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# MIT Modular X-Ray Source Systems for the Study of Plasma Diagnostics

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### MIT Modular X-ray Source Systems

#### For The Study **Of** Plasma Diagnostics

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#### ABSTRACT

Two new X-ray source systems are now on line at our facility. Each provides an e-beam to **25 kV.** Targets are interchangeable between machines, and four x-ray detectors may be used simultaneously with a target. The gridded e-gun of the *RACEHORSE* system gives a **0.5** to 1.0-cm pulsable spot on target. The non-gridded e-gun of the *SCORPION* system provides a 0.3-mm or smaller **DC** microspot on target. *RACEHORSE* is being used to study and characterize Type-II Diamond photoconductors for use in diagnosing plasmas, while *SCORPION* is being used to develop a slitless spectrograph using photographic film. Source design details and some *RACEHORSE* results are presented.

## I. INTRODUCTION

Work in our laboratory includes the characterization and calibration of x-ray detectors **(1)** to refine/develop new calibration standards, and (2) to study/select types of detectors for plasma diagnostics. To expand our capability we have built two new x-ray sources **I:** *RACEHORSE,* a pulsable macrosource, and *SCORPION,* a **DC** microsource. Both sources employ metal targets bombarded with e-guns. With either source, four detectors may monitor the target simultaneously.

#### **II.** *RACEHORSE* DESIGN

The gridded e-gun design has a theoretical pulsing limit of **1** GHz (Fig **1).** The e-gun operates at **2-25 kV,** with beam currents to **10** mA (Fig 2). **A** telefocus cathode housing aids beam auto-collimation, while *PULSE* and *ACCEL* grids provide pulse tailoring to **1** MHz with pulse widths of **100 - <sup>10</sup>** ns. The electron spot on target is **0.5** to **1.0-** cm in diameter.

**A** control panel provides Variac power to five isolation transformers which energize the e-gun circuits: (a) filament heating; (b)  $+5volts_{ref}$ ; (c)  $Pulsevolts_{-}$ ; (d)  $Pulsevolts_{+}$ ; and (e) *ACCEL volts.* The high voltage itself is selected from the HV power supply unit. An optical emitter driver converts an externally-generated TTL pulse to an optical pulse which drives the e-gun switching grid via fiberoptc cable. **All** system power is supplied through a 6-connector relay controlled **by** an interlock system, which also enables the high voltage. **A** circuitry block diagram is shown in Fig **3.**

## *III. SCORPION* **DESIGN**

The purpose of the *SCORPION* non-gridded e-gun is to produce a **DC** microspot or 'point-source' of x-rays. Shown in Fig 4, the e-gun incorporates a thermionic point emitter, an energy filter aperture, and a Butler electrostatic lens. The egun operates optimally at **10-20kV** with beam currents to **<sup>10</sup> pA,** delivering a spot variable from 0.3-mm diameter downward depending upon filtering voltage. The total circuitry

for the system is the bleeder resistor chain.

## **IV. TARGETS**

Targets for the two systems are interchangeable, mounting coaxially with the e-beam in either instrument. The target support is a 1.0-inch diameter copper bar, insertable with bayonet-seal into either vacuum chamber. The bar is finned at the *atmosphere* end for air-cooling. At the *vacuum* end, there is provision for mounting metal discs or foils or a Faraday cup. The *vacuum* end face is machined either perpendicular to the bar axis (circular target area) or at an angle to the bar axis (elliptical target area). When the elliptical target area is rotated, the x-rays may be 'flashed' from position to position with frequencies as high as 360Hz. The detector access to target in both systems is **by** means of **2.75** inch diameter vacuum flanges, and four ports for such flanges face the target position. Fig **5** shows a typical spectrum from a *Cu* target taken with *RACEHORSE.*

#### **V. EXAMPLES OF USAGE**

*RACEHORSE* is now being used to study diamond photoconductor detectors (PCDs) for plasma diagnostics. Type II diamond transmits to 5.49 eV, and has flat spectral and excellent time responses and driftless sensitivity **2,3.** It is also rugged, dependable, and long-lived, and smoothly saturates as x-ray fluxes become higher. allowing continuous operation over a broad range of incident power  $(10 - 10^4 W/cm^2)$ . Due to the large band gap in Type-II diamond, the detector can operate in visible light without sacrificing its x-ray detection characteristics.

We are studying diamond **PCD** as a means of obtaining high temporal resolution rather than as a means for measuring total output from a pulsed x-ray source. We monitor targets with diamond **PCD** and a **SBD** simultaneously, recording both pulse outputs photographically from dual traces on an oscilloscope. Data for a *Cu* target are shown in Fig 6a; for an *Al* target in Fig **6b;** and for a Mo target in Fig 6c.

Low-fidelity response in PCDs is exhibited when excitation times are much longer than the primary response time (carrier lifetimes) of the PCD. For Type II diamond, carrier lifetimes are about equal and are between **90** and 200 ps. For a known pulse shape and rise time into the gridded egun, we can elicit a variety of output pulse shapes and rise times from both the **PCD** and the **SBD,** primarily because of signal amplification problems. This is especially true as we go to higher repetition rates. We are now in the process of isolating the variables involved in the electronic effects and artifacts.

The *SCORPION* source is being used at present to develop a slitless spectrograph with photographic emulsion output. Use of the spectrograph involves long exposure times, but will enable us to derive spectral dispersions without recourse to an electronic link in obtaining the data. This bentcrystal spectrograph will be used primarily for purposes of cross-verification and absolute calibration of our electronic detectors.

# **VI.** ACKNOWLEDGEMENTS

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**-USDOE** Postdoctoral Fellow

**\*\* USDOE** MFET Fellow

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#### **Figure Captions**

Fig **1.** In this tetrode gridded e-gun. the axial electrode spacing is not time-of-flight limiting for beam pulsing to **1** MHz at e-gun voltages as low as **2kV.**

Fig 2. Shown are three curves for *'beam* (arbitrary units) vs High Voltage, for fixed filament Variac heating settings. Beam current is in arbitrary units (absolute values depend upon all gun electrode voltages as well as on pulse repetition rate and shape). The upper limit on *Ibeam* is near **10** mA.

# Fig **3.** *RACEHORSE* electrical supply and control.

Fig 4. The purpose of this non-gridded e-gun is to provide a finely-focused microsource. The beam may be chopped or deflected post-anode only.

#### Fig **5.** *Cu* Target Spectrum

Fig **6.** (a) shows dual-trace oscilloscope signals from *Cu* at  $HV_{beam} = 18.0Kv$  and  $I_{beam} = 0.5mA$ . (b) is from Al at 20.0Kv, and (c) is from *Mo* at 21.0Kv. Pulse frequency is **30-50** KHz. The disparity between **SBD** and **PCD** signal amplitudes is due in part to detector collection area **(SBD:PCD**  $= 12:1$ ).

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# *RACEHORSE* GRIDDED e-GUN







# *SCORPION* MICROSOURCE e-GUN SYSTEM





(a):  $Cu$  TARGET

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 $\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2$ 

 $\sim$   $\sigma$ 

(b):  $AI$  TARGET



(c): Mo TARGET