),UPSCAT(REG,GRP)	PRDCCC10
	DIMENSION FUEL(REG)	PRDCCC11
	DIMENSION NUSIGF(REG,GRP)	PRDCCC12
	DIMENSION SIGX(REG,GRP,GRP)	PRDCCC13
	X=0.0	PRDCCC14
	IF(FUEL(R).EQ.0) GO TO 215	PRDCCC15
205	IF(BAR.EQ.0.0) GO TO 215	PRDCCC16
	DO 210 GP=1,GRP	PRDCCC17
210	X=X+BAR*NUSIGF(R,GP)*PSI(P,GP)	PRDCCC18
215	IF(UPSCAT(R,G)) 220,250,220	PRDCCC19
220	GPL=G+1	PRDCCC20
	GPU=UPSCAT(R,G)	PRDCCC21
	DO 230 GP=GPL,GPU	PRDCCC22
230	X=X+SIGX(R,G,GP)*PSI(P,GP)	PRDCCC23
250	IF(DNSCAT(R,G)) 255,270,255	PRDCCC24
255	GPL=DNSCAT(R,G)	PRDCCC25
	GPU=G-1	PRDCCC26
	DO 260 GP=GPL,GPU	PRDCCC27
260	X=X+SIGX(R,G,GP)*PSI(P,GP)	PRDCCC28
270	PROD=X	PRDCCC29
	RETURN	PRDCCC30
	END	PRDCCC31

SUBROUTINE PUN(PSI,NU,SIGF,SIGC,SIGT,SIGX,XENON,IODINE)	PUN 0001
IMPLICIT REAL*8 (A-H,O-Z)	PUN 0002
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	PUN 0003
1 UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPL,CUT,	PUN 0004
2 P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SOR,	PUN 0005
3 SCRCE , SORG , SCZ , STEADY , STEP , TAGC , TAGF , TAGT	PUN 0006
REAL*8 IODINE	PUN 0007
REAL*8 LR,NU,NUSIGF,NX	PUN 0008
COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	PUN 0009
COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	PUN 0010
DIMENSION PSI(PT,GU)	PUN 0011
DIMENSION NU(GRP)	PUN 0012
DIMENSION XENON(REG),IODINE(REG)	PUN 0013
DIMENSION SIGC(REG,GRP),SIGF(REG,GRP),SIGT(REG,GRP),	PUN 0014
1SIGX(REG,GRP,GRP)	PUN 0015
XX=0.0	PUN 0016
I1=0	PUN 0017
I2=2	PUN 0018
I3=0	PUN 0019
ASSIGN 120 TO NSWTCH	PUN 0020
IF (GRP.EQ.1) ASSIGN 160 TO NSWTCH	PUN 0021
NGRP=GRP-1	PUN 0022
DO 180 R=1,REG	PUN 0023
PUNCH 110, R, I1, I2, I3	PUN 0024
110 FORMAT (10H REGION ,I3,47X,3I4)	PUN 0025
GO TO NSWTCH, (120,160)	PUN 0026
120 DO 150 G=1,NGRP	PUN 0027
PUNCH 190, NU(G),SIGF(R,G),SIGC(R,G),SIGT(R,G),XX,SIGX(R,G+1,G)	PUN 0028
DO 130 K=1,GRP	PUN 0029
130 SIGX(R,K,K)=0.0	PUN 0030
DO 140 K=1,GRP	PUN 0031
140 PUNCH 190, (SIGX(R,GP,K),GP=1,GRP)	PUN 0032
150 CONTINUE	PUN 0033
PUNCH 190, NU(GRP),SIGF(R,GRP),SIGC(R,GRP),SIGT(R,GRP),XX,XX	PUN 0034
PUNCH 190, (SIGX(R,GP,GRP),GP=1,NGRP),XX	PUN 0035
GO TO 170	PUN 0036

160 PUNCH 190, NU(1),SIGF(R,1),SIGC(R,1),SIGT(R,1),XX,XX	PUN C037
PUNCH 190, XX	PUN C038
170 CONTINUE	PUN C039
180 CCNTINUE	PUN C040
190 FORMAT (6E12.7)	PUN C041
IF (XEN.EQ.0) GC TC 220	PUN C042
DO 210 R=1,REG	PUN C043
IF ((XENCN(R).NE.0.0).OR.(ICDINE(R).NE.0.0)) PUNCH 200, R,XENCN(R)	PUN C044
1,ICDINE(R)	PUN C045
200 FORMAT (I6,6X,2E12.7)	PUN C046
210 CCNTINUE	PUN C047
220 DO 230 G=1,GU	PUN C048
PUNCH 190, (PSI(P,G) ,P=1,PT)	PUN C049
230 CONTINUE	PUN C050
RETURN	PUN C051
END	PUN C052

```
SUBROUTINE RESCAL(X,PSI)
  IMPLICIT REAL*8 (A-H,O-Z)
  INTEGER G,GRP,REG,PT,GL,GU,DEL,THG,IDEL,P
  COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL
  DIMENSION PSI(PT,GRP)
  CALL      SCALE(Y,PSI)
  Y=X/Y
  DO 110 G=1,GRP
  DO 110 P=1,PT
110 PSI(P,G)=PSI(P,G)*Y
  RETURN
  END
```

```
RESCCC01
RESCCC02
RESCCC03
RESCCC04
RESCCC05
RESCCC06
RESCCC07
RESCCC08
RESCCC09
RESCCC10
RESCCC11
RESCCC12
```

	SUBROUTINE RHS(G,PSI,FF1,FF2,TI1,NX,NUSIGF,VINV,SIGX ,FUEL,SD,	RHS C001
	IXL,XR,PB,IPL,IPR)	RHS C002
	IMPLICIT REAL*8 (A-H,O-Z)	RHS C003
	INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	RHS 0004
1	UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GU,GRP,GPU,CUT,	RHS CCC5
2	P,PL,PR,PB, PRBENC , PT , PUNBAL , PUNFRS , R,REG,SOR,	RHS C006
3	SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	RHS C007
	REAL*8 LR,NU,NUSIGF,NX	RHS C008
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	RHS CCC9
	COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	RHS C010
	DIMENSION PSI(PT,GU)	RHS C011
	DIMENSION FF1(PT)	RHS C012
	DIMENSION FF2(PT)	RHS C013
	DIMENSION VINV(GRP)	RHS C014
	DIMENSION TI1(REG)	RHS C015
	DIMENSION IPL(REG),IPR(REG),PB(REG),XL(REG),XR(REG)	RHS C016
	DIMENSION FUEL(REG)	RHS C017
	DIMENSION SD(GRP,IDEL)	RHS C018
	DIMENSION NX(GRP),NUSIGF(REG,GRP)	RHS C019
	DIMENSION SIGX(REG,GRP,GRP)	RHS C020
C	THIS ROUTINE EVALUATES THE RHS OF THE ALGORITHM AT ALL INTERIOR	RHS C021
C	POINTS OF EACH REGION IN A GIVEN GROUP	RHS C022
	X3=NX(G)	RHS C023
	PL=1	RHS C024
	IF (BCL.EQ.0) PL=2	RHS C025
	DO 20 R=1,REG	RHS C026
	PR=IPR(R)	RHS C027
	IF((R.EQ.REG).AND.(BCR.EQ.1)) PR=PT	RHS C028
	DO 19 P=PL,PR	RHS C029
	T1=0.0	RHS C030
	T2=0.0	RHS C031
	IF(GRP.EQ.1) T2=X3*NUSIGF(R,G)*PSI(P,G)	RHS C032
	IF(G.EQ.1) GO TO 12	RHS C033
	GPU=G-1	RHS C034
	DO 11 GP=1,GPU	RHS C035
11	T1=T1+(X3*NUSIGF(R,GP)+SIGX(R,G,GP))	RHS C036

	1*PSI(P,GP)	RHS CC37
12	IF(G.EQ.GRP) GO TO 14	RHS C038
	GPL=G+1	RHS C039
	DO 13 GP=GPL,GRP	RHS CC40
13	T2=T2+(X3*NUSIGF(R,GP)+SIGX(R,G,GP))*	RHS C041
	1PSI(P,GP)	RHS 0042
C	NOW ADD DELAY CONTRIBUTIONS	RHS CC43
14	T3=0.0	RHS C044
	IF(DEL) 18,18,15	RHS C045
15	IF(FUEL(R)) 16,18,16	RHS C046
16	DO 17 GP=GL,GU	RHS CC47
	GD=GP-GRP	RHS C048
	T3=T3+SD(G,GD)*PSI(P,GP)	RHS C049
17	CONTINUE	RHS CC50
	T1=T1*FF2(P)	RHS C051
	T2=T2*FF1(P)	RHS 0052
	T3=T3*FF1(P)	RHS CC53
18	T4=T1+T2+T3	RHS CC54
	PSI(P,G)=VINV(G)*PSI(P,G)+T4	RHS C055
19	CONTINUE	RHS C056
	PL=PR+2	RHS CC57
20	CONTINUE	RHS C058
C	THIS ROUTINE EVALUATES THE RHS OF THE ALGORITHM AT ALL REGION	RHS C059
C	BOUNDARY POINTS IN GROUP G	RHS CC60
	IP=REG-1	RHS C061
	IF (IP) 220,220,110	RHS C062
110	DO 210 R=1,IP	RHS C063
	JRP=R+1	RHS C064
	P=PB(R)	RHS C065
	X1=XL(R)	RHS CC66
	X2=XR(R)	RHS CC67
	T1=0.0	RHS C068
	T2=0.0	RHS C069
	IF(GRP.EQ.1) T2=X3*(NUSIGF(R,G)*X1+NUSIGF(R+1,G)*X2)*PSI(P,G)	RHS CC70
	IF (G.EQ.1) GO TO 130	RHS C071
	GPU=G-1	RHS C072

	DO 120 GP=1, GPU	RHS C073
120	T1=T1+(X3*(NUSIGF(R,GP)*X1+NUSIGF(R+1,GP)	RHS C074
	1*X2)+SIGX(R,G,GP)*X1+SIGX(R+1,G,GP)*	RHS C075
	2X2)*PSI(P,GP)	RHS C076
130	IF (G.EQ.GRP) GO TO 150	RHS C077
	GPL=G+1	RHS C078
	DO 140 GP=GPL, GRP	RHS C079
140	T2=T2+(X3*(NUSIGF(R,GP)*X1+NUSIGF(R+1,GP)	RHS C080
	1*X2)+SIGX(R,G,GP)*X1+SIGX(R+1,G,GP)*	RHS C081
	2X2)*PSI(P,GP)	RHS C082
C	THEN ADD PRECURSOR CONTRIBUTIONS	RHS C083
150	T3=0.	RHS C084
	IF (DEL) 200,200,160	RHS C085
C	WE CHECK FOR ANY FUEL AT THE BOUNDARY POINT	RHS C086
160	IF (FUEL(R)) 180,170,180	RHS C087
170	IF (FUEL(R+1)) 180,200,180	RHS C088
180	DO 190 GP=GL, GU	RHS C089
	GD=GP-GRP	RHS C090
	T3=T3+SD(G, GD)*PSI(P, GP)	RHS C091
190	CONTINUE	RHS C092
	T1=T1*FF2(P)	RHS C093
	T2=T2*FF1(P)	RHS C094
	T3=T3*FF1(P)	RHS C095
200	T4=T1+T2+T3	RHS C096
	PSI(P, G)=VINV(G)*PSI(P, G)+T4	RHS C097
210	CONTINUE	RHS C098
220	RETURN	RHS C099
	END	RHS C100

	SUBROUTINE SCALE(Y,PSI)	SCL C001
	IMPLICIT REAL*8 (A-H,O-Z)	SCL C002
	INTEGER G,GRP,REG,PT,GL,GU,DEL,THG,IDEL,P	SCL C003
	COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	SCL C004
	DIMENSION PSI(PT,GRP)	SCL C005
C	THIS FUNCTION FINDS THE LENGTH OF THE FLUX VECTOR	SCL C006
	X=C.0DC	SCL C007
	DC 110 G=1,GRP	SCL C008
	DC 110 P=1,PT	SCL C009
11C	X=X+PSI(P,G)*PSI(P,G)	SCL C010
	Y=DSQRT(X)	SCL C011
	RETURN	SCL C012
	END	SCL C013

SUBROUTINE SETUP(PSI,WPT,NU,NUSIGF,CM,CP,SIGX,PB,IPR,IPL,XL,XR,	SET C001
1FUEL,NX,SDIN,UPSCAT,DNSCAT,PSISTO,DD,DL,DU,WA,GA)	SET C002
IMPLICIT REAL*8 (A-H,O-Z)	SET C003
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	SET C004
1 UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GC,GL,GU,GRP,GPU,CLT,	SET C005
2P,PL,PR,PB,PRBEND,PT,PUNBAL,PUNFRS,R,REG,SCR,	SET C006
3 SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	SET C007
REAL*8 ICDINE	SET C008
REAL*8 LR,NU,NUSIGF,NX	SET C009
REAL*8 KEFF	SET CC1C
COMMON /A1/GRP,REG,PT,GL,GU,DEL,THG,IDEL	SET CC11
COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	SET CC12
COMMON /A3/PUNBAL,SORCE,GECM,NTAG,NUM2,PUNFRS	SET C013
COMMON /A4/TIGHT1,TIGHT2,TIGHT3	SET CC14
COMMON/A5/IN,OUT,NERR	SET C015
C THIS ROUTINE CORRECTS THE INITIAL ESTIMATES TO AN EXACTLY CRITICAL	SET C016
C PROBLEM AND CALCULATES THE PRECURSOR CONCENTRATIONS	SET CC17
DIMENSION PSI(PT,GU)	SET CC18
DIMENSION WPT(NUM)	SET C019
DIMENSION PSISTO(NUM)	SET CC20
DIMENSION NU(GRP)	SET C021
DIMENSION NUSIGF(REG,GRP)	SET C022
DIMENSION CM(PT,GRP),CP(PT,GRP)	SET C023
DIMENSION SIGX(REG,GRP,GRP)	SET CC24
DIMENSION PB(REG),IPL(REG),IPR(REG),XL(REG),XR(REG)	SET C025
DIMENSION FUEL(REG)	SET C026
DIMENSION NX(GRP)	SET CC27
DIMENSION SDIN(GRP,IDEL)	SET CC28
DIMENSION UPSCAT(REG,GRP),DNSCAT(REG,GRP)	SET CC29
DIMENSION DD(PT),DL(PT),DU(PT),WA(PT),GA(PT)	SET CC30
ABS(X)=DABS(X)	SET CC31
SQRT(X)=DSQRT(X)	SET CC32
FLOAT(I)=DFLOAT(I)	SET CC33
IF (STEADY.EQ.3) GO TO 201	SET CC34
KEFF=0.	SET C035
XKK=0.0	SET C036

```

Y=0.
INDX=0
CALL      SCALE(X,PSI)
110 CONTINUE
DO 130 N=1,NUM
P=WPT(N)
PSISTO(N)=PSI(P,THG)
130 CONTINUE
CALL      ITER(PSI,CM,CP,SIGX,PB,IPL,IPR,XL,XR,SDIN,FUEL,
INX,NUSIGF,UPSCAT,DNSCAT,DD,DL,DU,WA,GA)
CALL      SCALE(Y,PSI)
KEFF=Y/X
CALL      RESCAL(X,PSI)
IF (XKK) 140,140,150
140 XKK=KEFF
INDX=1
GO TO 110
150 IF (ABS(KEFF/XKK-1.0)-TIGHT1) 160,160,140
160 CONTINUE
IF (ABS(KEFF-1.0)-TIGHT2) 190,190,170
170 DO 180 G=1,GRP
NU(G)=NU(G)/KEFF
DO 180 R=1,REG
NUSIGF(R,G)=NUSIGF(R,G)/KEFF
180 CONTINUE
INDX=2
GO TO 110
190 CONTINUE
INDX=3
DO 200 N=1,NUM
P=WPT(N)
IF(DABS(PSISTO(N)/PSI(P,THG)-1.0)-TIGHT3) 200,200,110
200 CONTINUE
201 CONTINUE
CALL      EQPREC(PSI,FUEL,NUSIGF,IPL,IPR,XL,XR)
II=GL

```

```

SET C037
SET C038
SET C039
SET C040
SET C041
SET C042
SET C043
SET C044
SET C045
SET C046
SET C047
SET C048
SET C049
SET C050
SET C051
SET C052
SET C053
SET C054
SET C055
SET C056
SET C057
SET C058
SET C059
SET C060
SET C061
SET C062
SET C063
SET C064
SET C065
SET C066
SET C067
SET C068
SET C069
SET C070
SET C071
SET C072

```

IF (STEADY.EQ.3) WRITE (OUT,330)	SET C073
IF (STEADY.EQ.3) GO TO 210	SET C074
II=1	SET C075
WRITE (OUT,270) (G,NU(G),G=1,GRP)	SET C076
WRITE (OUT,280)	SET C077
210 CONTINUE	SET C078
DO 220 G=II,GU	SET C079
220 WRITE (OUT,300) (P,PSI(P,G),P=1,PT)	SET C080
IF (PUNBAL.EQ.1) GO TO 225	SET C081
RETURN	SET C082
225 CONTINUE	SET C083
DO 230 G=1,GRP	SET C084
230 PUNCH 310,NU(G)	SET C085
WRITE (OUT,290)	SET C086
DO 240 G=1,GU	SET C087
240 PUNCH 310,(PSI(P,G),P=1,PT)	SET C088
RETURN	SET C089
270 FORMAT (19H0 EQUILIBRIUM NU(G),3X,4(1H(,I3,1H),E14.7)/22X,(4(1H(,I	SET C090
13,1H),E14.7)))	SET C091
280 FORMAT (20H0 EQUILIBRIUM FLUXES)	SET C092
290 FORMAT (53H0 EQUILIBRIUM NU(G) AND FLUX DISTRIBUTION ARE PUNCHED)	SET C093
300 FORMAT (6(1H(,I3,1H),E13.7))	SET C094
310 FORMAT (6E12.7)	SET C095
330 FORMAT (33H0INITIAL PRECURSOR CONCENTRATIONS)	SET C096
END	SET C097

SUBROUTINE SOURCE(G,PSI,SORG,SOR,SRCEC,SRCE1,XL,XR,PB,IPL,IPR)	SRCEC001
IMPLICIT REAL*8 (A-H,O-Z)	SRCECC02
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	SRCECC03
1 UPSCAT,WPT, FUEL,G,GEOM,GP,GPL,GPR,GD,GL,GL,GRP,GPL,CLT,	SRCECC04
2P,PL,PR,PB,PRBEND,PT,PUNBAL,PUNFRS,R,REG,SCR,	SRCECC05
3 SORCE , SORG , SCZ , STEADY , STEP , TAGC , TAGF , TAGT	SRCECC06
REAL*8 LR,NU,NUSIGF,NX	SRCECC07
INTEGER PLB,PRB	SRCECC08
COMMON /A1/GRP,REG,PT,CL,GU,DEL,THG,IDEL	SRCECC09
COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	SRCECC10
COMMON /A3/PUNBAL,SORCE,GEOM,NTAG,NUM2,PUNFRS	SRCECC11
COMMON /B1/H,HP,TIME,TZ,ZERC,TZO,TIMZ	SRCECC12
DIMENSION PSI(PT,GU)	SRCECC13
DIMENSION IPL(REG),IPR(REG),PB(REG),XL(REG),XR(REG)	SRCECC14
DIMENSION SCR(REG),SORG(REG,GRP),SRCEC(PT,GRP),SRCE1(PT,GRP)	SRCECC15
FLOAT(I)=DFLOAT(I)	SRCECC16
C THIS ROUTINE EVALUATES THE CONTRIBUTION OF EXTERNAL SOURCES	SRCECC17
TI=0.0	SRCECC18
DO 320 R=1,REG	SRCECC19
IF (SORG(R,G).EQ.0) GO TO 320	SRCE0020
IF (R-1) 110,110,140	SRCECC21
110 IF (BCL.EQ.1) GO TO 120	SRCECC22
PL=2	SRCECC23
GO TO 130	SRCE0024
120 PL=1	SRCECC25
130 PLB=0	SRCECC26
GO TO 150	SRCECC27
140 PLB=PB(R-1)	SRCECC28
PL=PLB+1	SRCECC29
150 PR=IPR(R)	SRCECC30
PRB=PR+1	SRCECC31
IF (R-REG) 170,160,160	SRCECC32
160 IF (BCR.EQ.1) PR=PT	SRCECC33
PRB=0	SRCECC34
170 CONTINUE	SRCECC35
180 XI=H	SRCECC36

	X2=H*H/2.0	SRCEC037
	GC TC 200	SRCEC038
200	X3=TIME-TI+H/2.0	SRCEC039
	IF (SOR(R)-1) 320,270,210	SRCEC040
210	LP=PT-1	SRCEC041
	X4=H*(SRCE0(LP,G)+SRCE1(LP,G)*X3)	SRCEC042
	DC 220 P=PL,PR	SRCEC043
220	PSI(P,G) =PSI(P,G) +X4	SRCEC044
	IF (PLB) 230,240,230	SRCEC045
230	PSI(PLB,G)=PSI(PLB,G)+X4*XL(R)	SRCEC046
240	IF (PRB) 250,260,250	SRCEC047
250	PSI(PRB,G)=PSI(PRB,G)+X4*XR(R)	SRCEC048
260	GC TC 320	SRCEC049
270	DC 280 P=PL,PR	SRCEC050
	X4=H*(SRCE0(P,G)+SRCE1(P,G)*X3)	SRCEC051
	PSI(P,G)=PSI(P,G)+X4	SRCEC052
280	CONTINUE	SRCEC053
	IF (PLB) 290,300,290	SRCEC054
290	X4=H*(SRCE0(PLB,G)+SRCE1(PLB,G)*X3)	SRCEC055
	PSI(PLB,G)=PSI(PLB,G)+X4*XL(R)	SRCEC056
300	IF (PRB) 310,320,310	SRCEC057
310	X4=H*(SRCE0(PLB,G)+SRCE1(PLB,G)*X3)	SRCEC058
	PSI(PRB,G)=PSI(PRB,G)+X4*XR(R)	SRCEC059
320	CONTINUE	SRCEC060
330	RETURN	SRCEC061
	END	SRCEC062

SUBROUTINE TEST(STPRN,PSI,PSITOT,POWREG,WPT,WZ,WHZ)	TESTC001
IMPLICIT REAL*8 (A-H,C-Z)	TESTC002
REAL*8 IODINE	TESTC003
INTEGER BCL,BCR,CHANGE,DEL,DNSCAT,TAGX,TESTS,THG,XEN,	TESTC004
1 UPSCAT,WPT, FUEL,G,GECM,GP,GPL,GPR,GC,CL,GU,GRP,GPU,CUT,	TESTC005
2 P,PL,PR,PB, PRBEND , PT , PUNBAL , PUNFRS , R,REG,SCR,	TESTC006
3 SORCE , SORG , SOZ , STEADY , STEP , TAGC , TAGF , TAGT	TESTC007
COMMON /A1/GRP,REG,PT,CL,GU,DEL,THG,IDEL	TESTC008
COMMON /A2/NUM,NCOMP,BCL,BCR,MTZ,NTZ,XEN,STEADY	TESTC009
COMMON /A3/PUNBAL,SORCE,GECM,NTAG,NUM2,PUNFRS	TESTC010
COMMON /B1/H,HP,TIME,TZ,ZERC,TZO,TIMZ	TESTC011
COMMON /B2/NPRT,NZ,ISX,STEP,NZSAVE,PRBEND,IPRN	TESTC012
DIMENSION STPRN(50)	TESTC013
DIMENSION PSI(PT,GU)	TESTC014
DIMENSION PSITCT(REG,GRP),PCWREG(REG)	TESTC015
DIMENSION WHZ(PT),WZ(PT),WPT(NUM)	TESTC016
IFLAG=0	TESTC017
STEP=STEP+1	TESTC018
TIME=TIME+H	TESTC019
IF (NUM2.EQ.0) GO TO 120	TEST0020
IF((DABS(TIME-STPRN(NPRT))).GT.ZERO) GO TO 120	TESTC021
NPRT=NPRT+1	TESTC022
IFLAG=1	TEST0023
120 IF((DABS(TIME-TZ)).LT.ZERO) GO TO 150	TESTC024
IF(IPRN.EQ.0) GO TO 125	TESTC025
IF ((MOD(STEP,IPRN)).EQ.0) GO TO 140	TESTC026
125 IF(IFLAG.EQ.1) GO TO 140	TESTC027
130 RETURN	TESTC028
140 CALL PRINTA(PSI,PSITCT,POWREG,WPT,WZ,WHZ)	TESTC029
GO TO 130	TESTC030
150 CALL PRINTA(PSI,PSITOT,POWREG,WPT,WZ,WHZ)	TESTC031
NZ=NZ+1	TESTC032
IF(NZ.GT.NTZ) PRBEND=1	TESTC033
GO TO 130	TESTC034
END	TESTC035

	SUBROUTINE TITLE (K)	TITLCC01
	INTEGER CUT	TITLCC02
	COMMON/A5/IN,OUT,NERR	TITLCC03
C	READS AND PRINTS CASE TITLE	TITLCC04
C	K=1 TITLE IS READ IN	TITLCC05
C	K=2 TITLE IS WRITTEN OUT AT THE TOP OF A NEW PAGE	TITLCC06
C	K=3 TITLE IS WRITTEN OUT, NO NEW PAGE	TITLCC07
C		TITLCC08
	100 FORMAT (15H END OF PROBLEM)	TITLCC09
C		TITLCC10
	110 FORMAT (72H	TITLCC11
	1)	TITLCC12
	120 FORMAT (1H1)	TITLCC13
C		TITLCC14
C		TITLCC15
	GO TO (130,140,150,145),K	TITLCC16
	130 READ (IN,110)	TITLCC17
	GO TO 160	TITLCC18
	140 WRITE (6,120)	TITLCC19
	GO TO 150	TITLCC20
	145 WRITE (6,110)	TITLCC21
	WRITE (6,100)	TITLCC22
	GO TO 160	TITLCC23
	150 WRITE (6,110)	TITLCC24
	160 RETURN	TITLCC25
	END	TITLCC26

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SUBROUTINE UPDAT(TAGT, TAGX, TAGC, TAGF, CHANGE, NUSIGF, PSIBAR, ICDINE,
1XABS, XENCN, CTRL, CTRQ, CXL, CXQ, CCL, CCQ, CFL, CFQ, SIGT, SIGX, SIGF,
2SIGC, PSIB1, NU, FUEL)
  IMPLICIT REAL*8 (A-H, O-Z)
  INTEGER BCL, BCR, CHANGE, DEL, DNSCAT, TAGX, TESTS, THG, XEN,
1      UPSCAT, WPT, FUEL, G, GEOM, GP, GPL, GPR, GC, GL, GU, GRP, GPU, OUT,
2      P, PL, PR, PB, PRBEND, PT, PUNBAL, PUNFRS, R, REG, SOR,
3      SORCE, SORG, SOZ, STEADY, STEP, TAGC, TAGF, TAGT
  REAL*8 ICDINE
  REAL*8 LR, NU, NUSIGF, NX
  COMMON /A1/GRP, REG, PT, GL, GU, DEL, THG, IDEL
  COMMON /A2/NUM, NCCMP, BCL, BCR, MTZ, NTZ, XEN, STEADY
  COMMON /B1/H, HP, TIME, TZ, ZERO, TZO, TIMZ
  COMMON /B2/NPRT, NZ, ISX, STEP, NZSAVE, PRBEND, IPRN
  DIMENSION CHANGE(REG)
  DIMENSION TAGC(REG), TAGF(REG), TAGT(REG), TAGX(REG)
  DIMENSION NUSIGF(REG, GRP)
  DIMENSION SIGC(REG, GRP), SIGF(REG, GRP), SIGT(REG, GRP),
1SIGX(REG, GRP, GRP)
  DIMENSION CCL(REG, GRP), CCQ(REG, GRP), CFL(REG, GRP), CFQ(REG, GRP),
1CTRL(REG, GRP), CTRQ(REG, GRP), CXL(REG), CXQ(REG)
  DIMENSION XENCN(REG)
  DIMENSION NU(GRP)
  DIMENSION PSIBAR(REG, GRP), PSIB1(REG, GRP)
  DIMENSION XABS(REG, GRP)
  DIMENSION IODINE(REG)
  DIMENSION FUEL(REG)
  T=TZO
20 Y=(TIME-TIMZ)/(TZ-T)
  YSQ=Y*(TIME+TIMZ-2*T)/(TZ-T)
  TIMZ=TIME
  IF(XEN.EQ.0) GC TC 40
  CALL FEDBKX(PSIBAR, SIGF, XABS, XENON, IODINE, PSIB1, FUEL)
40 CONTINUE
  DO 350 R=1, REG

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UPCT0001
UPCTCCC2
UPCTCCC3
UPCTC004
UPCTC005
UPCTCCC6
UPCTC007
UPCTC008
UPDTCCC9
UPCTCC10
UPCTC011
UPCTCC12
UPCTC013
UPCTC014
UPCTC015
UPDTCC16
UPCTC017
UPCTC018
UPCTCC19
UPCTCC20
UPCTC021
UPCTCC22
UPCTC023
UPCTC024
UPCTC025
UPCTC026
UPCTC027
UPCTCC28
UPCTCC29
UPCTCC30
UPCTCC31
UPCTCC32
UPCTC033
UPCTC034
UPCTCC35
UPCTC036

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    IF (TAGT(R)-1) 160,110,130
110 DC 120 G=1,GRP
120 SIGT(R,G)=SIGT(R,G)+CTRL(R,G)*Y
    GC TC 150
C
130 DO 140 G=1,GRP
140 SIGT(R,G)=SIGT(R,G)+CTRL(R,G)*Y+CTRQ(R,G)*YSQ
150 CHANGE(R)=1
    GO TO 170
160 CHANGE(R)=0
C
170 IF (TAGX(R)-1) 220,180,210
180 X=CXL(R)*Y
190 DC 200 G=1,GRP
    DO 200 GP=1,GRP
200 SIGX(R,G,GP)=SIGX(R,G,GP)*(1.0+X)
    CHANGE(R)=2
    GC TC 220
C
210 X=CXL(R)*Y+CXQ(R)*YSQ
    GC TC 190
C
220 IF (TAGC(R)-1) 270,230,250
230 DC 240 G=1,GRP
240 SIGC(R,G)=SIGC(R,G)+CCL(R,G)*Y
    CHANGE(R)=2
    GC TO 270
C
250 DC 260 G=1,GRP
260 SIGC(R,G)=SIGC(R,G)+CCL(R,G)*Y+CCQ(R,G)*YSQ
    CHANGE(R)=2
C
270 IF (TAGF(R)-1) 320,280,300
280 DC 290 G=1,GRP
    SIGF(R,G)=SIGF(R,G)+CFL(R,G)*Y
    NUSIGF(R,G)=NU(G)*SIGF(R,G)

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UPDTC037
UPDTC038
UPDTC039
UPDTC040
UPDTC041
UPDTC042
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UPDTC044
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UPDTC064
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UPDTC066
UPDTC067
UPDTC068
UPDTC069
UPDTC070
UPDTC071
UPDTC072

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290 CONTINUE
    CHANGE(R)=2
    GO TO 320
C
300 DO 310 G=1,GRP
310 SIGF(R,G)=SIGF(R,G)+CFL(R,G)*Y+CFQ(R,G)*YSQ
    CHANGE(R)=2
320 IF (((TAGF(R).EQ.0).AND.(TAGC(R).EQ.0)).AND.(TAGX(R).EQ.0)) GO TO
1350
    DO 340 G=1,GRP
    SIGX(R,G,G)=SIGF(R,G)+SIGC(R,G)
    X=C.0
    DO 330 GP=1,GRP
330 X=X+SIGX(R,GP,G)
    SIGX(R,G,G)=X
340 CONTINUE
C
    IF (XEN.EQ.0) GO TO 350
    DO 345 G=1,GRP
    Z=XABS(R,G)*XENGN(R)
    SIGX(R,G,G)=SIGX(R,G,G)+Z
345 SIGC(R,G)=SIGC(R,G)+Z
350 CONTINUE
370 RETURN
    END

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UPDTCC73
UPDTCC74
UPDTCC75
UPDTCC76
UPDTCC77
UPDTCC78
UPDTCC79
UPDTCC80
UPDTCC81
UPDTCC82
UPDTCC83
UPDTCC84
UPDTCC85
UPDTCC86
UPDTCC87
UPDTCC88
UPDTCC89
UPDTCC90
UPDTCC91
UPDTCC92
UPDTCC93
UPDTCC94
UPDTCC95
UPDTCC96
UPDTCC97

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